



The effects of wind on the rise of volcanic plumes and the intrusions of volcanic ash

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Wind effects: *plume rise & ash dispersion*



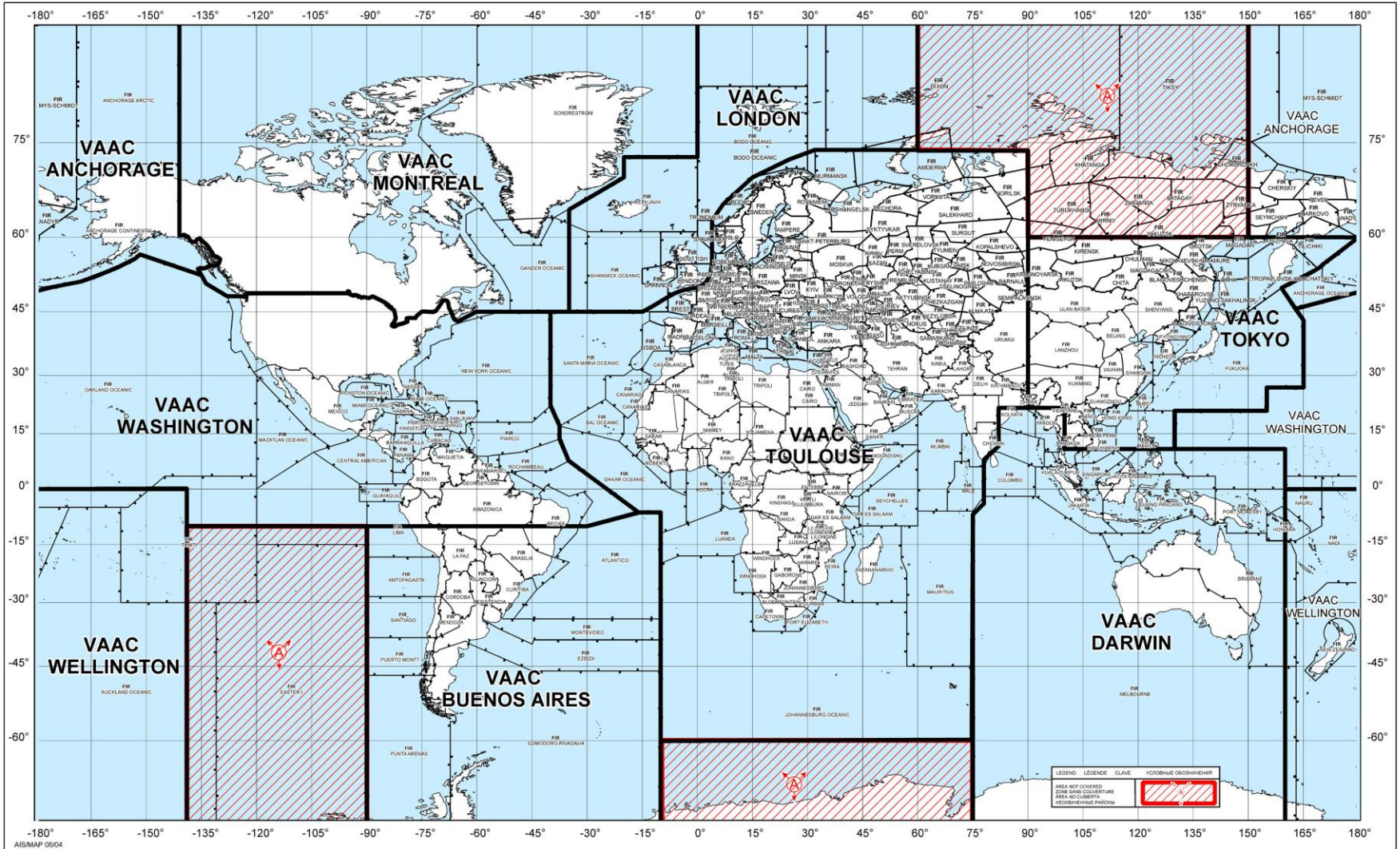
Volcanic Ash and the risk to aviation



- International airspace is advised by 9 Volcanic Ash Advisory Centres (VAACs) that provide guidance to airlines on the safety of flight paths.



CURRENT STATUS OF ICAO VOLCANIC ASH ADVISORY CENTRES (VAAC) - AREAS OF RESPONSIBILITY
 SITUATION ACTUELLE DES CENTRES OACI D'AVIS DE CENDRES VOLCANIQUES (VAAC) - ZONES DE RESPONSABILITÉ
 ESTADO ACTUAL DE LOS CENTROS DE AVISOS DE CENIZAS VOLCÁNICAS (VAAC) DE LA OACI - ÁREAS DE RESPONSABILIDAD
 СУЩЕСТВУЮЩЕЕ РАСПРЕДЕЛЕНИЕ КОНСУЛЬТАТИВНЫХ ЦЕНТРОВ ИКАО ИО ВУЛКАНИЧЕСКОМУ ПЕПЛУ (VAAC) - РАЙОНЫ ОТВЕТСТВЕННОСТИ



