

bio soft-matter theory



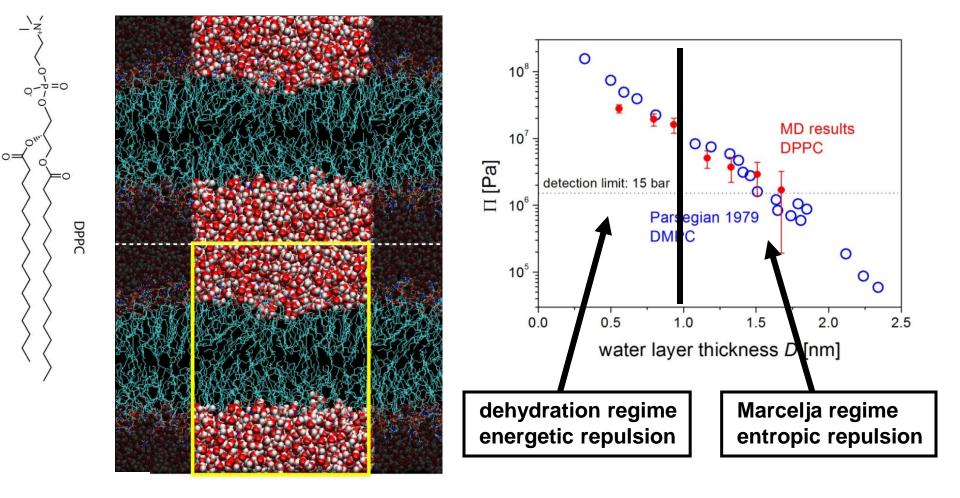
physics department - T37

DNA dynamics and convolution theory for dynamic mechanic networks

M. Hinzewski, Y. von Hansen, R. Netz, TU München

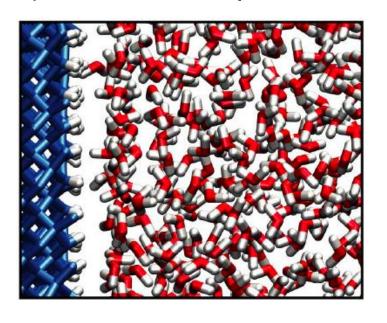
- 1) Aqueous Appetizer:
- a) hydration repulsion
- b) interfacial dielectric effects
- c) dielectric spectroscopy
- d) hydrogen bond friction
- 2) Polymeric Main Course: DNA dynamics (see KITP 2006)
- 3) **Dessert:** ,,the measurement problem" in single-molecule force spectroscopy (polymers as dynamic force transducers)

I) Hydration repulsion between lipid bilayers (Schneck/Netz)



- novel simulation method, constant water chemical potential via thermodynamic extrapolation
- fluid membranes (L_a-phase)
- main transition is obtained

II) Dielectric response at Planar Interface (Bonthuis, Gekle, RRN)



$$\Delta \boldsymbol{E}\left(\boldsymbol{r}\right) = \varepsilon_{0}^{-1} \int \varepsilon_{nl}^{-1} \left(\boldsymbol{r}, \boldsymbol{r}'\right) \cdot \Delta \boldsymbol{D}\left(\boldsymbol{r}'\right) d\boldsymbol{r}'$$

$$abla \cdot oldsymbol{D}(z) = 0$$
 $\Delta D_{\perp}(z) = D_{\perp}$ $\Delta oldsymbol{E}_{\perp}(r) = arepsilon_{0}^{-1} arepsilon_{\perp}^{-1}(r) \cdot \Delta oldsymbol{D}_{\perp}$

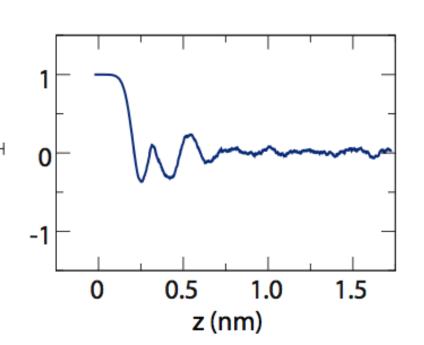
Perpendicular dielectric response

$$\varepsilon_{\perp}^{-1}(z) = 1 - \frac{\Delta m_{\perp}(z)}{D_{\perp}}$$



Significant contribution from higher order moments

 ε_{\perp}^{-1} < 0: overscreening (bulk: Kornyshev)



III) Dielectric spectroscopy at interfaces (Gekle/RRN)

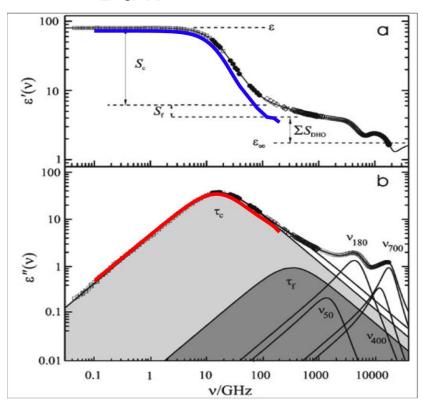
Dipole correlation function (E=0)

$$\Phi(t) = \frac{\langle M(0) \cdot M(t) \rangle}{\langle M^2 \rangle}$$

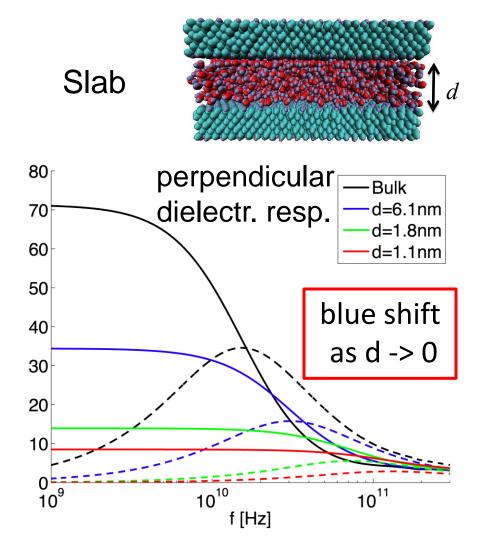


$$\varepsilon(\omega) = \frac{\langle M^2 \rangle}{\varepsilon_0 V k_B T} L(-\Phi) + 1$$

Bulk



spatially resolved dielectric spectroscopy possible!



