

Buoyancy-driven currents and sediment transport in the ocean

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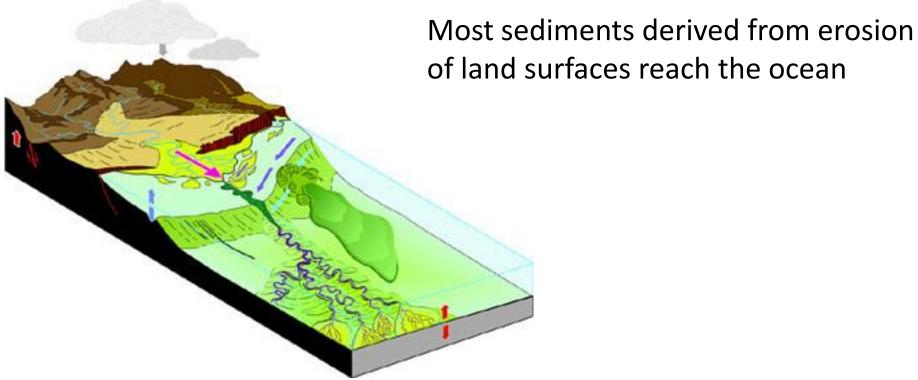
Mohamad Nasr Azadani (UCSB)

With Eckart Meiburg, Brendon Hall, Vineet Birman (UCSB)
Rolf Henniger (ETH)

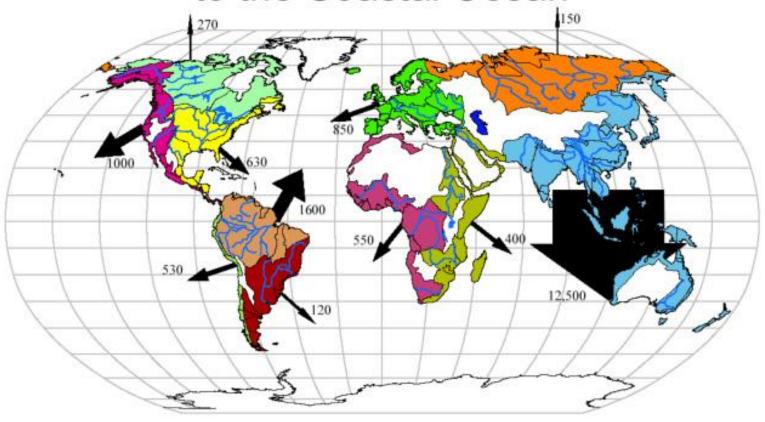
Carolina Boffo, Rafael Manica, (IPH, Federal University of Rio Grande do Sul, Brazil)

Thang Tat Nguyen (University of Aberdeen)



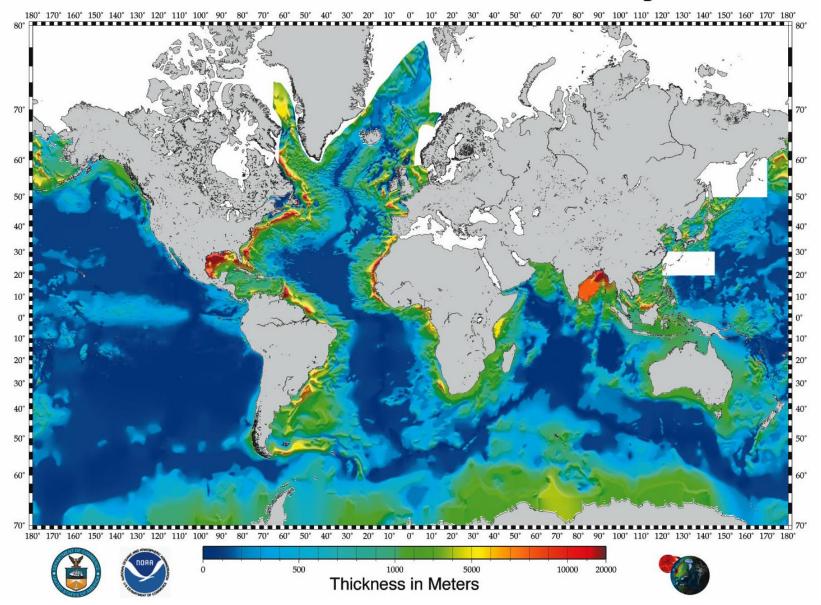


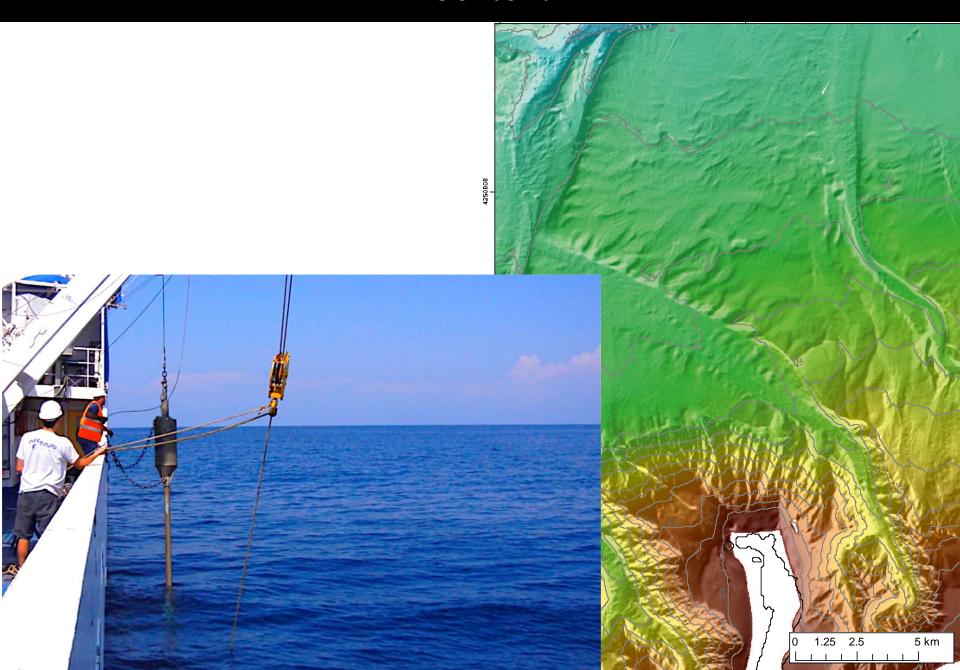
Fluvial Discharge of Suspended Sediment to the Coastal Ocean



