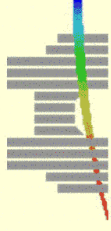


## Physics of contacts and cohesion effects in granular media

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Humidity affects friction properties of a number of materials

- Time and velocity dependent friction in rocks (Dieterich & Conrad 1984)
- Stiction in Micro-Electro-Mechanic-Systems (Scherge & Schaefer 1998)
- Granular materials (Hornbaker & al 1997)



<http://perso.wanadoo.fr/philippe.boeuff/robert/physique/chateau.htm>

This talk : Time dependent friction in granular material

Dieterich & Conrad 1984, friction of rocks :

« Drying inhibits the time-dependant increases in the coefficient of friction of nominally stationary surfaces »

Is there a similar effect in a granular material ?

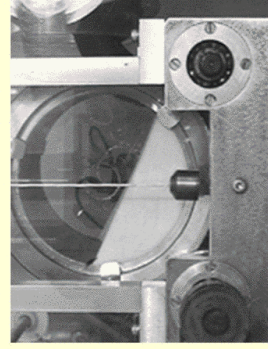
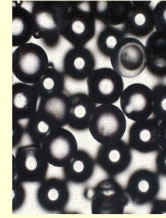
What are the mechanisms ?

## Time-dependant static friction in a granular medium

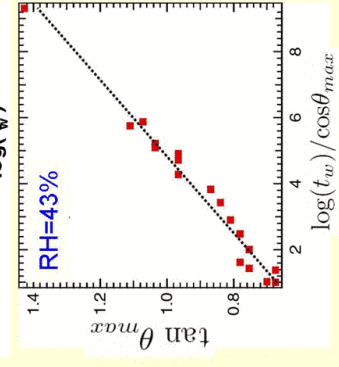
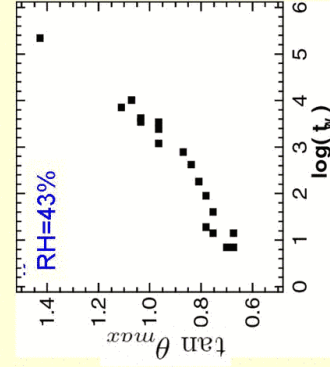
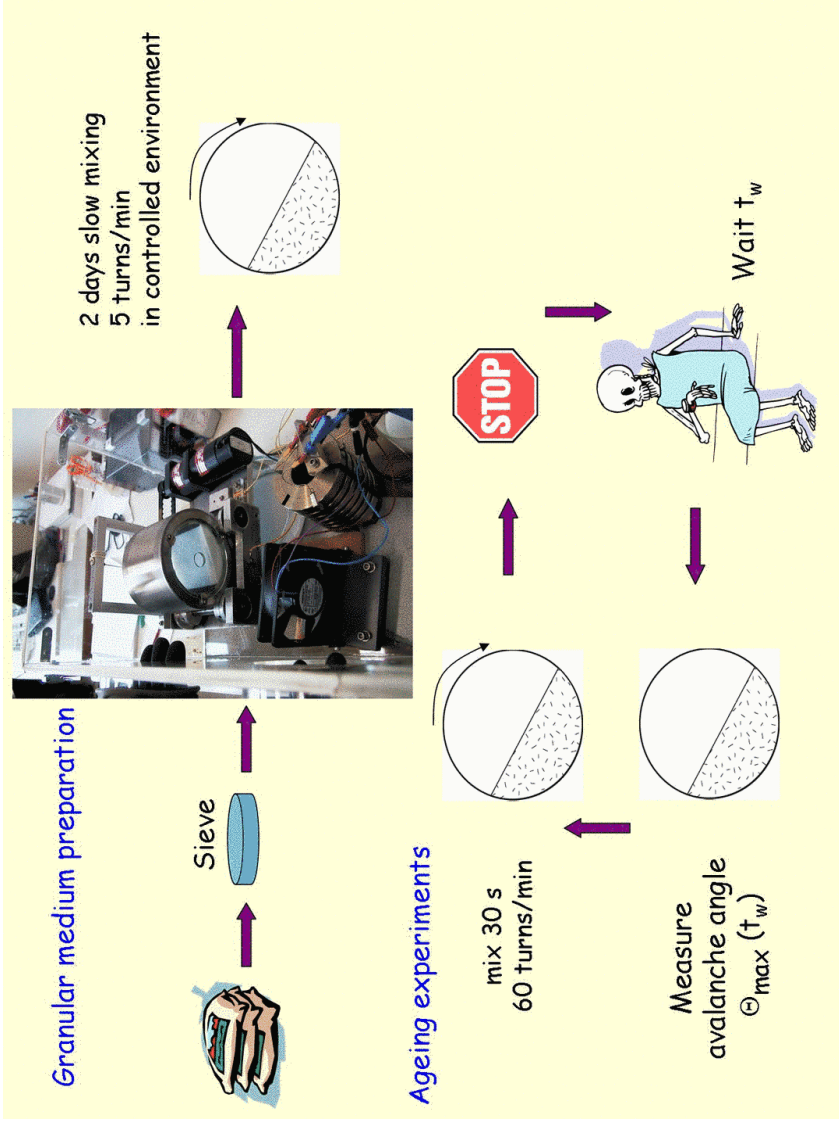
L.Bocquet, E. Charlaix, S. Ciliberto, J. Crassous Nature 1998  
Restagno, Ursini, Gayvallet, Charlaix, PRE 66 021304 (2002)

