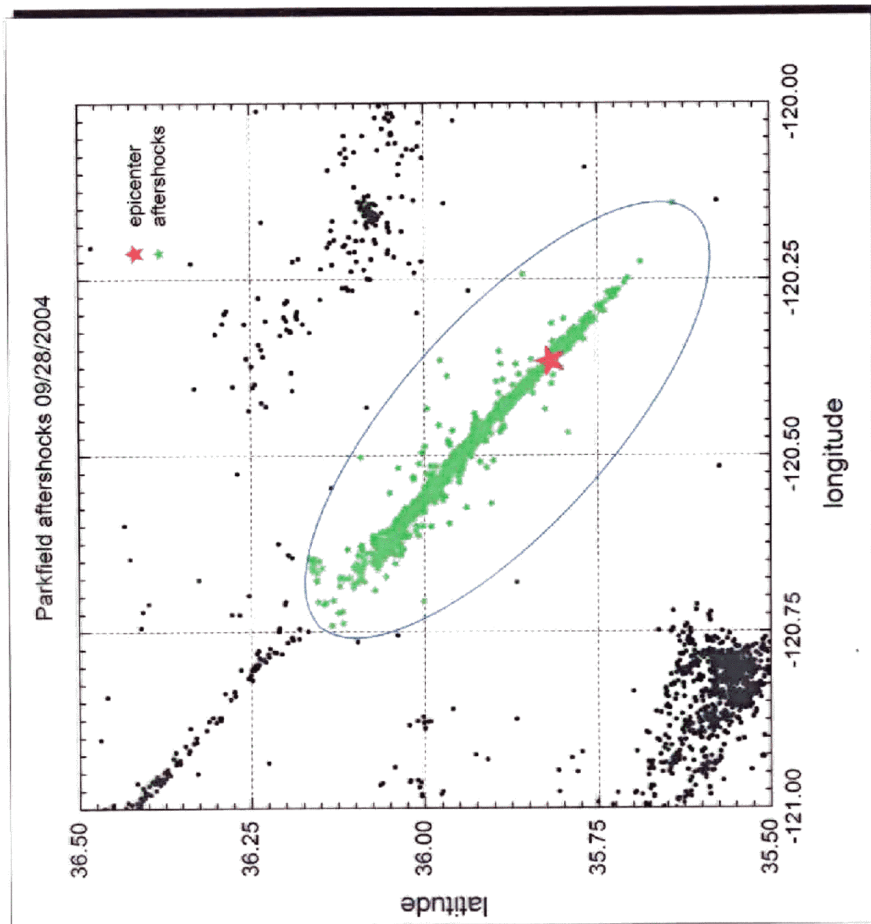


DAB-L



### The Modified Form of Bath's Law

- ▶ The Gutenberg-Richter scaling for aftershocks

$$\log N(> m) = a - b m.$$

- ▶ Infer the magnitude  $m^*$  of the greatest aftershock from an extrapolation of the Gutenberg-Richter scaling applied to the aftershock sequence:

$$m^* = m_{ms} - \Delta m.$$

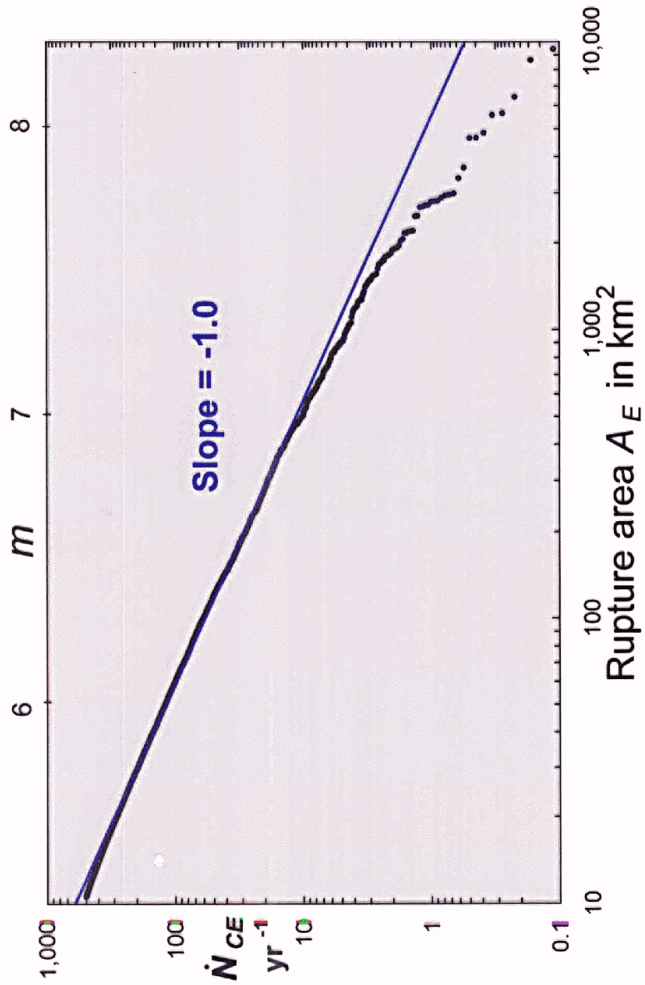
- ▶ The constant  $a$  is obtained by setting  $N(> m^*) = 1$  so that  $a = b m^*$ . Finally we obtain

$$\log N(> m) = b (m^* - m),$$

$$\log N(> m) = b (m_{ms} - \Delta m - m)$$

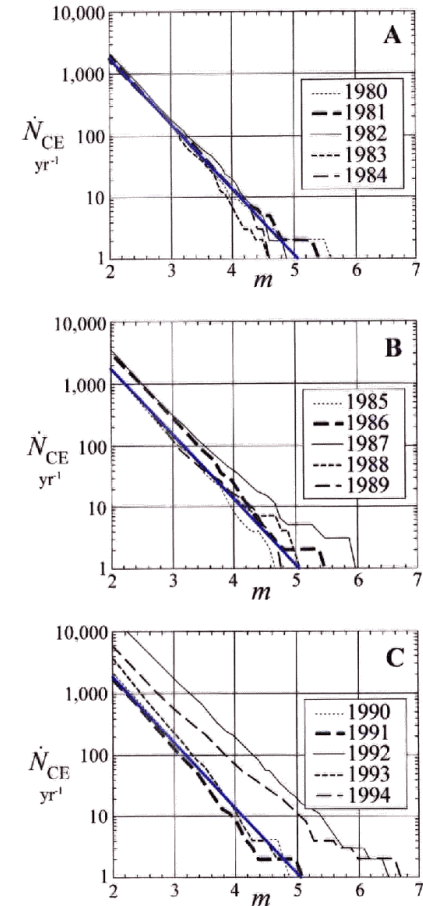
~~\_\_\_\_\_~~

*E&FS 2*



**Frequency-size Statistics of World Wide EQ's (1977-1994)**  
 (Harvard CMT database, theoretical  $A_E$  and  $m$  from earthquake moments)

*E&FS 11*



**Southern California Earthquakes, cumulative frequency-size distributions for 15 individual years.**

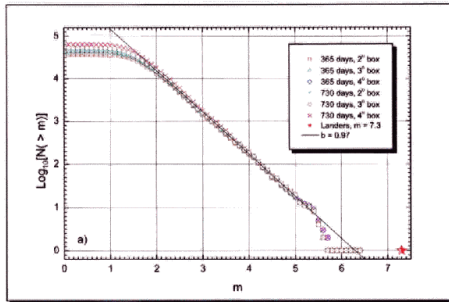
The solid blue straight line represents best-fit to all data 1980-1994,  $\log \dot{N}_{CE} = -1.05 m + 5.3$ .