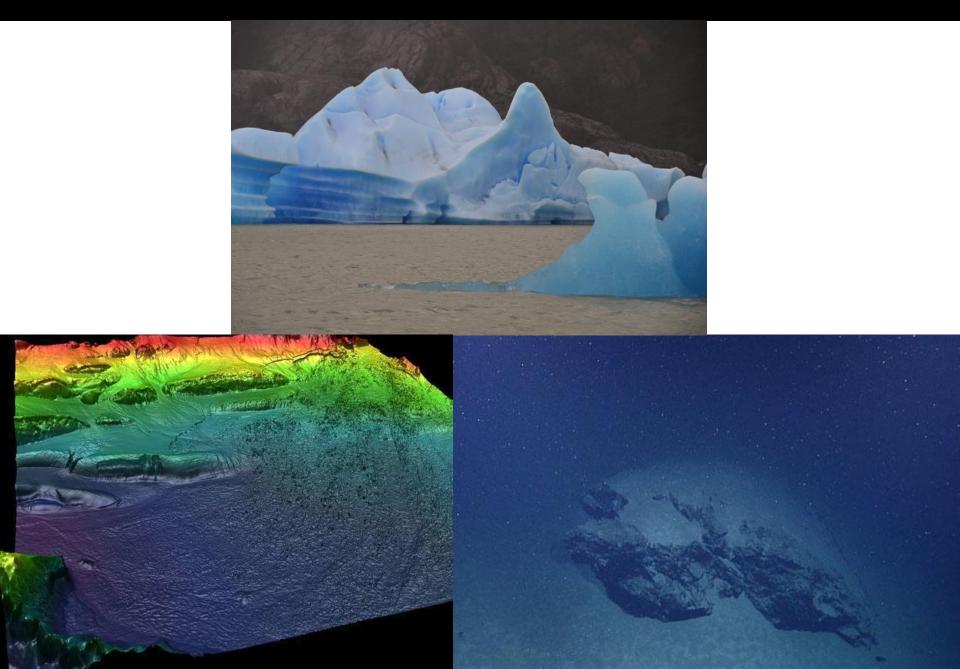
Total = 19×10^9 tonnes per year (Milliman and Farnsworth, 2011)

Total Sediment Thickness of the World's Oceans & Marginal Seas





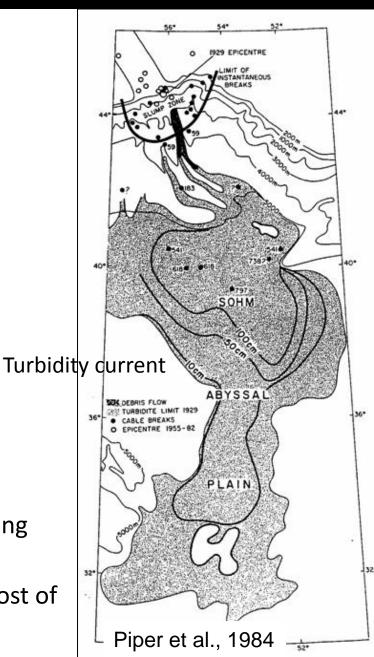
submarine landslides, ice-rafted debris, pelagic settling



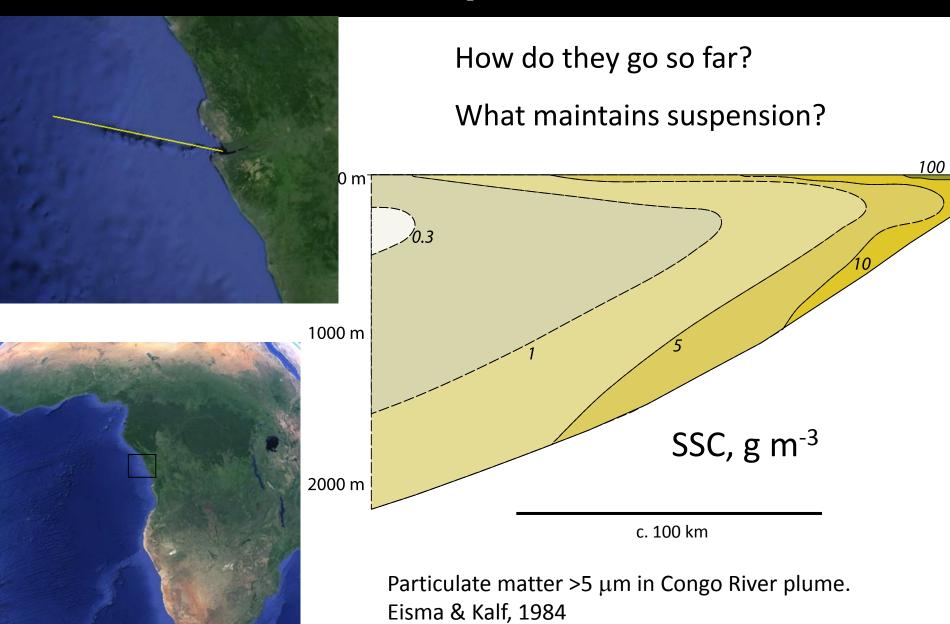
Fluid-mediated transport of sediment to deep water



- Both buoyancy-driven
- Turbulence maintains sediment suspension, affecting buoyancy
- Between them these two processes account for most of the sediment in the deep sea



River plumes



Positively buoyant surface plume



Turbulence generation in shear layer?

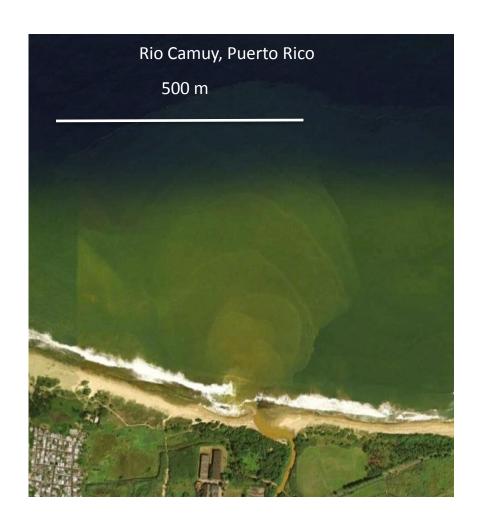
Fresh water

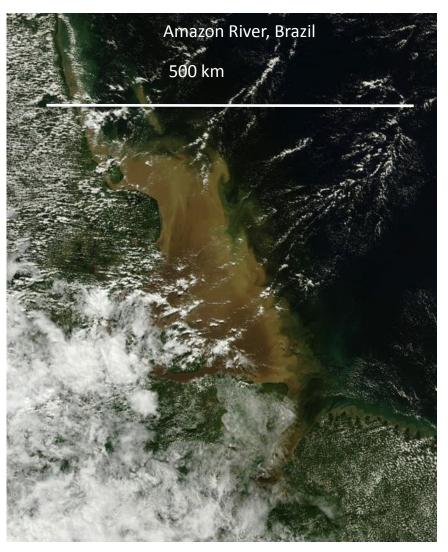
Salt front

Turbulence generation at lower boundary when attached to bed

TURBIDITY MAXIMUM associated with clay flocculation and turbulence decay

River plumes



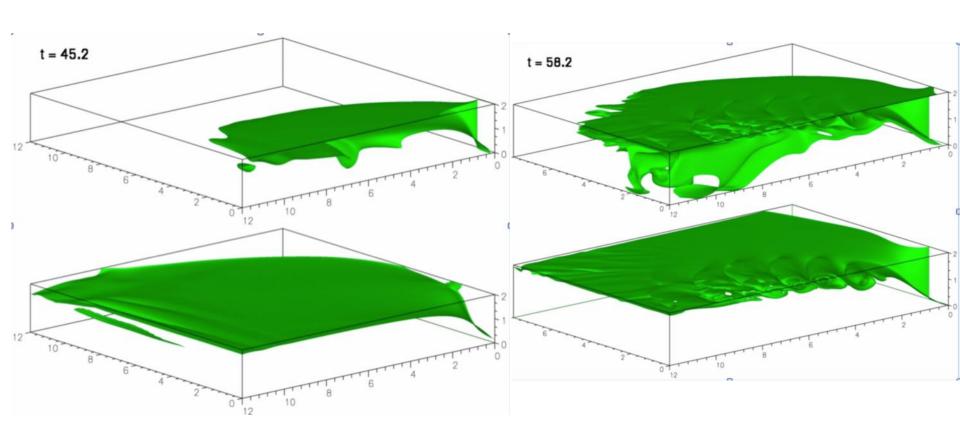


Plume lower boundary stability – numerical simulation

Stability of lower boundary is given by a gradient Richardson number Ri_g .