Zur Anzeige wird der Quick Time™ Dekompressor "YUV 420 codec"

IV) H-bond friction (Erbas, RRN) pulling rate v=0.1 m/s

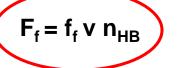
Vinci-Coulomb-Amonton law on nanoscopic scales?

macroscopia

nanoscopia for v->0
$$f_f = 5 \times 10^{-9} \text{ kg/s}$$

$$F_f = OF_N$$

O friction coeff.



f_f friction coeff. per H-bond universal constant

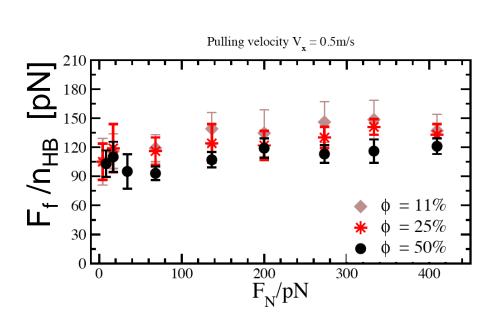
friction force per monomer

friction force per H bond

Pulling velocities on hydrophilic / hydrophobic surfaces 0.5 m/s, 10 m/s



Zur Anzeige wird der QuickTime Dekompressor "" benötigt.



normal force

Main course

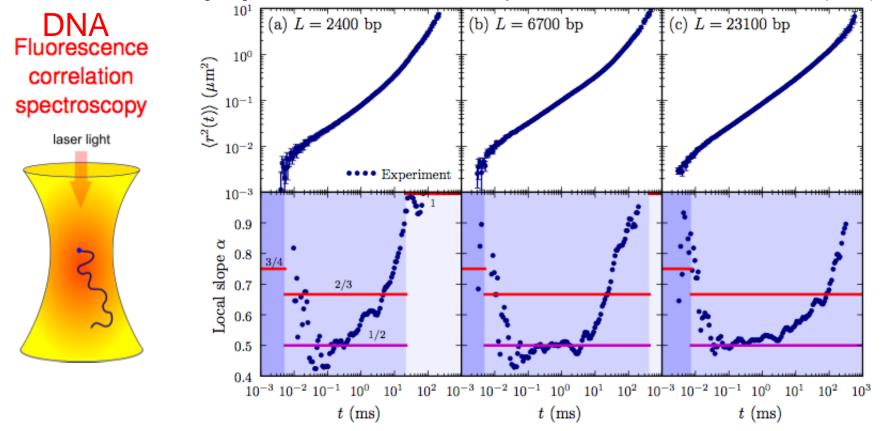
how good are standard models for predicting the equilibrium DNA dynamics?

(KITP 2006, Rubinstein & RRN)

Experimental motivation

Shusterman et. al., PRL 92, 048303 (2004)

M. Hinczewski, X. Schlagberger, M. Rubinstein, O. Krichevsky, R.R. Netz, Macromolecules 42, 860 (2009)

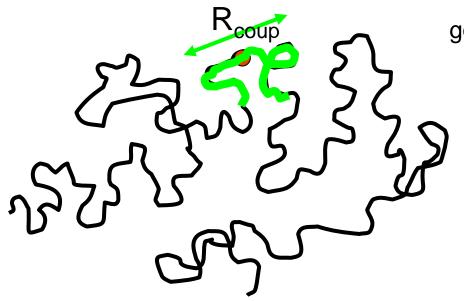


Theoretical expectations: three different power-law scaling regimes

Rouse regime with $\alpha = 1/2$ unclear!

fundamental problem of DNA model or theory ??? 2/43

single monomer diffusion is at increasing time scales dominated by progressively growing chain sections :



goal: monomer mean-square-displacement as function of time

coupled chain section at time t

$$R_{coup} \approx N^{V}$$

MSD of that section $R_{MSD}^2 \approx D t$

Zimm: $D \approx 1/R_{coup}$

Rouse : D ≈ 1/N

scaling assumption: diffusion radius determines coupling radius R_{coup} ≈ R_{MSD}

Zimm: $R_{MSD}^2 \approx t^{2/3}$ sub-diffusive behavior

Rouse: $R_{MSD}^2 \approx t^{-2\nu/(1+2\nu)}$ ideal chain $\nu=1/2 -> R^2 \approx t^{1/2}$ rod $\nu=1 -> R^2 \approx t^{2/3}$ (Zimm $R^2 \approx t^{2/3} ln^2 t$)

End-monomer dynamics of semiflexible polymers

Brownian hydrodynamics simulations (Michael Hinczewski)

many independent simulations are needed!! not applicable to long DNA chains!

polymer of 50 beads persistence length = 20*a* bead radius a = 1nm -> pers length 20 nm length 100 nm

> Zur Anæige wird der Quick Time™ Deko mpressor "mp eg4" benötigt.

Hydroynamic mean-field theory (MFT) for semiflexible chain (R. Winkler):

$$U = \frac{\epsilon}{2} \int ds \left(\frac{\partial \mathbf{u}(s)}{\partial s} \right)^2$$
 Constraint $\mathbf{u}^2(s) = 1$ at each s .

after saddle-point approx. for constraint: MFT Gaussian Hamiltonian

$$U_{\rm MF} = \frac{\epsilon}{2} \int ds \left(\frac{\partial \mathbf{u}(s)}{\partial s} \right)^2 + \nu \int ds \, \mathbf{u}^2(s) + \nu_0 \left(\mathbf{u}^2(L/2) + \mathbf{u}^2(-L/2) \right)$$

where:
$$\mathbf{u}(s) \equiv \partial \mathbf{r}(s,t)/\partial s$$
, $\epsilon = 3l_p k_B T/2$, $\sqrt{\nu \epsilon/2} = \nu_0 = 3k_B T/4$

and
$$\langle u^2(s) \rangle = 1$$

The dynamics are described by a Langevin equation:

$$rac{\partial}{\partial t}\mathbf{r}(s,t) = -\int_{-L/2}^{L/2} ds' \stackrel{\boldsymbol{\leftarrow}}{oldsymbol{\mu}} \left(s,s';\mathbf{r}(s,t) - \mathbf{r}(s',t)
ight) \, rac{\delta U_{\mathrm{MF}}}{\delta \mathbf{r}(s',t)} + oldsymbol{\xi}(s,t)$$

with pre-averaged Rotne-Prager hydrodynamic interaction $\mu_{
m avg}(s-s')$

$$\frac{\partial}{\partial t} \mathbf{r}(s,t) = \int_{L/2}^{L/2} ds' \, \mu_{\text{avg}}(s-s') \left(-\frac{\delta U_{\text{MF}}}{\delta \mathbf{r}(s',t)} \right) + \boldsymbol{\xi}(s,t)$$

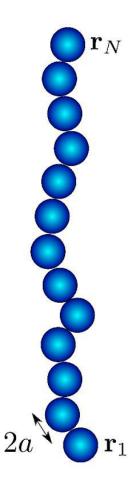
$$\langle \xi^{(i)}(s,t)\xi^{(j)}(s',t')\rangle = 2k_B T \delta_{ij}\delta(t-t')\mu_{\text{avg}}(s-s')$$

