

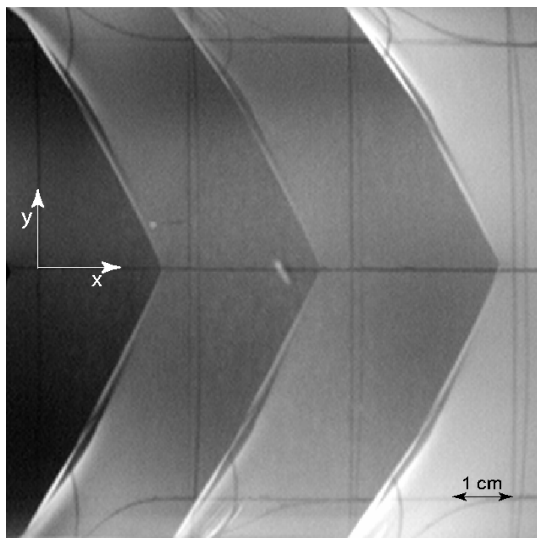


Rupture of Rubber

Experiment: Paul Petersan, Robert Deegan, Harry Swinney

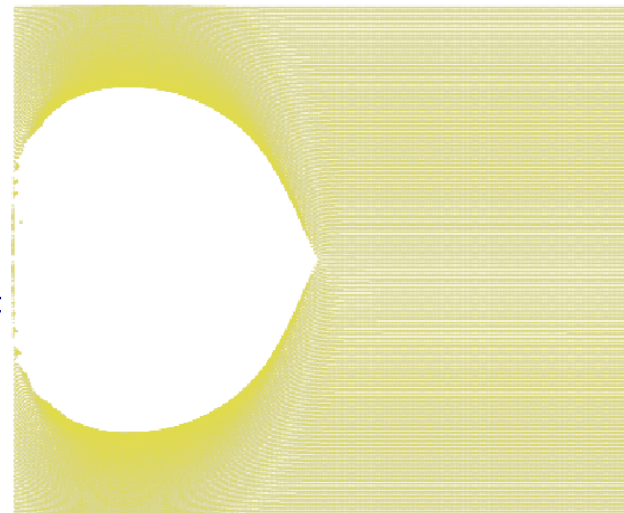
Theory: Michael Marder

Center for Nonlinear Dynamics
and Department of Physics
The University of Texas at Austin



PRL **93** 015505
(2004)

PRL **88** 014304
(2002)



PRL **94** 048001
(2005)

cond-mat/0504613

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Outline

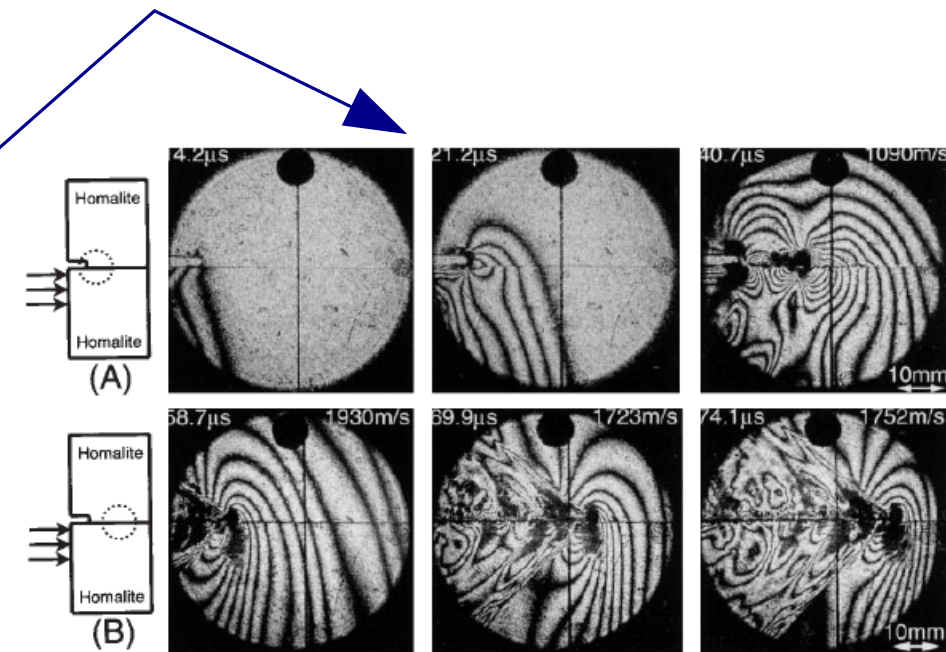
- Background: Limiting Speed of Cracks
- Experimental Observations
 - Oscillations
 - Sound and Rupture Speeds
- Numerical Investigations
 - Multi-Particle Modeling
 - Explorations
- Theory
 - Elementary Shock Theory
 - Continuum Theory
 - Discrete Theory and Scaling



Background

Limiting Speed of Cracks

- Rayleigh wave speed limits cracks in tension (Yoffe, 1951; Stroh, 1957; Freund, 1972)
- Shear waves can also travel at $\sqrt{2}c_s$ (Andrews, 1976; Burridge, Conn and Freund, 1979; Rosakis, Samudrala, Coker, 1999; Gao, Huang, Abraham, 2001)
- In a discrete medium, there is no limit to the speed of tensile cracks (Slepyan, 1982; MM, 1995; Buehler, Gao, and Abraham, 2003)
- Integrity of crack surface behind tip is key to whether supersonic solutions survive (Ravi-Chandar and Knauss, 1984; Fineberg et al, 1991; MM)



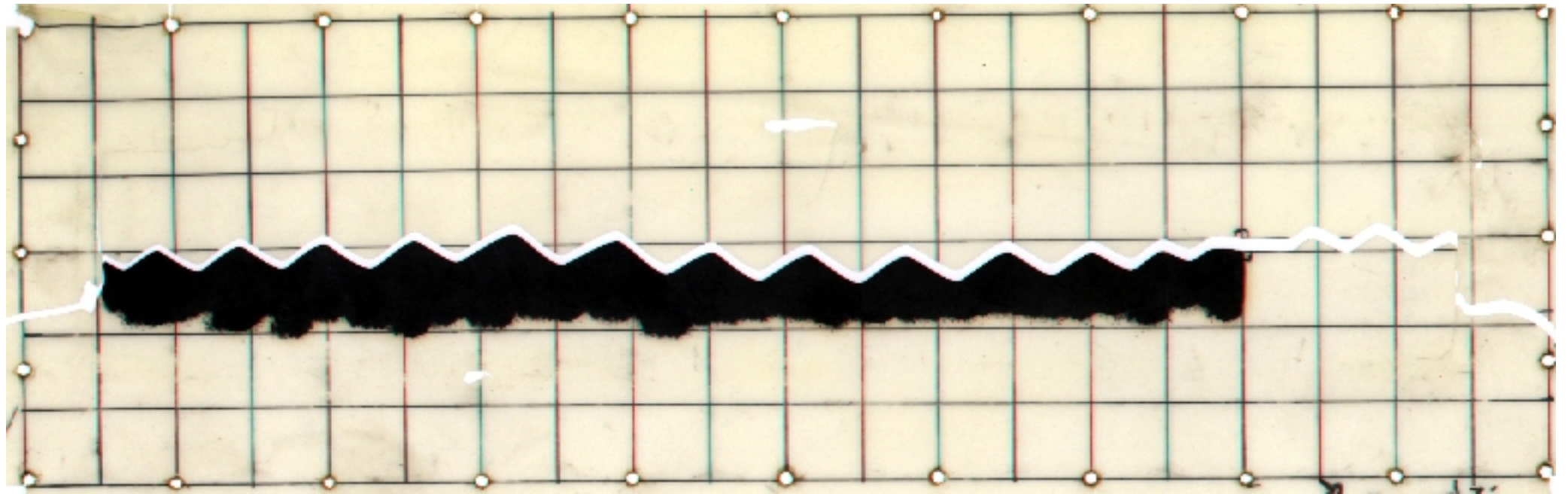
Experimental Observations

Balloons and First Experiments

Balloons

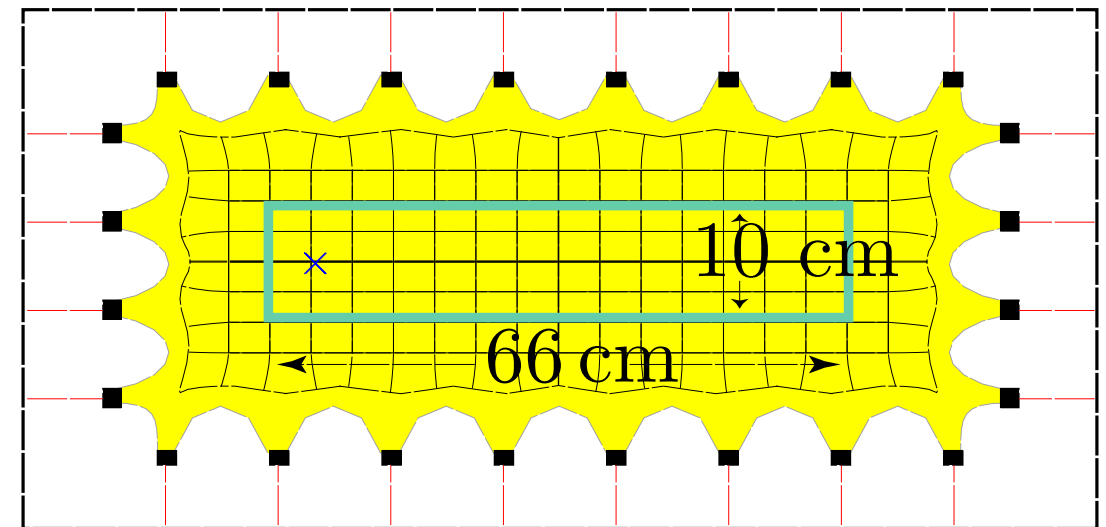
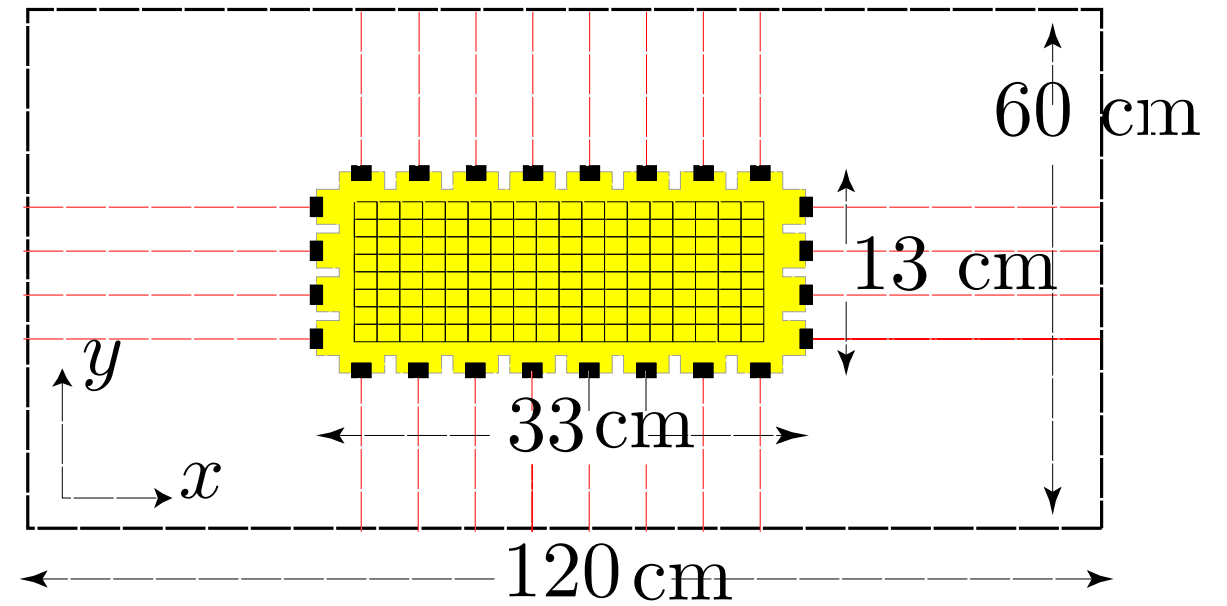
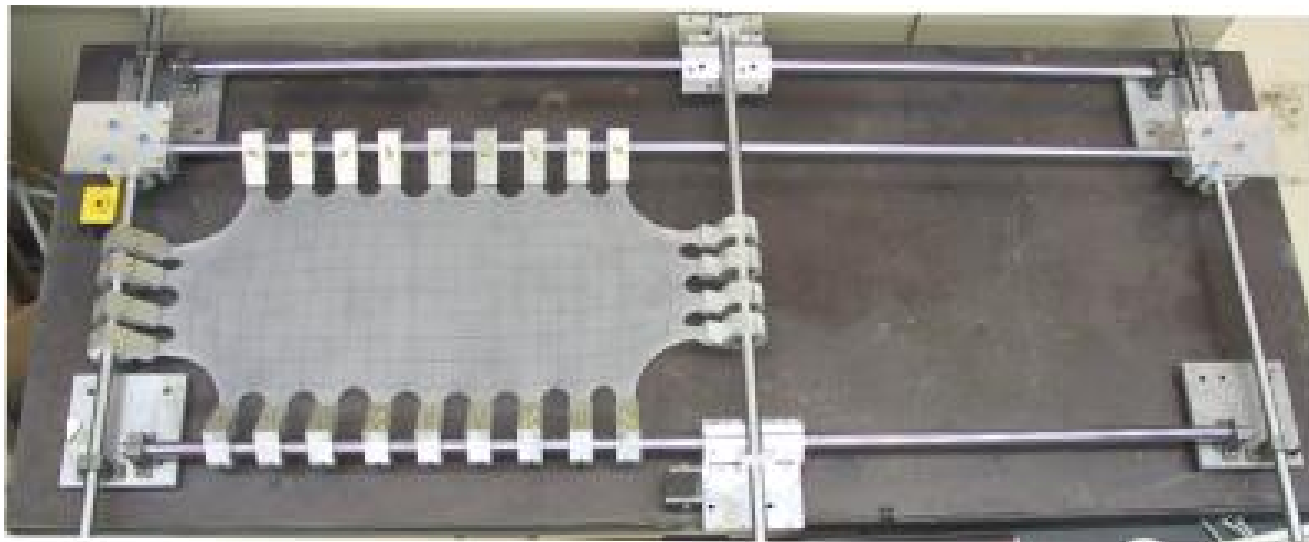


Controlled Experiments



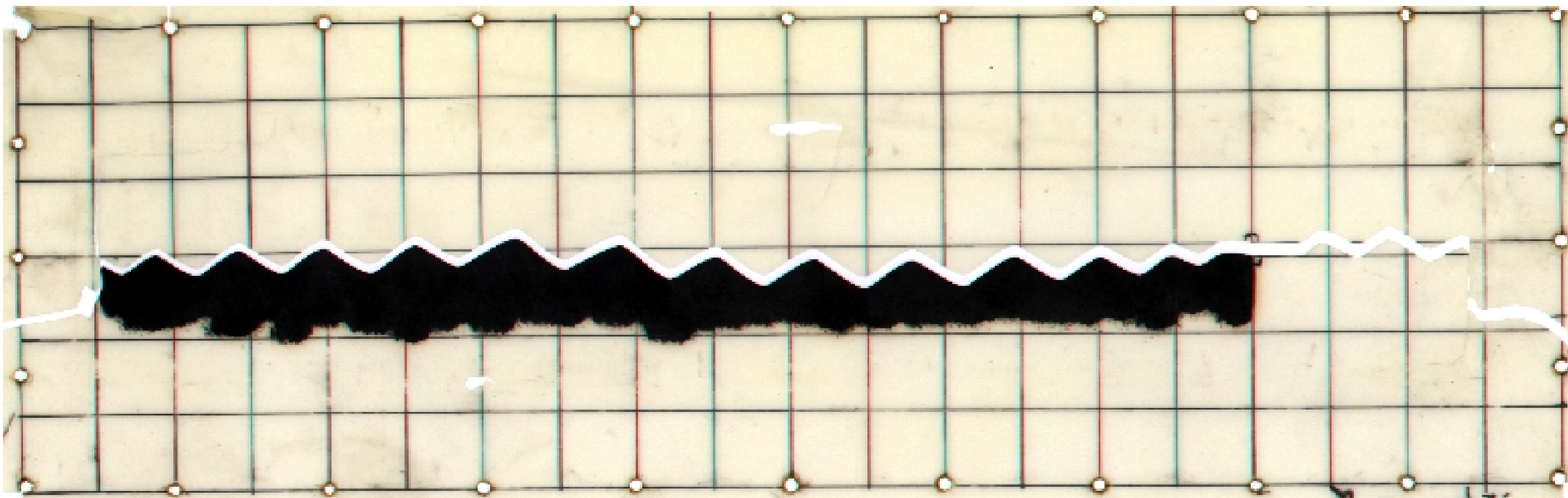
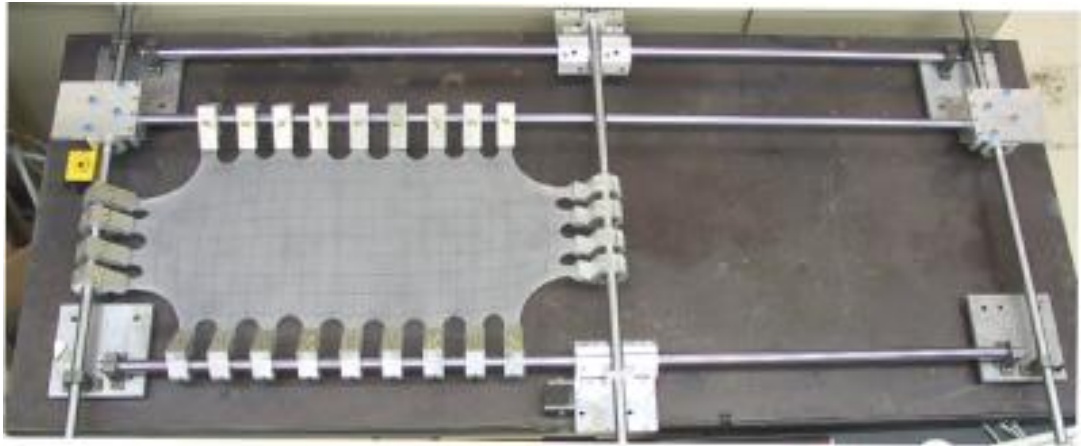
Experimental Observations