Typically the stratification is stable for $Ri_g > 0.25$.

$$Ri_{g} = \frac{\left(g \frac{\partial \rho / \partial z}{\rho_{a}}\right)}{\left(\partial u / \partial z\right)^{2}}$$

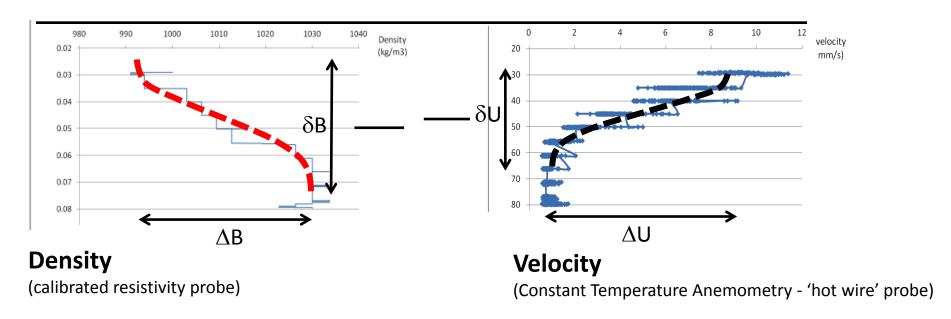


Courtesy of Rolf Henniger, ETH

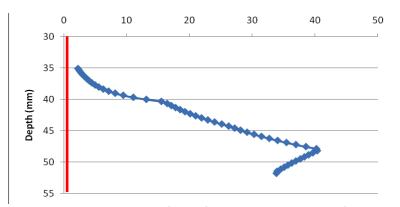
Plume lower boundary stability - laboratory experiment



Plume lower boundary stability - laboratory experiment



Gradient Richardson number

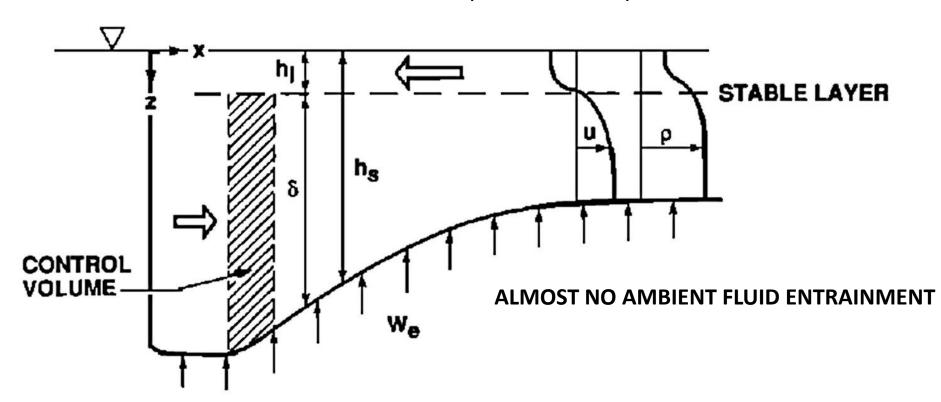


$$Ri_{g} = \frac{\left(g \frac{\partial \rho / \partial z}{\rho_{a}}\right)}{\left(\partial u / \partial z\right)^{2}}$$

Stability of stratification suggests that long-range sediment transport by river plumes depends upon wave-generated turbulence

Plume lower boundary stability - environmental measurement

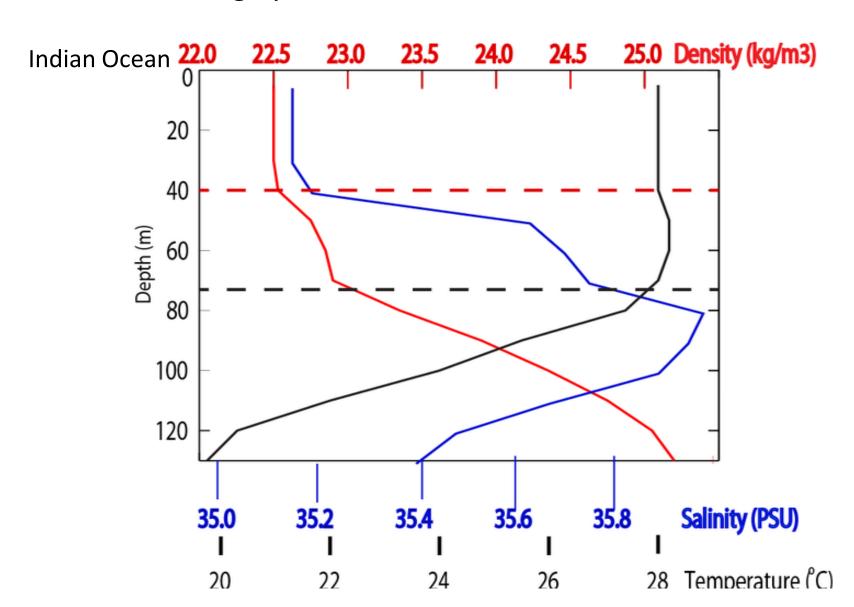
Leschenault Estuary, Koombana Bay, Western Australia

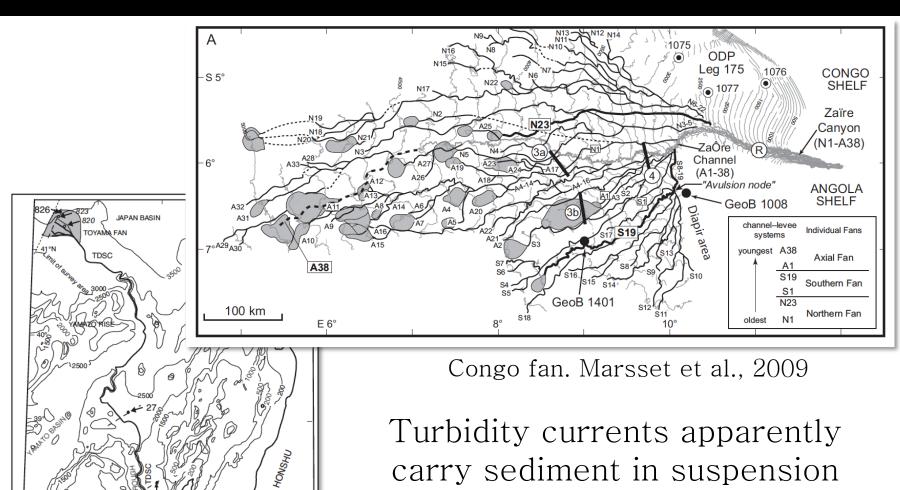


Luketina & Imberger, 1989

Ocean mixing layer

Turbulent mixing by surface waves and wind-induced shear



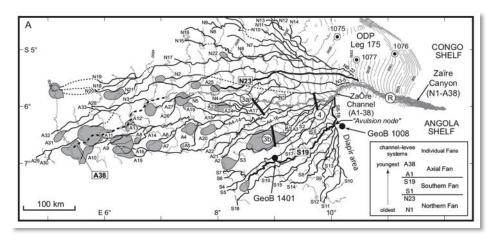


Turbidity currents apparently carry sediment in suspension through channels over very low gradients for 500 km···