DAB-03

### Application to Southern California

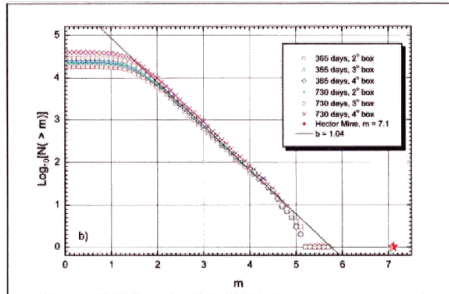
► Consider eight earthquakes with magnitude greater than 5 in southern and Baja California that occurred between 1987 and 2002.

$m_{0.1} = 7.3$   
 $m_{100} = 6.3$   
 $m^* = 8.2$   
 $\Delta m^* = 1.1$   
 $b = 0.97$

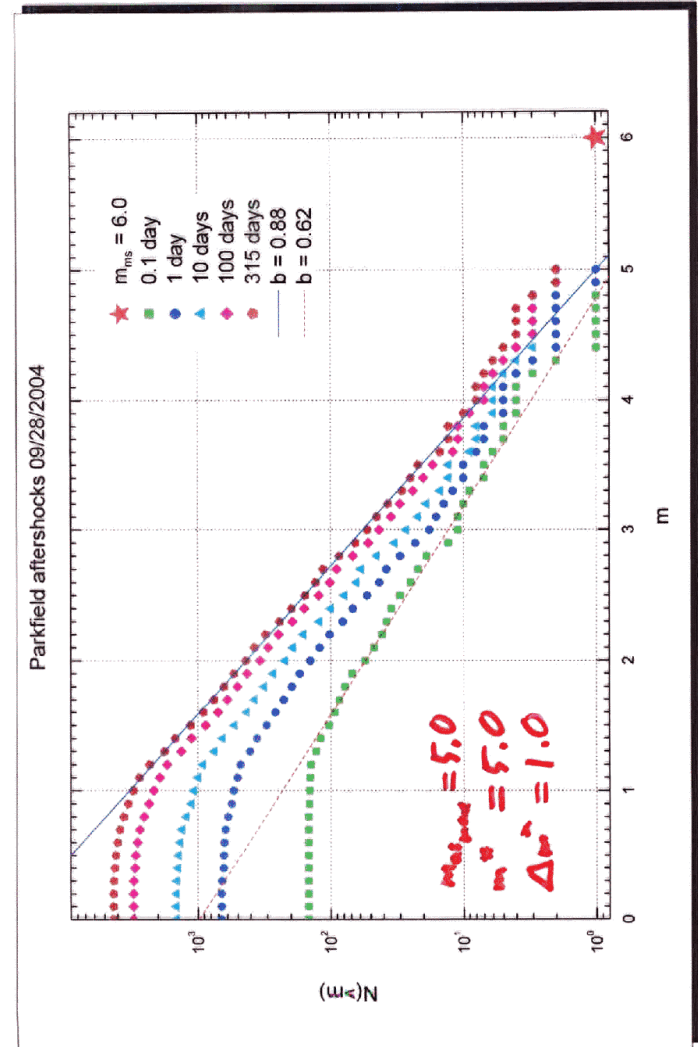


Landers 6/28/92

$m_{0.1} = 7.1$   
 $m_{100} = 5.8$   
 $m^* = 5.75$   
 $\Delta m^* = 1.35$   
 $b = 1.00$



Hector Mine 12/22/01



$m_{0.1} = 6.0$   
 $m^* = 5.0$   
 $\Delta m^* = 1.0$

DAB-10

### Partitioning of Energy

- ▶ The energy  $E$  radiated in an earthquake with moment magnitude  $m$

$$\log_{10} E(m) = \frac{3}{2}m + \log_{10} E_0$$

with  $E_0 = 6.3 \times 10^4$  Joules.

- ▶ The moment magnitude of the main shock  $m_{\text{ms}}$

$$E_{\text{ms}} = E_0 10^{\frac{3}{2}m_{\text{ms}}}$$

- ▶ The total radiated energy in the aftershock sequence

$$E_{\text{as}} = \int_{-\infty}^{m^*} E(m) \left( -\frac{dN}{dm} \right) dm.$$

DAB-11

- ▶ The aftershock rate

$$dN = -b (\ln 10) 10^{b(m_{\text{ms}} - \Delta m - m)} dm.$$

- ▶ Carrying out the integration we find

$$E_{\text{as}} = \frac{b}{\left(\frac{3}{2}-b\right)} E_0 10^{\frac{3}{2}(m_{\text{ms}} - \Delta m)}.$$

- ▶ The ratio of the total radiated energy in aftershocks  $E_{\text{as}}$  to the radiated energy in the main shock  $E_{\text{ms}}$

$$\frac{E_{\text{as}}}{E_{\text{ms}}} = \frac{b}{\frac{3}{2}-b} 10^{-\frac{3}{2}\Delta m}.$$

- ▶ The fraction of the total energy associated with aftershocks

$$\frac{E_{\text{as}}}{E_{\text{ms}} + E_{\text{as}}} = \frac{\frac{b}{\frac{3}{2}-b} 10^{-\frac{3}{2}\Delta m}}{1 + \frac{b}{\frac{3}{2}-b} 10^{-\frac{3}{2}\Delta m}}.$$

► Combined scaling gives Omori's law

$$\frac{dN}{dt} = \frac{(p-1) 10^{b(m_{ms}-\Delta m-m)}}{c(1+t/c)^p}$$

or

$$\frac{1}{N_T} \frac{dN}{dt} = \frac{(p-1)}{c(1+t/c)^p}$$

Identical to the form used by Reasenberg and Jones (1989) and by Yamanaka and Shimazaki (1990)

$$\frac{dN}{dt} = \frac{10^{a+b(m_{ms}-m)}}{(c+t)^p}$$

if

$$\Delta m = \frac{1}{b} [\log_{10}(p-1) + (p-1) \log_{10}(c) - a]$$

For 62 California aftershock sequences RJ give  $c = 0.04$  days,  $a = -1.67$ ,  $b = 0.9$ ,  $p = 1.08 \Rightarrow \Delta m = 0.52$ .