Apparatus



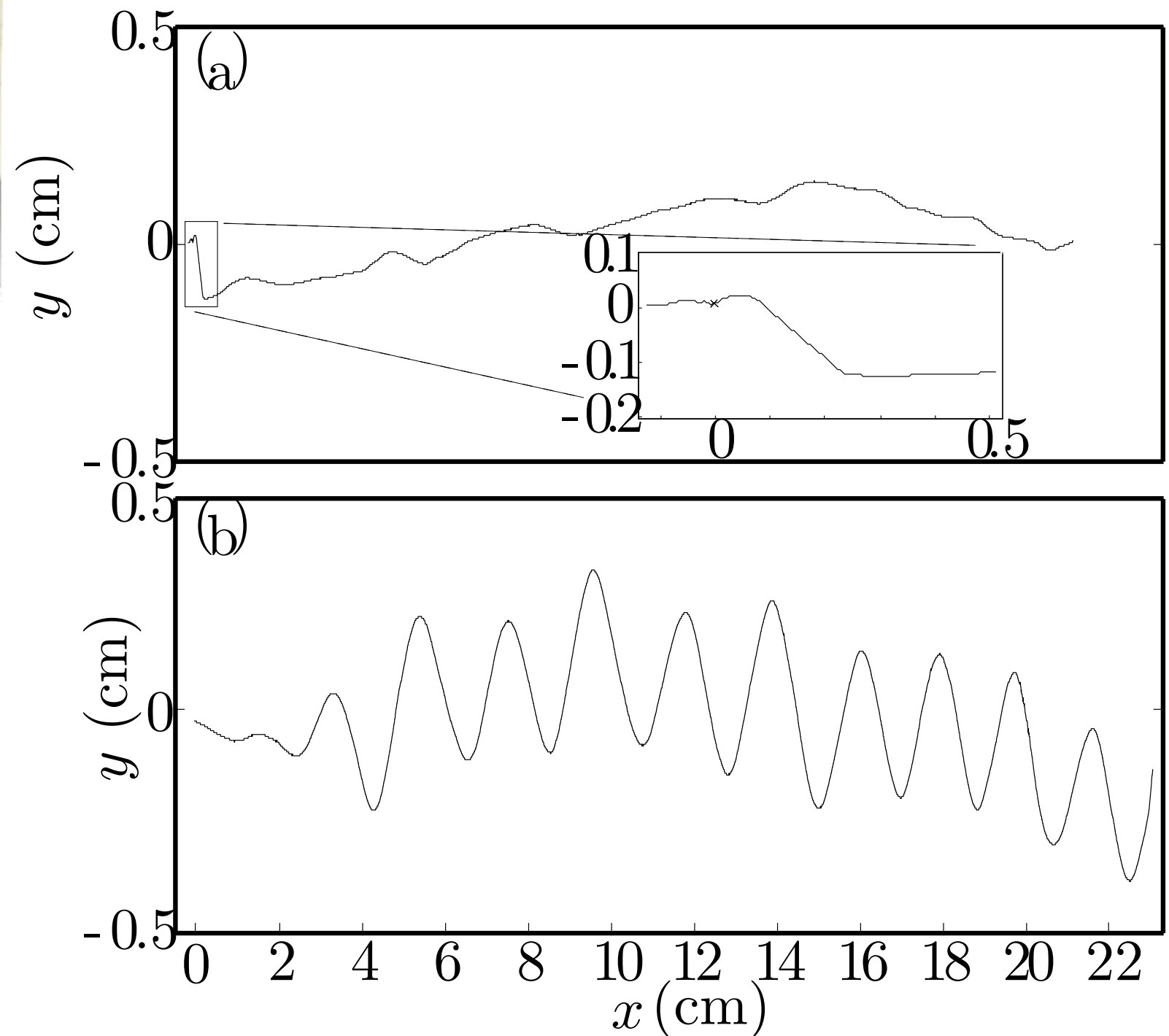
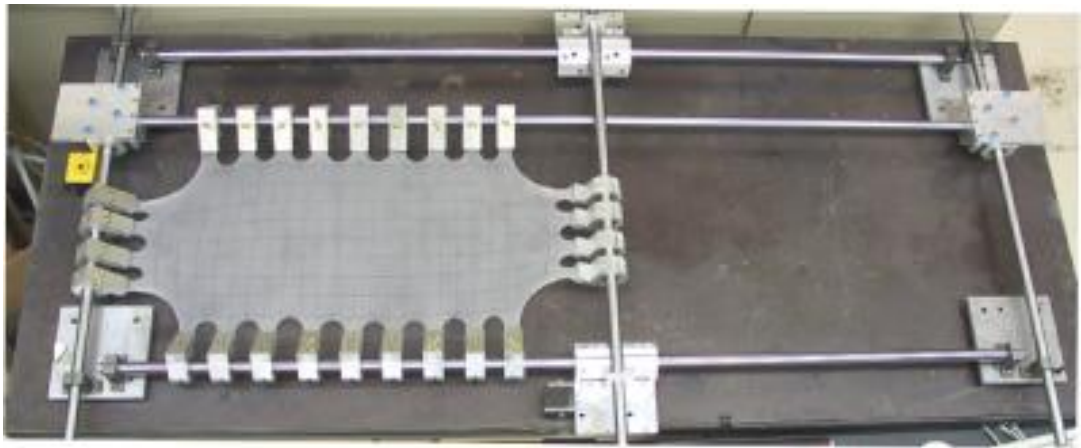
Experimental Observations

Oscillations



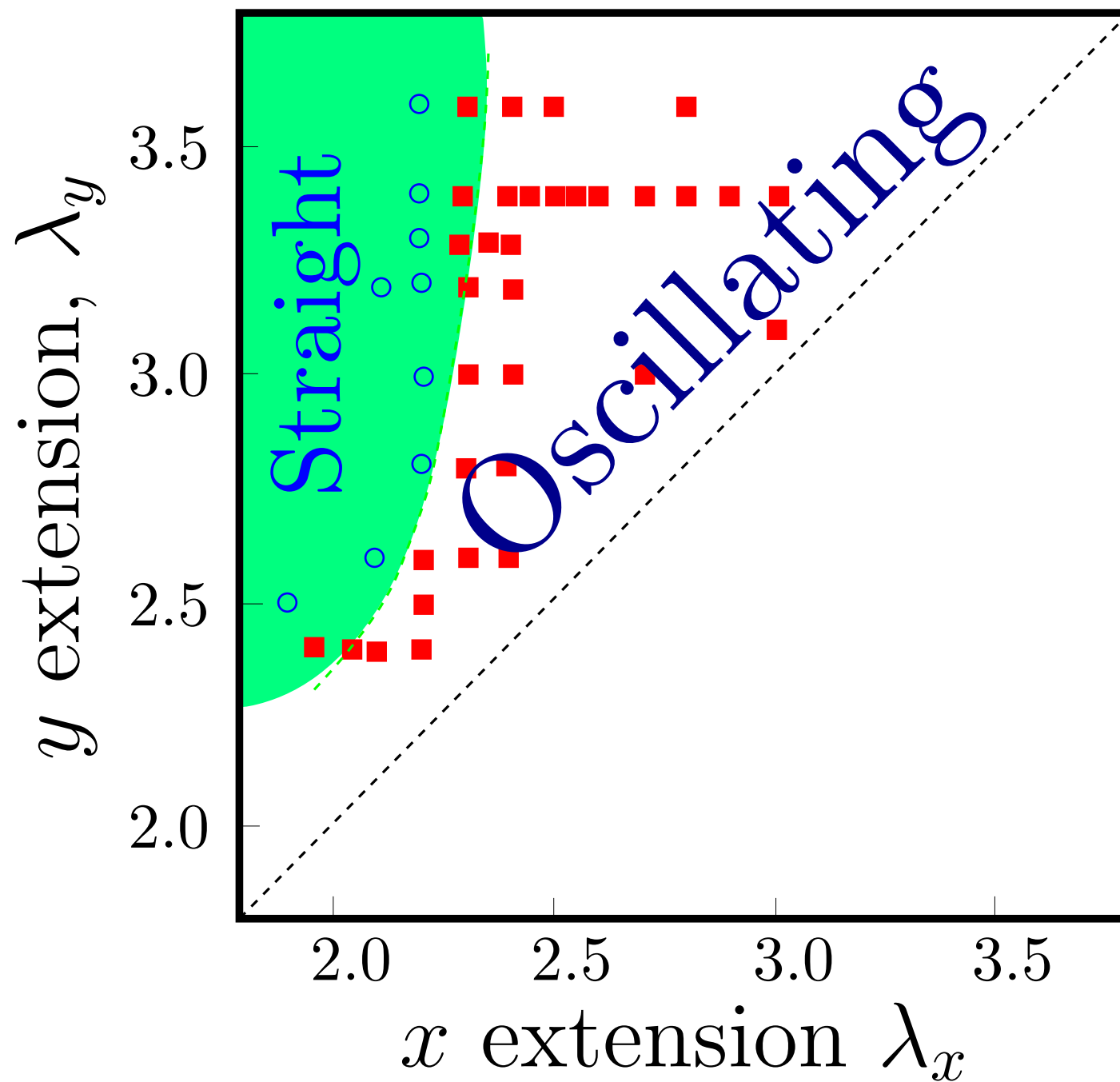
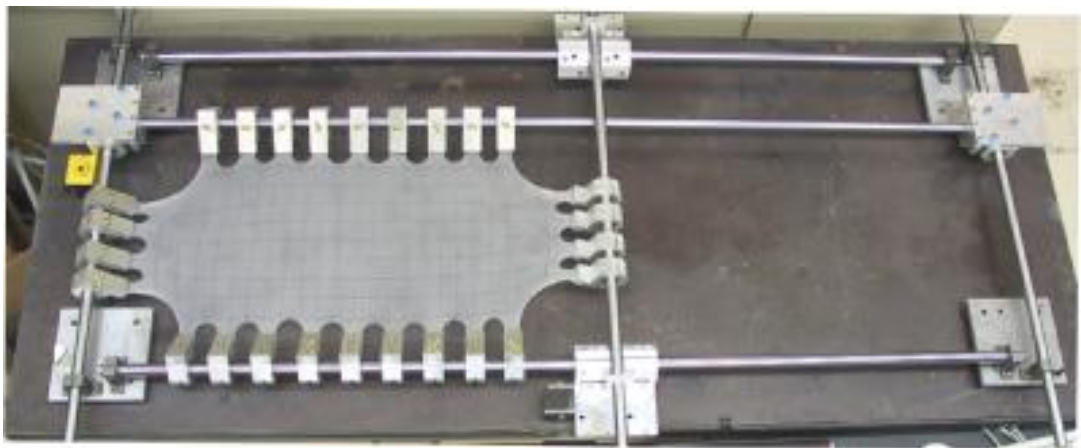
Experimental Observations

Oscillations



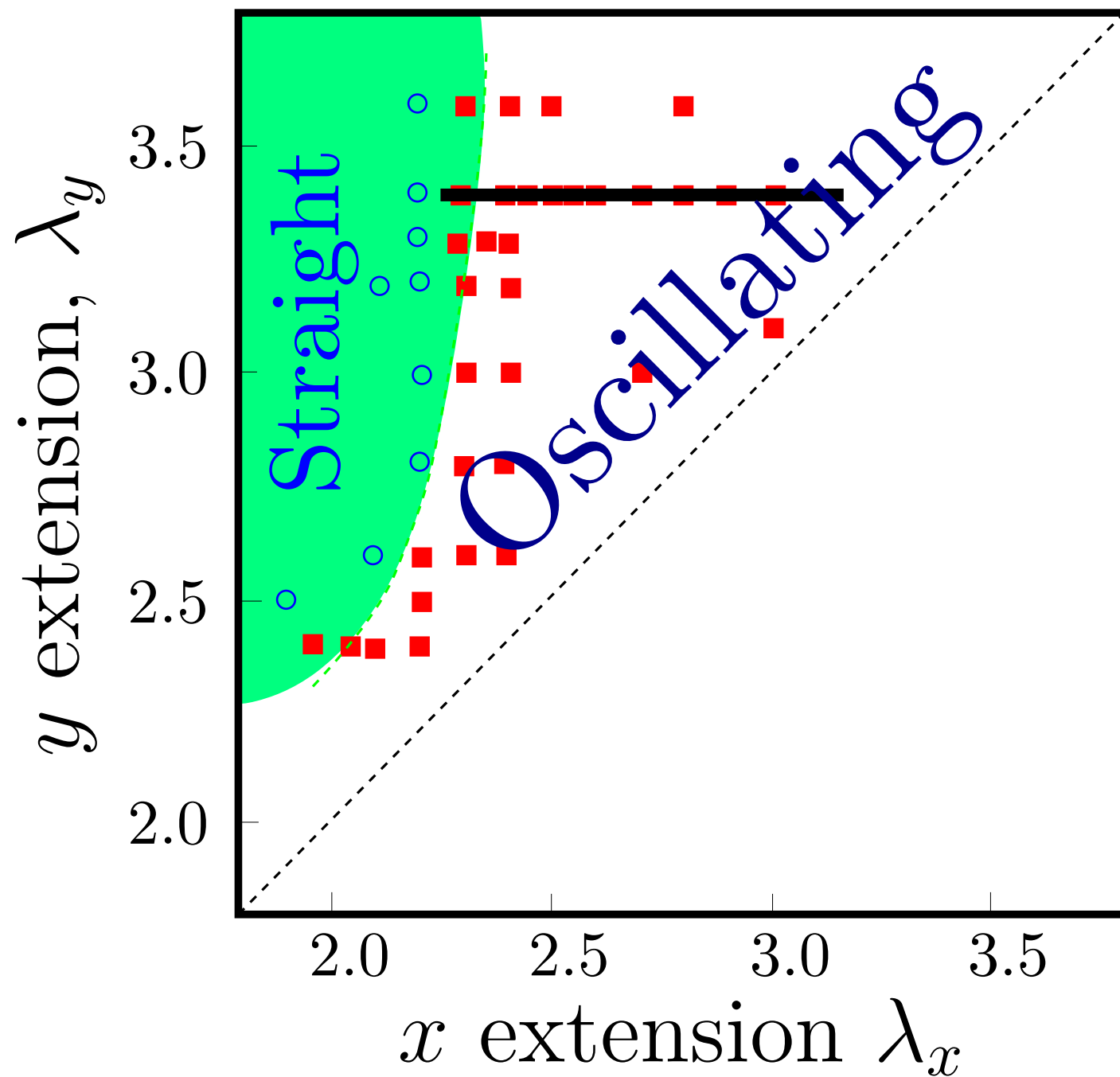
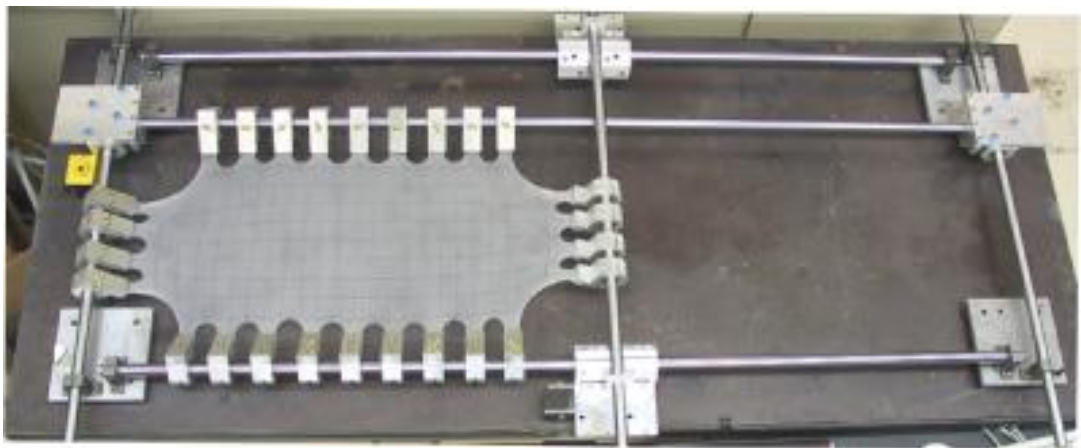
Experimental Observations