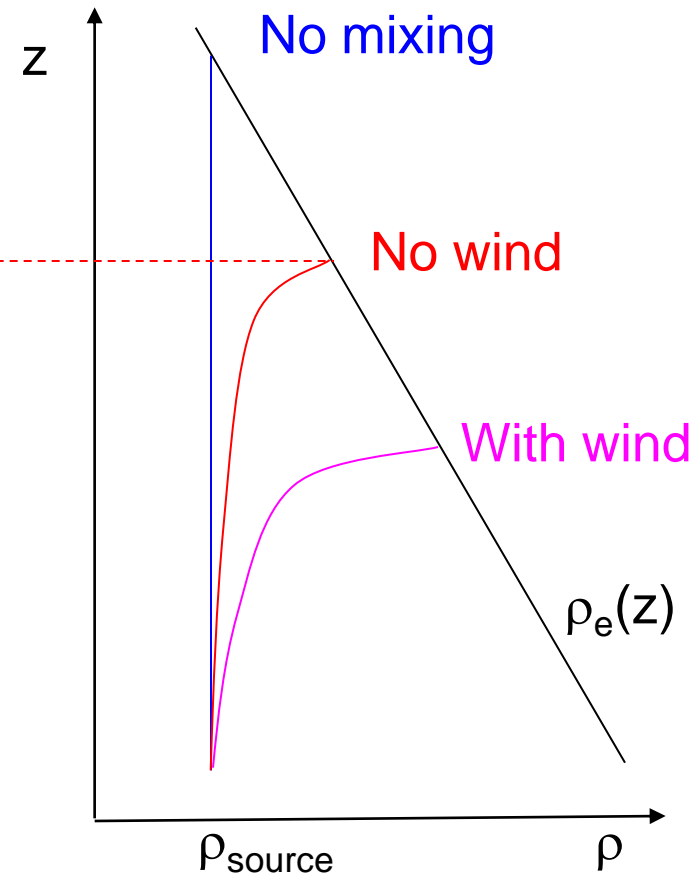
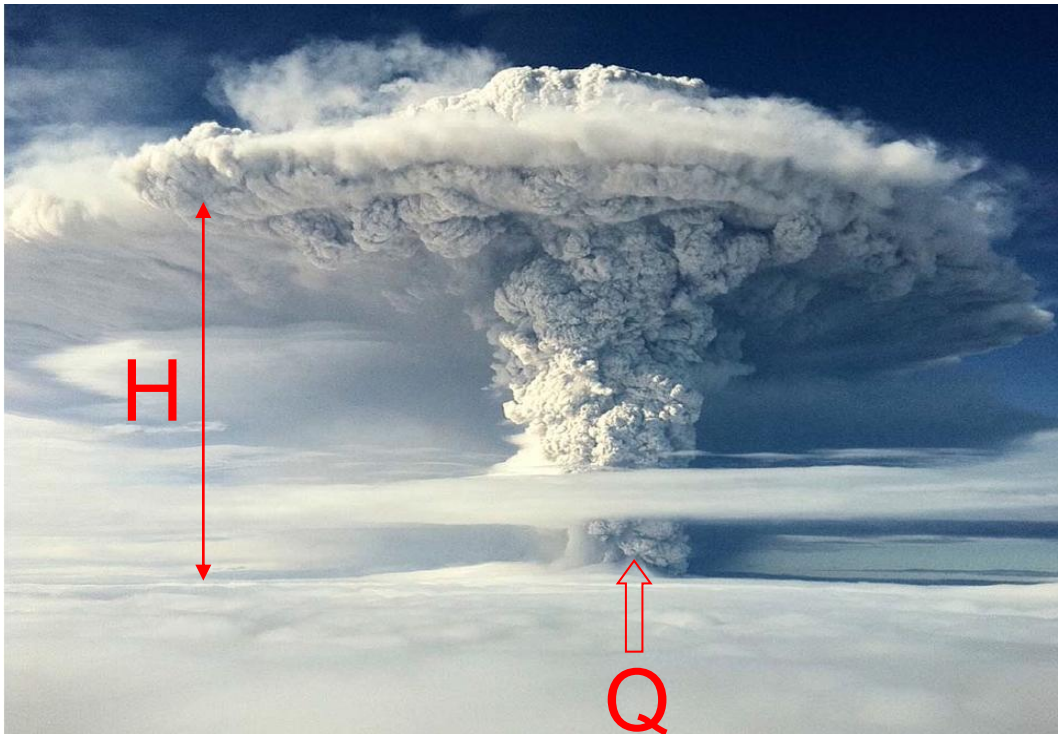
2010 Eruption of Eyjafjallajökull (Iceland)



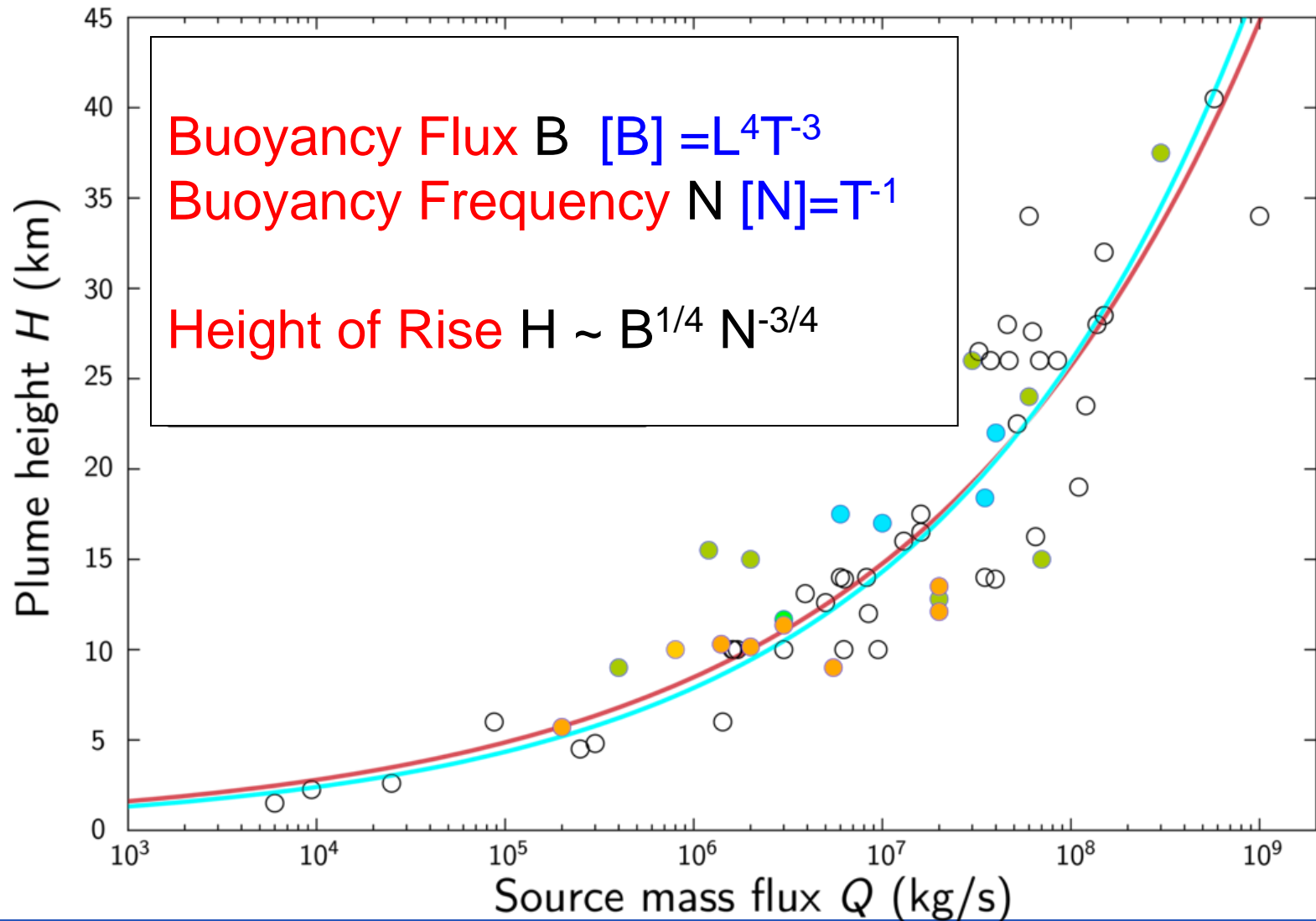
- The Eyja plume was relatively long-lived (April-May 2010)
- Forecasters did not have operational tools to predict its behaviour
- UK government policy changed during the eruption period (2mg/m³ threshold)
- Estimated cost to European economy £5bn.