For 27 Japanese aftershock sequences YS give  $c = 0.3$  days,  $a = -1.83$ ,  $b = 0.85$ ,  $p = 1.3 \Rightarrow \Delta m = 1.35$

DAO-2

DAO 12

► Modified form of Omori's law

$$\frac{dN_{as}}{dt} = \frac{1}{\tau} \frac{1}{(1+t/c)^p}$$

► Gutenberg-Richter law for aftershocks

$$N_{as}(\geq m) = 10^{a-bm}$$

► Modified form of Båth's law for aftershocks

$$\Delta m^* = m_{ms} - m^* \approx \text{constant} \approx 1.2$$

$m_{ms}$  - main shock magnitude

$m^*$  - "largest" aftershock (from GR)

$$1 = 10^{a-bm^*} \text{ or } a = bm^*$$

$$N_{as}(\geq m) = 10^{b(m_{ms}-\Delta m^*-m)}$$

$$N_{as}(\geq m) = \int_0^{\infty} \frac{dN_{as}}{dt} dt = \frac{c}{(p-1)\tau}$$

$$\frac{c}{\tau} = (p-1) 10^{b(m_{ms}-\Delta m^*-m)}$$



DAD 13

► Hypothesis I:

$c = c_0 = \text{constant}$

$\tau(m) = \frac{c_0}{(p-1)} 10^{-b(m_{ms} - \Delta m^* - m)}$

$$\frac{dN_{as}}{dt} = \frac{(p-1) 10^{b(m_{ms} - \Delta m^* - m)}}{c_0} \frac{1}{\left(1 + \frac{t}{c_0}\right)^p}$$

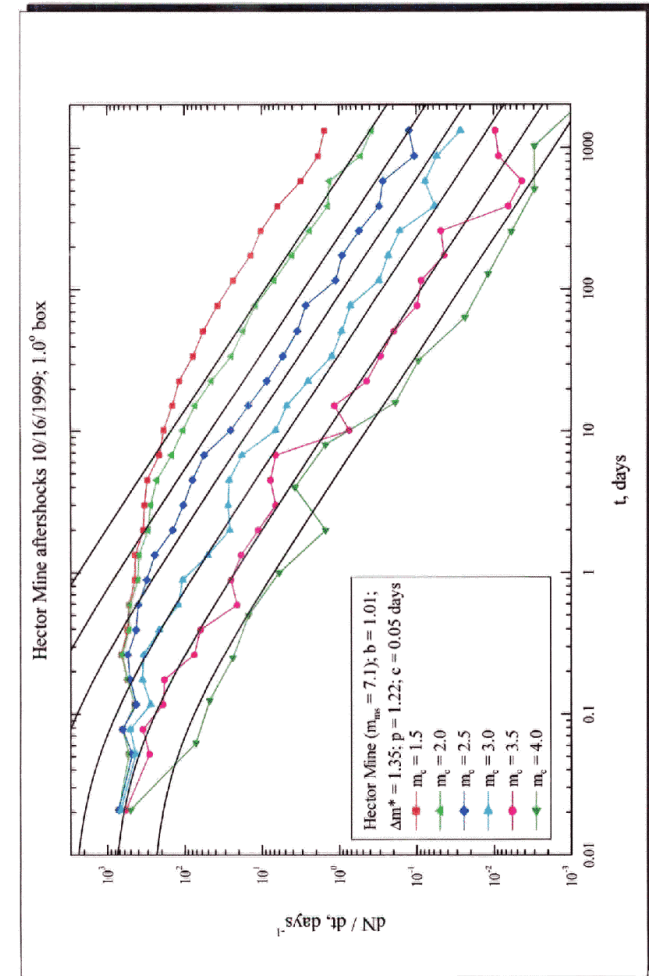
► Hypothesis II:

$\tau = \tau_0 = \text{constant}$

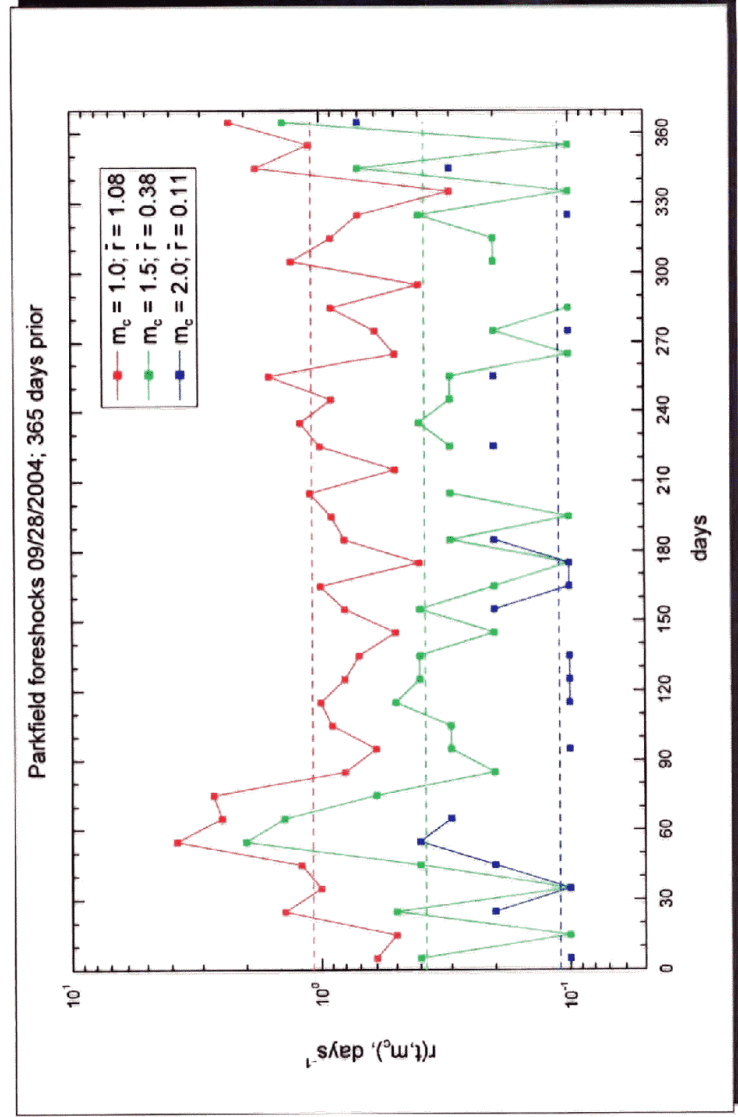
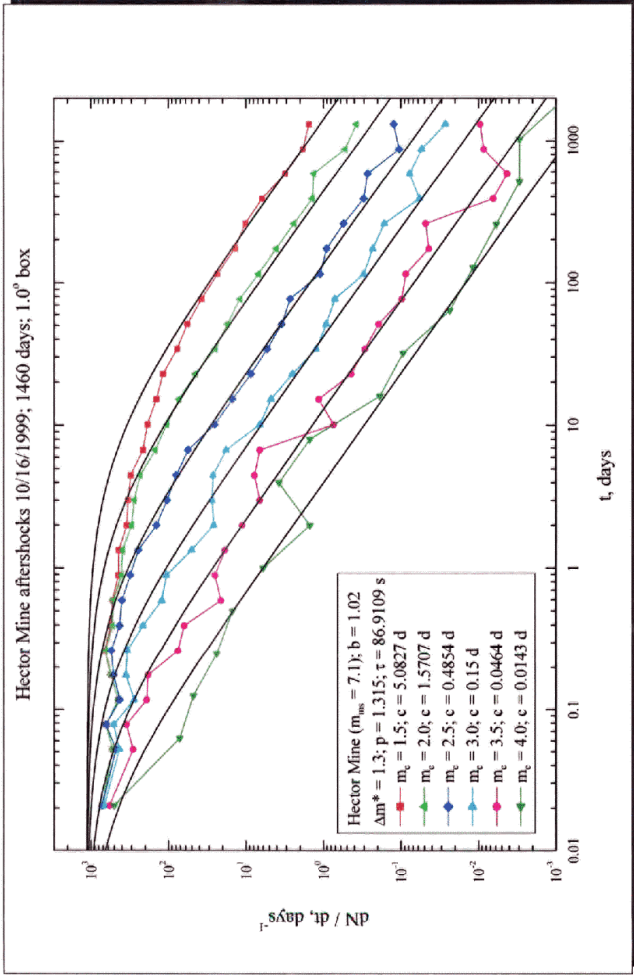
$c(m) = \tau_0 (p-1) 10^{b(m_{ms} - \Delta m^* - m)}$