Oscillations



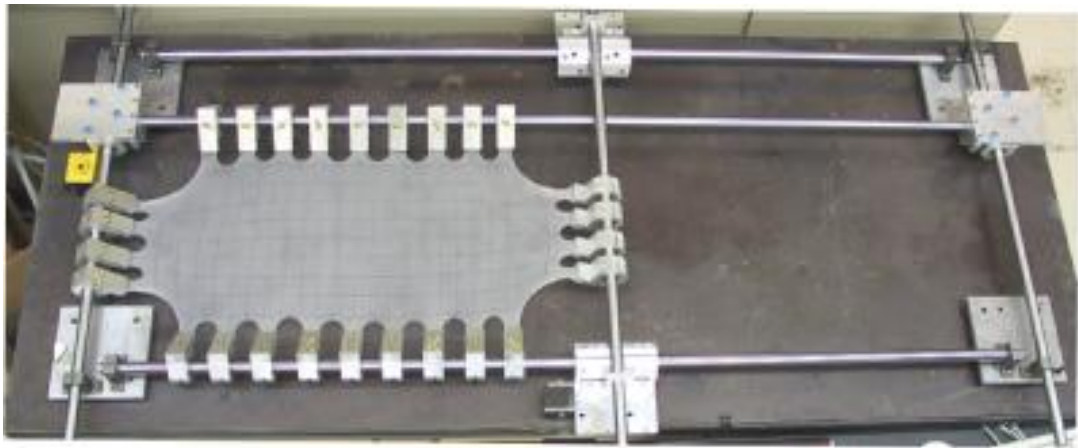
Experimental Observations

Oscillations

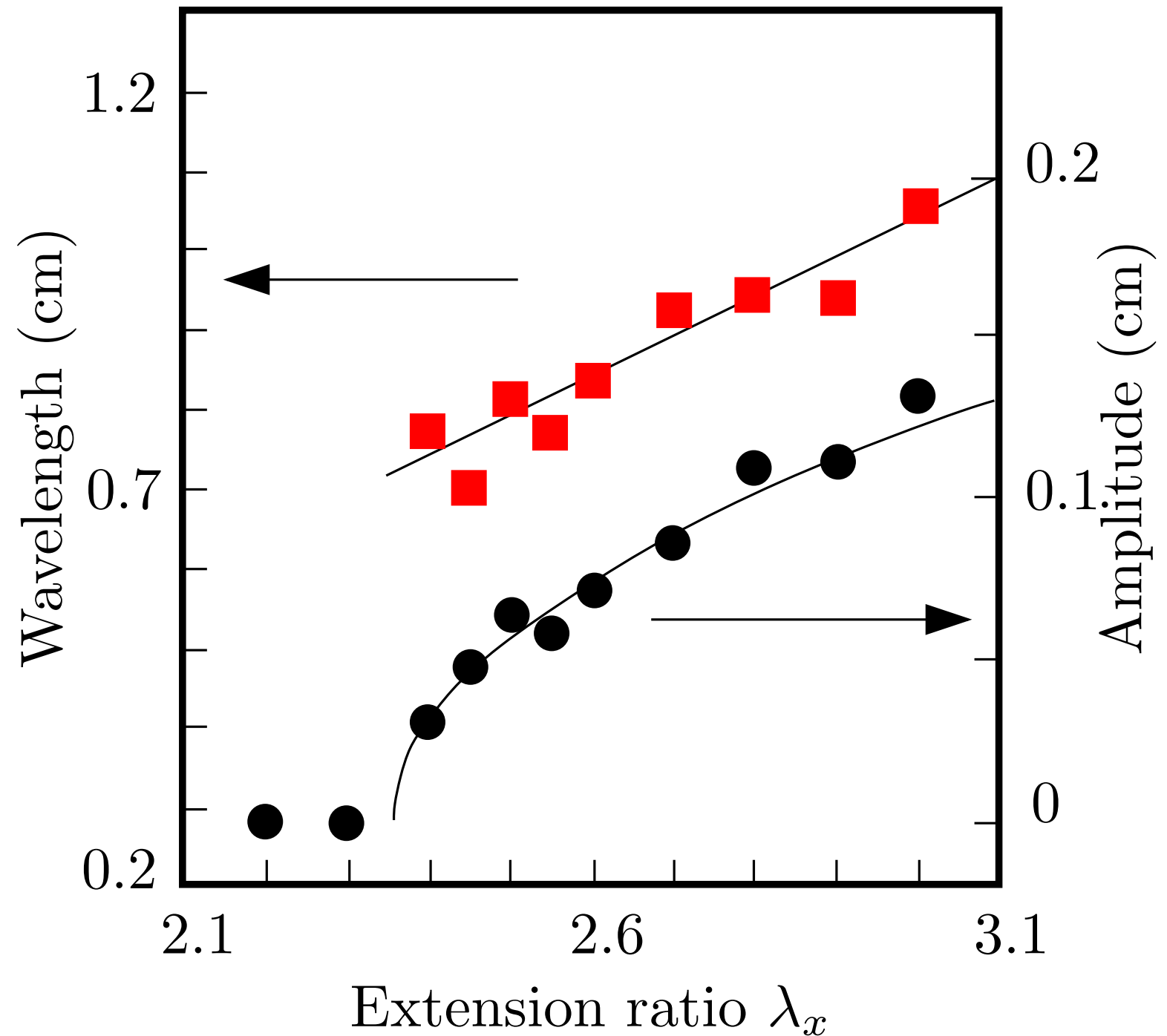


Experimental Observations

Oscillations

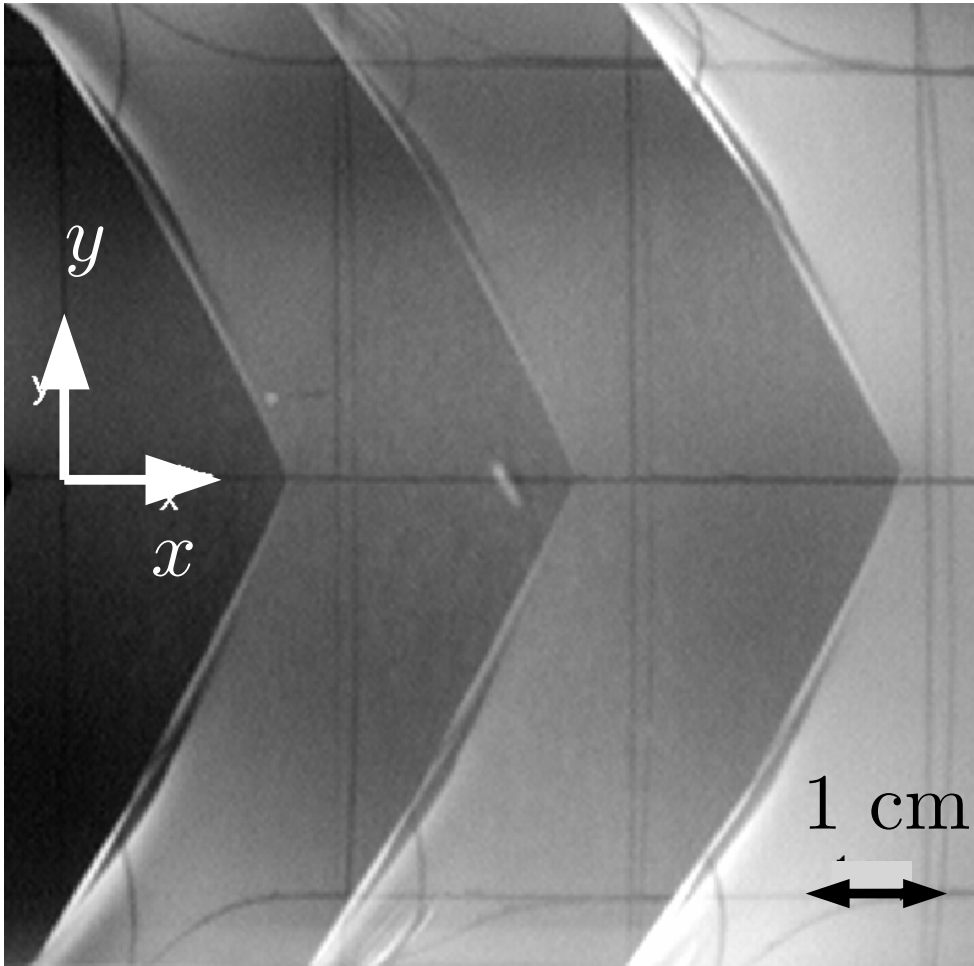


No detailed theory yet for oscillations... but see Yang and Chen, *Phys. Rev. Lett.* **95**, 144301 (2005)



Experimental Observations

Sound Speeds and Rupture Velocities

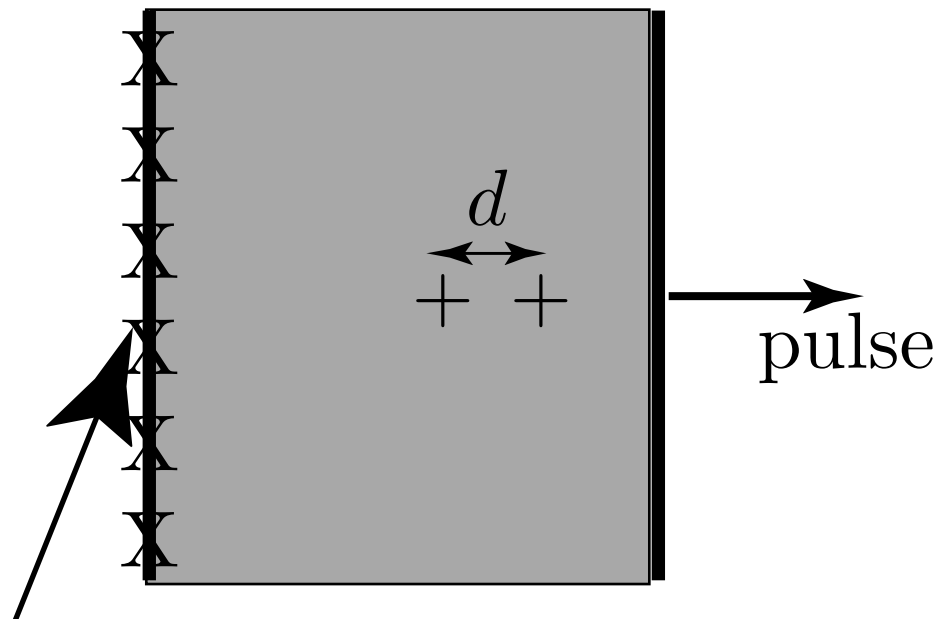


Tip has wedge-like shape like Mach cone

Experimental Observations

Sound Speeds and Rupture Velocities

Longitudinal speed measured by time of flight



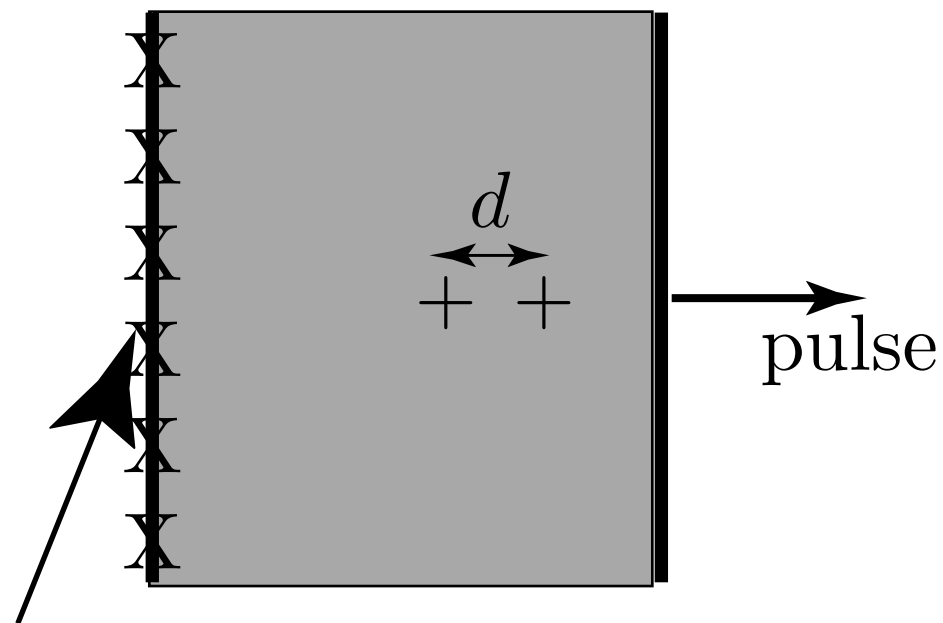
Fixed clamps

Experimental Observations

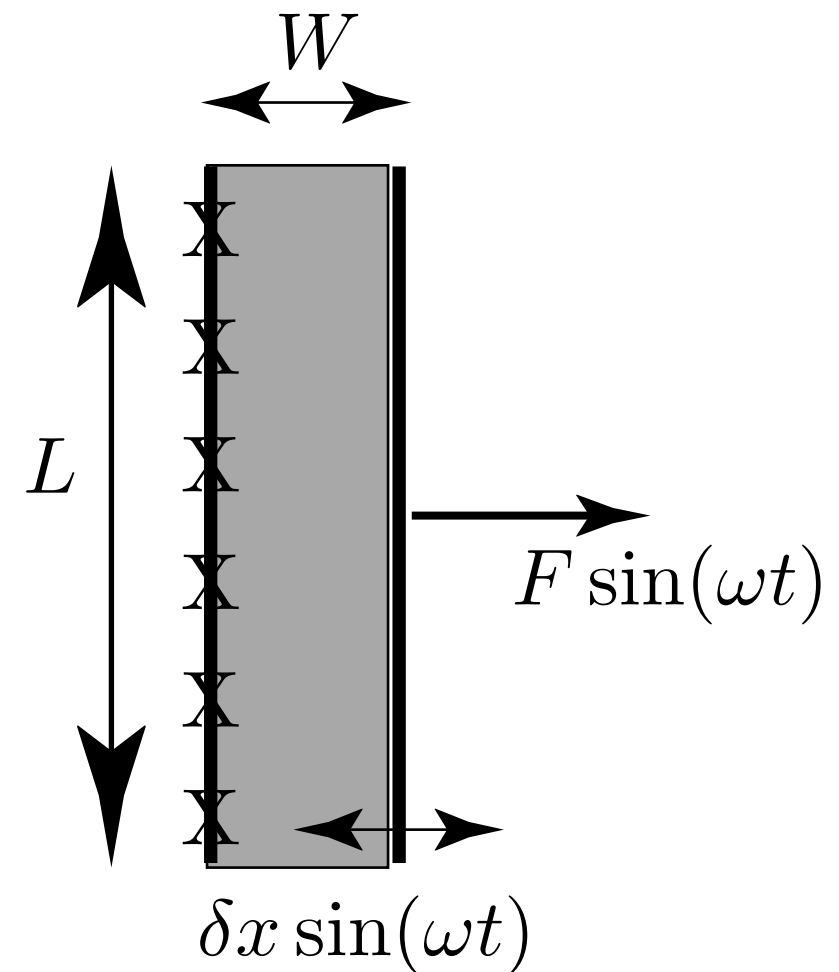
Sound Speeds and Rupture Velocities

Longitudinal speed measured by time of flight

Longitudinal speed measured from force extension curves.