M. Hinczewski:

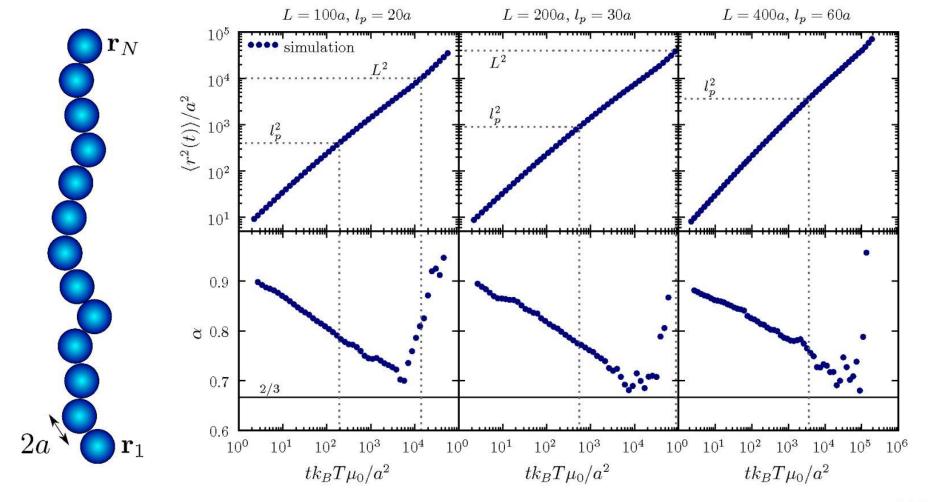
tangent

exact normal mode decomposition: $\mathbf{r}(s,t) = \sum_{n=0}^{\infty} \mathbf{P}_n(t) \Psi_n(s)$ $\xi(s,t) = \sum_{n=0}^{\infty} \mathbf{Q}_n(t) \Psi_n(s)$

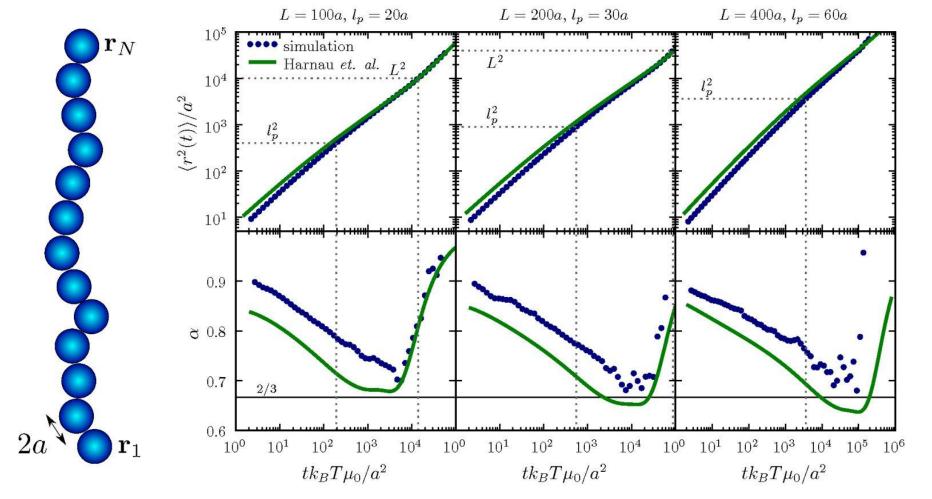
diagonalized Langevin equations $\frac{\partial}{\partial t}\mathbf{P}_n(t) = -\Lambda_n\mathbf{P}_n(t) + \mathbf{Q}_n(t)$



validation of the **hydrodynamic theory** by comparison with **Brownian hydrodynamic simulations** for N=50, 100, 200

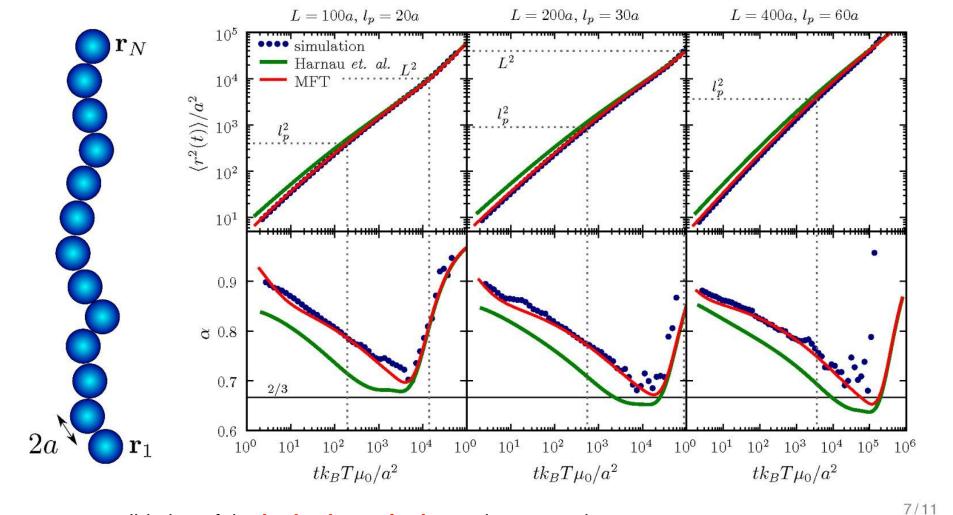


validation of the **hydrodynamic theory** by comparison with **Brownian hydrodynamic simulations** for N=50, 100, 200



validation of the **hydrodynamic theory** by comparison with **Brownian hydrodynamic simulations** for N=50, 100, 200

Harnau-Winkler solution with diagonal approximation = APPROX. ZIMM THEORY



validation of the **hydrodynamic theory** by comparison with **Brownian hydrodynamic simulations** for N=50, 100, 200

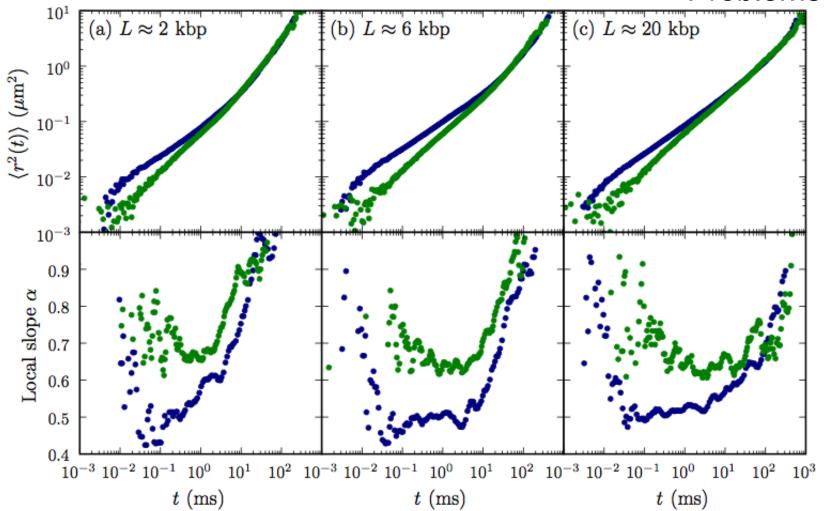
Harnau-Winkler solution with diagonal approximation = APPROX. ZIMM THEORY MFT: numerically exact solution = EXACT ZIMM THEORY excellent agreement between the MFT and simulation data --> confidently extend the MFT to larger chain lengths inaccessible to simulation (pre-averaging & MFT probably ok)

Comparison with experiments I

Blue data: Shusterman et. al., PRL 92, 048303 (2004)

Green data: Petrov et. al., PRL 97, 258101 (2006)

Experimental Problems ??