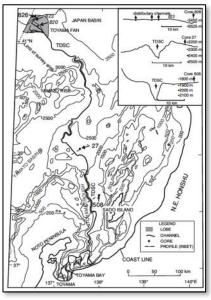
Toyama channel. Nakajima, 2009

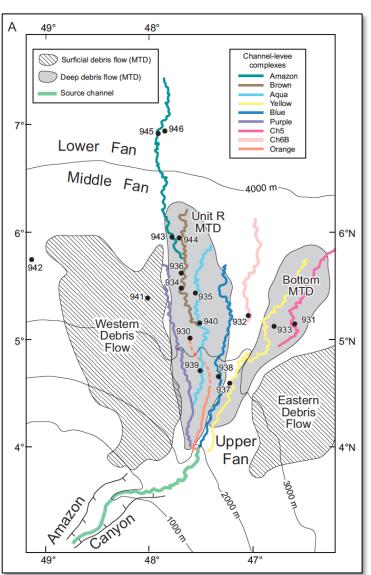
CORE PROFILE (INSET)

100 km



…1000 km…

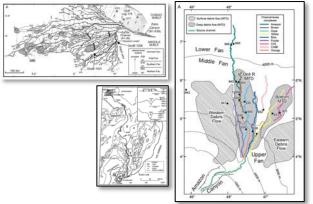


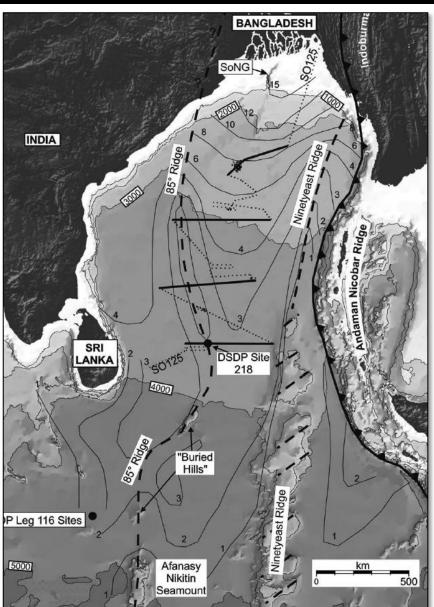


Amazon fan. Maslin, 2009

…even 3000 km

How?

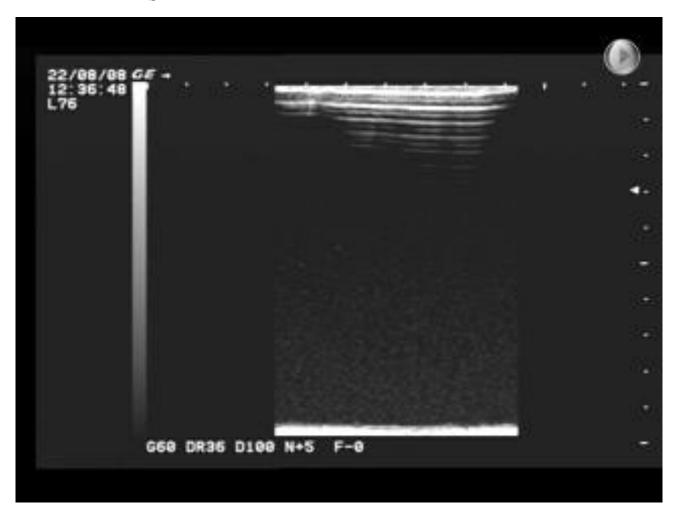




Bengal fan. Schwenk & Spieß, 2009

Unstable stratification - Kelvin-Helmholtz instabilities

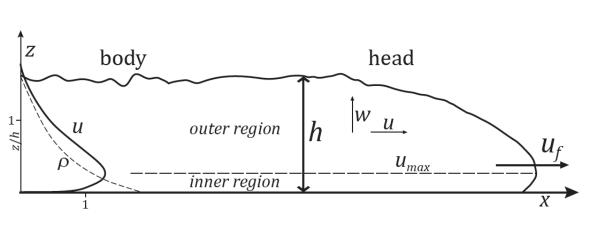
Froude subcritical laboratory turbidity current; crushed coal in water, imaged by medical ultrasound

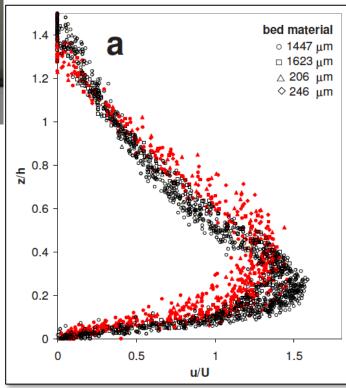


Carolina Boffo, UFRGS

The classic view – velocity profiles

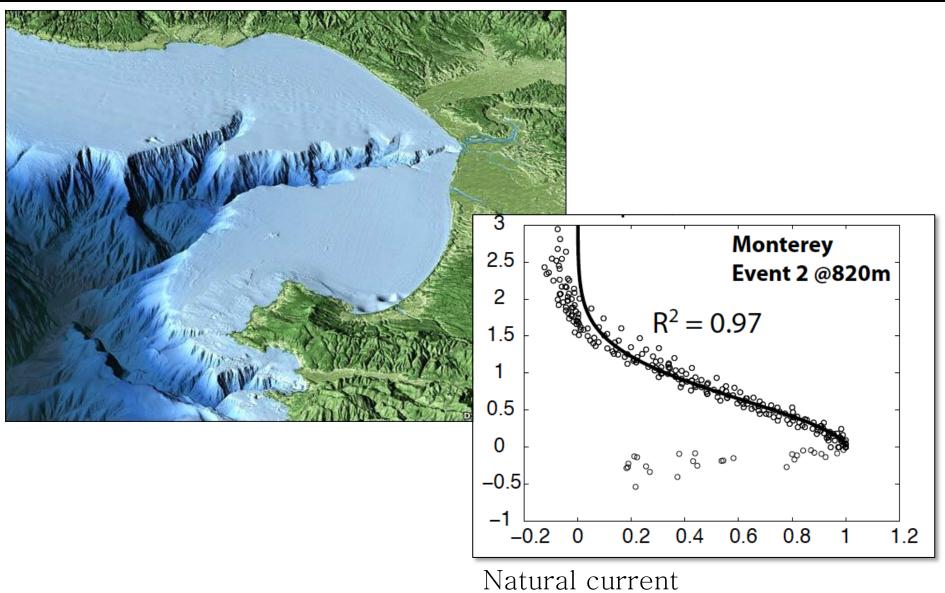






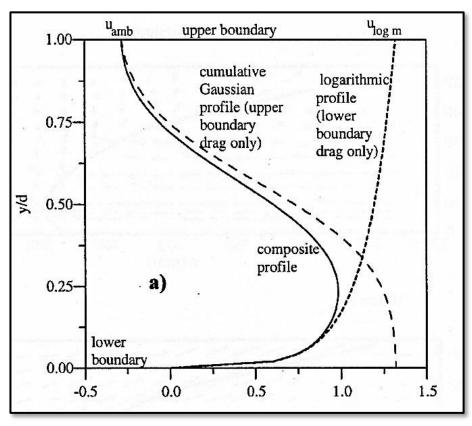
Experiments on supercritical flows Sequeiros et al. 2010