Maximum stability angle of a granular heap  
in a rotating drum  
as a function of resting time

Glass beads :  
200 - 250  $\mu\text{m}$



Environment:  
Temperature  
 $29,0 \pm 0,1 \text{ } ^\circ\text{C}$   
Humidity controlled  
at  $\pm 0,5 \%$   
 $\text{RH} = P_V / P_{\text{sat}}$



- Slow increase of friction in time (5 time decades)
- Evidence of cohesion effects

$$\theta_{max} > 90^\circ \text{ at RH} > 50\% \text{ and large } t_w$$

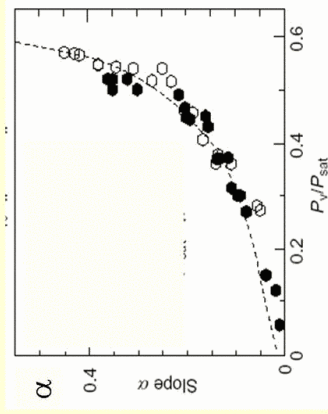
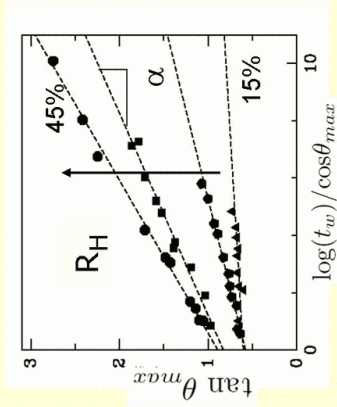
Coulomb's law with adhesion

$$\tan \theta_{max} = \mu_s \left( 1 + \frac{F_{adh}}{N \cos \theta_{max}} \right)$$

Weight and adhesion force  
for the layer above failure plane

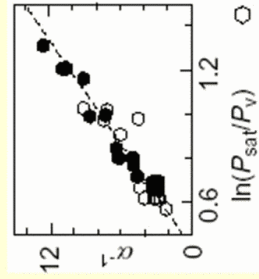
### Influence of humidity on time-dependant friction

L. Bocquet, E. Charlaix, S. Ciliberto, J. Crassous Nature 1998



No ageing at low RH

Empirical dependance :  $\alpha \sim 1 / \ln RH$



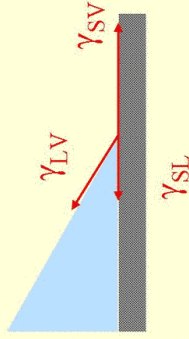
### Physico-chemical mechanisms for water-induced effects on friction :

- Water-assisted plastic deformation
- Contact strengthening (hydrogen bonding, desorption of water)
- Pressure solution
- Subcritical crack growth
- Capillary condensation