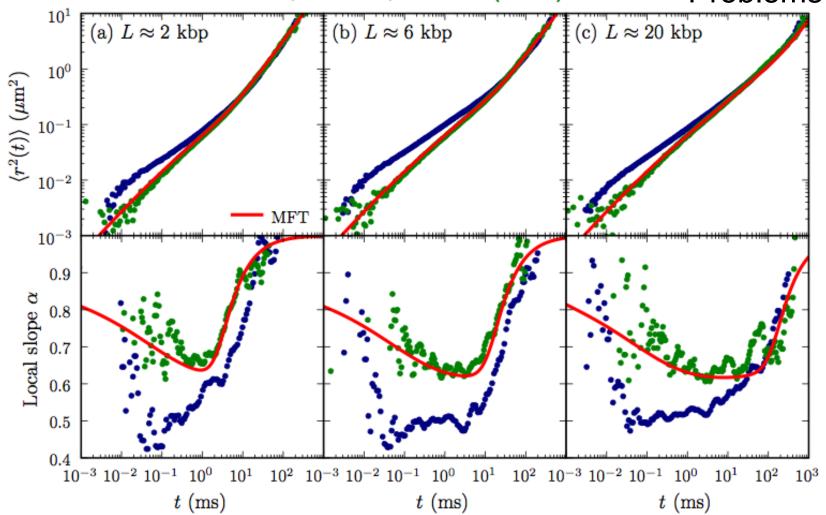


Comparison with experiments I

Blue data: Shusterman et. al., PRL 92, 048303 (2004)

Experimental Problems!!

Green data: Petrov et. al., PRL 97, 258101 (2006)



Parameters taken from the literature and experimental conditions: $I_p = 50$ nm, T = 293K, viscosity of water at 293K = 1 mPa s.

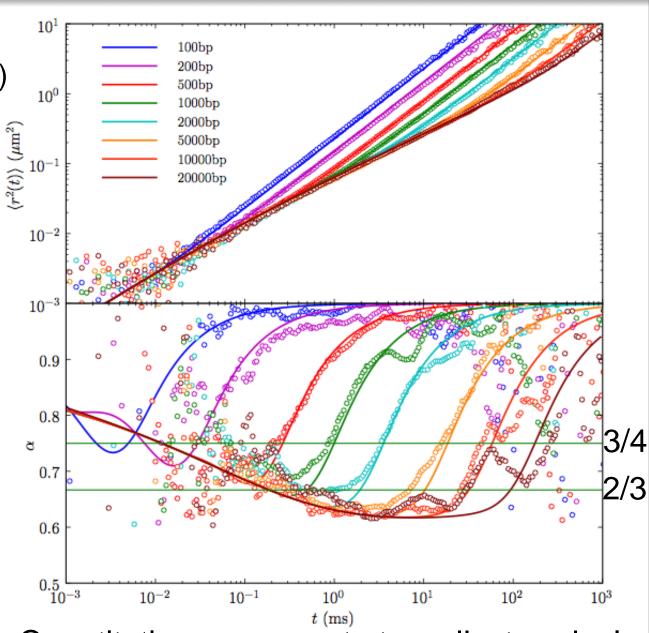
Comparison with experiments II

Hinczewksi/Netz, EPL 88, 18001 (2009)

Data: Petrov *et. al.*, PRL 97, 258101 (2006)

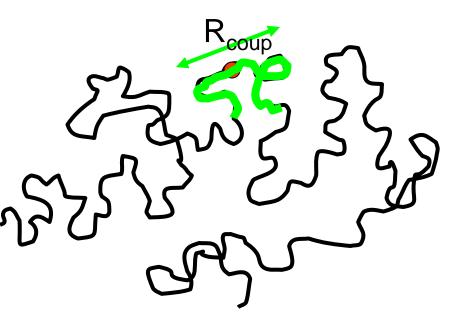
Parameters taken from the literature and experimental conditions: $I_p = 50$ nm, T = 293K, viscosity of water at 293K = 1 mPa s.

sub-Zimm scaling due to subtle crossover effects!



Quantitative agreement at smallest scales!

simple scaling for dynamic crossover



goal: monomer position a.s.f.o. time

coupled chain section at time t

$$R_{coup} \approx N^{V}$$

diffusion of that section $R_{MSD}^2 \approx D t$

general : D ≈ 1/N^c

Zimm flex: $c = v = 1/2 -> R^2 \approx t^{2/3}$

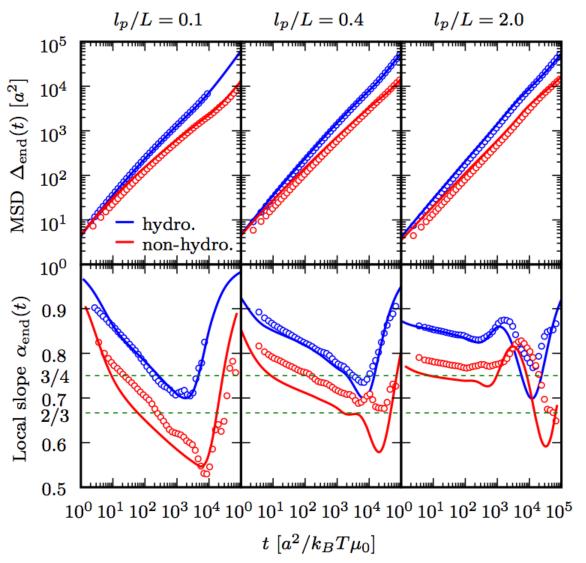
Zimm rod: $c = 1 v = 3/2 -> R^2 \approx t^{3/4}$

Rouse: $c=1 \ v=1/2 \ -> R^2 \approx t^{1/2}$

crossover from stiff rod (c = 1 ν = 3/2)to flexible polymer (c = ν = 1/2)

crossover for v ist quite fast crossover for c is somewhat slow ---> intermediate Rouse regime where c = 1 > v = 1/2

comparison of simulations/theory without hydrodynamic and simulations/theory with hydrodynamics



hydrodynamics relevant! Exponent shift by + 0.1 (= logarithm) mean-field theory better with long-range hydrodynamics!

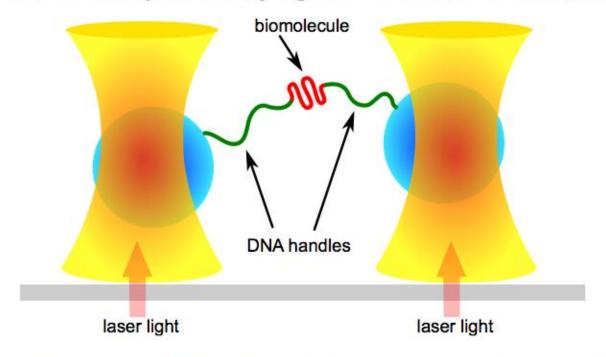
Dessert:

"the measurement problem" in single-molecule force spectroscopy:

dynamic mechanic networks

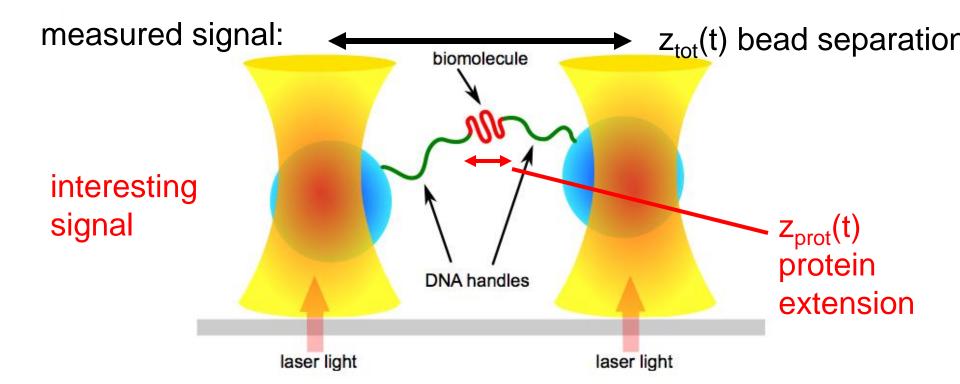
Optical Tweezers

Optical tweezer setup for studying biomolecules under tension:



- ▶ Two polystyrene / silica beads (\sim 1 μ m), each trapped in the focus of a laser beam.
- Double-stranded DNA handles (~ 100 nm) attached to the beads.
- ► The object of interest (~ 10 nm): for example a DNA/RNA hairpin, or a protein.

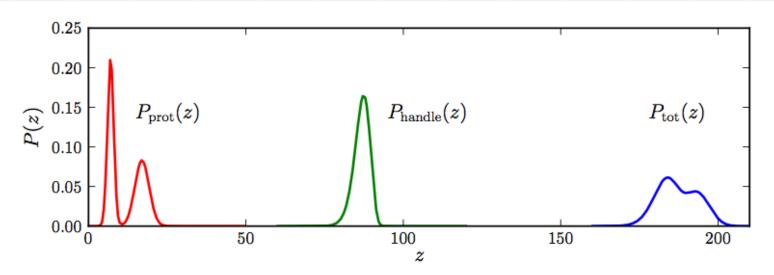
Optical Tweezers



The experimental setup is highly sensitive (force with \ll 1 pN precision) and probes the intrinsic dynamics the biomolecule, though filtered through the response of the DNA handles and the beads.

Key focus: How to recover information about those intrinsic properties from the raw output data (the spatial fluctuations of the beads in the trap).

Static Deconvolution of probability distribution of extension



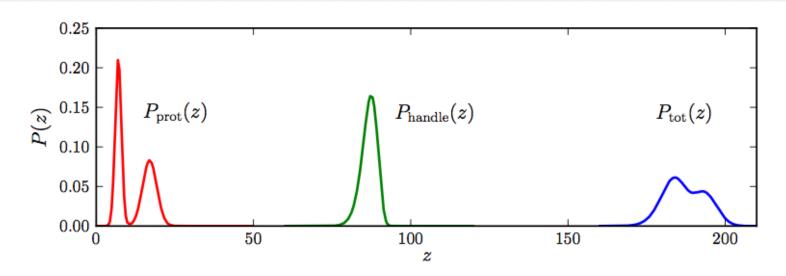
 $P_{\text{prot}}(z)$ and $P_{\text{tot}}(z)$ are related through the convolution

$$P_{\text{tot}}(z) = \int dz' \int dz'' P_{\text{handle}}(z') P_{\text{prot}}(z'') P_{\text{handle}}(z - z' - z'').$$

Knowing $P_{\text{handle}}(z)$ from experiment or using the worm-like chain theory, one can find $P_{\text{prot}}(z)$ from the experimental output $P_{\text{tot}}(z)$ using a standard deconvolution procedure. In Fourier space:

$$P_{\text{tot}}(k) = P_{\text{handle}}^2(k) P_{\text{prot}}(k).$$

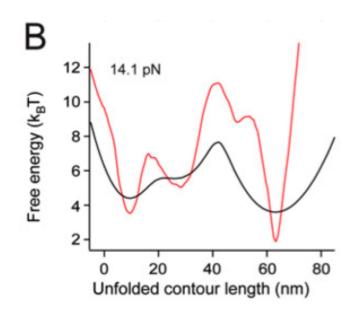
Static Deconvolution - fully understood



The protein's free energy landscape is obtained from $P_{\text{prot}}(z)$ by Boltzmann inversion:

$$F(z) = -k_B T \ln P_{\text{prot}}(z).$$

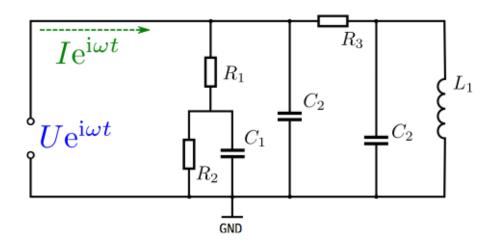
Exp. application: leucine zipper



[Gebhardt, Bornschlögl, Rief, PNAS 107 (2010)]

Dynamic (De-)Convolution of Electric Circuits

The behavior of an electric circuit



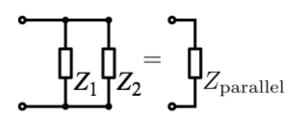
is specified by the (complex) impedance Z_{total} relating applied voltage and current

$$U = Z_{\text{total}}I$$
.

Decomposing the circuit into serial

$$Z_1$$
 Z_2 Z_{serial}

and parallel elements



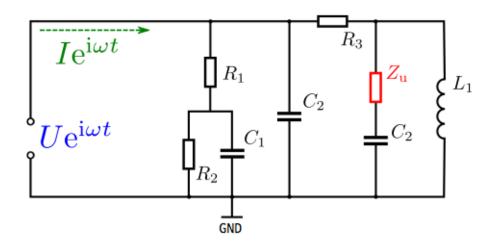
and knowledge of the basic rules

$$Z_{
m serial} = Z_1 + Z_2,$$
 $rac{1}{Z_{
m parallel}} = rac{1}{Z_1} + rac{1}{Z_2},$

allows to calculate Z_{total} .

Dynamic (De-)Convolution of Electric Circuits

The behavior of an electric circuit



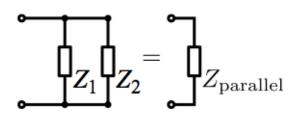
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$$U = Z_{\text{total}}I$$
.

Decomposing the circuit into serial

$$Z_1$$
 Z_2 Z_{serial}

and parallel elements



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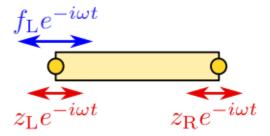
$$egin{aligned} Z_{ ext{serial}} &= Z_1 + Z_2, \ rac{1}{Z_{ ext{parallel}}} &= rac{1}{Z_1} + rac{1}{Z_2}, \end{aligned}$$

allows to calculate Z_{total} .

In turn, if the circuit's structure is known, the unknown impedance Z_u can be determined by measuring $Z_{\text{total}} = U/I$.

Force Response of Single Mechanical Elements

A small oscillatory force f_{L} on the left end-point of a mechnical component



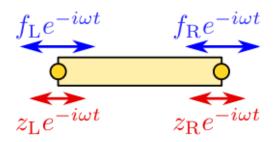
results in (average) oscillations of magnitude z_L and z_R of the two ends.

