Models for tensorial rheology of soft glassy materials

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Outline

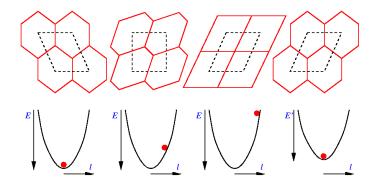
- Soft glassy materials
- The scalar SGR model
- Doing it right: SGR with tensors
- Some choices for mesoscale rheology
- Example predictions
- Discussion

Soft glassy materials

- Foams, dense emulsions, onion phases, colloidal glasses, clays, pastes, . . .
- Common rheological features:
 - flow curves $\sigma(\dot{\gamma}) \sigma_Y \sim \dot{\gamma}^p$ (0 < p < 1) Herschel-Bulkley (if yield stress $\sigma_Y \neq$ 0) or power-law
 - Nearly 'flat' viscoelastic spectra $G'(\omega)$, $G''(\omega)$ for low frequencies ω
 - Rheological aging
- Suggests common underlying features: arrangements of particles/droplets etc are disordered and metastable
- Analogy with glasses
- Soft glassy rheology approach exploits this; minimal model (based on Bouchaud's trap model)

SGR model (scalar version)

- Divide sample into mesoscopic elements
- Each has local shear strain *l*, which increments with macroscopic shear γ
- But when strain energy $\frac{1}{2}kl^2$ gets close to yield energy E, element can yield
- Yielding resets l=0, and element acquires new E from some distribution $\rho(E) \sim e^{-E}$
- Yielding is activated by an effective temperature x; models interactions between elements



Equation of motion

• In dimensionless units (for time, energy)

$$\dot{P}(E,l,t) = -\dot{\gamma}\frac{\partial P}{\partial l} - e^{-(E-kl^2/2)/x}P$$
$$+ \Gamma(t)\rho(E)\delta(l)$$

$$\Gamma(t) = \langle e^{-(E-kl^2/2)/x} \rangle$$
 = aver. yielding rate

- Macroscopic stress $\sigma(t) = k\langle l \rangle$
- Without shear, P(E,t) approaches equilibrium $P_{\text{eq}}(E) \propto \exp(E/x)\rho(E)$ for long t
- Get glass transition if $\rho(E)$ has exponential tail; happens at x = 1 if $\rho(E) = e^{-E}$ (possible justification from extreme value statistics)
- For x < 1, system is in glass phase; never equilibrates \Rightarrow aging

SGR predictions

- Find Herschel-Bulkley (x < 1) and power-law flow curves (1 < x < 2)
- Viscoelastic spectra G', $G'' \sim \omega^{x-1}$ are flat near x=1
- In glass phase (x < 1) find rheological aging, loss modulus $G'' \sim (\omega t)^{x-1}$ decreases with age t
- Steady shear always 'interrupts' aging, restores stationary state
- Stress overshoots in shear startup, nonlinear
 G' and G'', linear and nonlinear creep, . . .

Constitutive equation

 Solve equation of motion; get 'birth-death' relation between stress and strain:

$$\sigma(t) = G_0(z_{t0})k\gamma(t)$$
$$+ \int_0^t dt' \Gamma(t')G_1(z_{tt'})k \left[\gamma(t) - \gamma(t')\right]$$

• Survival probabilities from t = 0 & after yield:

$$G_0(z) = \langle e^{-z \exp(-E/x)} \rangle_{P_0}$$

 $G_1(z) = \langle e^{-z \exp(-E/x)} \rangle_{\rho}$

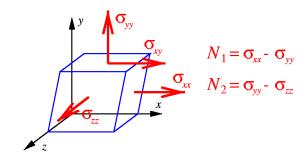
 Get nonlinearities only via effective time interval: strain 'speeds up the clock'

$$z_{tt'} = \int_{t'}^{t} dt'' \, \exp\left(k \left[\gamma(t'') - \gamma(t')
ight]^2/2x
ight)$$

• Yielding rate $\Gamma(t)$ determined from similar relation as for $\sigma(t)$ (from normalization of P)

Drawbacks of scalar SGR model

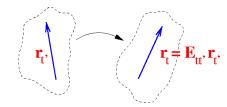
- Interpretation of effective temperature x; also so far constant but should have own dynamics
- Scalar description: only shear strain and stress considered
- Want a proper tensorial model to study e.g. normal stresses N₁, N₂, uniaxial deformations, . . .



- Also linear elasticity (stress = kl) at mesoscale (element level) very naive
- Want more flexible modelling of mesoscale rheology

Doing it right: SGR with tensors

Idea: deformation tensor E_{tt} replaces strain difference



• Changes constitutive equation to

$$\sigma(t) = G_0(z_{t0}) \mathbf{Q}(\mathbf{E}_{t0}) + \int_0^t dt' \, \Gamma(t') G_1(z_{tt'}) \mathbf{Q}(\mathbf{E}_{tt'})$$

with effective time interval

$$z_{tt'} = \int_{t'}^{t} \exp\left[\frac{\mathbf{R}(\mathbf{E}_{t''t'})}{x}\right] dt''$$

- Q(E): local stress tensor for deformation E
- R(E): lowering of energy barrier for yielding

Choices for mesoscale rheology

 By analogy with scalar SGR, assume energy barrier is lowered by stored elastic (free) energy (density):

$$R(\mathbf{E}) = \lambda \frac{\mathcal{F}(\mathbf{E}) - \mathcal{F}_0}{\mathcal{F}_0}$$

- $\lambda = O(1)$ determines which fraction of $\Delta \mathcal{F}$ can be converted into work to overcome yield barrier
- For small shear strains, $R(\gamma) = \lambda \chi \gamma^2/2$; $\chi = G/\mathcal{F}_0$ is dimensionless ratio of shear modulus G and \mathcal{F}_0
- **Q**(**E**) determines instantaneous stress response, in particular ratio $\varphi = N_1/N_2$ of normal stress differences