The classic view – velocity profiles



Natural current Xu, 2010

Origin of the velocity profile



Kneller et al., 1999

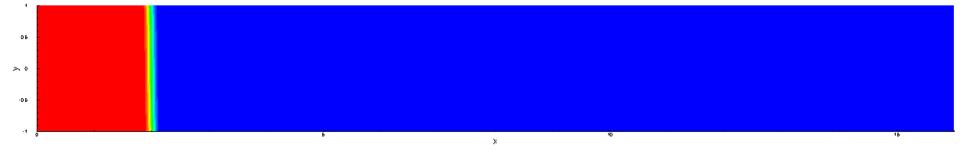
Sum of logarithmic boundary layer profile, and shear layer profile (error function) that extends to the bed where there is high turbulent drag

Kelvin-Helmholtz instabilities

Kelvin-Helmholtz instabilities generated at upper flow boundary when $Ri_g \le 0.25$

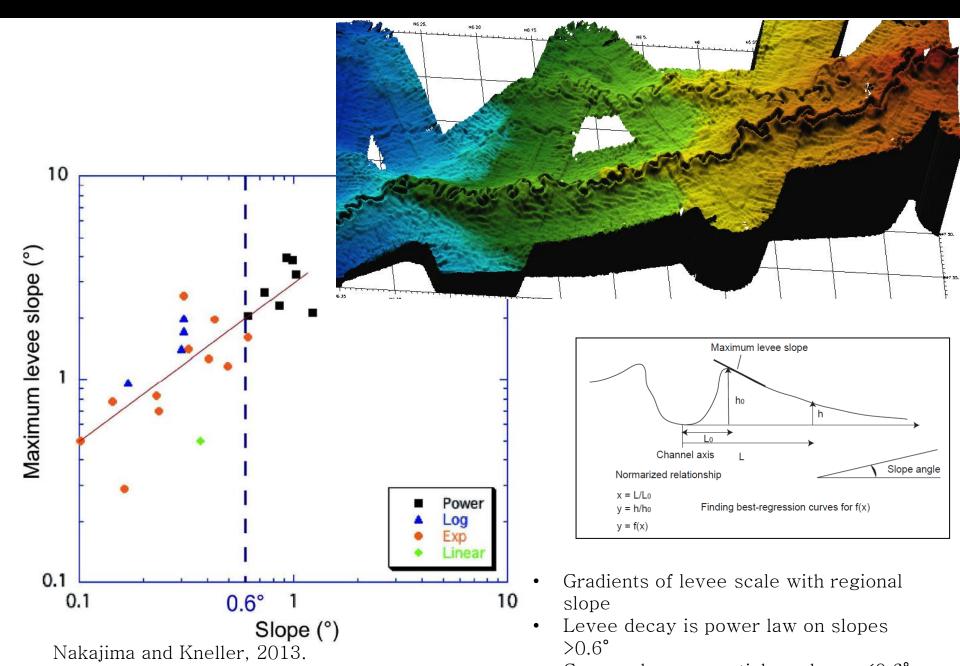
$$Ri_{g} = \frac{N^{2}}{\left(\P u / \P z\right)^{2}} = \frac{e^{\Re g} \frac{\P r / \P z \ddot{0}}{e^{\Im g} r_{a} g}}{\left(\P u / \P z\right)^{2}}$$

Large eddy simulation of turbidity current, Brendon Hall, UCSB



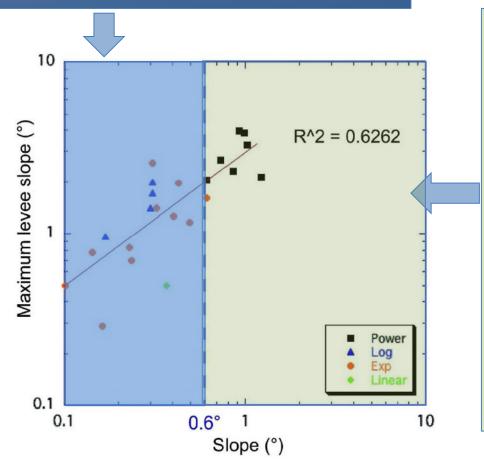
- Turbulent drag largely due to Kelvin-Helmholtz instabilities.
- Entrainment of ambient fluid mainly via KHIs that form when shear dominates and stratification becomes unstable (i.e. when gradient Richardson number is <0.25)