Within the regime of linear response force and position amplitudes are related by the complex self response function $J_{\text{self,L}}(\omega)$ of the left end and the cross response function $J_{\text{cross}}(\omega)$:

$$egin{aligned} \mathbf{z}_{\mathsf{L}} &= \mathbf{J}_{\mathsf{self,L}}(\omega) \ \mathbf{f}_{\mathsf{L}} \ \mathbf{z}_{\mathsf{R}} &= \mathbf{J}_{\mathsf{cross}}(\omega) \ \mathbf{f}_{\mathsf{L}} \end{aligned}$$

Force Response of Single Mechanical Elements

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$$egin{aligned} \mathbf{z}_{\mathrm{L}} &= \mathbf{J}_{\mathrm{self,L}}(\omega) \ \mathbf{f}_{\mathrm{L}} + \mathbf{J}_{\mathrm{cross}}(\omega) \ \mathbf{f}_{\mathrm{R}}, \ \mathbf{z}_{\mathrm{R}} &= \mathbf{J}_{\mathrm{cross}}(\omega) \ \mathbf{f}_{\mathrm{L}} + \mathbf{J}_{\mathrm{self,R}}(\omega) \ \mathbf{f}_{\mathrm{R}}. \end{aligned}$$

Real and imaginary parts of the response functions

$$J(\omega) = J'(\omega) + i J''(\omega),$$

are not independent. They are connected via Kramers-Kronig relations.

The fluctuation-dissipation theorem relates equilibrium fluctuations and the response w.r.t. external forces

$$S(\omega) = \frac{2k_{\rm B}T}{\omega}J''(\omega).$$

Recording the power-spectrum $S(\omega)$ in equilibrium is thus sufficient!

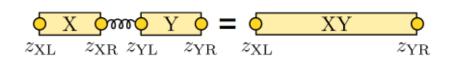
Constructing Basic Mechanical Networks

[Hinczewski, von Hansen, Netz, PNAS Dec. 2010



Serial Connection

Left end of X and right end of Y coincide and feel the same force.



Rules for response functions in series:

$$egin{align*} J_{ ext{self},\mathsf{X}}^{\mathsf{XY}} &= J_{ ext{self},\mathsf{L}}^{\mathsf{X}} - rac{\left(J_{ ext{cross}}^{\mathsf{X}}
ight)^2}{J_{ ext{self},\mathsf{R}}^{\mathsf{X}} + J_{ ext{self},\mathsf{L}}^{\mathsf{Y}}}, \ J_{ ext{self},\mathsf{Y}}^{\mathsf{XY}} &= J_{ ext{self},\mathsf{R}}^{\mathsf{Y}} - rac{\left(J_{ ext{cross}}^{\mathsf{Y}}
ight)^2}{J_{ ext{self},\mathsf{R}}^{\mathsf{X}} + J_{ ext{self},\mathsf{L}}^{\mathsf{Y}}}, \ J_{ ext{cross}}^{\mathsf{XY}} &= rac{J_{ ext{cross}}^{\mathsf{X}} J_{ ext{cross}}^{\mathsf{Y}}}{J_{ ext{self},\mathsf{R}}^{\mathsf{X}} + J_{ ext{self},\mathsf{L}}^{\mathsf{Y}}}. \end{aligned}$$

Parallel Connection

Both ends of X and Y coincide, the force is split between X and Y.

$$z_{XL} = z_{YL} \quad z_{XR} = z_{YR}$$

Rules for response functions in parallel:

DNA response functions from experiments

AND theory/simulations



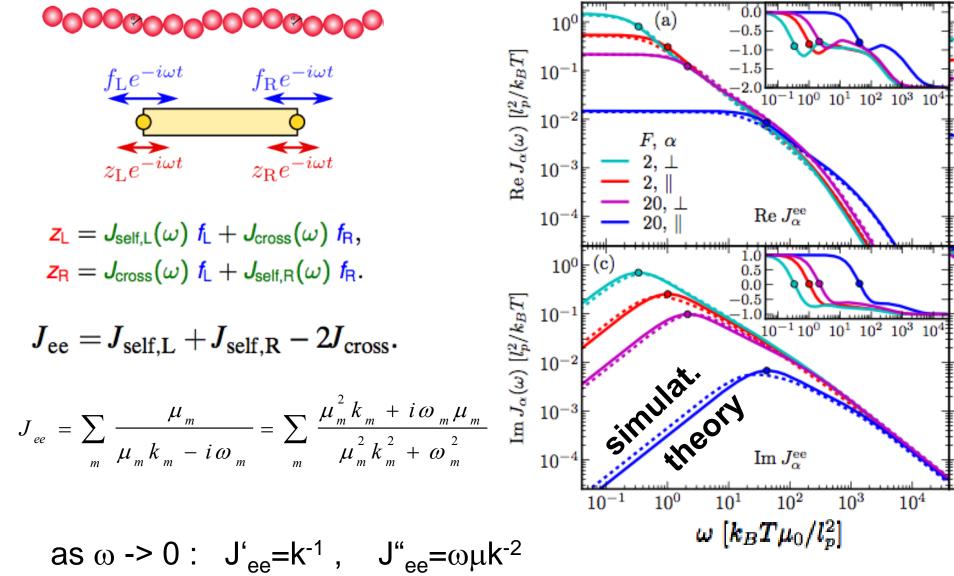
$$\begin{array}{ccc}
f_{\mathrm{L}}e^{-i\omega t} & f_{\mathrm{R}}e^{-i\omega t} \\
z_{\mathrm{L}}e^{-i\omega t} & z_{\mathrm{R}}e^{-i\omega t}
\end{array}$$

$$\mathbf{z}_{\mathsf{L}} = \mathbf{J}_{\mathsf{self,L}}(\omega) \mathbf{f}_{\mathsf{L}} + \mathbf{J}_{\mathsf{cross}}(\omega) \mathbf{f}_{\mathsf{R}},$$

$$\mathbf{z}_{\mathsf{R}} = \mathbf{J}_{\mathsf{cross}}(\omega) \mathbf{f}_{\mathsf{L}} + \mathbf{J}_{\mathsf{self},\mathsf{R}}(\omega) \mathbf{f}_{\mathsf{R}}.$$

$$J_{\text{ee}} = J_{\text{self,L}} + J_{\text{self,R}} - 2J_{\text{cross}}.$$

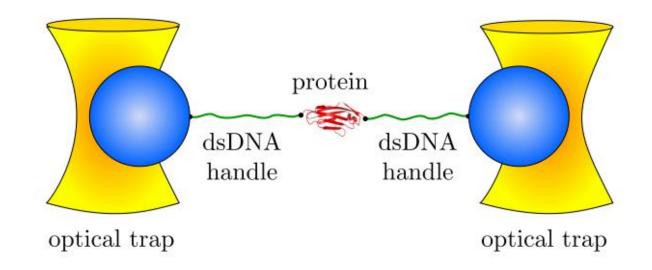
$$J_{ee} = \sum_{m} \frac{\mu_{m}}{\mu_{m} k_{m} - i \omega_{m}} = \sum_{m} \frac{\mu_{m}^{2} k_{m} + i \omega_{m} \mu_{m}}{\mu_{m}^{2} k_{m}^{2} + \omega_{m}^{2}}$$



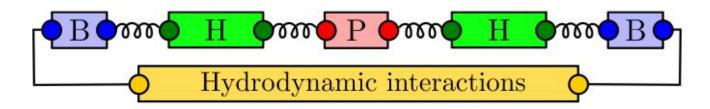
as
$$\omega -> 0$$
: $J'_{ee}=k^{-1}$, $J''_{ee}=\omega \mu k^{-2}$

Application To Optical Tweezers I

Optical tweezers dual trap setup:



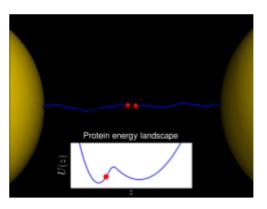
Equivalent mechanical network:



The beads in the traps, the DNA-handles, the protein as well as hydrodynamic interactions contribute to the total response of the system!