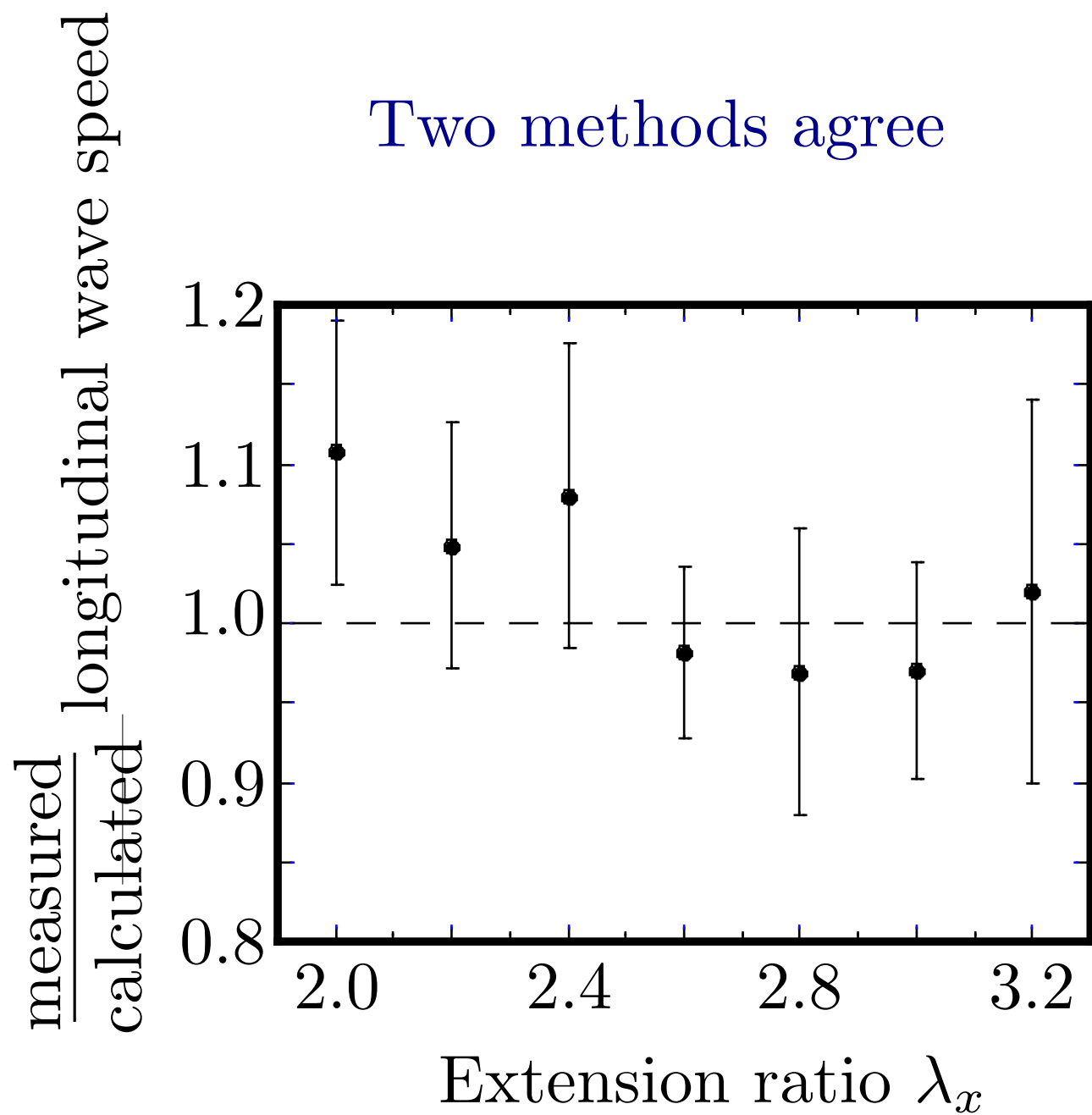
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Experimental Observations

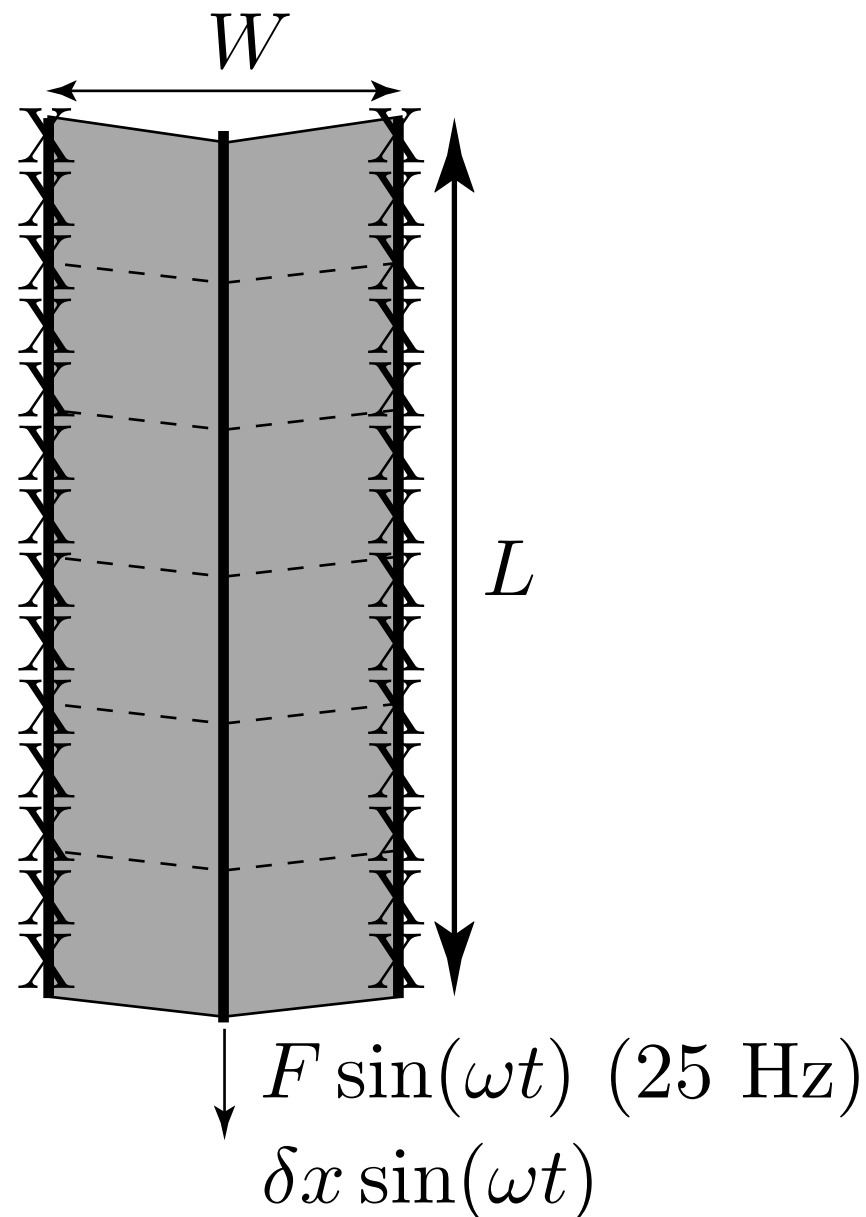
Sound Speeds and Rupture Velocities



Experimental Observations

Sound Speeds and Rupture Velocities

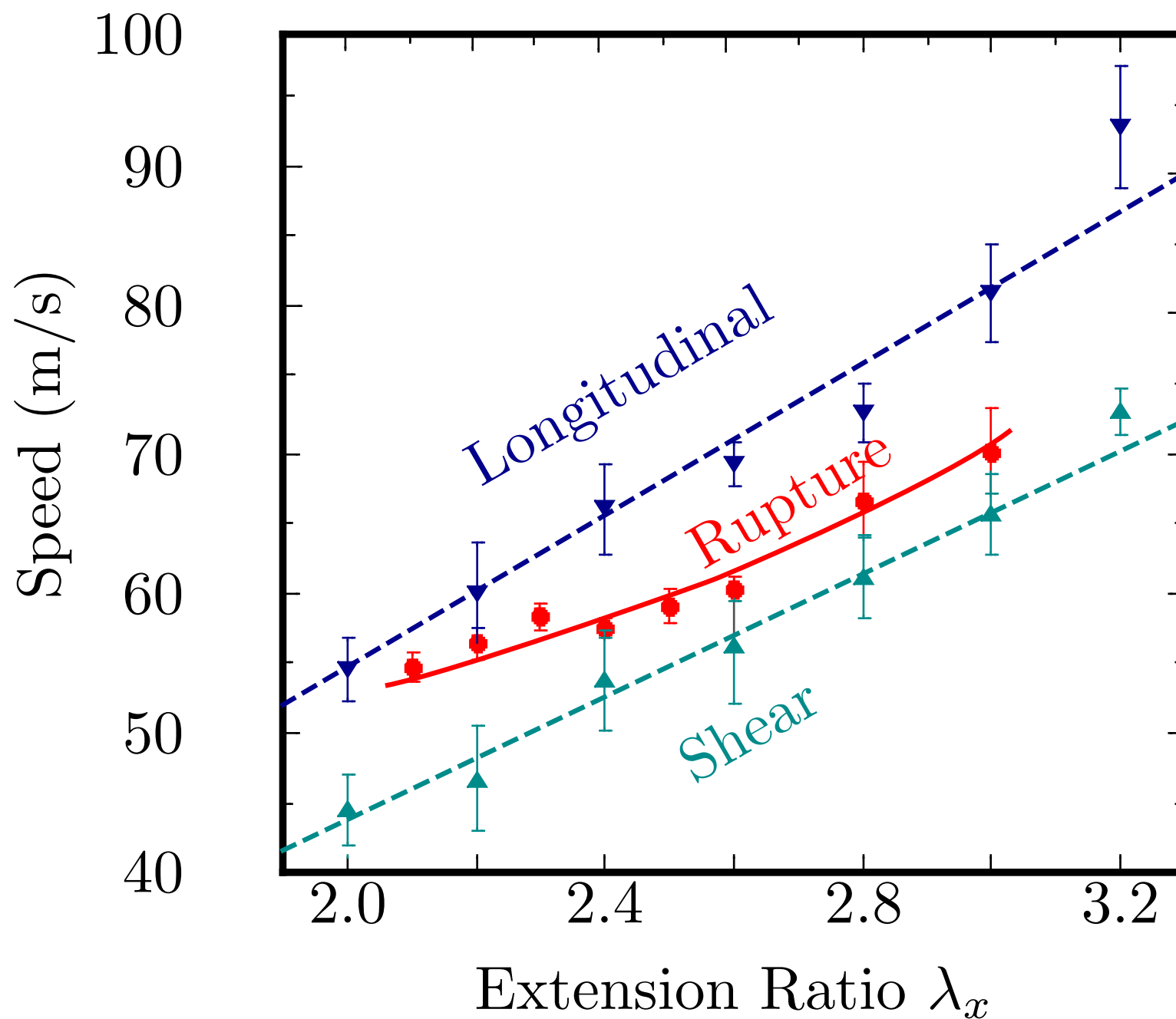
Shear wave speed measured from force extension curves.





Experimental Observations

Sound Speeds and Rupture Velocities

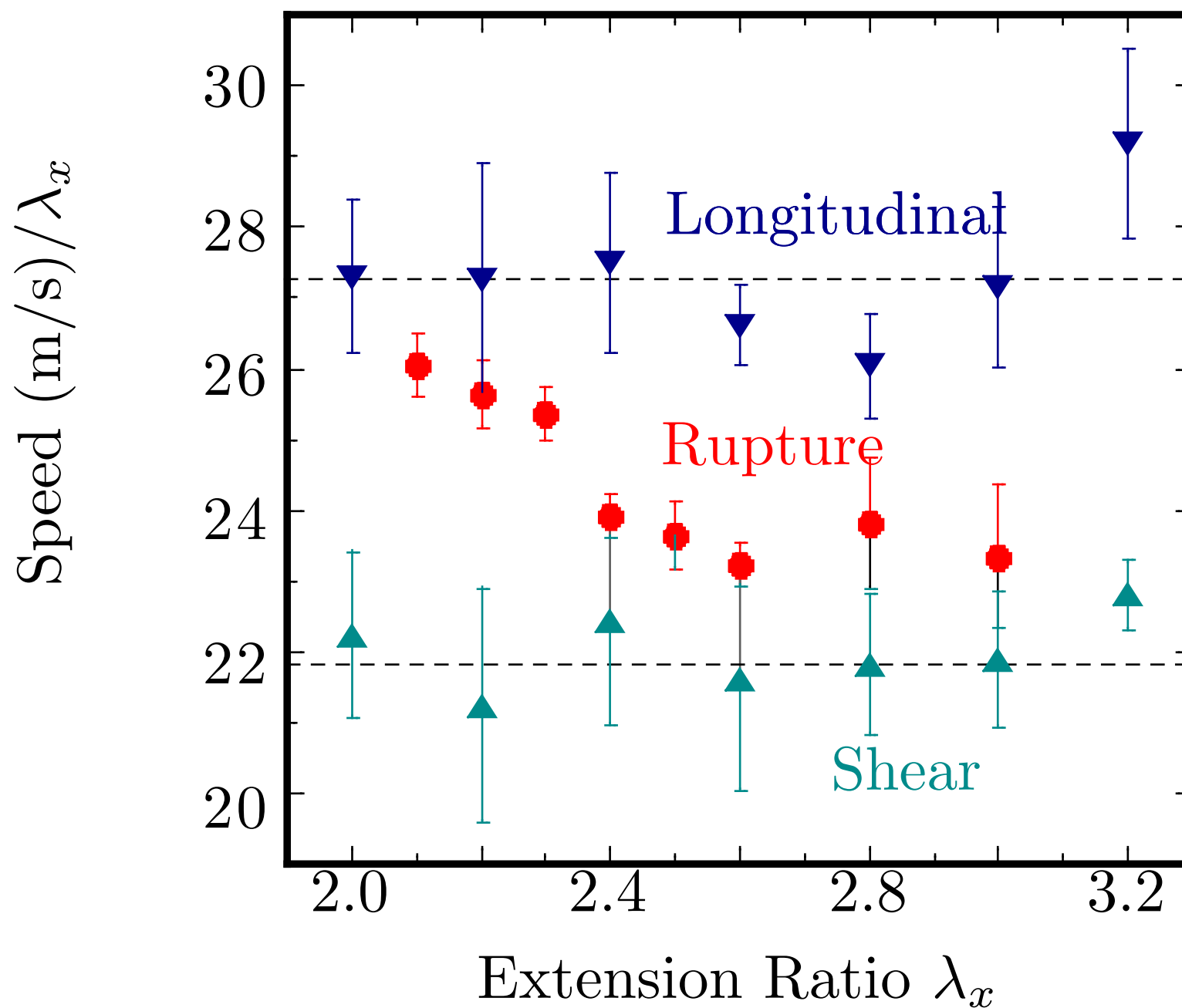




Experimental Observations

Sound Speeds and Rupture Velocities

Transform to reference frame





Experimental Observations

Sound Speeds and Rupture Velocities

Over range of extensions covered by our experiments ($\lambda_x, \lambda_y \sim 200\% - 350\%$), the speed of sound waves is well described by the **Mooney-Rivlin free energy**:

$$\begin{aligned} e(I_1, I_2) &= A(I_1 + 2BI_2) \\ &= A \left[(E_{xx} + E_{yy} + E_{zz}) + 2B (E_{xx}E_{yy} - E_{xy}^2) + 2BE_{zz}I_2 \right] \end{aligned}$$