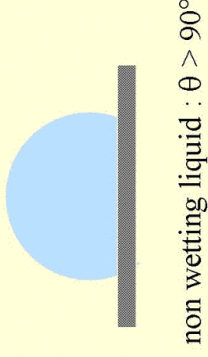
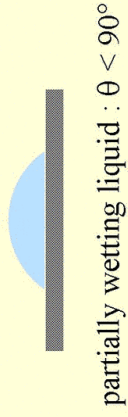
### BASICS OF WETTING

- $\gamma_{SL}$  : solid-liquid surface tension
- $\gamma_{SV}$  : solid-vapor surface tension
- $\gamma_{LV}$  : liquid-vapor surface tension



equilibrium contact angle :  
Young Dupré relation

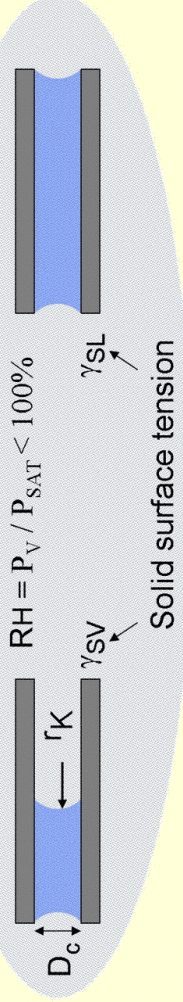
$$\gamma_{SV} - \gamma_{SL} = \gamma_{LV} \cos \theta$$



### Capillary condensation between surfaces

$$\Delta\mu = k_B T |\ln RH|$$

$$RH = P_V / P_{SAT} < 100\%$$



Liquid phase **stable** if

$$D < D_c = 2 r_K \cos \theta$$

partial wetting  $\theta > 0$

**Water :**

RH 50% 77%

$r_K$  7,8 Å 2nm

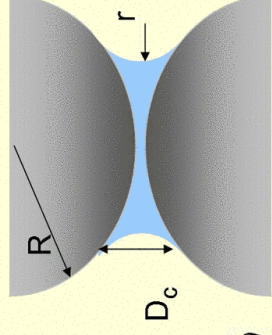
Pressure in the liquid phase 100 MPa 35 MPa

$$r_K = \frac{\gamma_{LV}}{\rho_L k_B T \ln(P_{sat} / P_V)}$$

Kelvin radius :  
equilibrium curved LV  
interface in undersaturation

### Capillary force between smooth grains

roughness << Liquid Bridge height  
macroscopic capillarity  
R >> LB height



$$F_{cap} = 2\pi R\gamma_{LV} \left( \cos\theta - \frac{D}{2r} \right)$$

➤ Maximum capillary force :  $F_{cap} = 2\pi R\gamma_{LV} \cos\theta$

➤ Estimation of the normal stress induced by capillary adhesion in a g.m. :  
partial wetting  $\theta > 0$

$$\sigma_{adh} = 2\pi R\gamma_{LV} \cos\theta \frac{N_{bead}}{\text{unit area}} \sim \frac{2\pi\gamma_{LV} \cos\theta}{R}$$

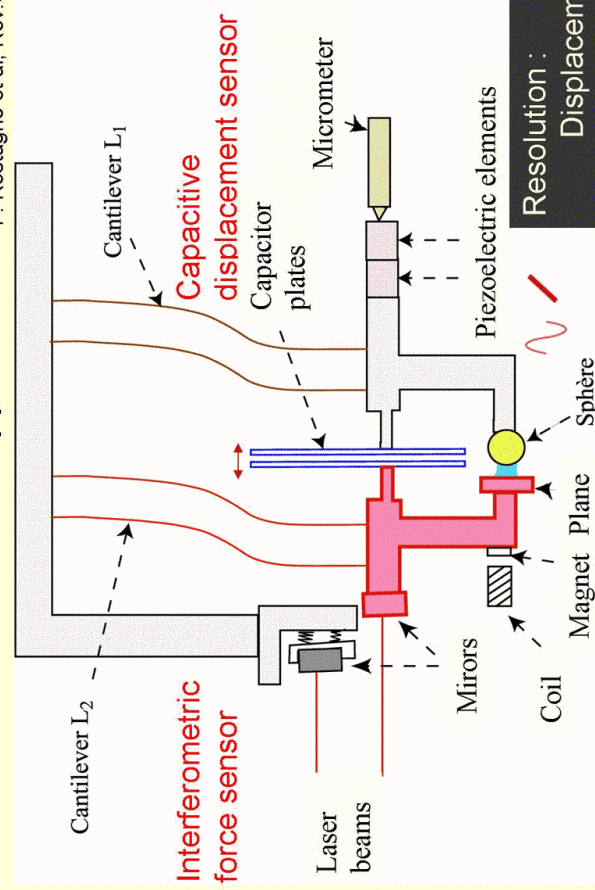
➤ "Capillary length" in a g.m. :  $\rho g l_{cap} = \sigma_{adh}$   $l_{cap} \sim \frac{2\pi\gamma_{LV} \cos\theta}{\rho g R}$