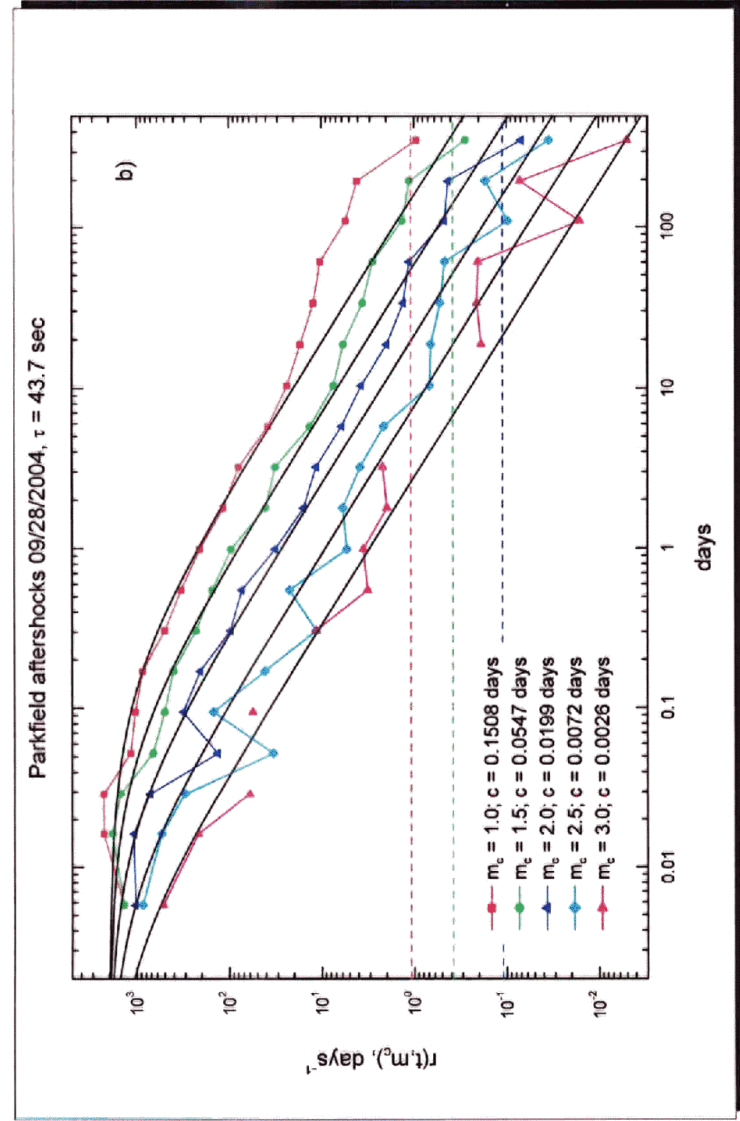
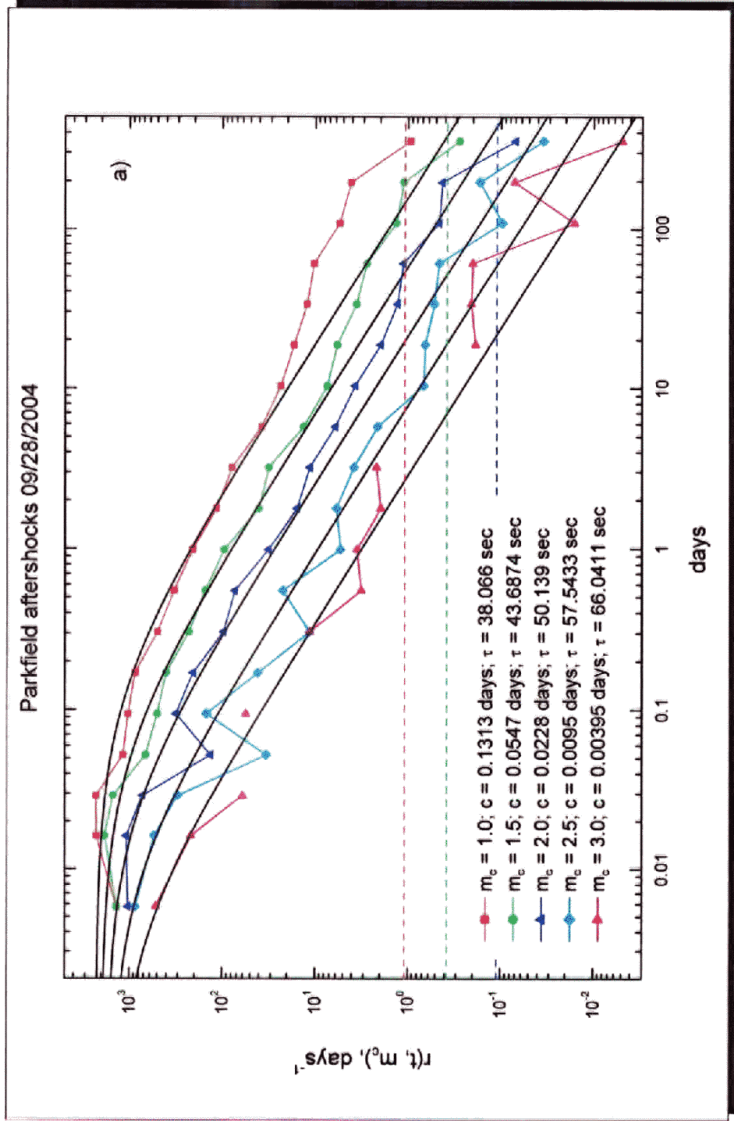
$$\frac{dN_{as}}{dt} = \frac{1}{\tau_0} \frac{1}{\left(1 + \frac{t}{c(m)}\right)^p}$$