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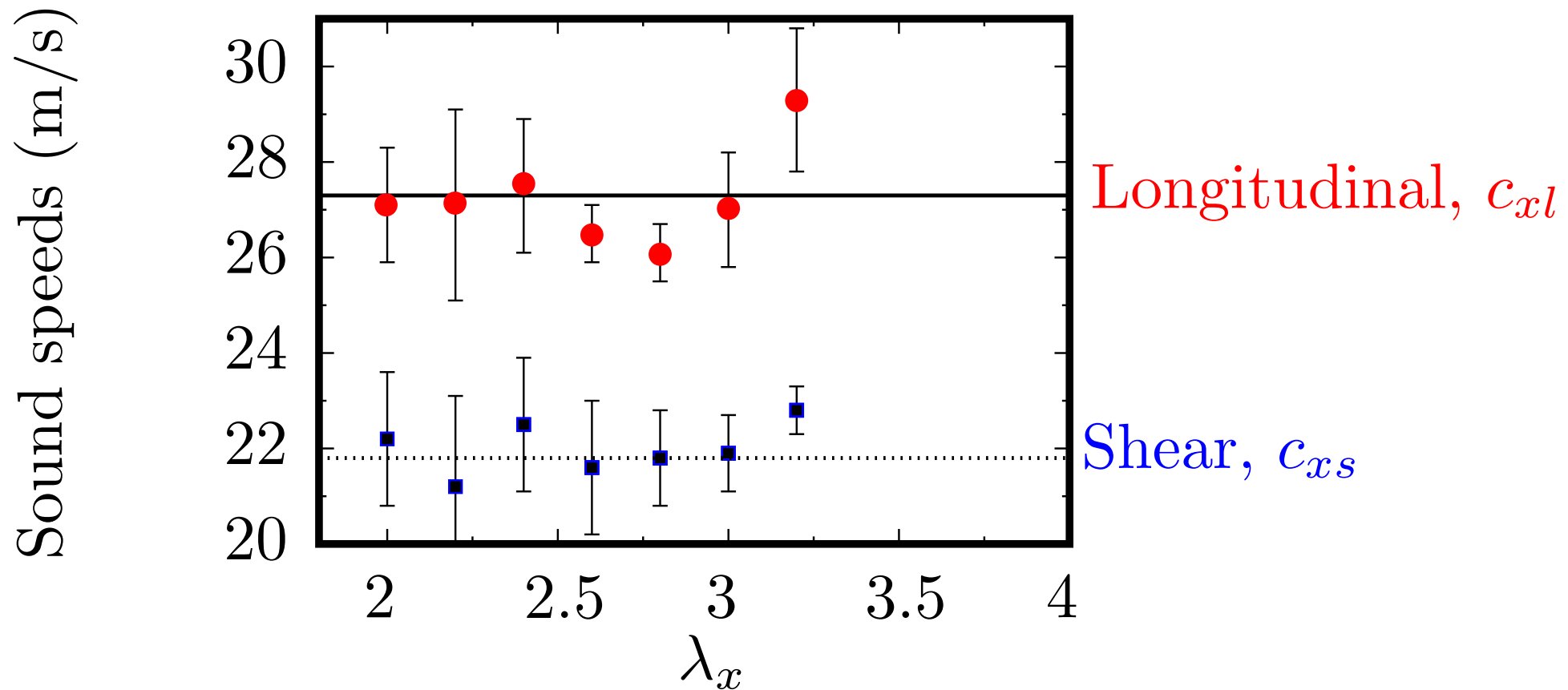


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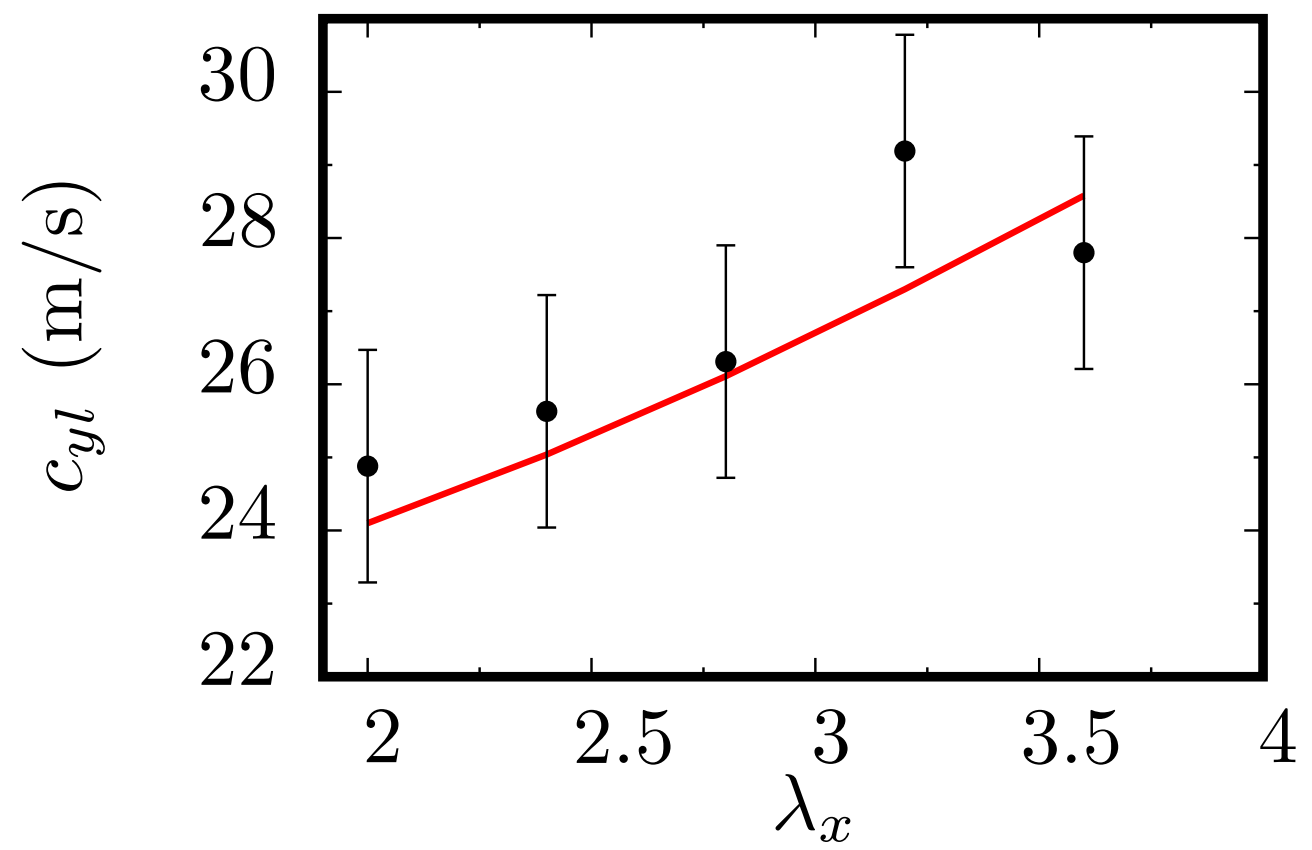


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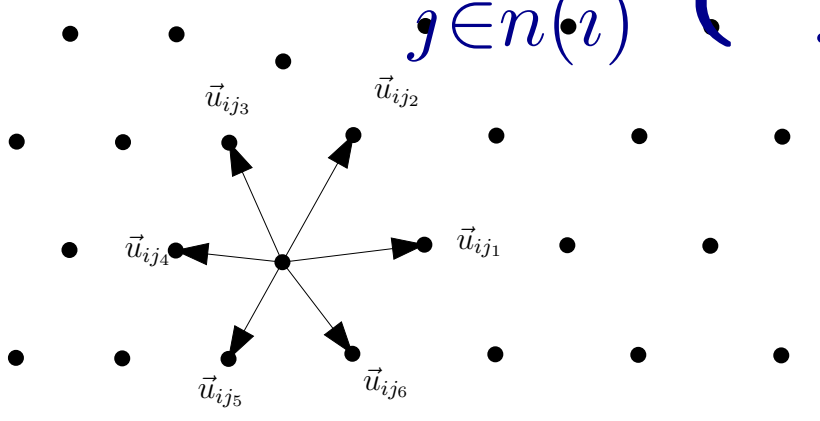
Numerical Studies

Multi-Particle Modeling

- Tethered Membranes (Nelson, *et al.*)
- Virtual Bond Method (Gao and Klein)
- Peridynamics (Silling and Bobaru)
- Mesodynamics (Holian)

Distance between near neighbors Lattice spacing

$$I_{1i} = \frac{1}{6a^2} \sum_{j \in n(i)} \begin{cases} (\vec{u}_{ij} \cdot \vec{u}_{ij} - a^2) & \text{if } u_{ij} < \lambda_f \\ \lambda_f^2 - a^2 & \text{else} \end{cases}$$



Failure extension



Numerical Studies

Multi-Particle Modeling

$$F_i = \frac{1}{6} \sum_{j \in n(i)} \begin{cases} (\vec{u}_{ij} \cdot \vec{u}_{ij} - a^2) & \text{if } u_{ij} < \lambda_f \\ \lambda_f^2 - a^2 & \text{else} \end{cases}$$

$$G_i = \frac{1}{9} \sum_{j \in n(i)} \begin{cases} (\vec{u}_{ij} \cdot \vec{u}_{ij} - a^2)^2 & \text{if } u_{ij} < \lambda_f \\ (\lambda_f^2 - a^2)^2 & \text{else} \end{cases}$$

$$H_i = \frac{1}{27} \sum_{j \neq k \in n(i)} h(u_{ij})h(u_{ik}) (\vec{u}_{ij} \cdot \vec{u}_{ik} + 2a^2)^2,$$

and $h(u) = 1/(1 + e^{(u - \lambda_f)/u_s})$.

$$I_1^i = \frac{F_i}{a^2}$$

$$I_2^i = \frac{3}{4} \frac{1}{a^4} (F_i^2 - G_i),$$

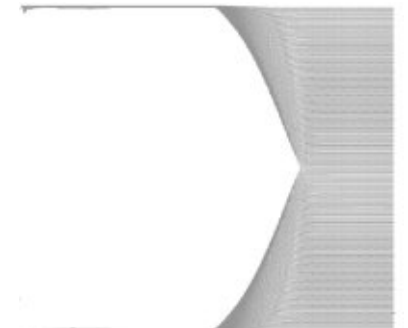
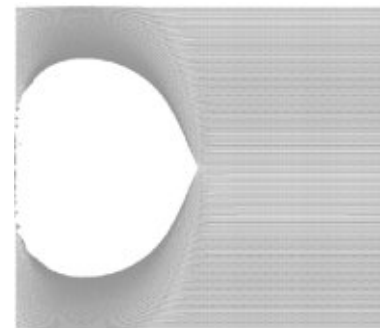
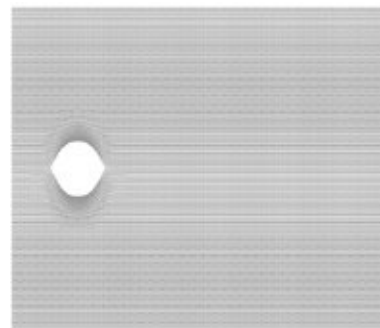
or alternatively,

$$I_2^i = \frac{9}{8} \frac{1}{a^4} (G_i - H_i + 4).$$

Numerical Studies

Investigations

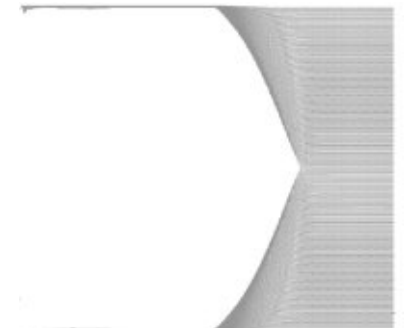
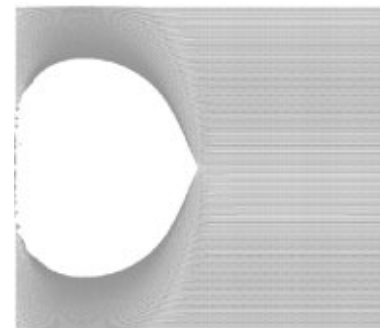
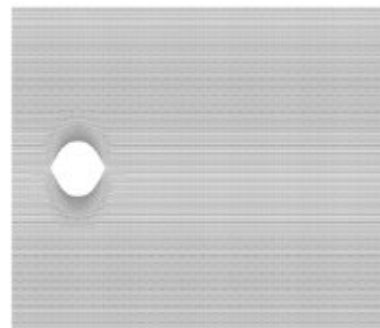
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Numerical Studies

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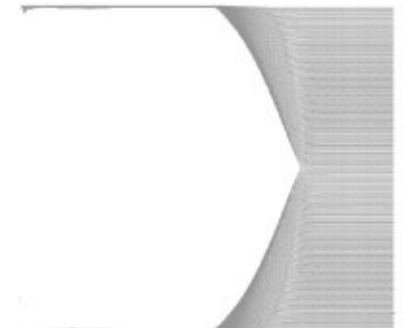
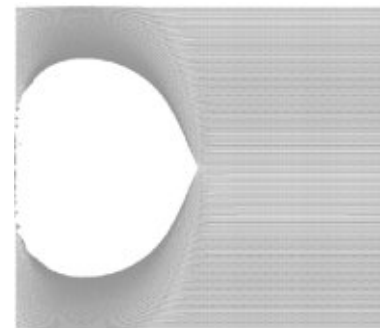
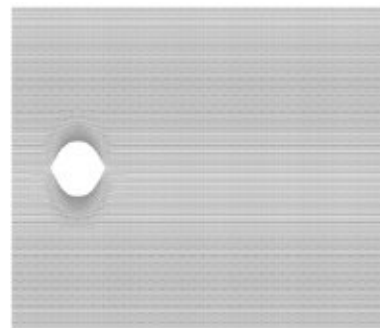
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- Increase in sound speed near tip of rupture (hyperelasticity)



Numerical Studies

Investigations

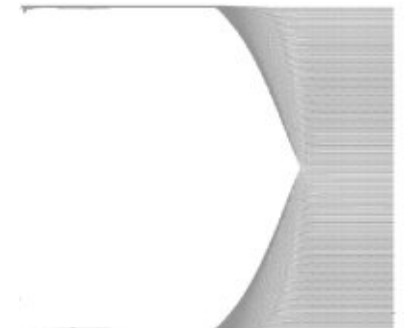
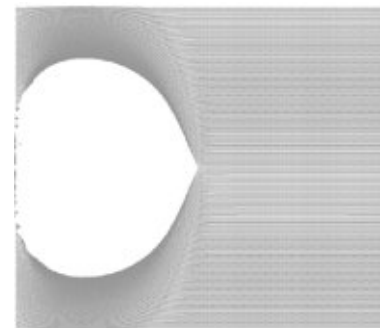
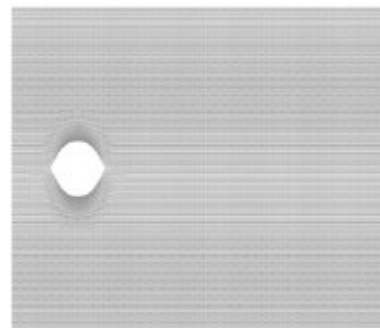
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Numerical Studies

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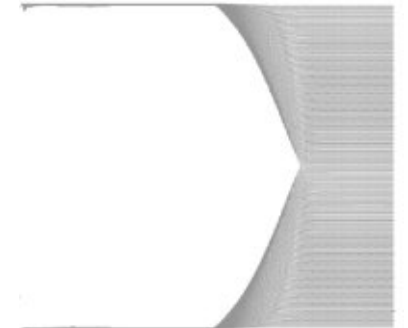
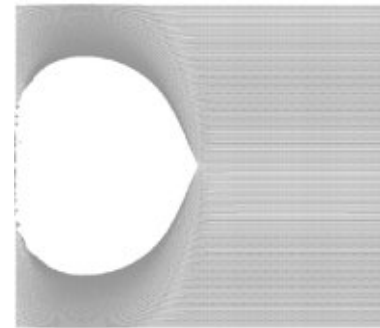
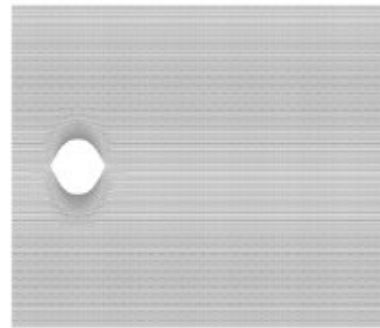
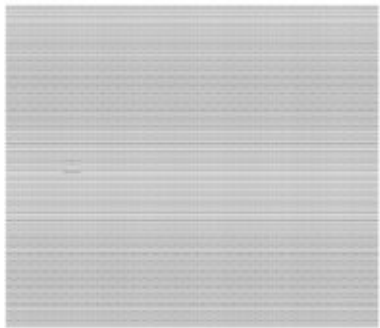
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- Increase in sound speed as rubber retracts



Numerical Studies

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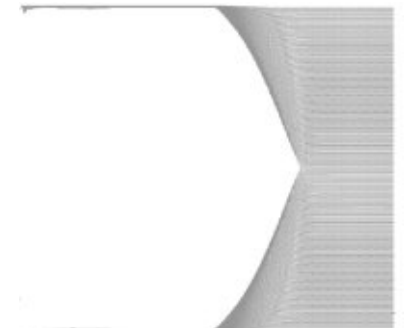
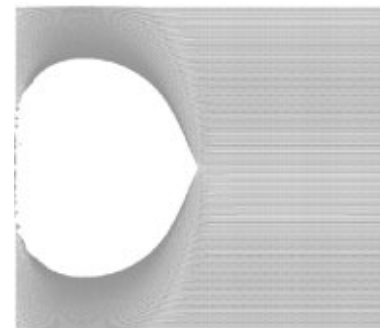
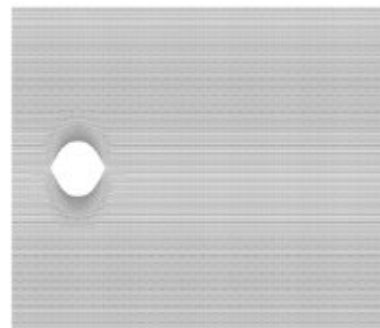
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Numerical Studies