Plume rise and entrainment

- How can mass flux of volcanic plume be determined?



Empirical relation: Sparks & Mastin curves



Plume model (Morton, Taylor, Turner 1956)

$\rho(z)$ =plume density,

$\rho_e(z)$ =atmosphere density

$N^2 = -g(d\rho_e/dz)/\rho(0)$ =Buoyancy Frequency

Mass

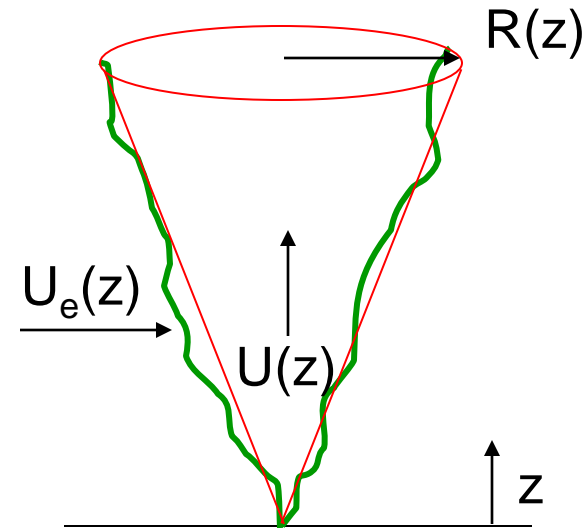
$$\frac{d}{dz} (\pi R^2 U) = 2\pi R U_e$$