Dependence of levee shape on slope gradient



$$f(x) = f_0 e^{-\left(\frac{u_s}{uh_0}\right)x}$$

Low gradient, exponential decay, no entrainment, No K-H instabilities

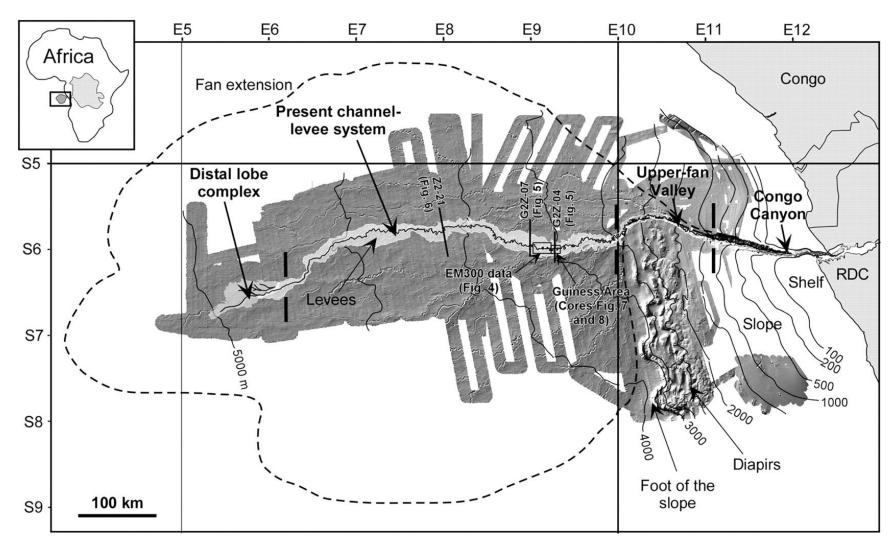


Slope controls presence or absence of entrainment

$$f(\hat{x}) = f_0 \left(\frac{uh_0}{\hat{x}} \right)^{\frac{-u_s + E_0}{E_0}}$$

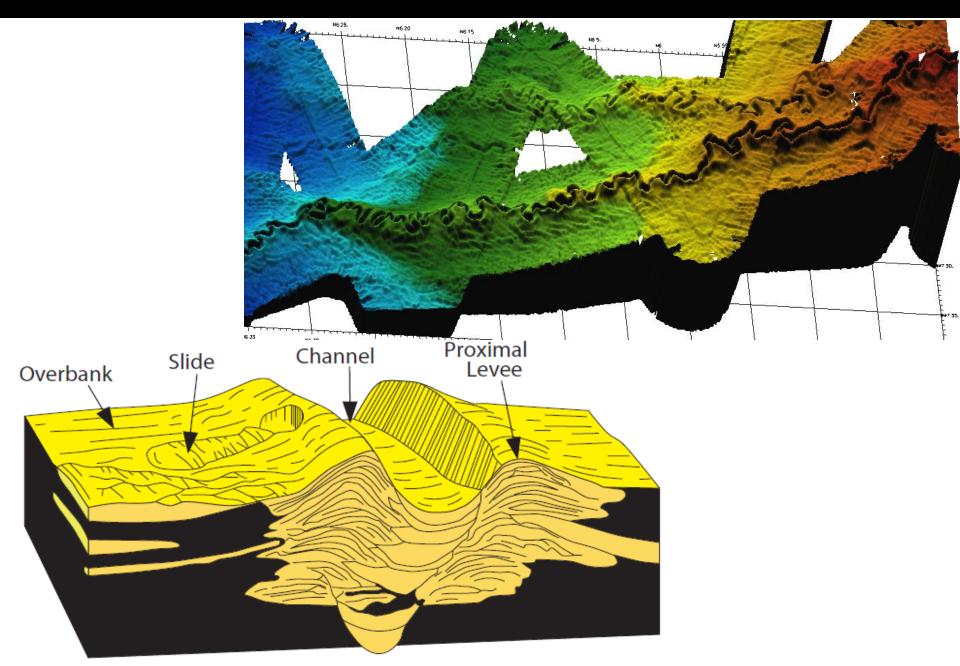
High gradient,
power law decay,
entrainment
via K-H instabilities

Birman et al., 2009



Babonneau et al., 2010

Characterising flow



Characterising flow

	Congo	Amazon	Bengal
Gradient of distal channel reaches	0.13°	0.11°	0.05°
Grain-size of lobe sediments $(u_s$ is proxy for min. shear velocity u_*)	Medium sand	Very fine sand	Silt
Approximate height of distal levees (proxy for flow height)	100m	50m	30m
Velocity	0.7 m s ⁻¹ (Vangriesheim et al., 2009)		
Minimum sediment conc. by volume	≥ 0.1%	≥ 0.01%	≥ 0.003%
Density difference Δho	≥ 1600 g/m ³	$\geq 160 \text{ g/m}^3$	≥ 50 g/m ³

$$u_* = \sqrt{g \frac{Dr}{r} h \sin a}$$

Continuity equation: Incompressible flow

$$\nabla \cdot \mathbf{u} = 0$$

Conservation of momentum: Navier-Stokes equations in Boussinesq approximations

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p + \frac{1}{Re} \nabla^2 \mathbf{u} + c \mathbf{e}^g$$

Small particle size: neglect inertia

$$\frac{\partial c}{\partial t} + (\mathbf{u} + u_s \mathbf{e}^g) \cdot \nabla c = \frac{1}{ScRe} \nabla^2 c$$

Reynolds number

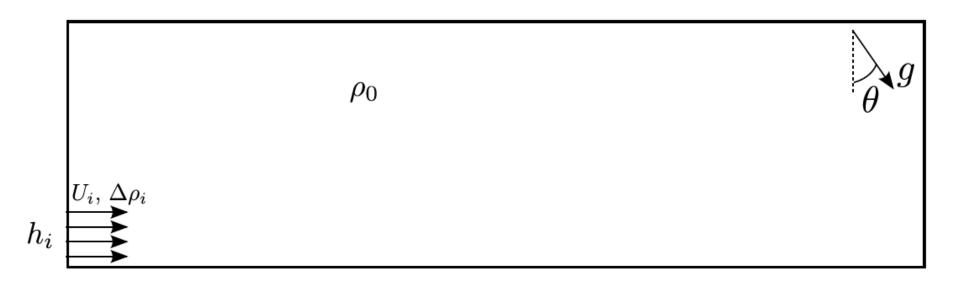
$$Re^{\circ} \frac{\hat{u}_b \hat{H}/2}{\hat{n}}$$
 where $\hat{u}_b = \sqrt{\hat{g} \frac{\hat{r}_1 - \hat{r}_0}{\hat{r}_0} \frac{\hat{H}}{2}}$

Schmidt number (no significant influence when $Sc \ge 1$)

$$Sc \circ \frac{\hat{n}}{\hat{k}}$$

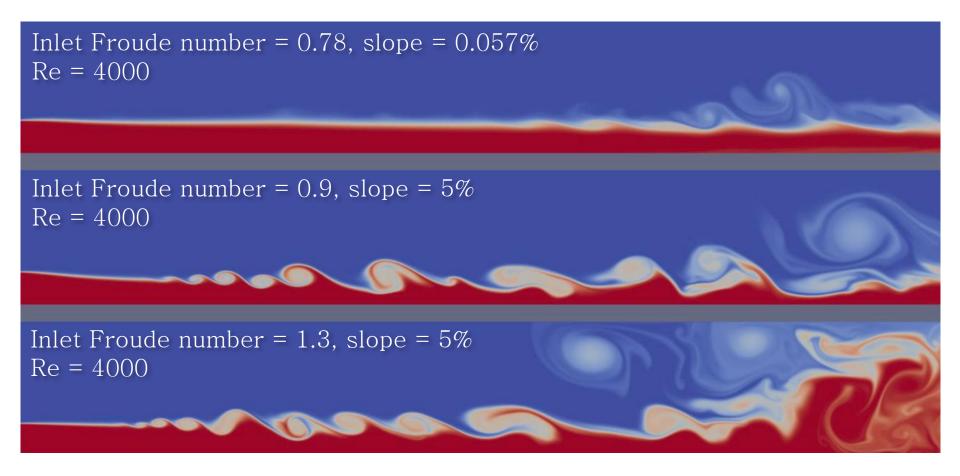
Dimensionless particle settling speed

$$u_s \circ \frac{\hat{U}_s}{\hat{u}_b}$$



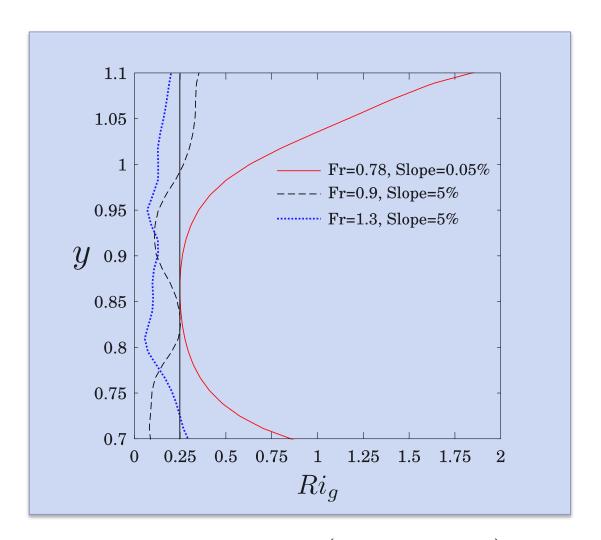
$$Fr_i = \frac{U_i}{u_h}$$
 But is a bulk Froude number appropriate in stratified flows?

```
Inlet Froude
number = 0.78,
slope = 0.057\%
Inlet Froude
number = 0.9,
slope = 5\%
Inlet Froude
number = 1.3,
slope = 5\%
```