Dense emulsions & foams

 Model 1: Assume affine deformation of isotropic ensemble of fluid interfaces; Doi & Ohta showed

$$Q_{\mu\nu}(\mathsf{E}) = \frac{15}{4} \int \frac{d^2\mathbf{u}}{4\pi} \frac{\frac{1}{3}\delta_{\mu\nu} - u_{\mu}u_{\nu}}{|\mathsf{E}^{\top} \cdot \mathbf{u}|^4}$$
 with $R(\mathsf{E})/\lambda = -1 + \int \frac{d^2\mathbf{u}}{4\pi} |\mathsf{E}^{\top} \cdot \mathbf{u}|^{-4}$

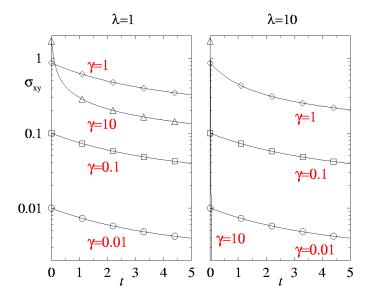
- Has $\chi = G/\mathcal{F}_0 = 4/15$, and for shear strains $\varphi = N_1/N_2 = -7/6...-1$ as γ increases
- Model 2: Analytic approximation for shear strains; has $\chi = 1/3$, and $\varphi = -1$ for all γ
- Model 3: Due to Larson, $R/\lambda = -1 + \frac{1}{3} \text{tr} (\mathbf{E}^{\mathsf{T}} \mathbf{E})^{-1/2}$
- Designed to allow for constant contact angles (120°) between films; gives $\chi = 1/6$ and $\varphi = -3/4...-1$, closer to numerical results for dry foams
- Focus mainly on models 1 & 2 in the following

Predictions: Step strain

• In equilibrium (requires x > 1) find after step deformation **E**, with $G_{eq}(z) \propto \int_{z}^{\infty} dz' G_{1}(z')$:

$$\sigma(t) = \mathbf{Q}(\mathbf{E}) G_{eq}(t \exp[R(\mathbf{E})/x])$$

- Nonlinearities in t-dependence only via factor $\exp[R(\mathbf{E})/x]$, as in scalar model
- Extra nonlinearities via instantaneous Q(E); but ratios of σ_{xy} , N_1 and N_2 constant in time

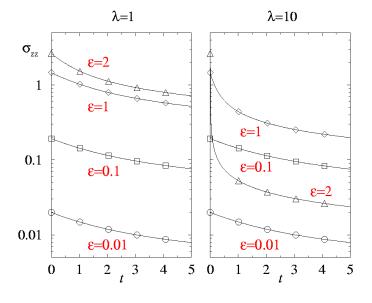


Uniaxial step strain

• Step deformation with

$$\mathbf{E}=\left(egin{array}{ccc} e^{-\epsilon/2} & 0 & 0 \ 0 & e^{-\epsilon/2} & 0 \ 0 & 0 & e^{\epsilon} \end{array}
ight)$$

- Can use unapproximated model 1
- As before, all stress tensor components have t-independent ratios

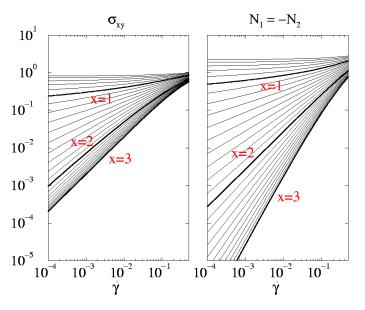


Steady shear flow

- For low shear rate $\dot{\gamma}$, Newtonian scalings are $\sigma_{xy} \sim \dot{\gamma}$, $N_{1,2} \sim \dot{\gamma}^2$
- Effects of glassiness (for any reasonable Q, R)

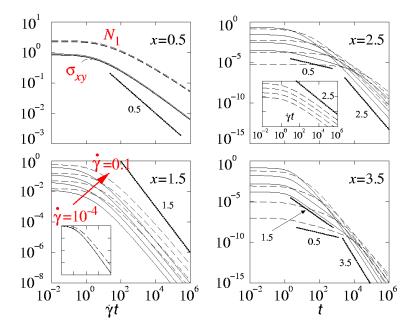
$$\sigma_{xy}, N_{1,2} \propto \left\{ egin{array}{ll} \dot{\gamma}^{x-1}, & 1\!<\!x\!<\!\left\{ egin{array}{ll} 2 \ 3 \end{array}
ight\} & ext{for } \left\{ egin{array}{ll} \sigma_{xy} \ N_{1,2} \end{array}
ight\} \ & ext{const.}, & x<1 \end{array}
ight.$$

• For model 2 with $\lambda = 1$:



Cessation of steady shear

- Steady shear $\dot{\gamma}$, stop at t = 0. Stress relaxation?
- In glassy regime, get scaling with $\dot{\gamma}t$: shear flow has 'imprinted' relaxation timescale $\sim 1/\dot{\gamma}$
- $N_{1,2}$ relax more slowly than shear stress
- For model 2 with $\lambda = 1$:



Conclusions

- Tensorial structure can be added to SGR model without 'damaging' appealing glassy phenomenology
- Flexible description of mesoscale rheology
- Examples for emulsions/foams but can be adapted to soft colloids etc
- Falsifiable predictions experiments welcome
- Foams? Aging caused by coarsening seems to produce ≈ single relaxation time; different from SGR model
- Dense emulsions, microgel beads etc better to see 'glassy' aging experimentally