DAD 14



DA015







DPO 16

Earthquake	$m_{ms}$	$b$	$\Delta m^*$	$p$	$R$	$\beta$	$bp$	$c(m^*), s$	$\tau_0, s$
Landers	7.3	0.98	1.10	1.22	4.0	1.20	1.19	33	107.3
Northridge	6.7	0.91	0.75	1.17	3.4	1.06	1.06	23	53.1
Hector Mine	7.1	1.02	1.35	1.22	4.1	1.23	1.24	32	83.7
San Simeon	6.5	1.0	1.10	1.12	3.5	1.09	1.12	55	50.2
Parkfield	6.0	0.88	1.0	1.09	3.16	0.96	0.96	5.2	43.7
Sumatra	9.3	1.26	1.8	1.11	3.46	1.60	1.4	50	172.8

$$\frac{r(0, m_c)}{r(0, m_c + d_m)} = 10^{\alpha d_m}, \quad \frac{r(t \gg 1, m_c)}{r(t \gg 1, m_c + d_m)} = 10^{\beta d_m}$$

$$\beta = bp \quad \text{if} \quad \alpha = 0$$

► Definition of the equilibration time  $t_e(m)$

- It is the time after a main shock required to establish the validity of GR scaling for aftershocks with magnitudes  $m$
- It is the time after a main shock when the aftershock rate given by the modified Omori's law

$$\frac{dN_{as}}{dt} = \frac{1}{\tau} \frac{1}{(1 + \frac{t}{c})^p}$$

deviates from power-law scaling

$$\left(\frac{dN_{as}}{dt}\right)_{ps} = \frac{1}{\tau} \left(\frac{c}{t}\right)^p$$

by 10%

$$\frac{(dN_{as}/dt)}{(dN_{as}/dt)_{ps}} = \frac{(t_e/c)^p}{(1 + t_e/c)^p} = 0.90$$

$$t_e = \frac{c(m)}{\left[\frac{1}{0.9^{1/p}} - 1\right]}$$

DAO 17

- Assume  $p = 1.2$

Equilibration time:  $t_e = 10.9 c(m)$

- Hypothesis II:  $c(m) = 0.2 \tau_0 10^{b(m_{ms} - \Delta m^* - m)}$
- Assume  $b = 1$ , “largest” aftershock  $m^* = m_{ms} - \Delta m^*$

but  $10^{m^* - m} = \frac{A^*}{A}$

where  $A^*$  rupture area of  $m^*$  earthquake and  $A$  rupture area of  $m$  earthquake

therefore

$$t_e = 2.18 \tau_0 \frac{A^*}{A}$$

### Continuum Damage Mechanics with a Yield Stress

- Uniaxial stress

$$\sigma = E_0 \epsilon \quad \text{if } \sigma \leq \sigma_y$$

$E_0$  – Young’s modulus (undamaged)

$$\sigma - \sigma_y = E_0 (1 - \alpha) (\epsilon - \epsilon_y) \quad \text{if } \sigma > \sigma_y$$

$\alpha$  – damage variable.

- Kinetic equation

$$\frac{d\alpha(t)}{dt} = 0 \quad \text{if } 0 \leq \sigma \leq \sigma_y$$

$$\frac{d\alpha(t)}{dt} = \frac{1}{t_d} \left( \frac{\sigma}{\sigma_y} - 1 \right)^\rho \left( \frac{\epsilon}{\epsilon_y} - 1 \right)^2 \quad \text{if } \sigma > \sigma_y$$

$t_d$  – characteristic time for damage

DAO-7

► Constant stress  $\sigma_0 > \sigma_y$  applied instantaneously at  $t = 0$

$$\frac{d\alpha(t)}{dt} = \frac{1}{t_d} \left( \frac{\sigma_0}{\sigma_y} - 1 \right)^\rho \left( \frac{\epsilon}{\epsilon_y} - 1 \right)^2$$

$$\left( \frac{\sigma_0}{\sigma_y} - 1 \right) = \left( \frac{\epsilon}{\epsilon_y} - 1 \right) (1 - \alpha)$$

with  $\alpha = 0$  at  $t = 0$ .

► Integration gives

$$\alpha = 1 - (1 - t/t_f)^{1/3}, \quad t_f = \frac{t_d}{(\sigma_0/\sigma_y - 1)^{\rho+2}}$$

$$\epsilon = \epsilon_y \left[ 1 + \frac{\sigma_0/\sigma_y - 1}{(1 - t/t_f)^{1/3}} \right]$$

► Energy in acoustic emissions

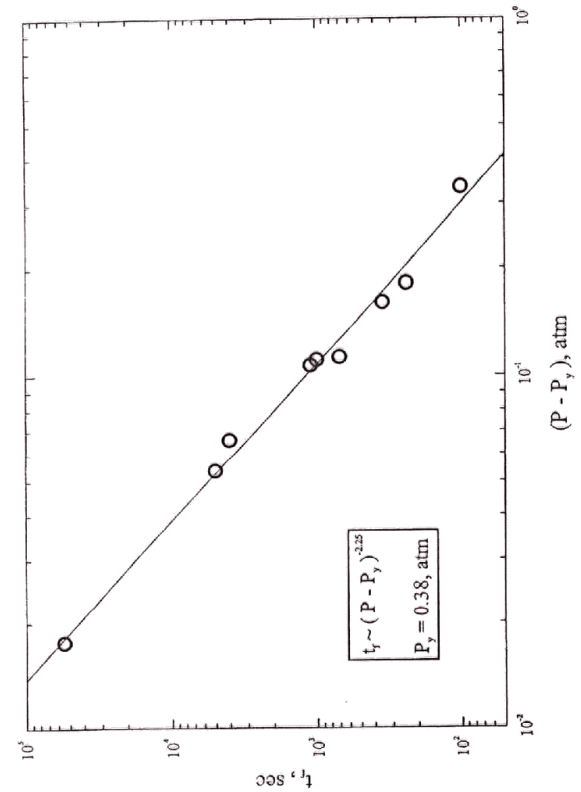
$$e_a = \frac{1}{2}(\sigma_0 - \sigma_y)(\epsilon - \epsilon_y) = \frac{(\sigma_0 - \sigma_y)^2}{2E_0} \left[ \frac{1}{(1 - t/t_f)^{1/3}} - 1 \right]$$

$$\frac{de_a}{dt} = \frac{(\sigma_0 - \sigma_y)^2}{6t_f E_0} \frac{1}{(1 - t/t_f)^{4/3}}$$