Application To Optical Tweezers II

Validation through BD simulation data:

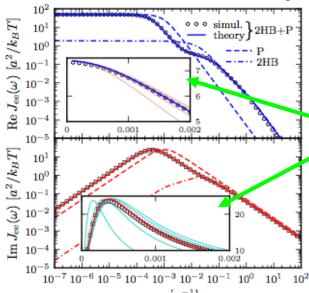


mobility/internal friction of protein extracable!!

application to exp. data: work in progress

Force response: Simulation vs Theory

2HB: 2 handle/beads without protein, 2HB+P: with protein

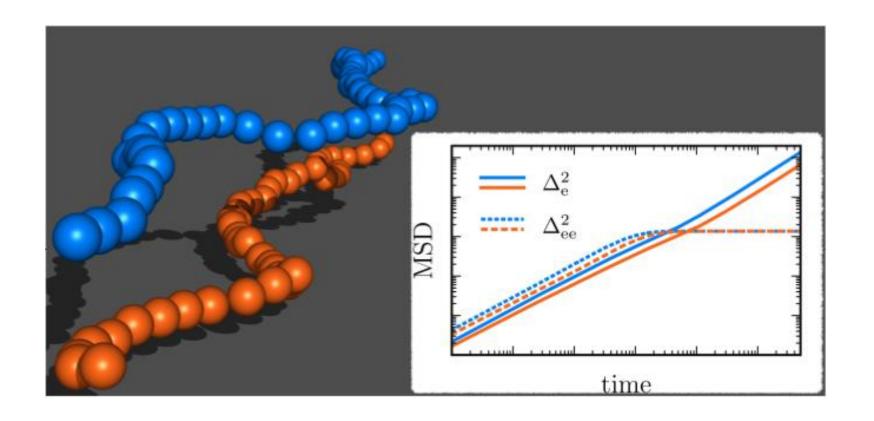


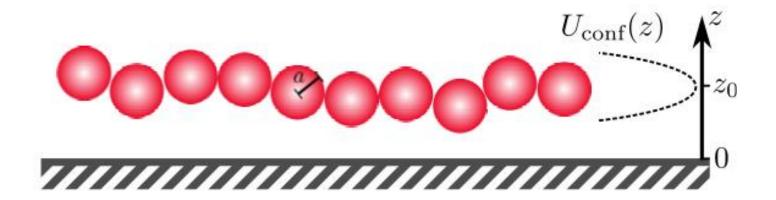
real part of total response funct. (storage contribution)

total convoluted signal with different protein viscosities

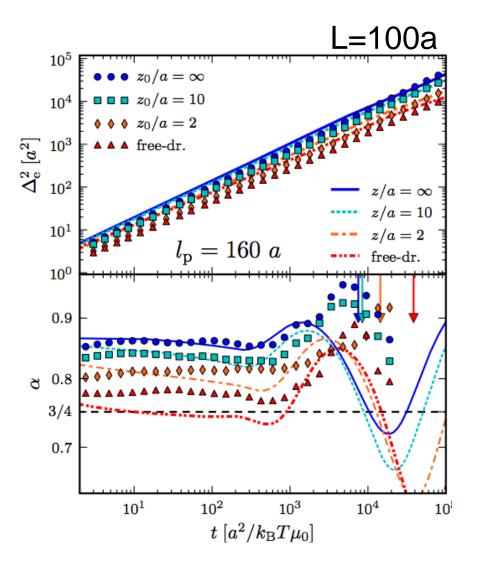
imaginary part (loss contribution)

effects of nearby surface: hydrodyn. screening, crowding





end-point MSD at varying distance z/a from a no-slip surface



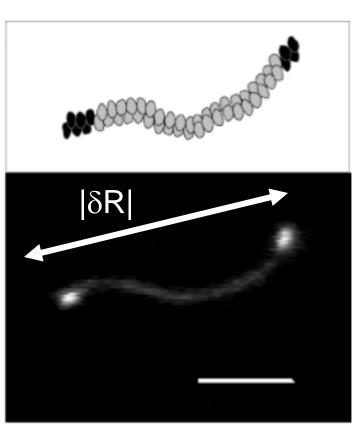
effect of wall only strong at small distances of z/a = 2! even at distance z/a strong deviations from Rouse!

Tracer Studies on F-Actin Fluctuations

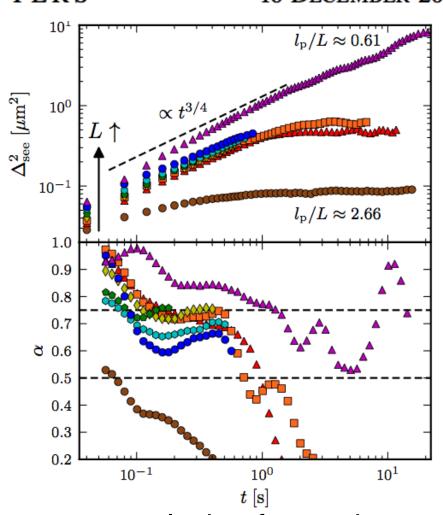
Loïc Le Goff,^{1,*} Oskar Hallatschek,² Erwin Frey,^{2,3} and François Amblard¹

PHYSICAL REVIEW LETTERS

16 DECEMBER 2002

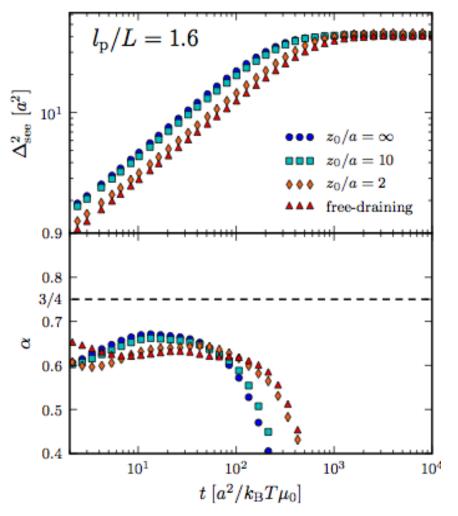


analysis based on scalar end-to-end distance (difficult in MFT!)