Momentum

$$\frac{d}{dz} (\pi R^2 U^2) = \pi R^2 g'$$

Buoyancy

$$\frac{d}{dz} (\pi R^2 g' U) = \pi R^2 N^2 U$$



- **Source** ($z=0$): **Buoyancy flux** $R^2 g' U = B$
Momentum and Mass fluxes

$$R^2 U^2 \rightarrow 0$$

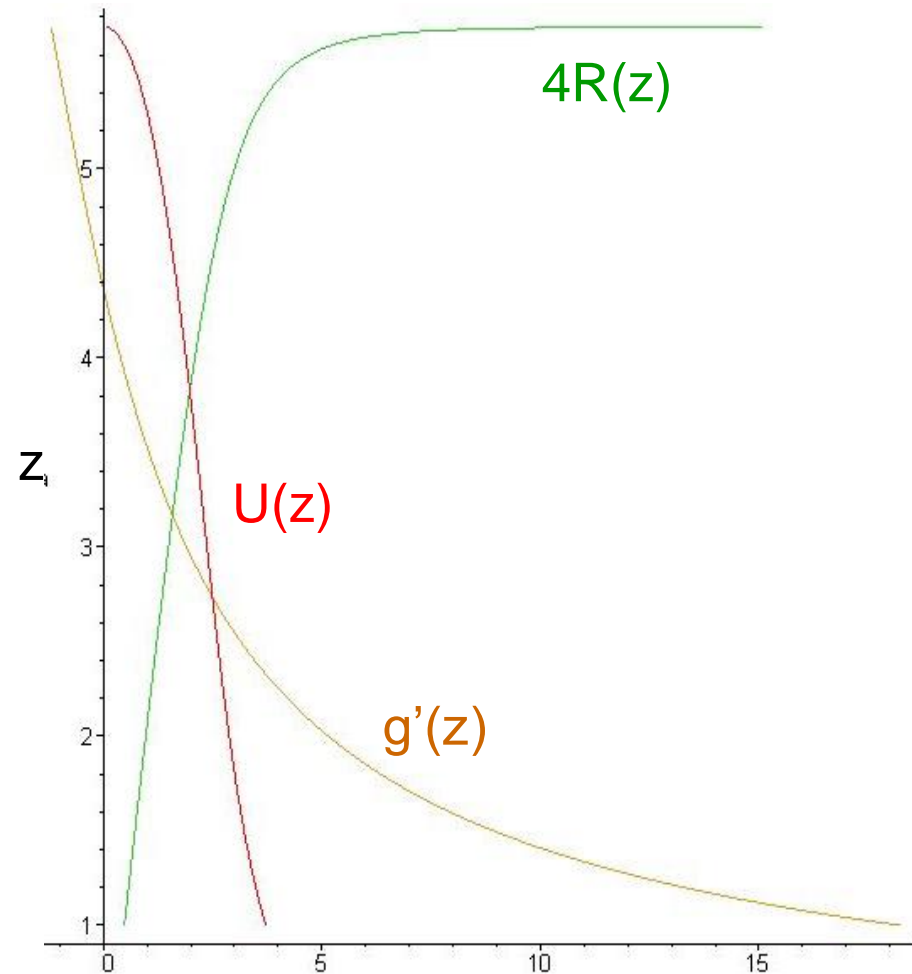
$$R^2 U \rightarrow 0$$

- **Entrainment assumption** $U_e = kU$

Plumes: *typical results*

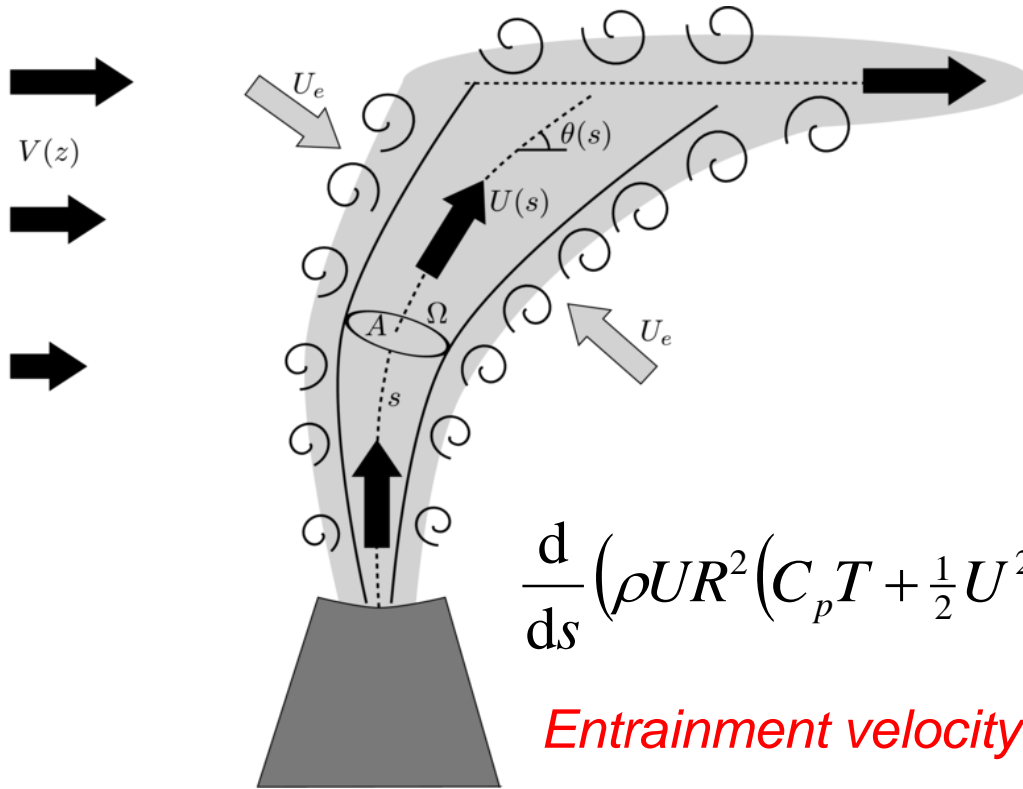


- Plume rises to neutral buoyancy level and overshoots due to inertia



Plume model

- Integral model of wind-blown plumes
 - Model evolution of mass, momentum (vertical & horizontal) & energy
 - Mixing with atmosphere plays a key role



$$\frac{d}{ds} (\rho U R^2) = 2 \rho_a U_e R$$

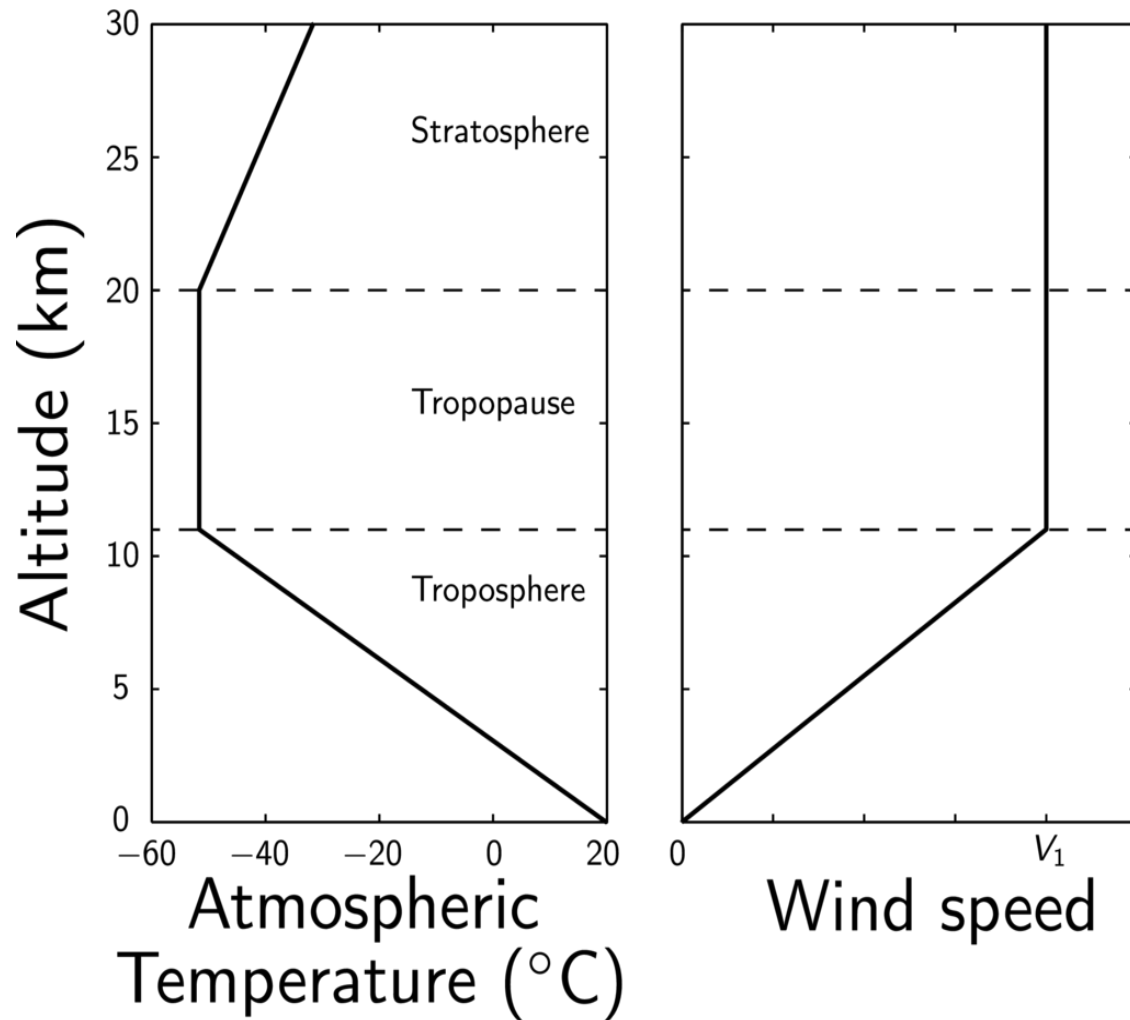
$$\frac{d}{ds} (\rho U^2 R^2 \sin \theta) = (\rho_a - \rho) g R^2$$