water,  $\theta=0$ ,  $R=10\mu\text{m}$   
 $R=10\text{nm}$

$\sigma_{adh} \sim 0.02 \text{ MPa}$   $l_{cap} \sim 1 \text{ m}$   
 $\sigma_{adh} \sim 20 \text{ MPa}$

### Surface Force Apparatus

F. Restagno et al, Rev.Sci. Inst. 2002



Resolution :	
Displacement	Force
Static 0.1 nm	600 nN

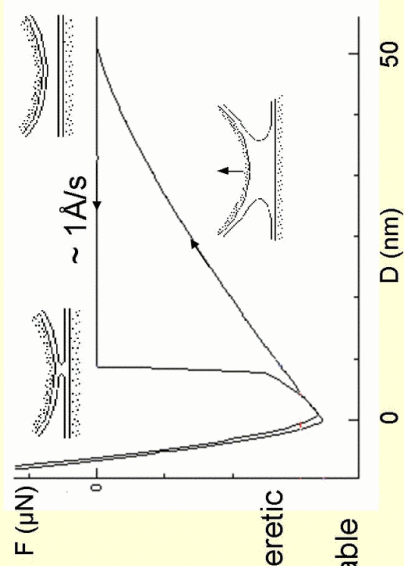
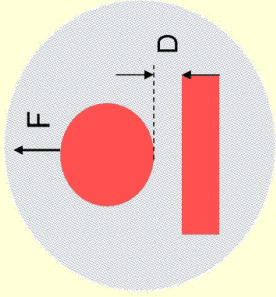
Israealachvili et al, JCIS 1981, PRB 1989, PNAS 2003

Christenson et al, JCIS 1988, JCIS 1989, PRL 1994, J Phys Cond Mat 2001

Crassous et al, Europhys Letter 1994, J. Chem Phys 2005

### Capillary condensation between smooth grains :

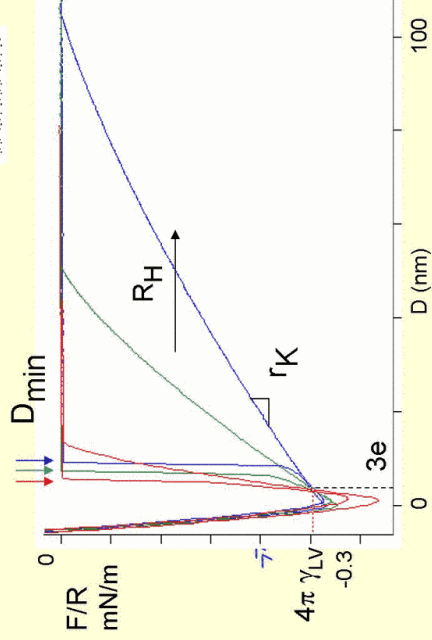
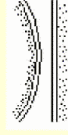
#### Surface Forces experiments



Crassous, Loubet Charlaix, Europhys Letter 1994

- Capillary force is strongly hysteretic
- Liquid is stable, vapor metastable
- How does the LB form ?