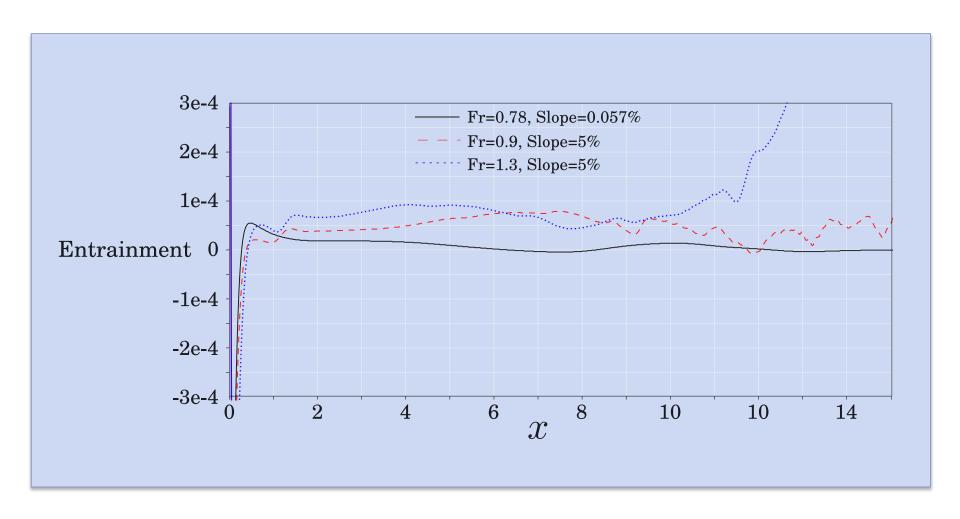
Full Navier-Stokes with Boussinesq approximation. Method in Nasr-Azadani and Meiburg, 201

2D Direct numerical simulation Gradient Richardson number



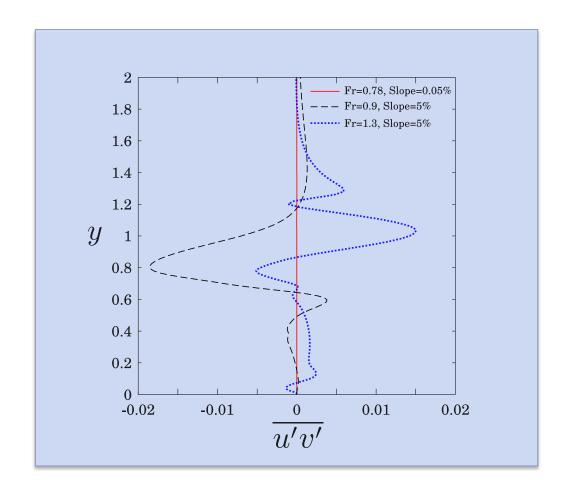
Flows on lower gradients (subcritical) have stable stratification

2D Direct numerical simulation, entrainment



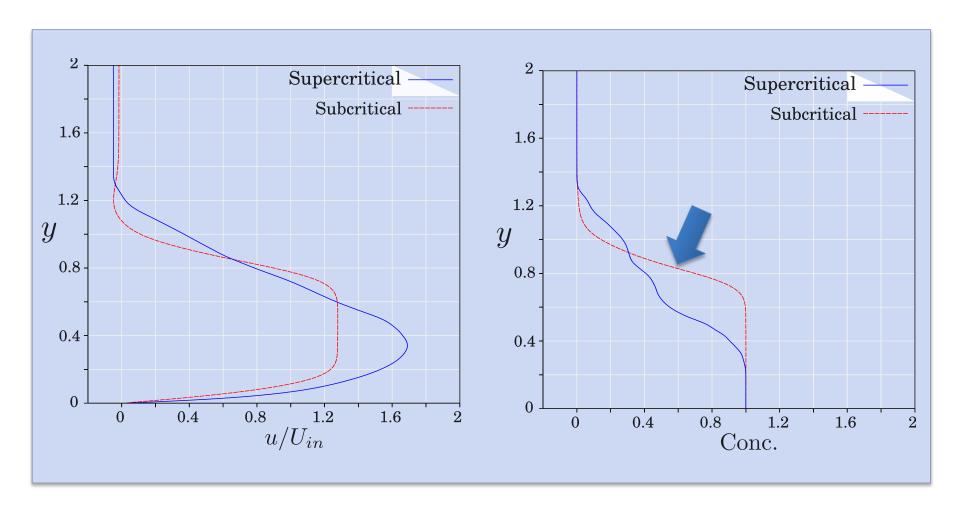
Flows on lower gradients show minimal entrainment

2D Direct numerical simulation, 'turbulent' drag



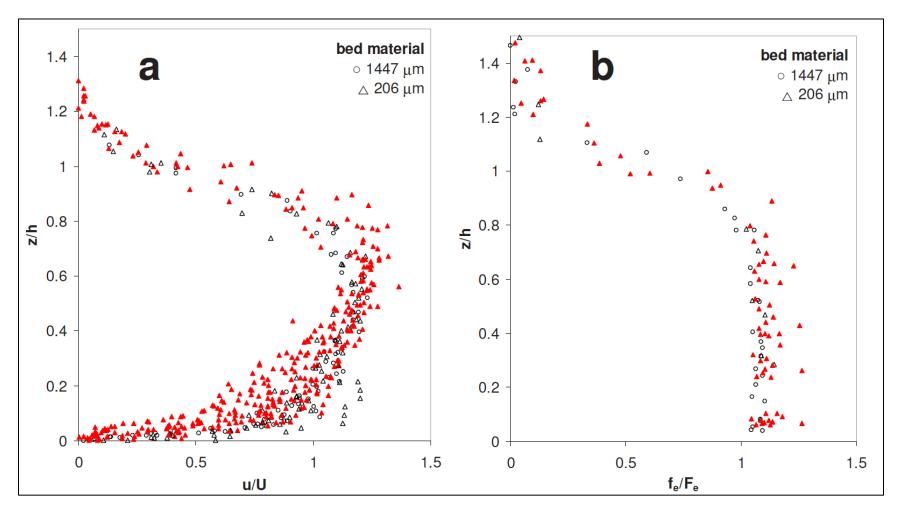
Flows on lower gradients show minimal turbulent drag

2D Direct numerical simulation, velocity and density profiles



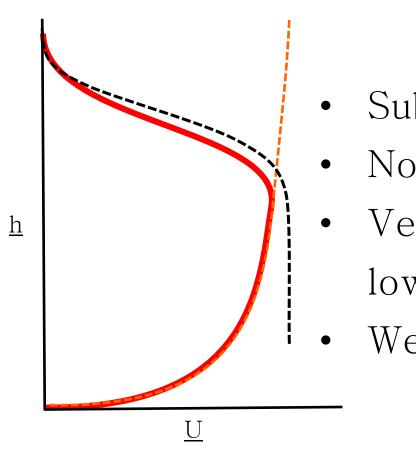
Flows on lower gradients have radically different velocity and density profiles