$$\frac{d}{ds} (\rho U^2 R^2 \cos \theta) = 2 \rho_a U_e R V$$

$$\frac{d}{ds} \left(\rho U R^2 \left(C_p T + \frac{1}{2} U^2 + g z \right) \right) = 2 \rho_a R U_e \left(C_a T_a + \frac{1}{2} U_e^2 + g z \right)$$

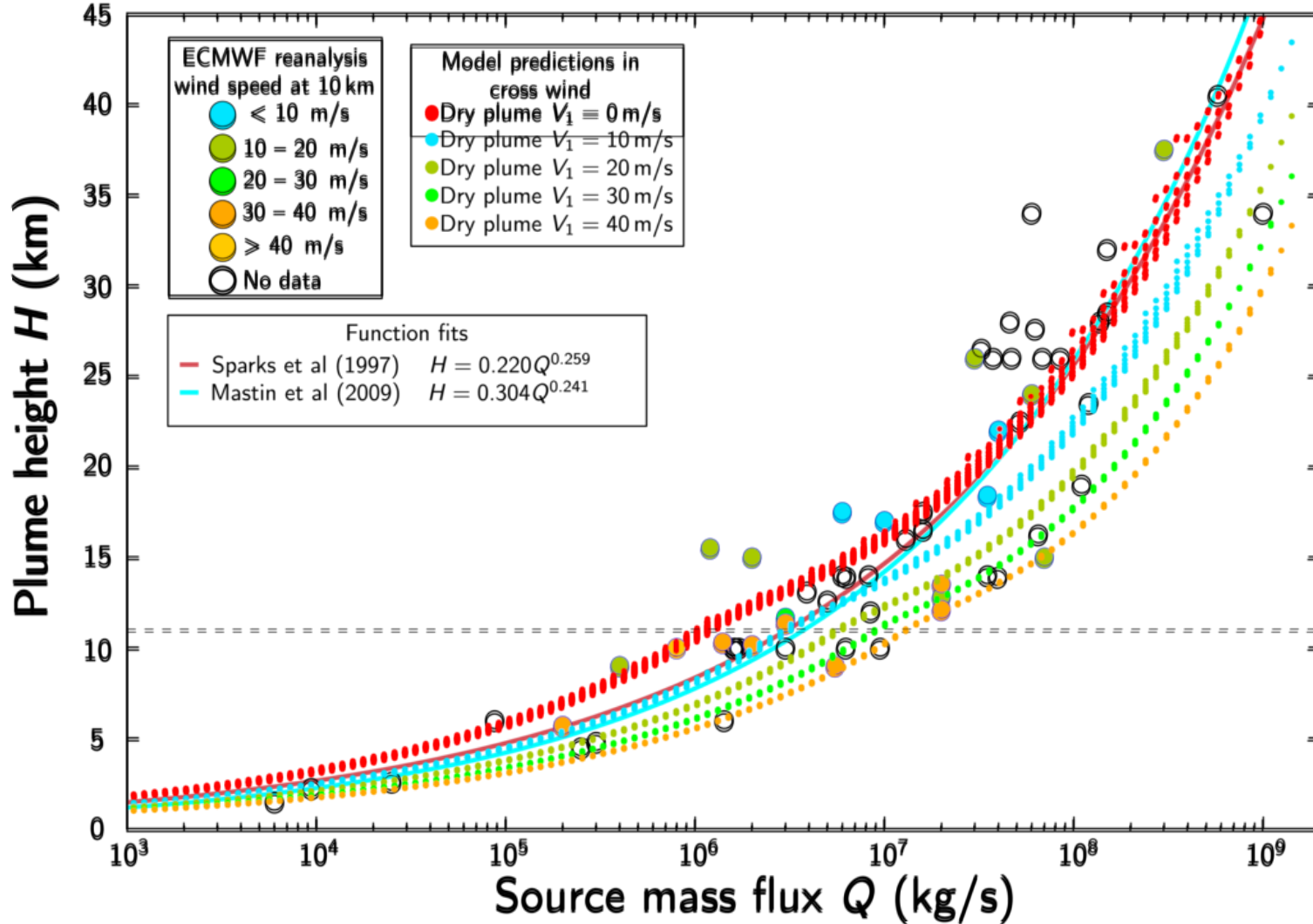
Entrainment velocity $U_e = k_s |U - V \cos \theta| + k_w |V \sin \theta|$