### Liquid Bridges in perfect wetting ( $\theta=0$ )



The LB forms by spinodal decomposition (instability of the wetting films covering the surfaces)

Christenson et al, PRL 1994  
Crassous et al, EPL 1994

Van der Waals interactions :

$$\frac{\gamma_{LV}}{r_K} = \frac{-A_{SLV}}{6\pi e^3}$$

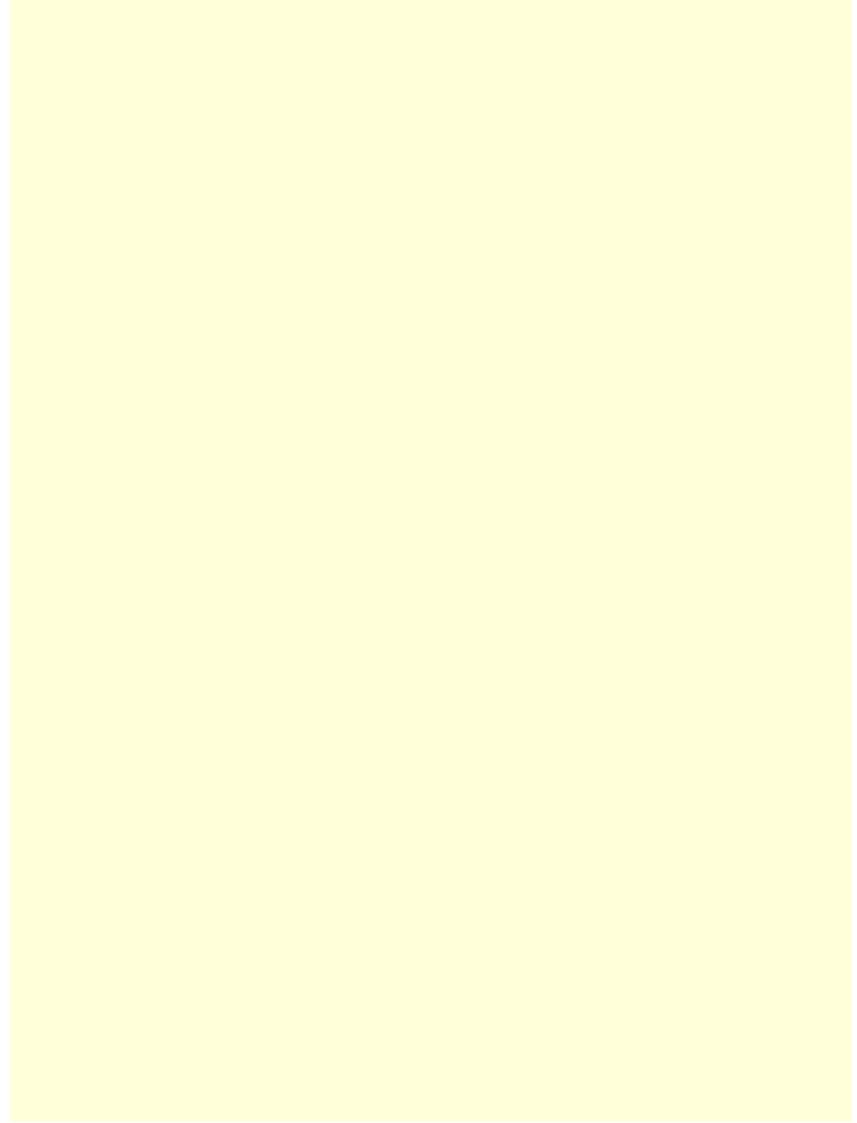
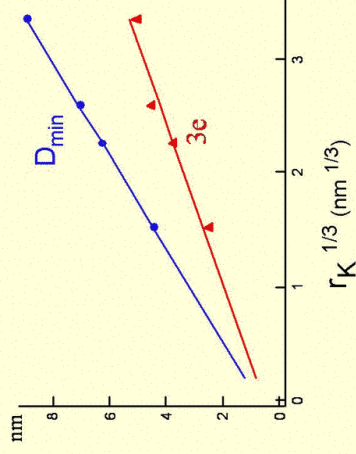
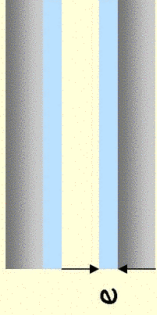
$A_{SLV}$  : Hamaker constant