DAO-8

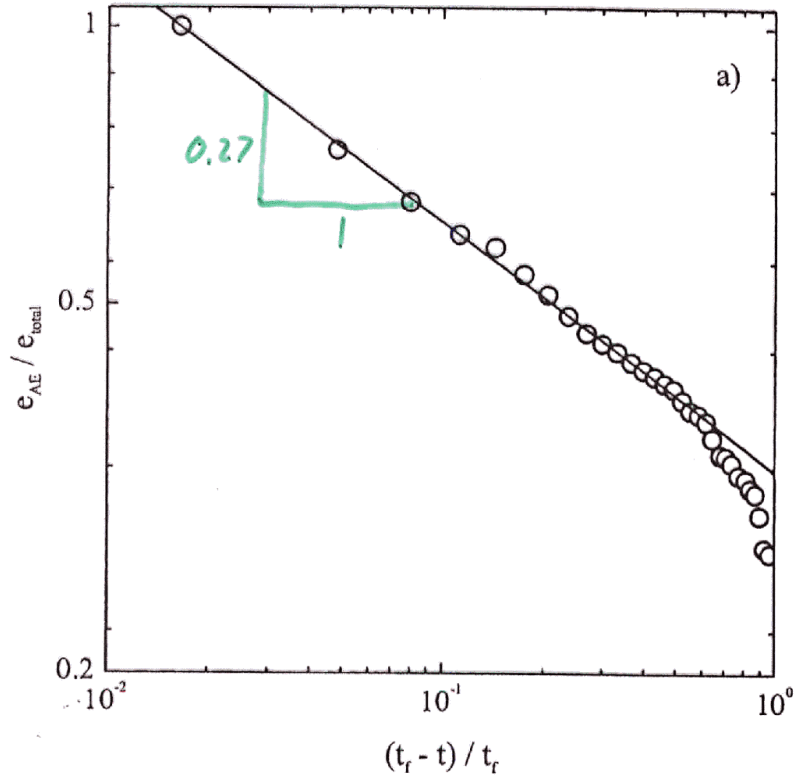
Fig 11'

Time to failure  $t$  after the instantaneous application of a differential pressure at  $t = 0$ .



Guarino et al. (1999)

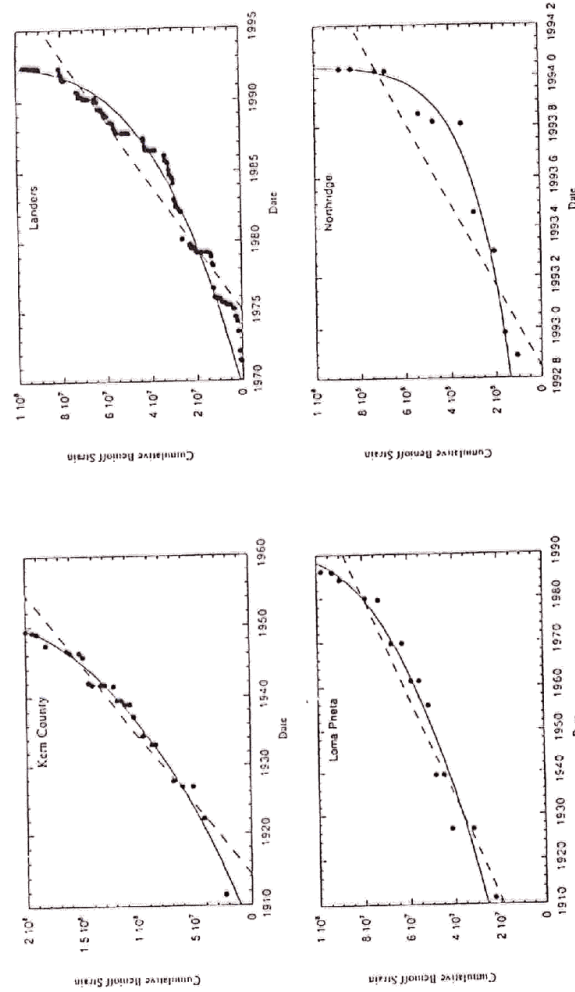
DiG 12



acoustic emissions after instantaneous application of stress  $\sigma_0$

$t_f$  time to failure after stress application

Guarino et al. (1999)



EAP 6

Power-law activation  
 Bufe and Vannor JGR 98, 9871 (1993)  
 Bowman et al. JGR 103, 24357 (1998)

Fig. 21

► Constant strain  $\epsilon_0 > \epsilon_y$  applied instantaneously at  $t = 0$

$$\frac{d\alpha(t)}{dt} = \frac{1}{t_d} \left( \frac{\sigma}{\sigma_y} - 1 \right)^\rho \left( \frac{\epsilon_0}{\epsilon_y} - 1 \right)^2$$

$$\left( \frac{\sigma}{\sigma_y} - 1 \right) = \left( \frac{\epsilon_0}{\epsilon_y} - 1 \right) (1 - \alpha)$$

with  $\alpha = 0$  at  $t = 0$ .

► Integration gives

$$\alpha = 1 - [1 + (\rho - 1)(\epsilon_0/\epsilon_y - 1)^{\rho+2} t/t_d]^{-1/(\rho-1)}$$

$$\frac{\sigma}{\sigma_y} = 1 + \frac{(\epsilon_0/\epsilon_y - 1)}{[1 + (\rho - 1)(\epsilon_0/\epsilon_y - 1)^{\rho+2} t/t_d]^{1/(\rho-1)}}$$

► Energy in acoustic emissions

$$e_{ae} = \frac{E_0}{2} (\epsilon_0 - \epsilon_y)^2 \left[ 1 - [1 + (\rho - 1)(\epsilon_0/\epsilon_y - 1)^{\rho+2} t/t_d]^{-1/(\rho-1)} \right]$$

$$\frac{de_{ae}}{dt} = \frac{\frac{E_0 \epsilon_y^2}{2 t_d} (\epsilon_0/\epsilon_y - 1)^{\rho+4}}{[1 + (\rho - 1)(\epsilon_0/\epsilon_y - 1)^{\rho+2} t/t_d]^{\rho/(\rho-1)}}$$

DAO-10

► Damage mechanics applied to aftershocks

$$e_{ae} = \frac{E_0}{2} (\epsilon_0 - \epsilon_y)^2 \left[ 1 - [1 + (\rho - 1)(\epsilon_0/\epsilon_y - 1)^{\rho+2} t/t_d]^{-1/(\rho-1)} \right]$$

$$t \rightarrow \infty, e_{aet} = \frac{E_0}{2} (\epsilon_0 - \epsilon_y)^2 \quad (\text{total ae})$$

$$\frac{1}{e_{aet}} \frac{de_{ae}}{dt} = \frac{\frac{1}{t_d} (\epsilon_0/\epsilon_y - 1)^{\rho+2}}{[1 + (\rho - 1)(\epsilon_0/\epsilon_y - 1)^{\rho+2} t/t_d]^{\rho/(\rho-1)}}$$

Let  $\frac{\rho}{\rho-1} = p$  and  $c = \frac{t_d}{(\rho-1)(\epsilon_0/\epsilon_y - 1)^{\rho+2}}$