Plume models with Standard Atmosphere

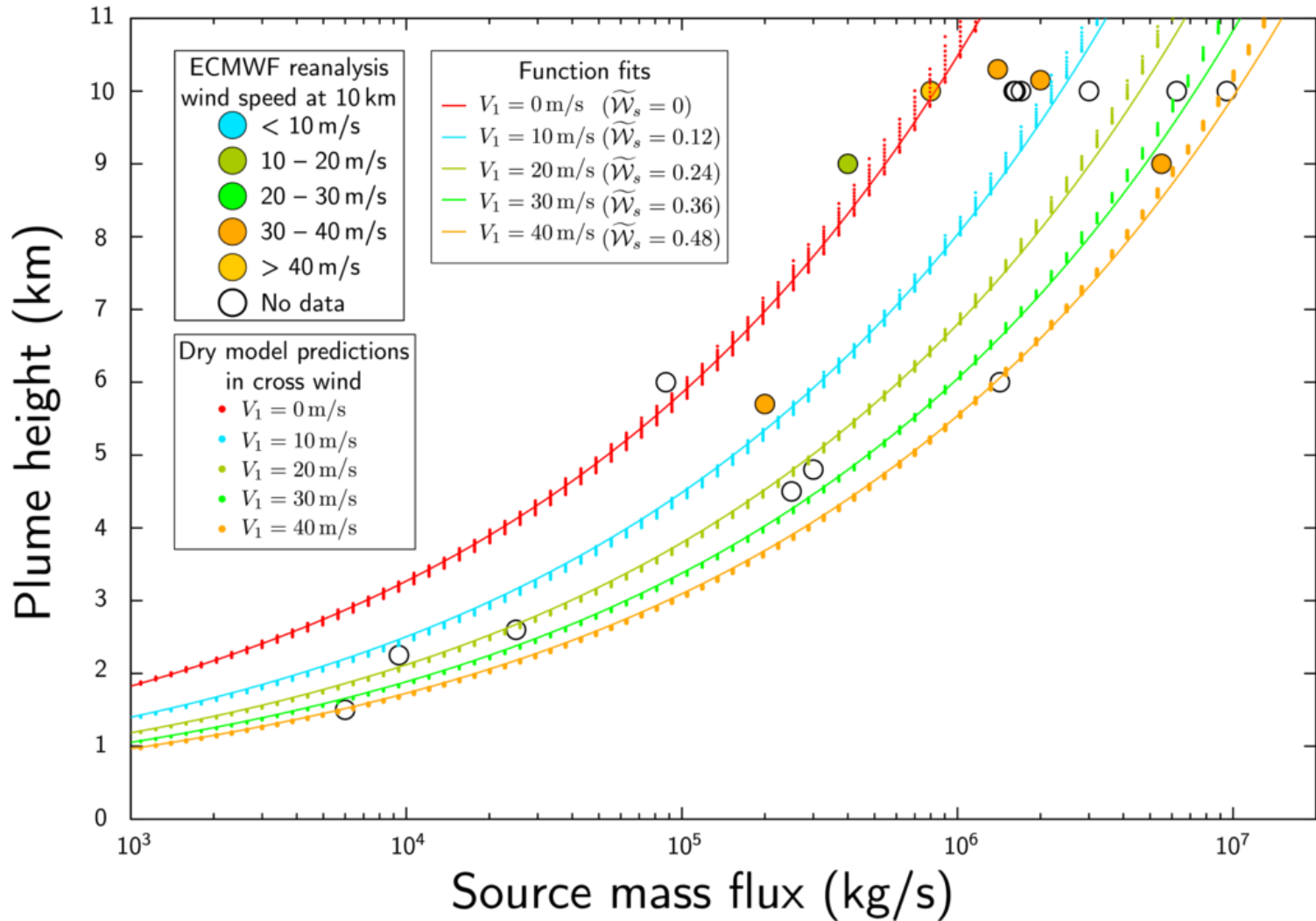


- Plume model integrated in a standard atmosphere for various wind speeds at the tropopause (V_1)