Capillary force :

$$F_{cap} = 4\pi R\gamma_{LV} \left( 1 - \frac{D - 3e}{2r_K} \right)$$

Distance for films instability

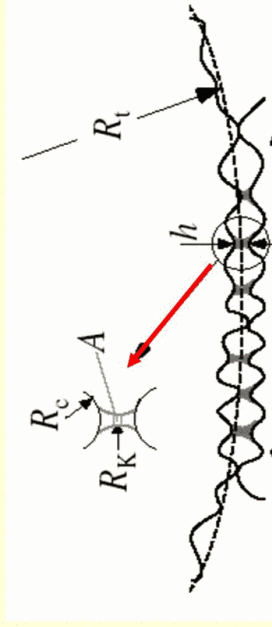
$$D_{sp} = e f \left( \frac{A_{SLV}}{A_{LL}} \right)$$





### Slow kinetics of capillary condensation on rough surfaces

Bocquet, Charlaix, Ciliberto, Crassous Nature 1998



#### Surface parameters

Radius of curvature  $R_c$  of asperities

Random gap  $h$  at condensation sites

Width of  $h$  distribution :  $\lambda$

$N_{\text{site}} (\leq h) = N_0 + h/\lambda$

#### Fluid parameters

Undersaturation

$$\Delta\mu = k_B T |\ln RH|$$

$$\text{Kelvin's radius } r_K = \frac{\gamma_{LV}}{\rho_L \Delta\mu}$$

➤ Activation energy at a given site

$$E_{ACT}^* = \rho_L \Delta\mu A h$$

➤ Typical condensation time for an asperity of height  $h$

$$t = t_A \exp\left(\frac{\Delta\mu \rho_L A h}{k_B T}\right)$$

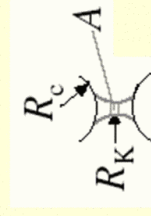
➤ Maximum height of asperity having condensed at time  $t_w$  :

$$h(t_w) = \frac{\ln(t_w/t_A)}{|\ln RH| \rho_L A}$$

➤ Capillary force at time  $t_w$  :  $F_{cap}(t_w) = 2\pi\gamma_{LV} R_c N_{\text{site}} [h \leq h(t_w)]$

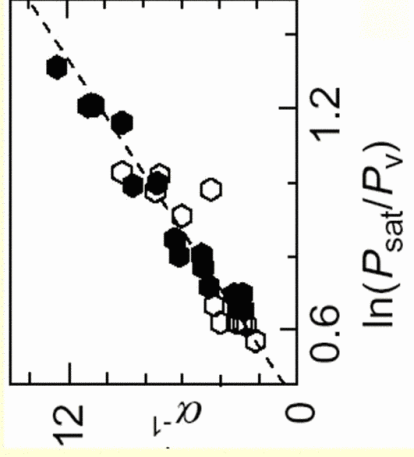
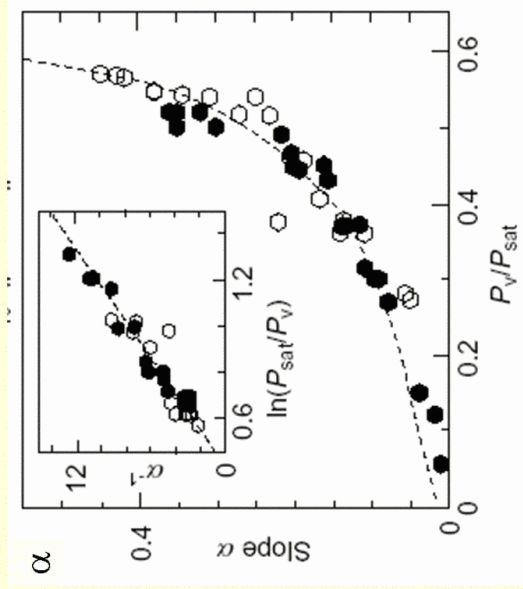
➤ Friction at contact age  $t_w$  :

$$\mu_s = \mu_0 + \alpha \ln t_w / t_A$$



$$= \underbrace{\frac{R_c}{\lambda A \rho_L |\ln RH|}}_{\text{roughness}} \ln \frac{t_w}{t_o} \quad \text{environment}$$