$$\frac{1}{e_{aet}} \frac{de_{ae}}{dt} = \frac{p-1}{c} \frac{1}{(1-t/c)^p}$$

Parkfield  
 $p = 1.09$   
 $\rho = 12$

► Omori's law for aftershocks

$$\frac{1}{N_T} \frac{dN}{dt} = \frac{p-1}{c} \frac{1}{(1-t/c)^p}$$

DAO-11



► Time dependent rate for the decay of the aftershock activity

$$r(t) = \frac{1}{\tau (1 + t/c)^p}$$

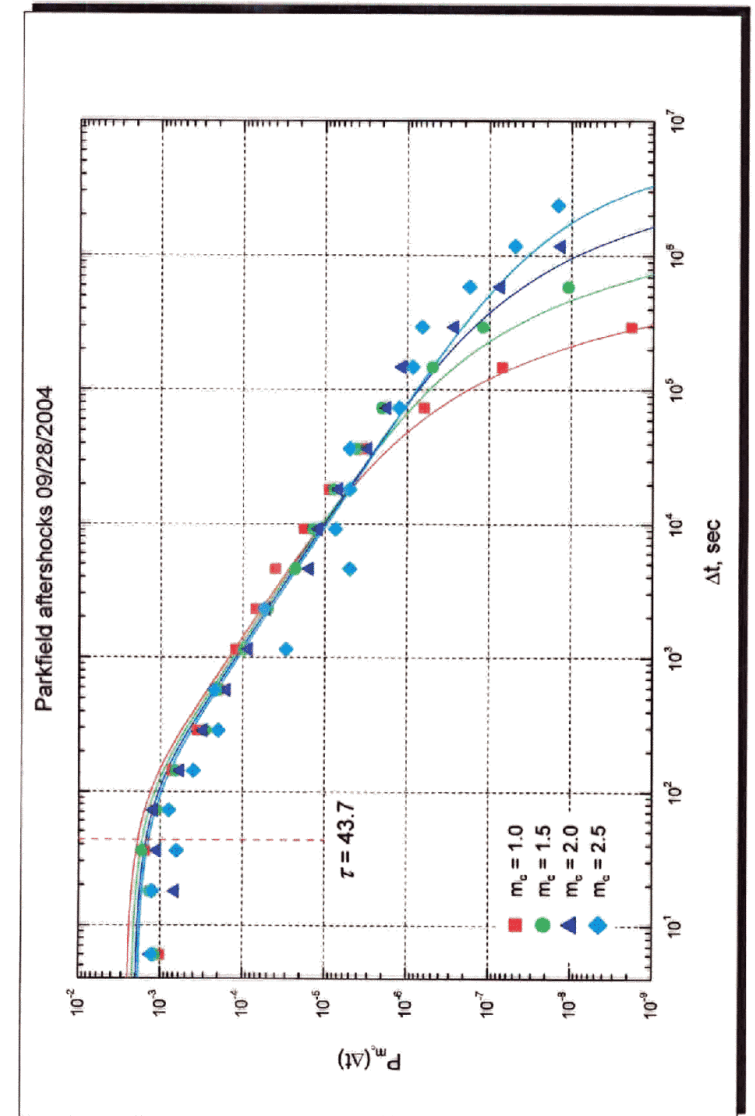
► The probability density function of inter-occurrence times over a finite time period  $T$

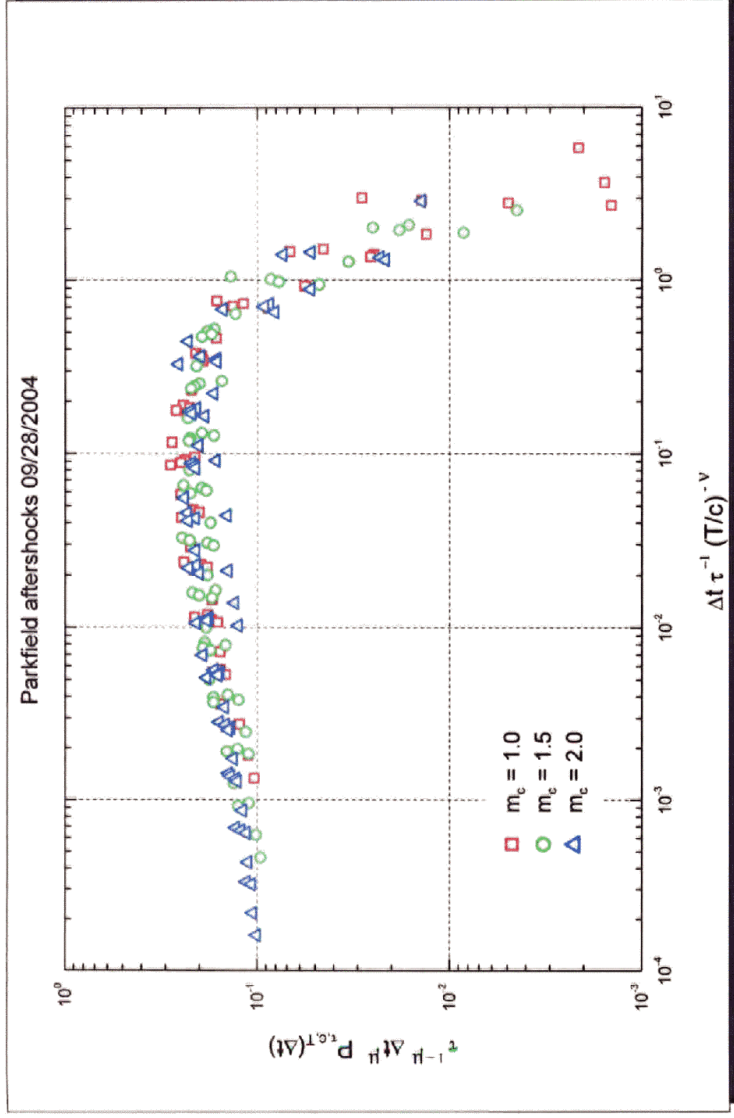
$$P_T(\Delta t) = \frac{1}{N} \left[ r(\Delta t) e^{-\int_0^{\Delta t} r(u) du} + \int_0^{T-\Delta t} r(s) r(s + \Delta t) e^{-\int_s^{s+\Delta t} r(u) du} ds \right],$$

where  $N = \int_0^T r(u) du$  is the total number of events during a time period  $T$ .

► Scaling law for the above distribution

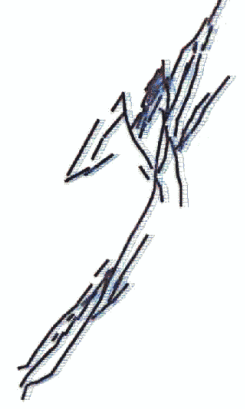
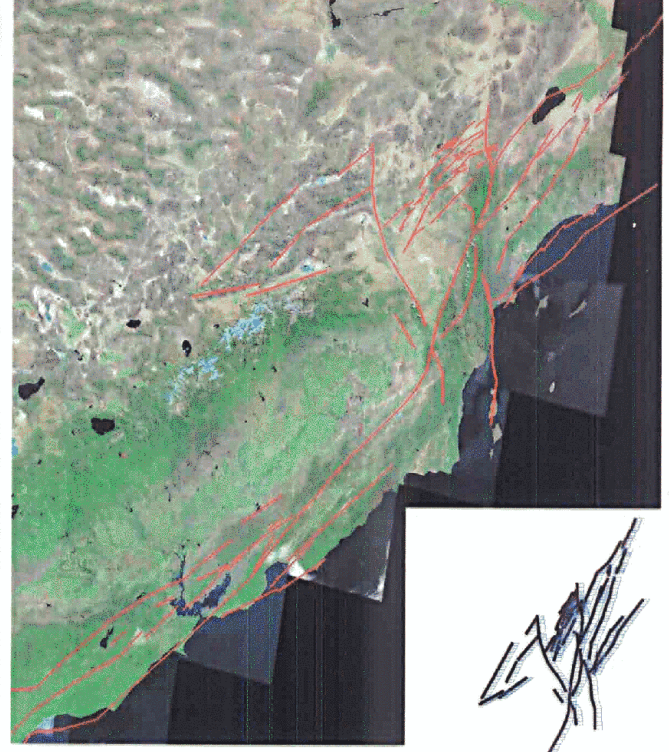
$$P_{\tau,c,T}(\Delta t) = \frac{1}{\tau} \left( \frac{\Delta t}{\tau} \right)^{-\alpha} f \left[ \frac{\Delta t}{\tau} \left( \frac{T}{c} \right)^{-\beta} \right]$$