Rise heights in Standard Atmosphere



New empirical relationship with wind

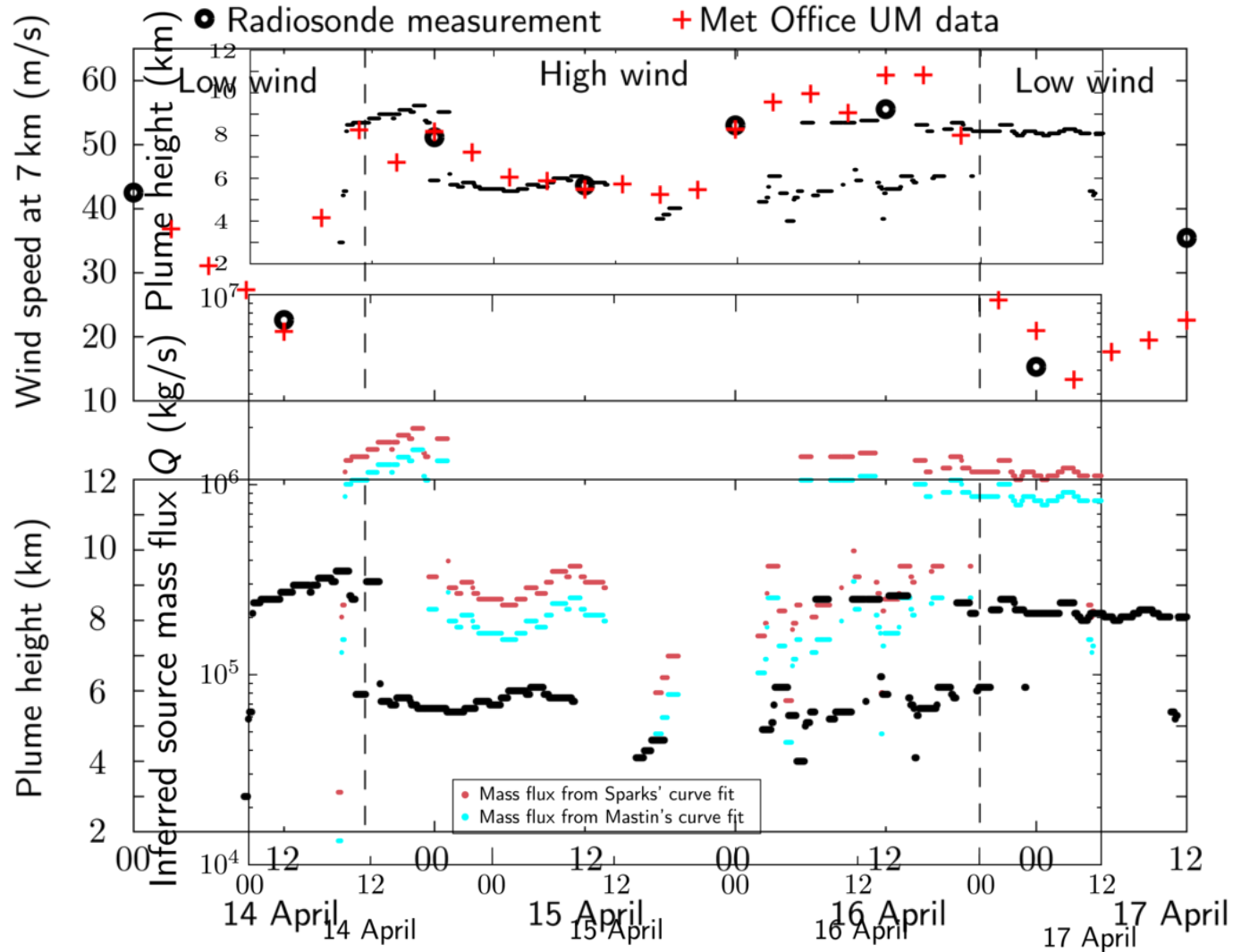


Application to 2010 eruption of Eyjafjallajökull

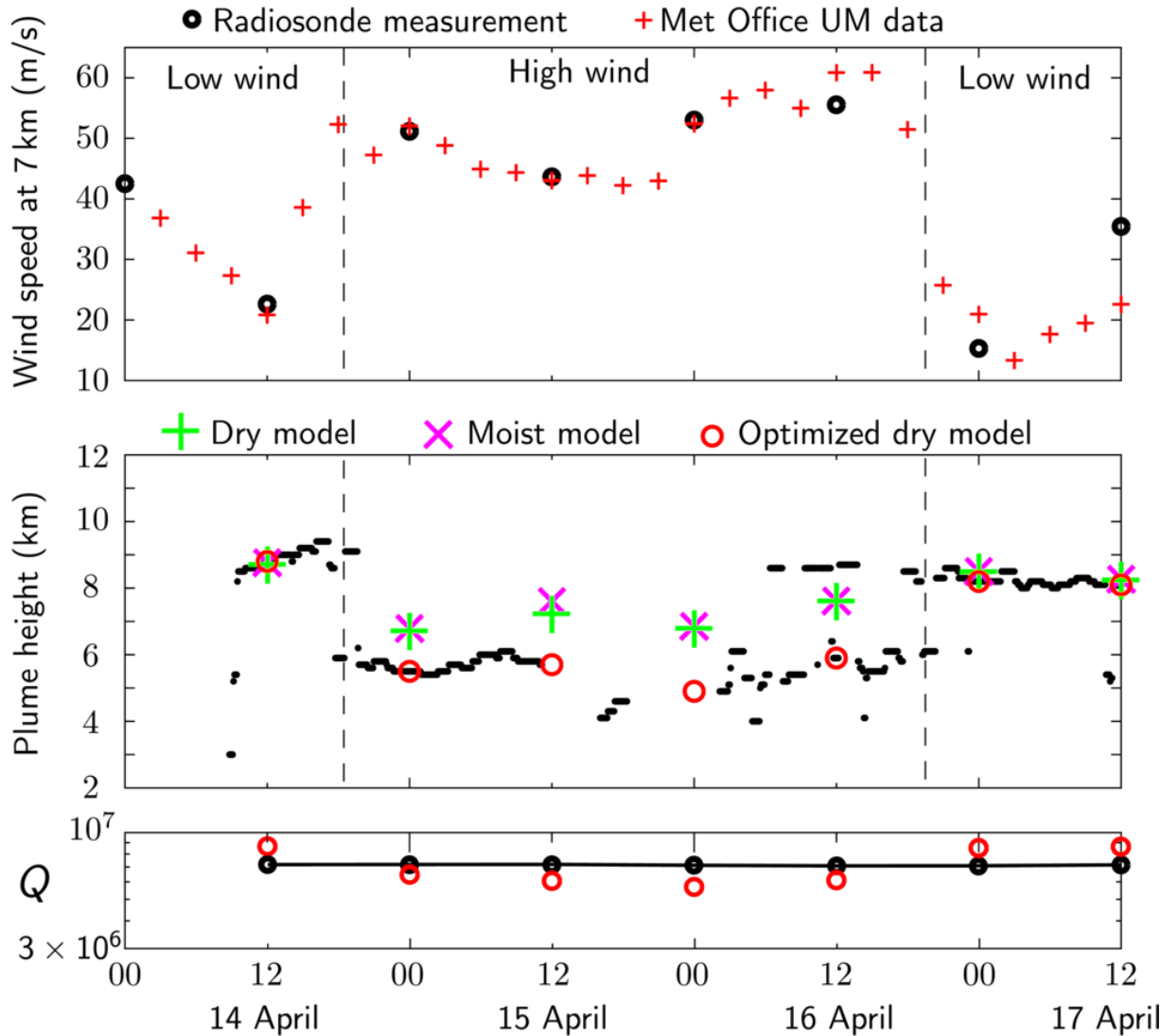


- Observations of
- plume height
 - wind
 - temperature

Plume height 14-17 April



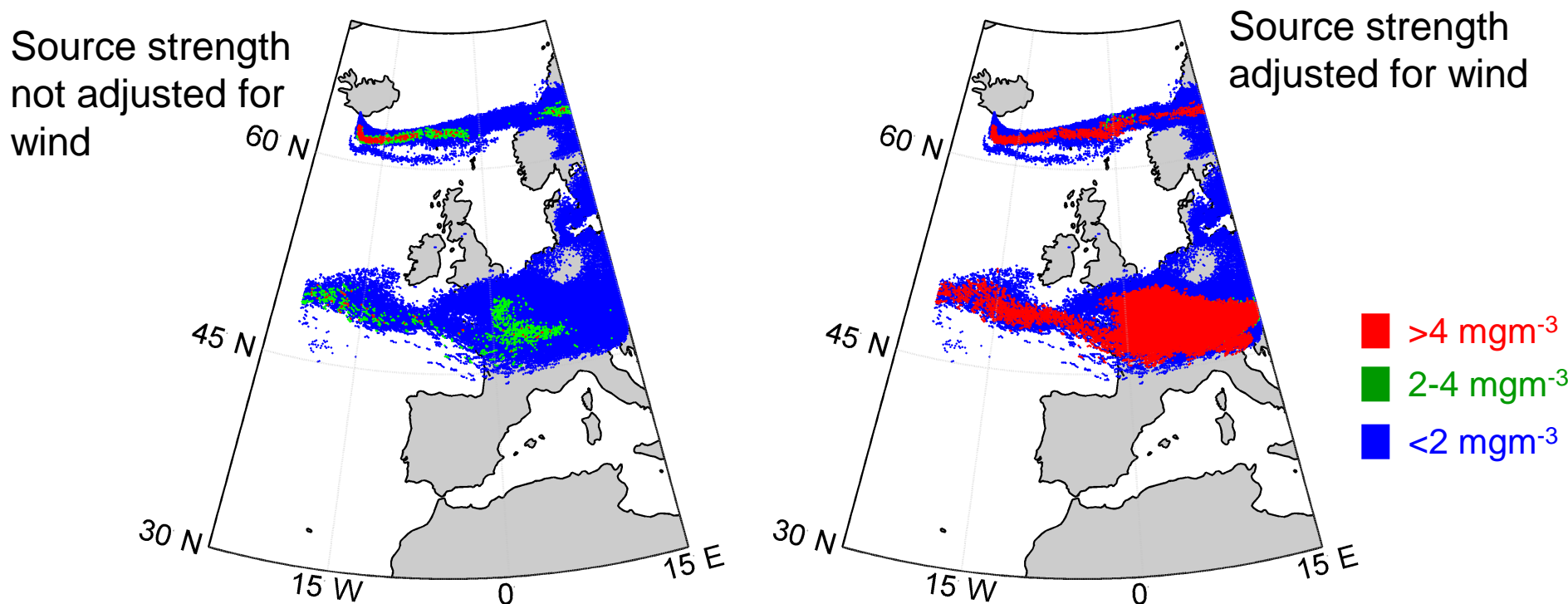
Source flux: wind effect