Humidity dependence in glass beads

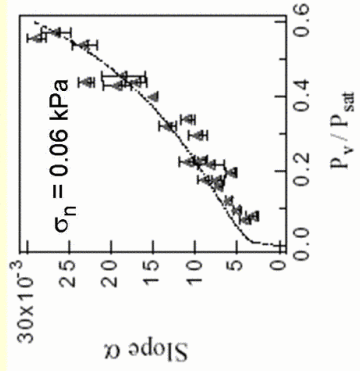


Ageing of static friction in humidity of bristol paper, glass and teflon

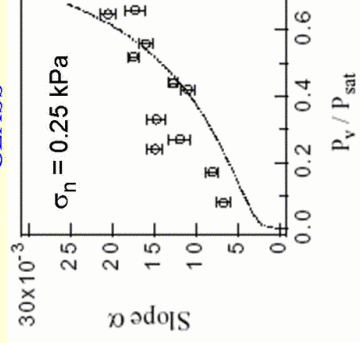
Crassous, Bocquet, Ciliberto, Laroche EPL 1999

$$\mu_s = \mu_0 + \alpha \ln t_w$$

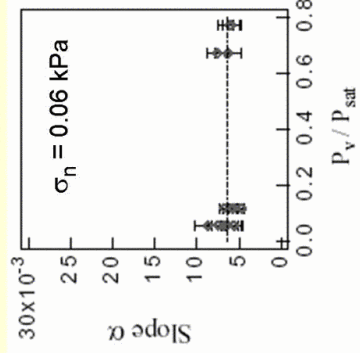
BRISTOL



GLASS



TEFLON



Highly hydrophilic

hydrophilic

hydrophobic

### Amplitude of ageing induced by activated LB condensation

In this mechanism the increase in friction is due to the increase in cohesion :

$$\Delta\mu = \mu \frac{F_{adh}}{N} \leftarrow \text{external normal load}$$

The amplitude of ageing depends on the ratio of capillary pressure to external normal stress

$$\frac{\Delta\mu}{\mu} = \frac{P_{cap}}{\sigma_n} \frac{\Delta A_{LB}}{A}$$

external normal stress  
fraction of surface area lying in LB

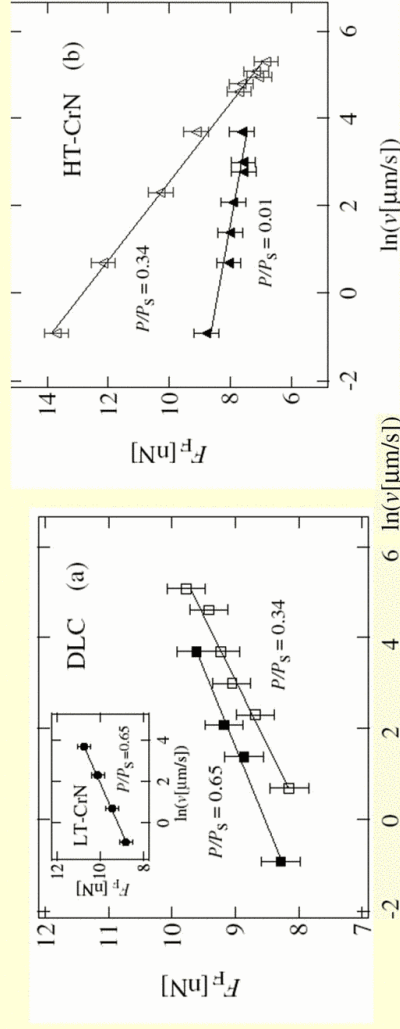
In Crassous & al experiments :

$$\text{Over } 10^4 \text{ s at RH=50\% : } \Delta\mu=0.015 \Rightarrow \frac{\Delta A_{LB}}{A} \sim 7 \cdot 10^{-7}$$

### Kinetics of capillary condensation in sliding nanoscopic friction

E. Riedo, F. Levy, H. Brune, PRL 2002

Sliding friction measure with an AFM silicon tip



Hydrophobic materials :  
Diamond Like Carbon ( $\theta=85^\circ$ )  
LT- CrN ( $\theta=93^\circ$ )