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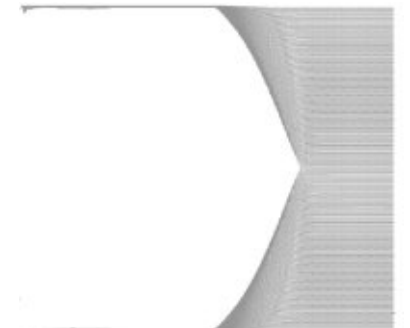
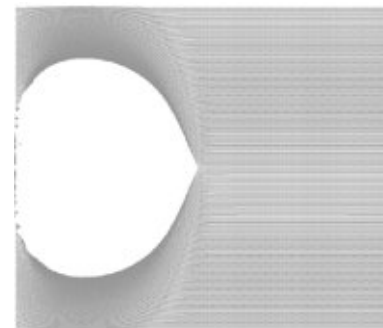
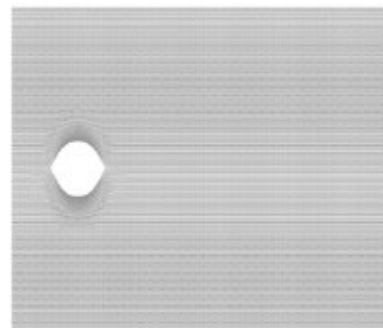
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- Second term in Mooney-Rivlin theory proportional to I_2



Numerical Studies

Investigations

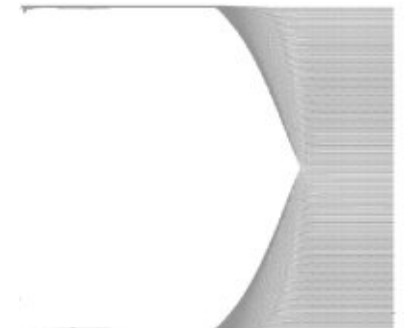
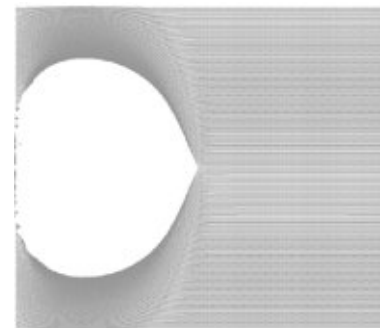
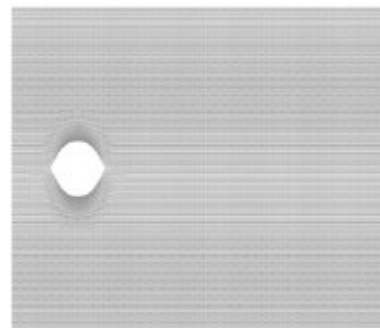
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Numerical Studies

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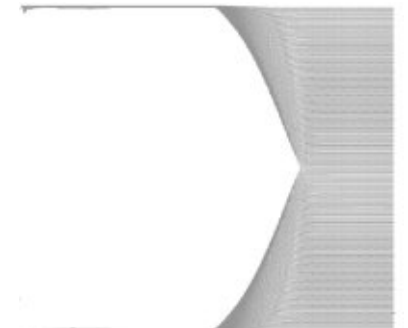
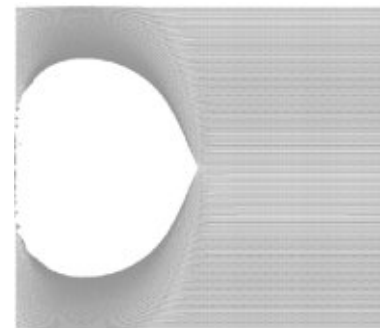
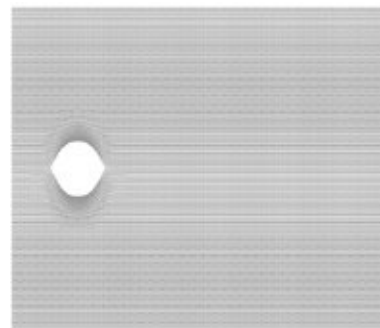
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Numerical Studies

Investigations

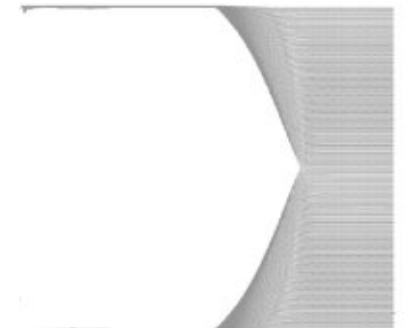
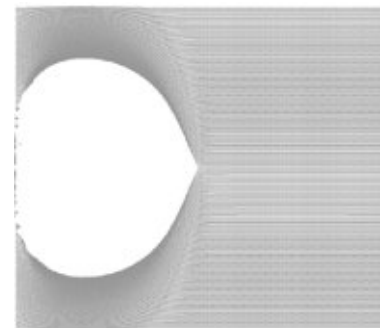
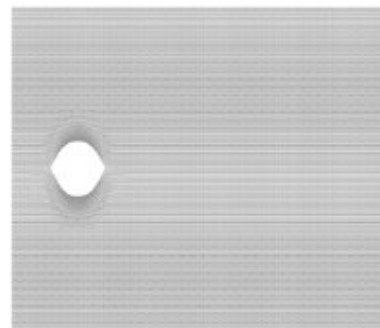
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Yes. $\beta c^2 \nabla^2 \frac{\partial u}{\partial t} \dots$ (or more elaborate models)



Numerical Studies

Investigations

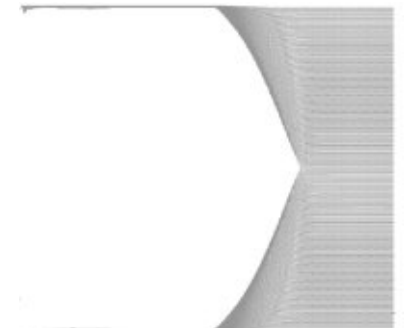
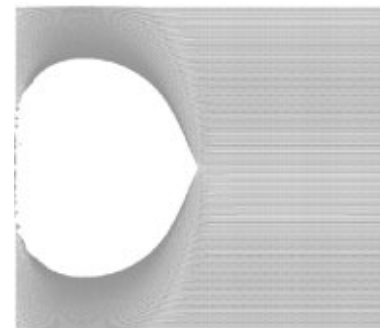
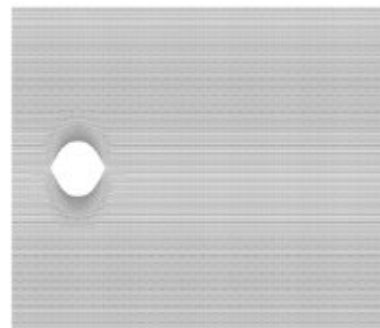
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Numerical Studies

Investigations

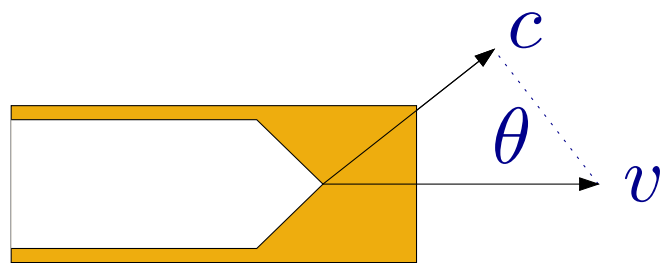
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Theoretical Views

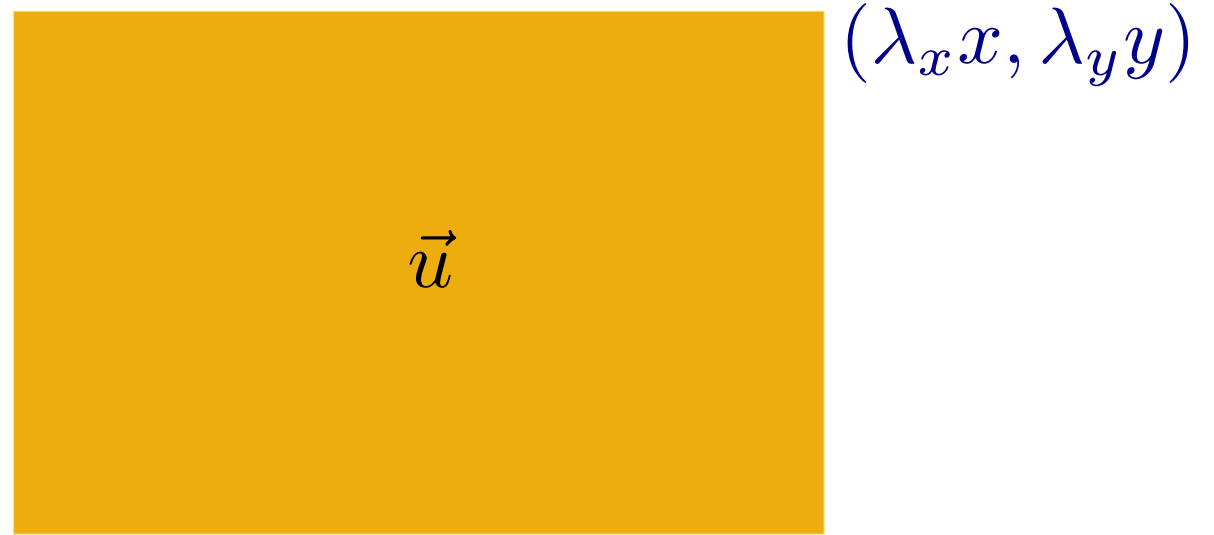
Elementary Considerations

Reference Frame



$$\frac{c}{v} = \sin \theta$$

Laboratory Frame



$$\text{laboratory slope} = \frac{\lambda_y}{\lambda_x \sqrt{v^2/c^2 - 1}}$$

Theoretical Views

Continuum Theory

Following suggestion of Rice (following Shield) adopt Neo–Hookean theory. Horizontal displacements are static, so obtain theory for vertical displacement u .

$$\ddot{u} = c^2 \nabla^2 u + c^2 \beta \nabla^2 \dot{u}$$

- u is not small.
- β describes Kelvin dissipation ($E_\infty \rightarrow \infty$)

Boundary conditions:

$$\frac{\partial u}{\partial y} = -\beta \frac{\partial^2 u}{\partial t \partial y} \quad \text{for } x < 0; \quad u = 0 \quad \text{for } x > 0.$$

Theoretical Views

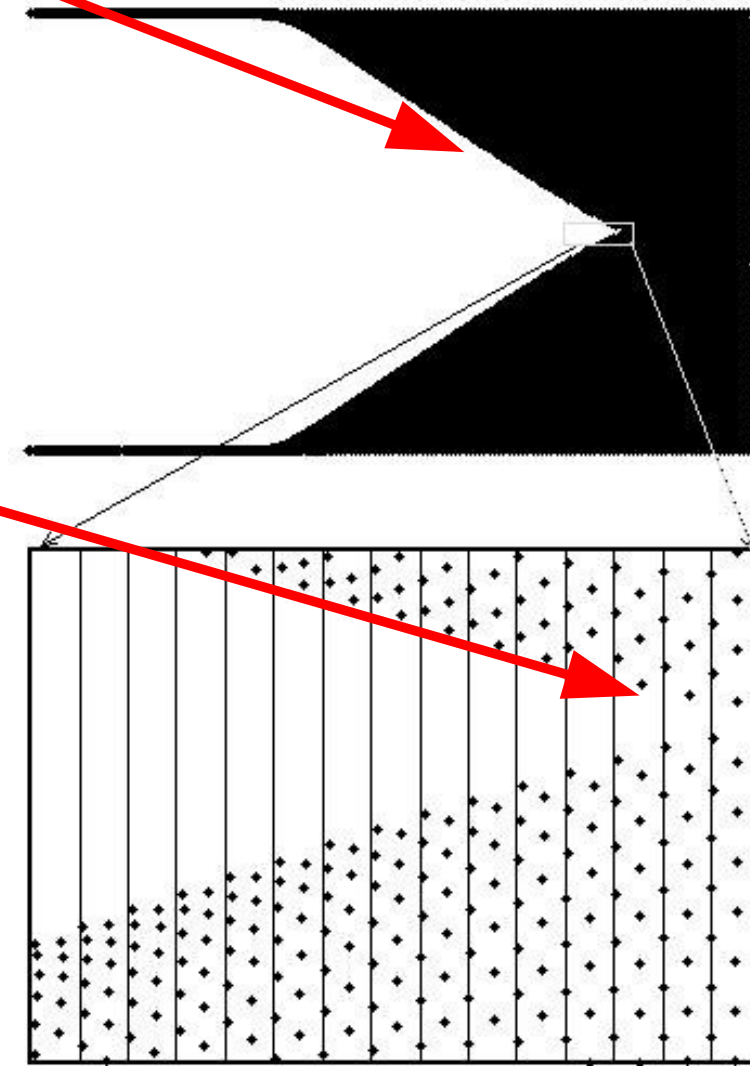
Continuum Theory

This theory has supersonic solutions ($v > c$).

Recover laboratory slope of back edge = $-\frac{\lambda_y}{\lambda_x \sqrt{v^2/c^2 - 1}}$

At the origin, the slope of the rupture is

$$\left. \frac{\partial u}{\partial y} \right|_{x=0, y=0} = \frac{\lambda_y}{\sqrt{1 - c^2/v^2}}$$



The theory can be closed with rupture criterion

$$\frac{\lambda_y}{\sqrt{(4\lambda_f^2 - \lambda_x^2)/3}} = \sqrt{1 - c^2/v^2}$$



Theoretical Views

Continuum Theory

Kelvin dissipation

Sound speed

Lattice spacing

- Dimensionless measure of dissipation is $\beta c / \Delta$:
this theory applies when $\beta c / \Delta \geq 1$.
- Displacements and strains are finite near tip.
- Stress diverges as $\exp[-x / (\beta c)] / \sqrt{x}$ near tip
- There is no energy release.

Theoretical Views

Discrete Theory

Discrete theory can be solved using Wiener-Hopf techniques (Slepyan, MPM); find rupture speeds of 800-million-particle systems in five minutes

$$\ddot{u}_i^y = \frac{2c^2}{3a^2} \sum_{j \in n(i)} (u_{ij}^y + \beta \dot{u}_{ij}^y) \theta(\lambda_f - u_{ij}).$$



Theoretical Views

Discrete Theory

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$$\ddot{u}_i^y = \frac{2c^2}{3a^2} \sum_{j \in n(i)} (u_{ij}^y + \beta \dot{u}_{ij}^y) \theta(\lambda_f - u_{ij}).$$

$$\tilde{v} = v/c, \quad \tilde{\beta} = \beta c/a; \quad z = \frac{3 - \cos(\omega/\tilde{v}) - 3\omega^2/[4(1 - i\tilde{\beta}\omega)]}{2 \cos(\omega/2\tilde{v})}$$

$$y = z + \sqrt{z^2 - 1} \text{ with } \text{abs}(y) > 1, ; F(\omega) = \left\{ \frac{y^{[N-1]} - y^{-[N-1]}}{y^N - y^{-N}} - 2z \right\} \cos(\omega/2\tilde{v}) + 1$$

$$Q(\omega) = \frac{F}{F - 1 - \cos(\omega/2\tilde{v})}; \quad \tilde{\lambda}_y = \lambda_y / \sqrt{(4\lambda_f^2 - \lambda_x^2)/3}$$