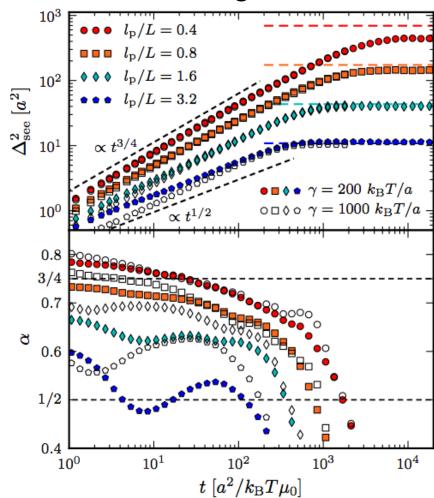


our re-analysis of exp. data: systematic depend. on I_P/L in data

no hydrodynamic effects on scalar e.-to-e. distance



but dependence on stretching modulus!

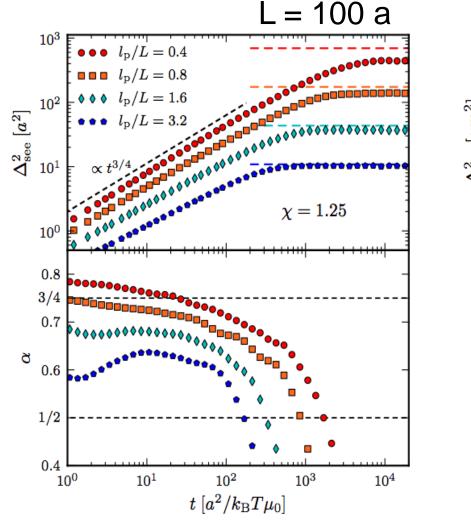


stretching modulus

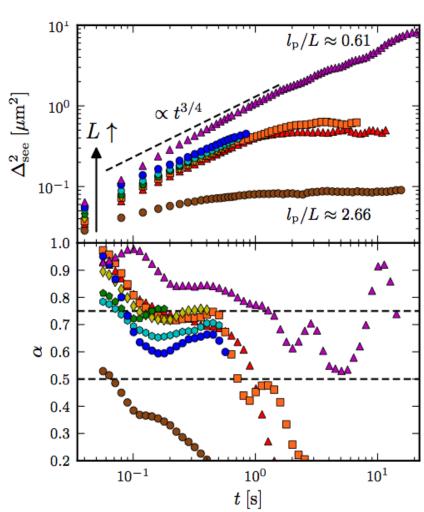
modulus bending modulus
$$U_{\mathrm{WLC}} = \left(\frac{\gamma}{4a}\right)_{i=1}^{M-1} (r_{i+1,i}-2a)^2 + \left(\frac{\kappa}{2a}\right)_{i=2}^{M-1} (1-\cos\theta_i)$$

free-drain. BD simulation for constant elasticity ratio

$$\chi \equiv rac{\gamma a^2}{4\kappa}$$



universal I_P/L dependence for isotropic elastic material ? (= weak L dependence ?)



comparison with exp. data for actin L = $6 - 25 \mu m$

self mobilities at no-slip surface on Rotne-Prager level

$$\mu_{\parallel}^{\text{RPB}}(z) = \mu_0 \left(1 - \frac{9a}{16z} + \frac{1}{8} \left(\frac{a}{z} \right)^3 \right) + \mathcal{O}(a^4),$$

$$\mu_{\perp}^{\text{RPB}}(z) = \mu_0 \left(1 - \frac{9a}{8z} + \frac{1}{2} \left(\frac{a}{z} \right)^3 \right) + \mathcal{O}(a^4).$$

$$\begin{array}{c} 1.0 \\ 0.8 \\ \hline 0.8 \\ 0.4 \\ 0.2 \\ 0.0 \\ \end{array}$$

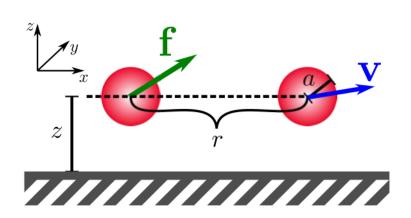
$$\begin{array}{c} \mu_{\parallel}^{\text{PJ}} \\ -\mu_{\parallel}^{\text{SJ}} \\ -\mu_{\perp}^{\text{SJ}} \\ -\mu_{\perp}^{\text{RPB}} \\ \end{array}$$

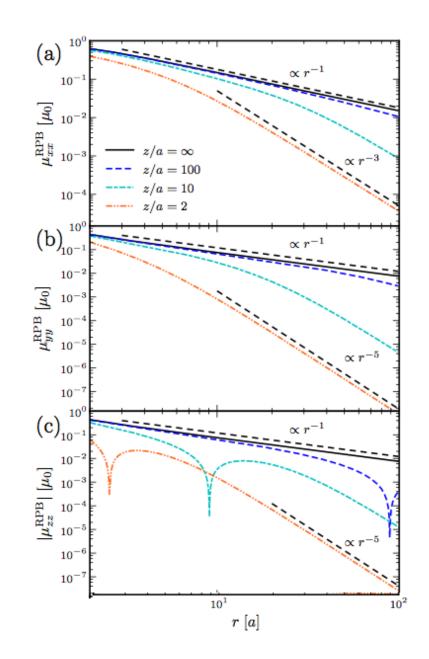
$$\begin{array}{c} \mu_{\perp}^{\text{RPB}} \\ -\mu_{\perp}^{\text{RPB}} \\ -\mu_{\perp}^{\text{RPB}} \\ \end{array}$$

$$z [a]$$

FIG. 1. Parallel (||) and perpendicular (\perp) self-mobilities of a sphere of radius a located at a vertical distance z from a no-slip wall (z=0). The approximations of Eqs. 8 and 9 (dashed lines) are compared to the result for the parallel mobility of Eq. 10 (solid blue line), and to the exact expression for the perpendicular mobility of Eq. 11 (solid red line). Self-mobilities are given in units of the bare self-mobility $\mu_0 = 1/(6\pi\eta a)$ in a fluid of viscosity η ; the region z < a is inaccessible due to excluded-volume effects.

hydrodynamic screening at a surface





Entropic Repulsion between Fluctuating Surfaces

$$V_{Fl}(\ell)pprox c_{Fl}T^2/\kappa\ell^2$$
 $V_{Fl}(\ell)pprox (b_0T/a_\parallel^2)e^{-\ell/l_\sigma}(l_\sigma/\ell)^{1/4}$ $l_\sigma\equiv\sqrt{T/2\pi\overline{\sigma}}.$

$$\sigma \simeq 10^{-9} \text{ to } 10^{-6} J/m^2,$$

tension of rupture, which is $\simeq 10^{-3} J/m^2$.

crossover length
$$l^* = \hat{z}^* \sqrt{T/\sigma} \simeq 2 - 2000 nm$$

crossover pressure
$$P^* \simeq (\hat{p}^*/c_{max}^2)\sqrt{\sigma^3 T/\kappa^2} \simeq 10^{-7} - 10^2 J/m^3$$
,

Netz, Lipowsky, EPL 29, 345 (1995)