Friction is strengthening with velocity  
Low influence of humidity

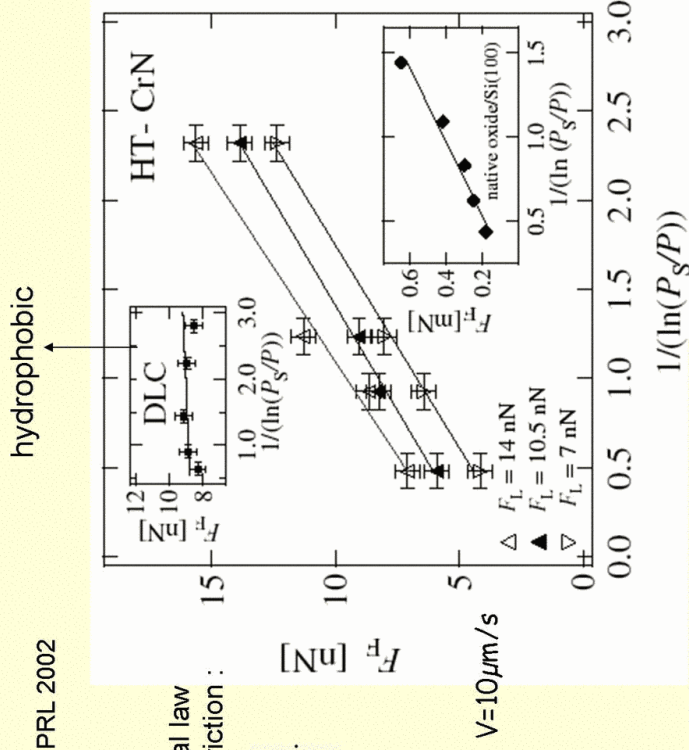
Hydrophilic material  
HT- CrN ( $\theta=45^\circ$ )

Friction is weakening with velocity  
High influence of humidity

E. Riedo, F. Levy, H. Brune, PRL 2002

At fixed velocity : empirical law for effect of humidity on friction :

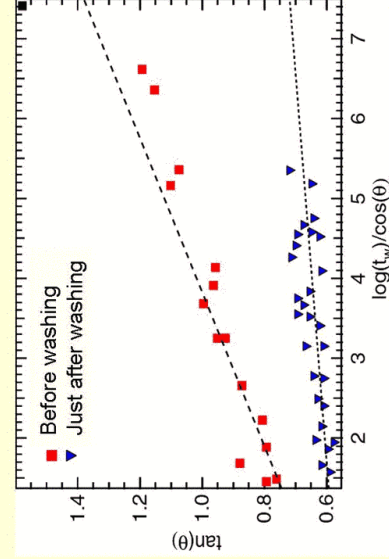
$$F_F = F_{0p} + F_{1p} \frac{P_s}{\ln P}$$



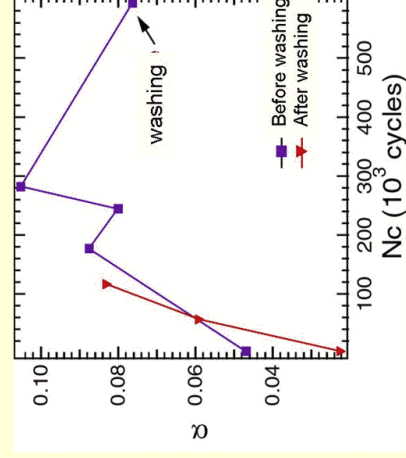
$$\bar{F}_F = \mu \bar{F}_N + m \ln \frac{v}{v_B} - \mu \frac{2\pi R \cos \theta}{\lambda A \rho_L} \frac{1}{|\ln R_H|} \ln \frac{v}{v_A}$$

### Influence of wear

Restagno, Ursini, Gayvallet, Charlaix, PRE 66 021304 (2002)



- Washing : suppresses fine particles
- Ageing increases with wear



Nb of drum turns



## Summary

- ❑ Humidity induces logarithmic ageing of static friction in granular media (glass beads), as measured by the maximum avalanche angle
- The increase in friction is associated with cohesion effects
- The amplitude of ageing (slope of the  $\ln t$  dependence) follows an empirical law in  $1/\ln RH$
- ❑ These features can be reproduced by a model of thermally activated condensation of liquid bridges between rough surfaces
- ❑ This mechanism also accounts for ageing of static friction in materials (glass, bristol) at low normal load
- ❑ Ageing is significantly enhanced by the presence of fine particules created by wear