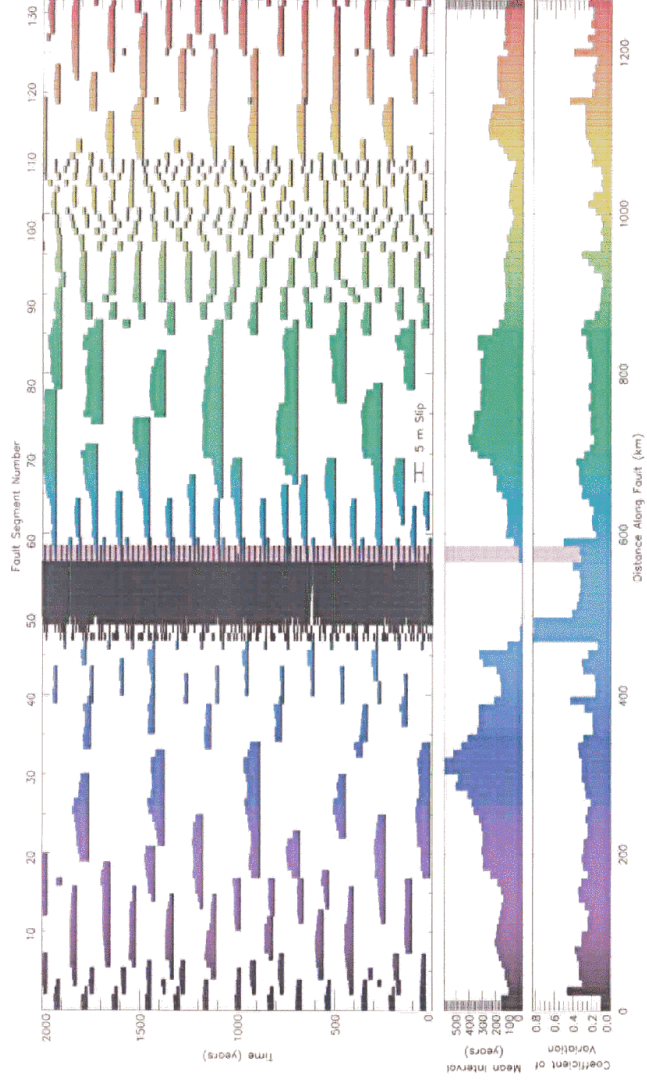


**Virtual California 2001 Represents All the Major Active Strike Slip Faults in California**  
 (PB Rundle et al, to be submitted, 2004)

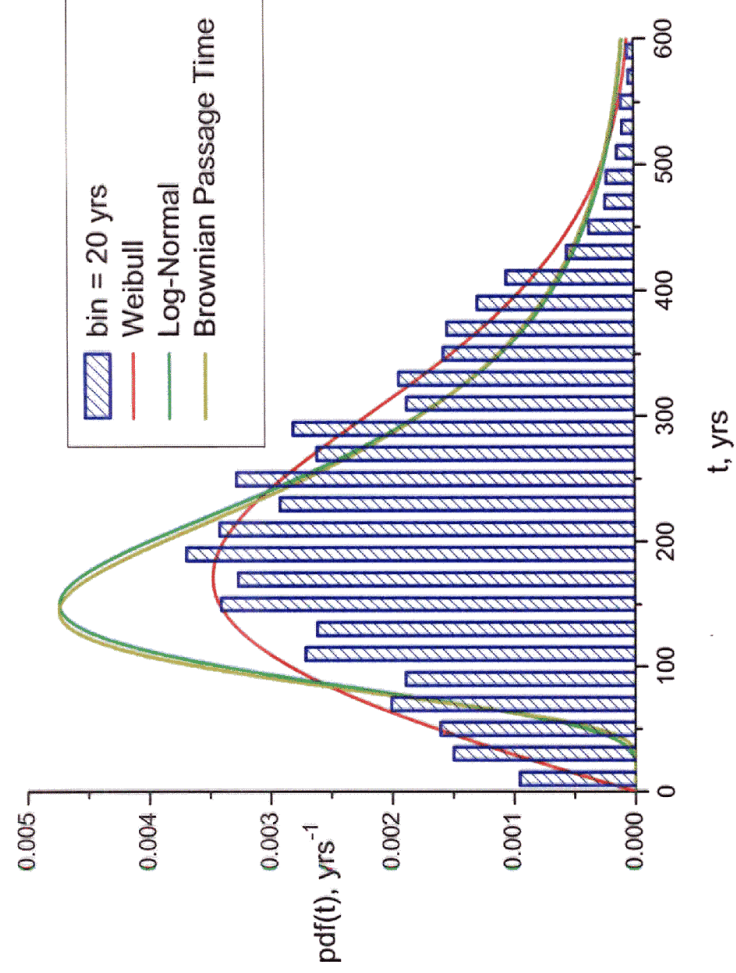
Faults in RED are shown superposed on a Landsat image of California. (Image courtesy of Peggy Li, JPL)



EQVCI



Northern San-Andreas,  $M_c = 7.5$ ,  $N = 4606$ ,  $\mu = 217.1$  yrs,  $\sigma = 114.7$  yrs,  $c_y = 0.528$



**EQVC6**



ERVC 13

► Dynamic fiber-bundle model

$$\frac{dN}{dt} = -\nu \left( \frac{\sigma}{\sigma_0} \right) N = -\nu_0 \left( \frac{\sigma}{\sigma_0} \right)^\rho N$$

$N$  – number of fibers,  $\sigma$  – stress

$\nu_0$  — reference hazard rate

► Assume  $\frac{\sigma}{\sigma_0} = \frac{t}{\tau}$ , let  $\rho = \beta - 1$ ,  $\nu_0 = \frac{\beta}{\tau}$

$$\frac{dN}{dt} = -\frac{\beta}{\tau} \left( \frac{t}{\tau} \right)^{\beta-1} N$$

with  $N = N_0$  at  $t = 0 \Rightarrow \frac{N}{N_0} = \exp \left[ - \left( \frac{t}{\tau} \right)^\beta \right]$

► Number of failed fibers  $N_f = N_0 - N$

► Cumulative probability of failure

$$P(t) = 1 - \exp \left[ - \left( \frac{t}{\tau} \right)^\beta \right] \text{ Weibull dist.}$$

► Conditional cumulative probability of failure at time  $t$  if no failure at time  $t_0$

$$P(t, t_0) = 1 - \exp \left[ \left( \frac{t_0}{\tau} \right)^\beta - \left( \frac{t}{\tau} \right)^\beta \right]$$