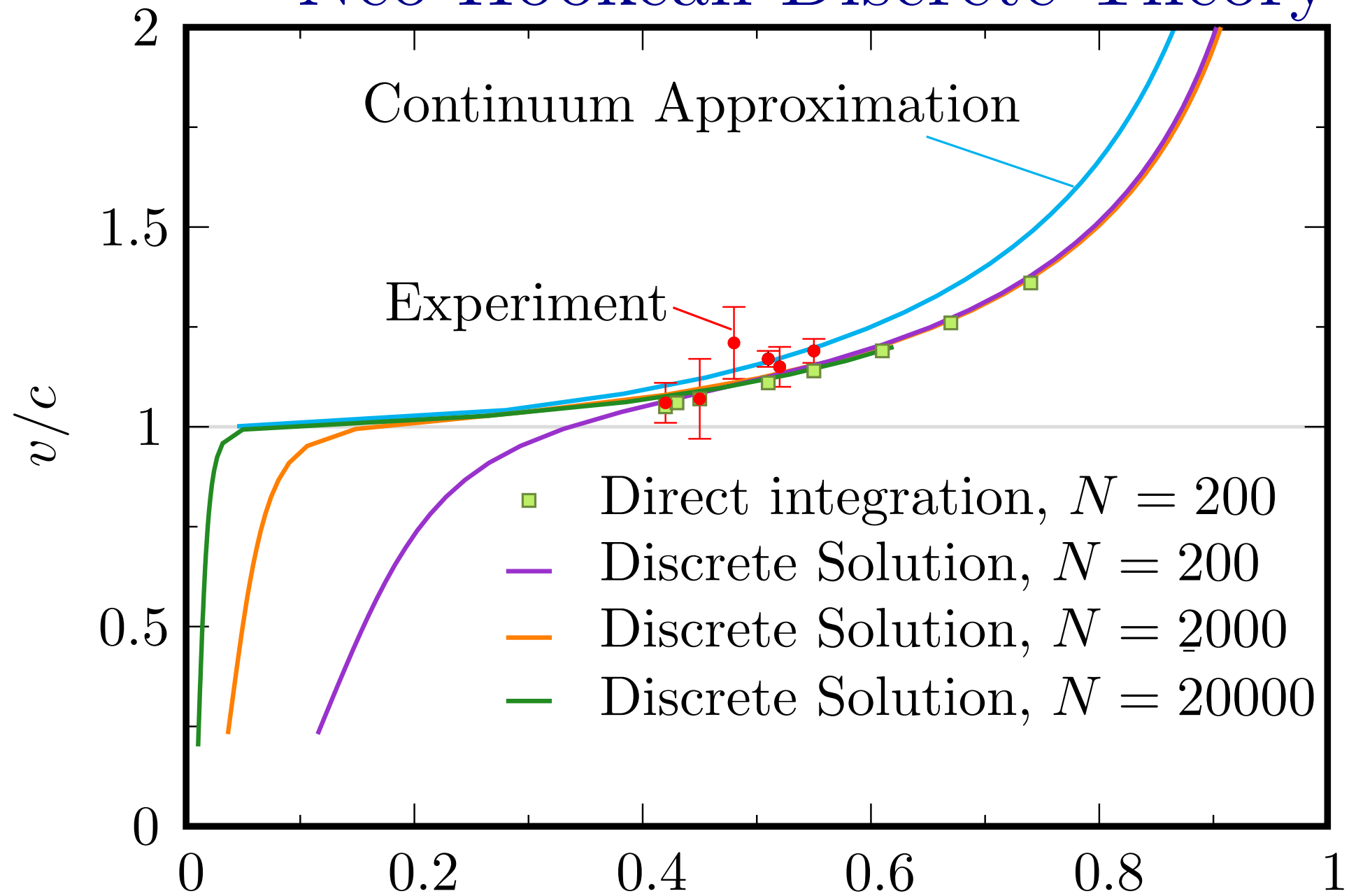
$$\tilde{\lambda}_y = \frac{1}{\sqrt{2N+1}} \exp \left[- \int \frac{d\omega'}{4\pi} \left\{ \frac{1}{i\omega'(1 + \tilde{\beta}^2\omega'^2)} \left[\ln Q(\omega') - \overline{\ln Q(\omega')} \right] + \frac{\tilde{\beta} \ln |Q(\omega')|^2}{1 + \tilde{\beta}^2\omega'^2} \right\} \right].$$



Theoretical Views

Discrete Theory

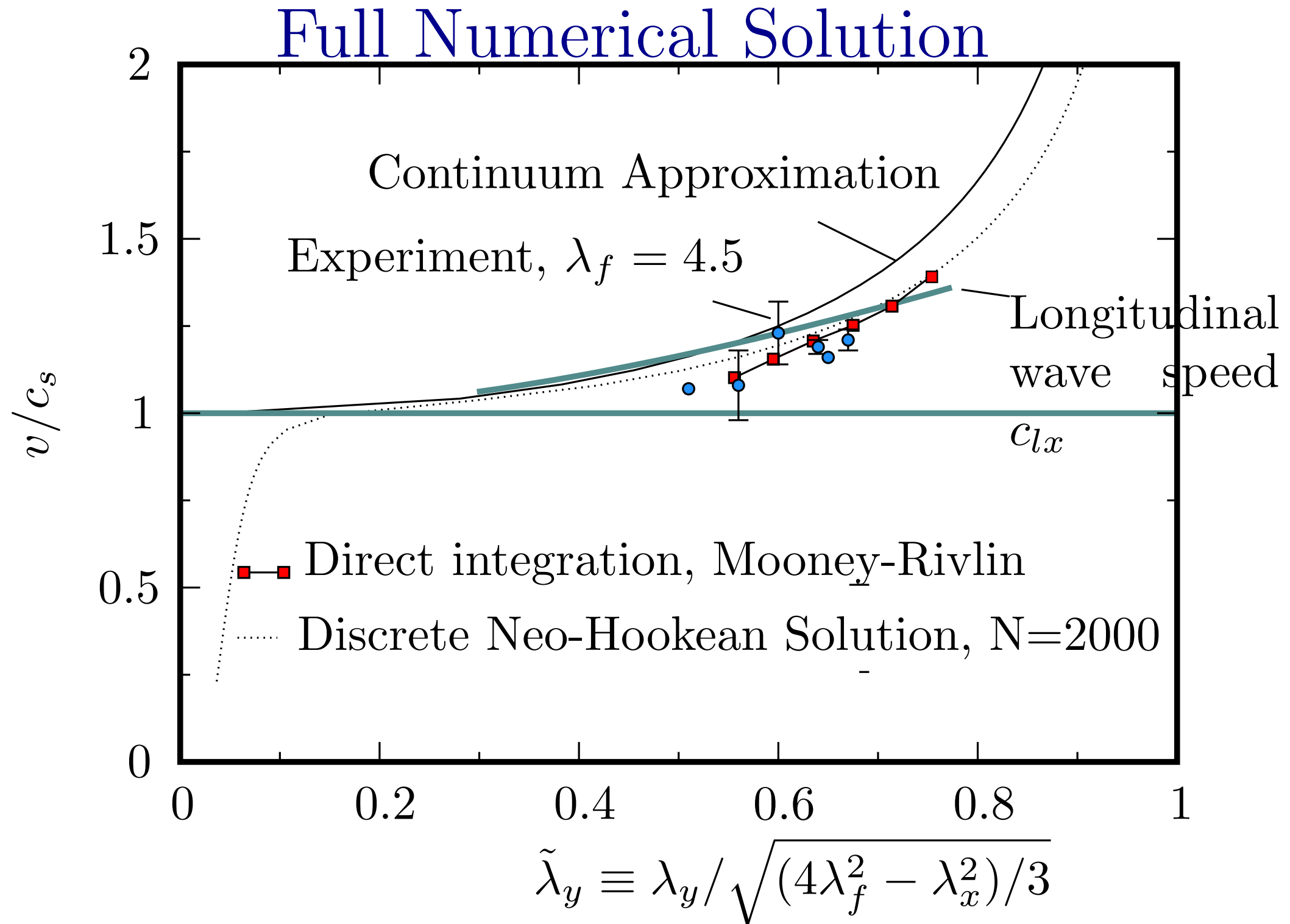
Neo-Hookean Discrete Theory



$$\tilde{\lambda}_y \equiv \lambda_y / \sqrt{(4\lambda_f^2 - \lambda_x^2)/3}$$

Theoretical Views

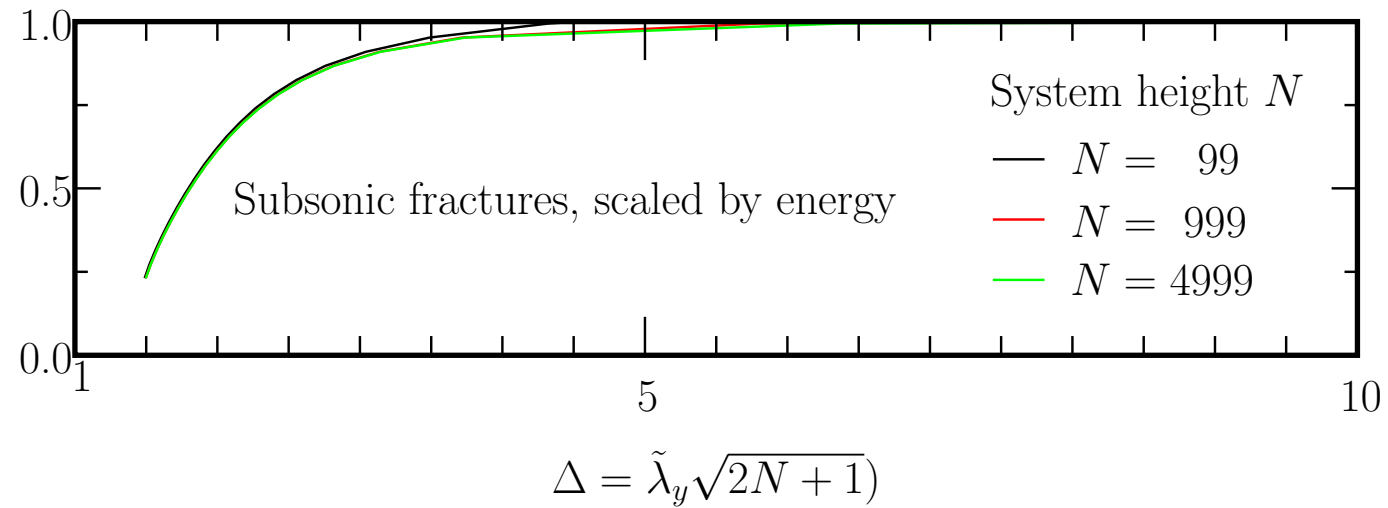
Discrete Theory





Theoretical Views

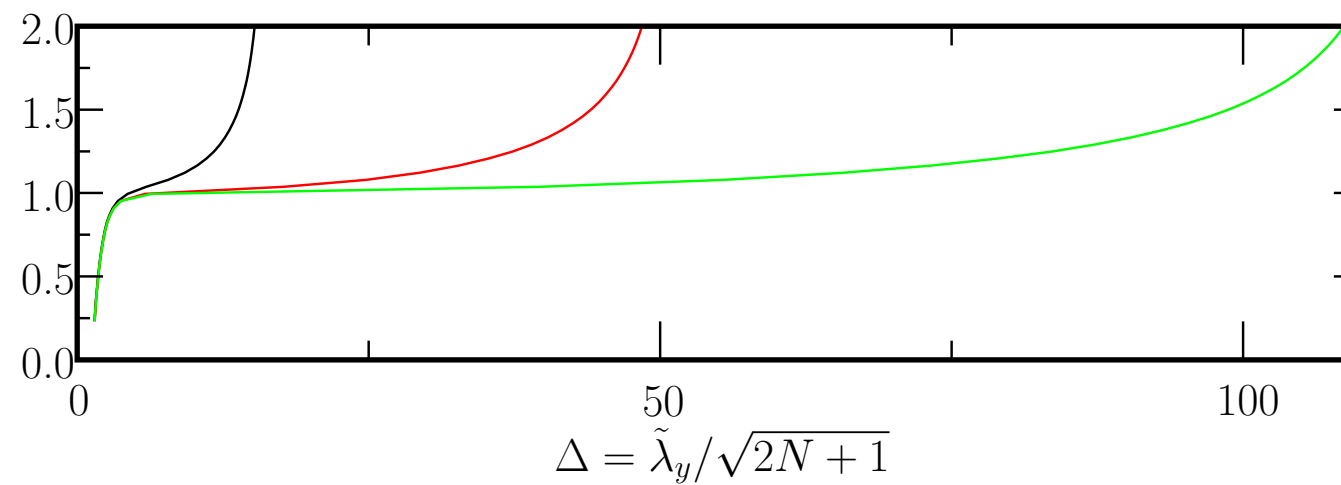
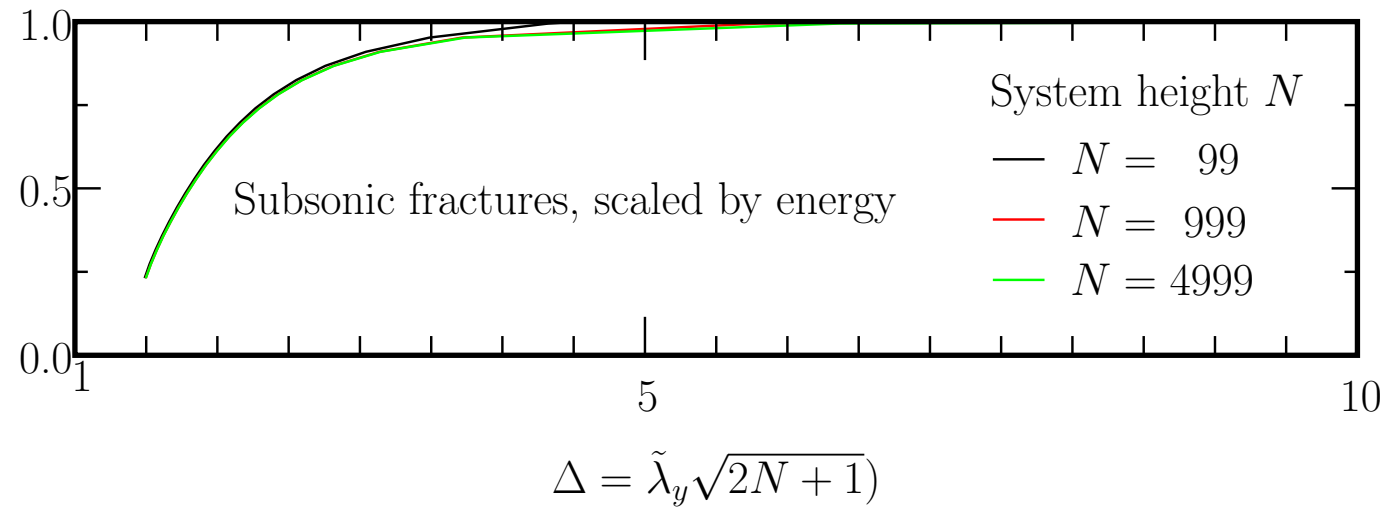
Scaling Theory





Theoretical Views

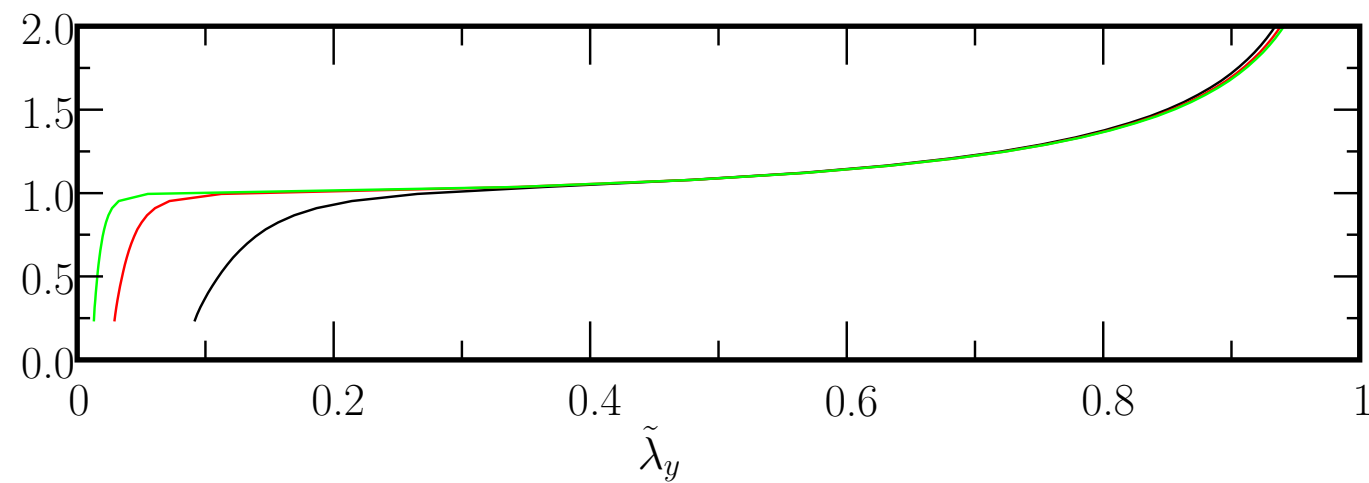
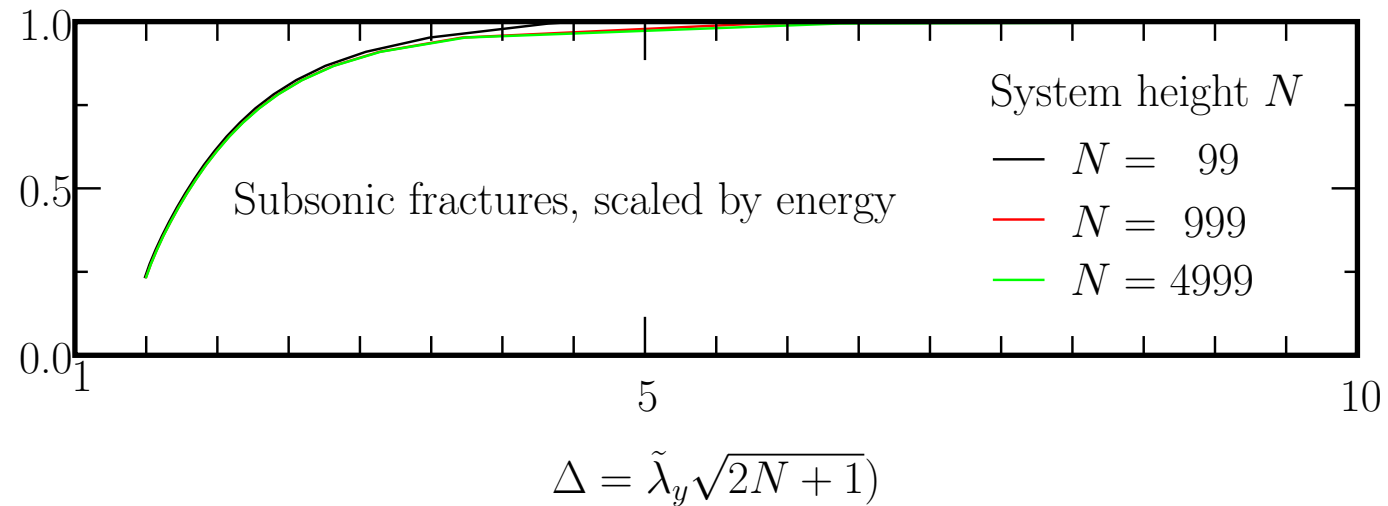
Scaling Theory