Experimental flows show similar behaviour



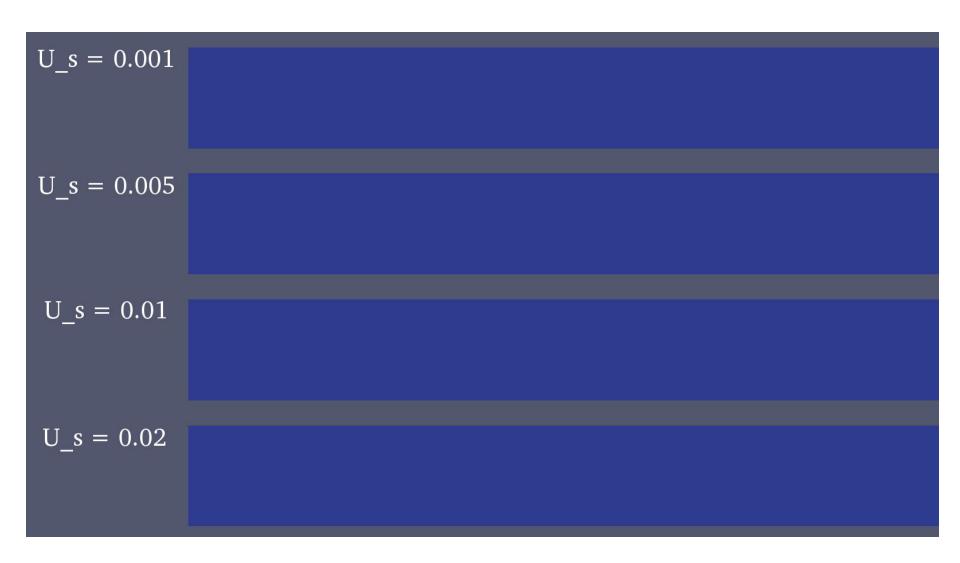
Sub-critical gravity flows. Sequeiros et al. 2010

Absence of Kelvin-Helmholtz instabilities...

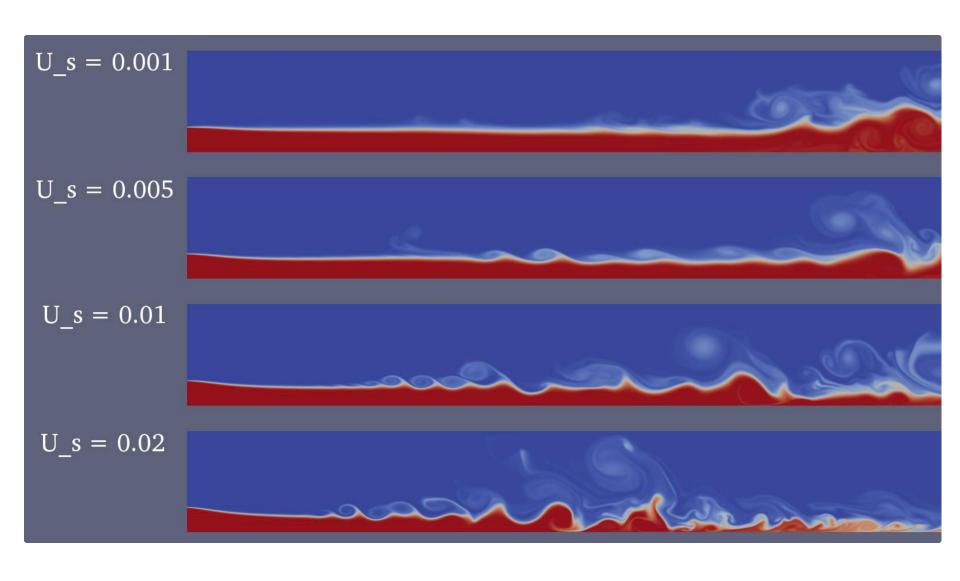


- Substantially reduced drag
- No ambient fluid entrainment
- Velocity profile dominated by lower boundary
 - Weak density stratification

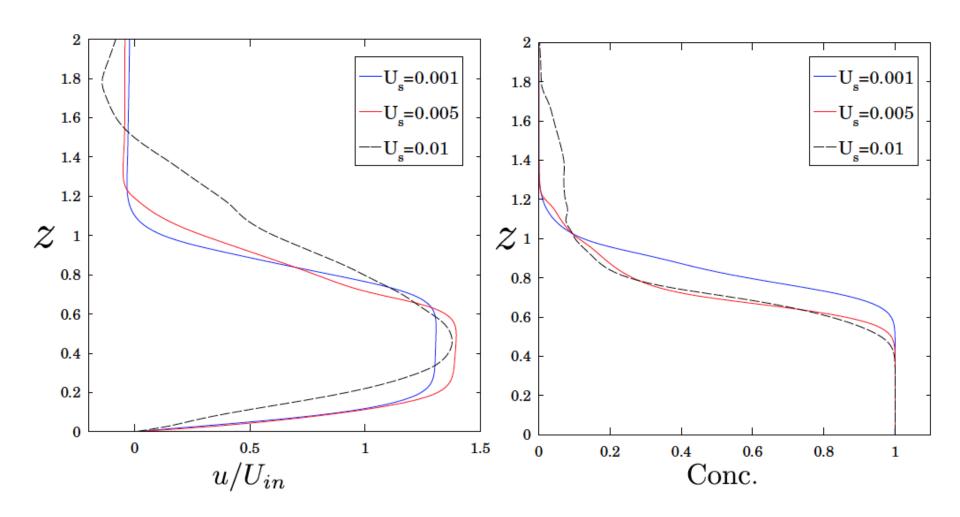
Influence of settling velocity



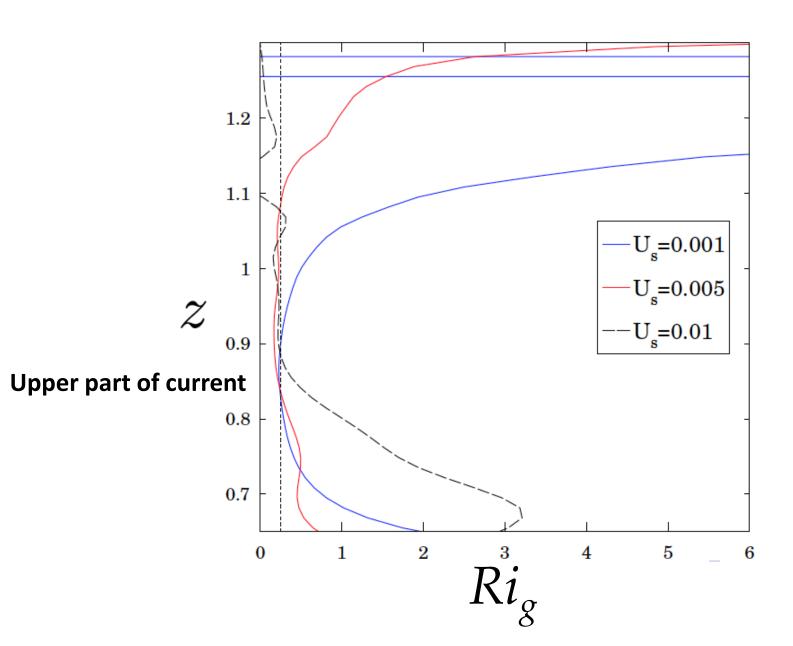
Influence of settling velocity



Influence of settling velocity on density and velocity profiles



Influence of settling velocity on gradient Richardson number



Constraints on flow parameters

	u*	U _b	SSC (u*)	SSC (Ub)
Congo	0.037	0.87	0.03-0.1%	~1%
Amazon	0.012	0.28	0.001-0.01%	~0.50%
Bengal	0.003	0.09	0.0005-0.003%	~0.01%

Is buoyancy velocity the appropriate characteristic velocity with which to scale u_s?

Conclusions

- Turbidity currents on very low gradients probably have stable stratification, do not exhibit Kelvin Helmholtz instabilities, experience little entrainment of ambient seawater, and far lower drag than flows with Kelvin Helmholtz instabilities
- This accounts for their persistence over enormous distances
- Fundamental difference in character between flows on steep slopes and gentler slopes is driven by change in Ri_g



Thank you for listening