Theoretical Views

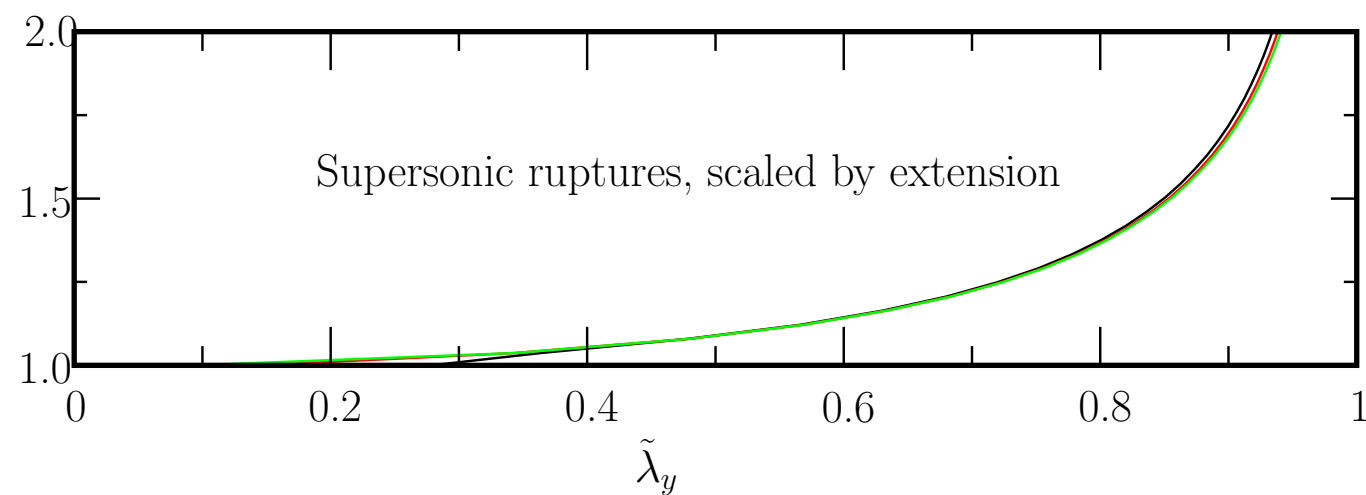
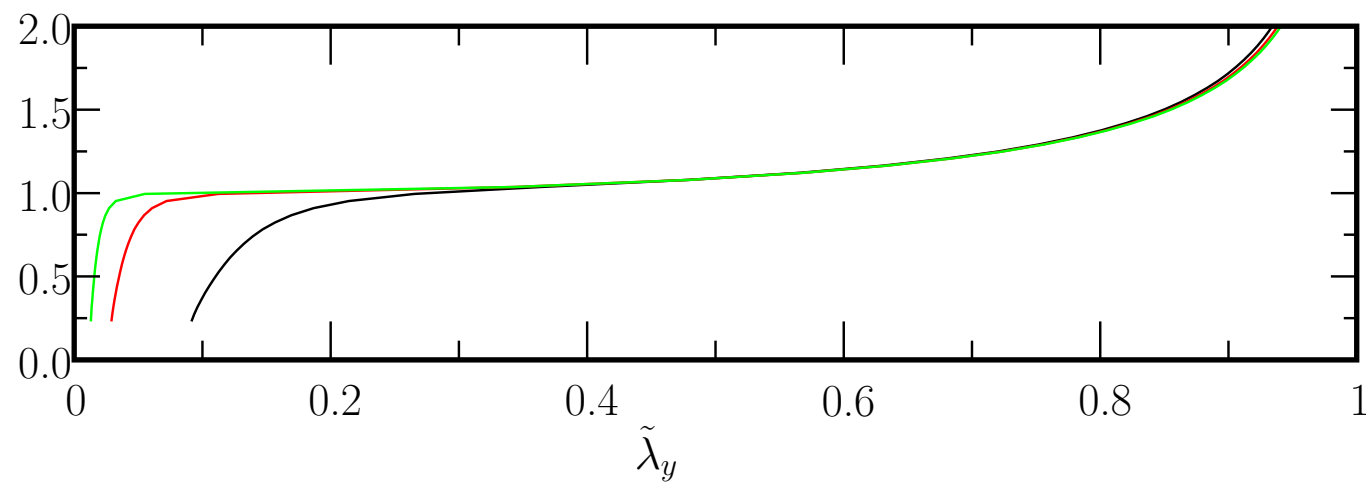
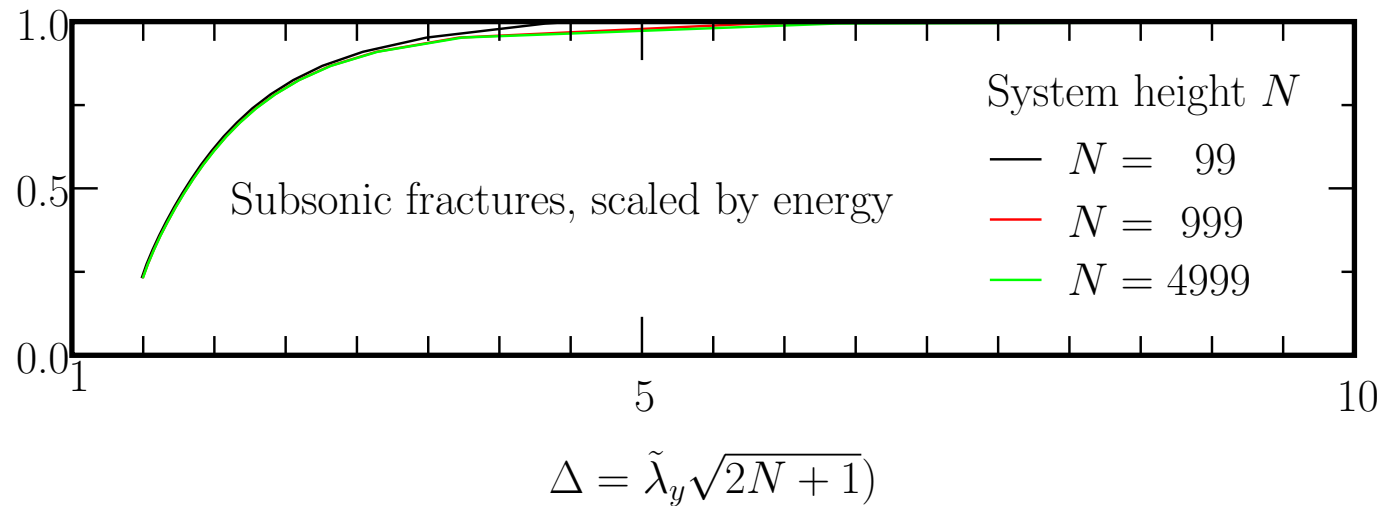
Scaling Theory





Theoretical Views

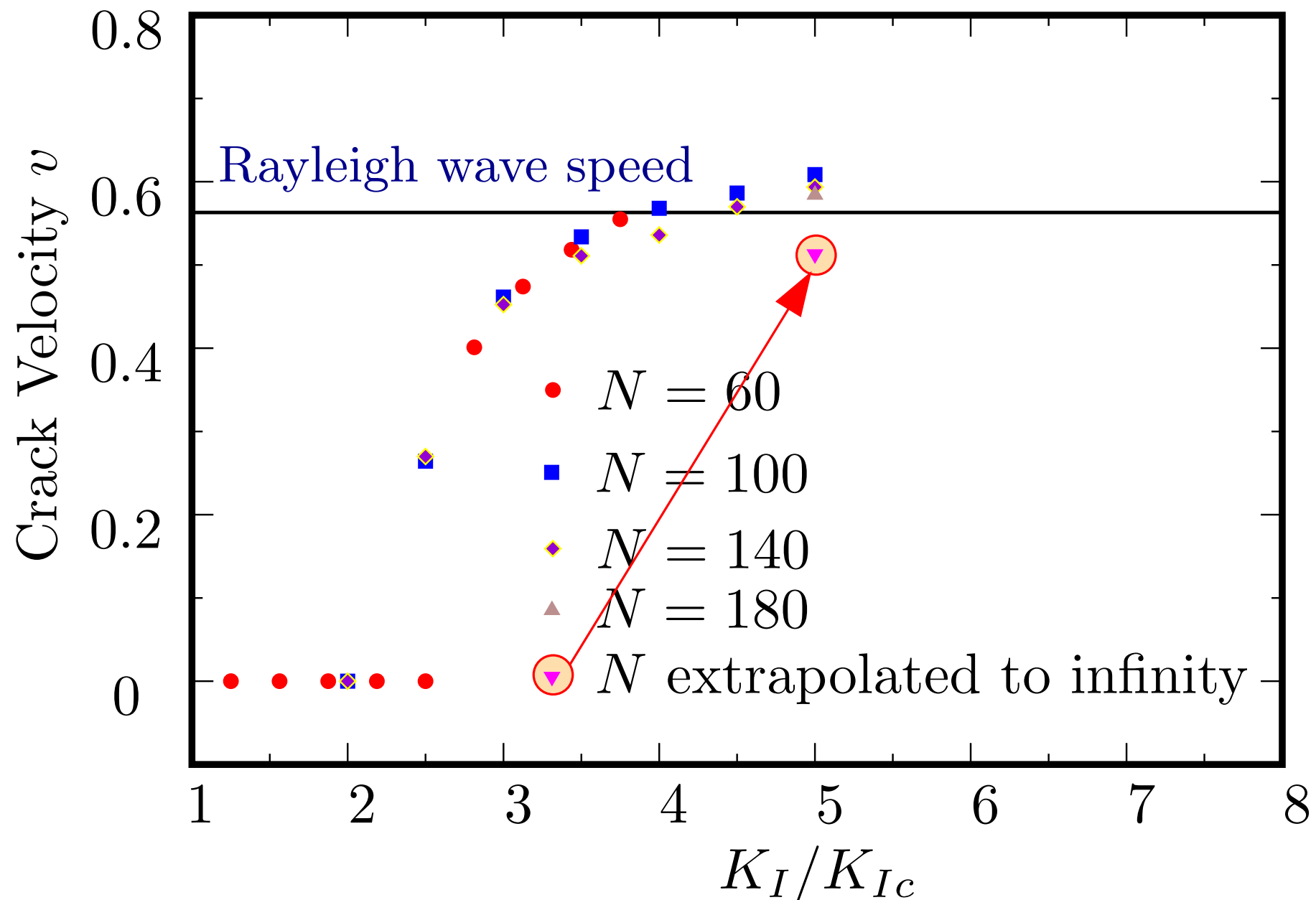
Scaling Theory



Theoretical Views

Scaling Theory

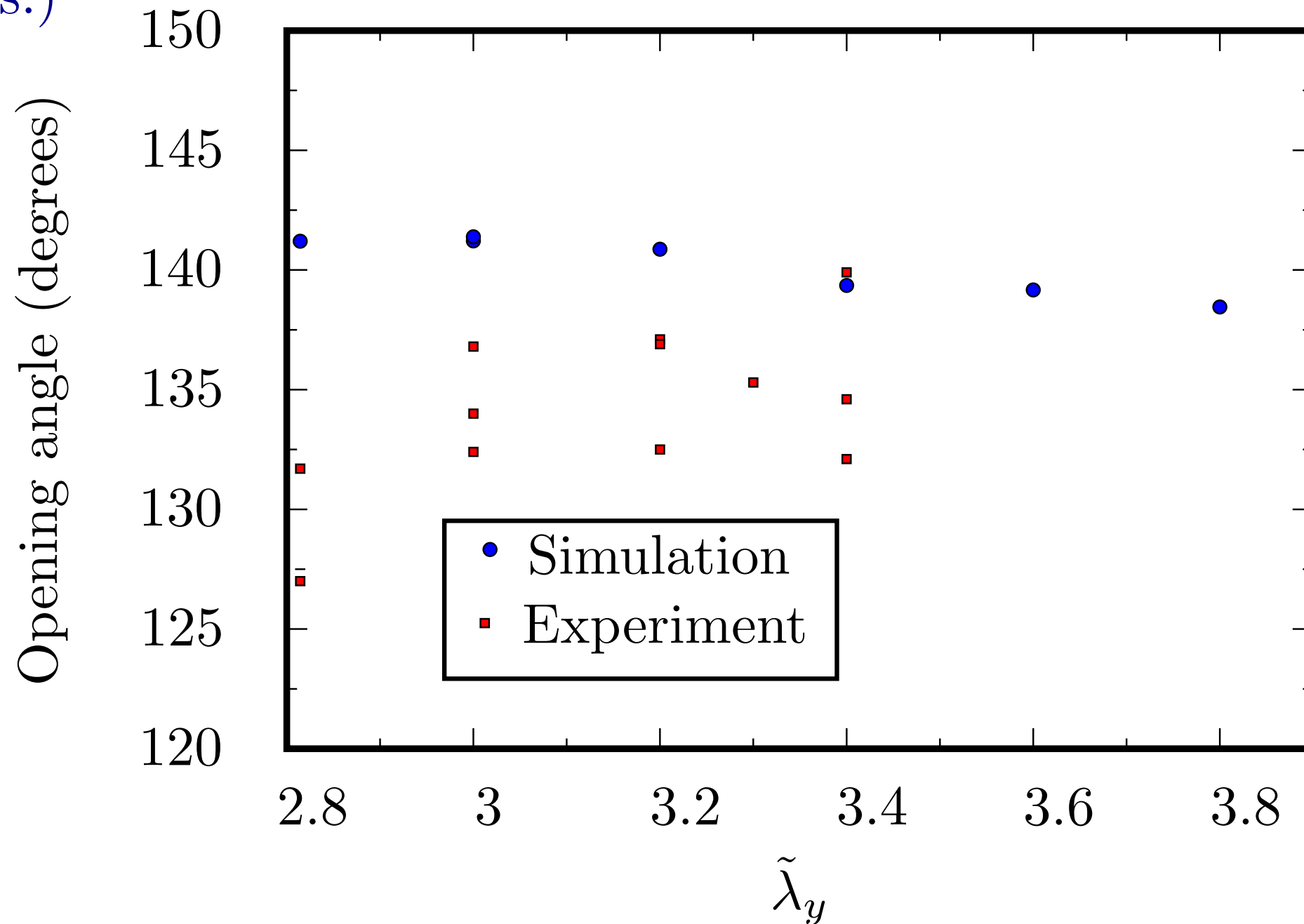
Lattice dynamics, constraint of crack along line, explains work of Buehler, Abraham, and Gao (2003), not hyperelasticity



Theoretical Views

Opening Angles

Opening angle comparisons are less successful (simulations involve all measured features of experiment, including all sound speed variations.)



Conclusions

New Sort of Failure

- The rupture is supersonic
- There is no energy release; energy arrives from very near tip.
- Dissipation and toughening of front behind tip are key physical ingredients; variations in sound speed are present in real system but play no role in theory.
- Problem can be solved exactly in continuum and discrete formulations
- Comparison of rupture speeds with experiment is good.
- Comparison of rupture angles with experiment less satisfactory.
- Oscillatory instability and application to other systems remain to be studied.