**Mass flux upto
100 greater than
predicted using
wind-free
formulae**

Ash dispersal in atmosphere

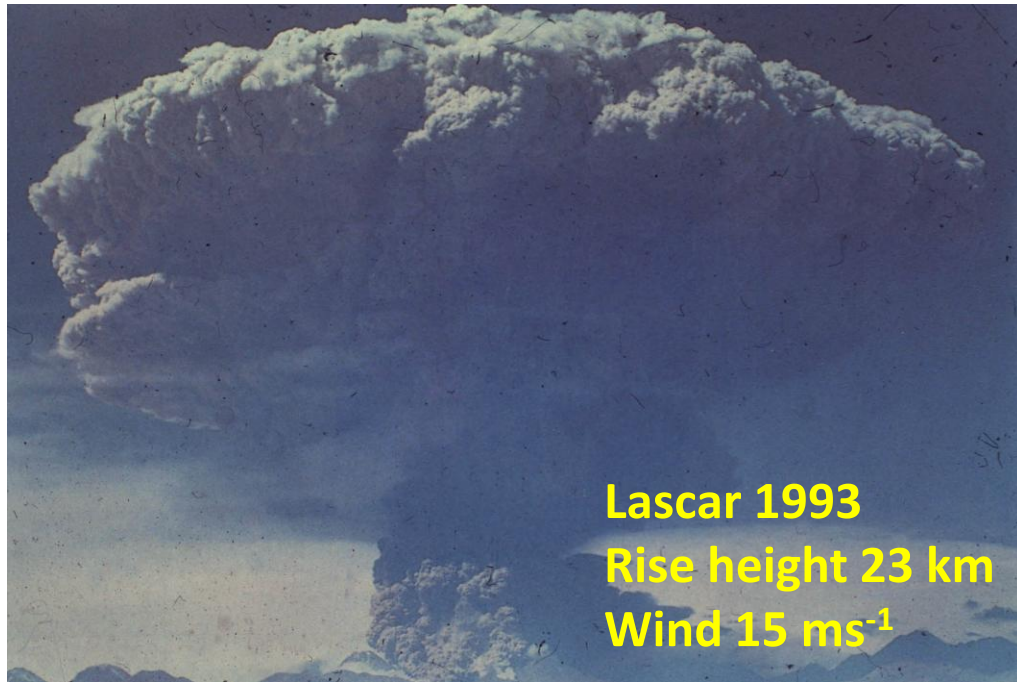
- Use NAME (*Numerical Atmospheric dispersion Modeling Environment*) to calculate dispersal
 - 72 hours after eruption; Concentrations at 3km; No proximal adjustment



Wind effects: *plume rise & ash dispersion*

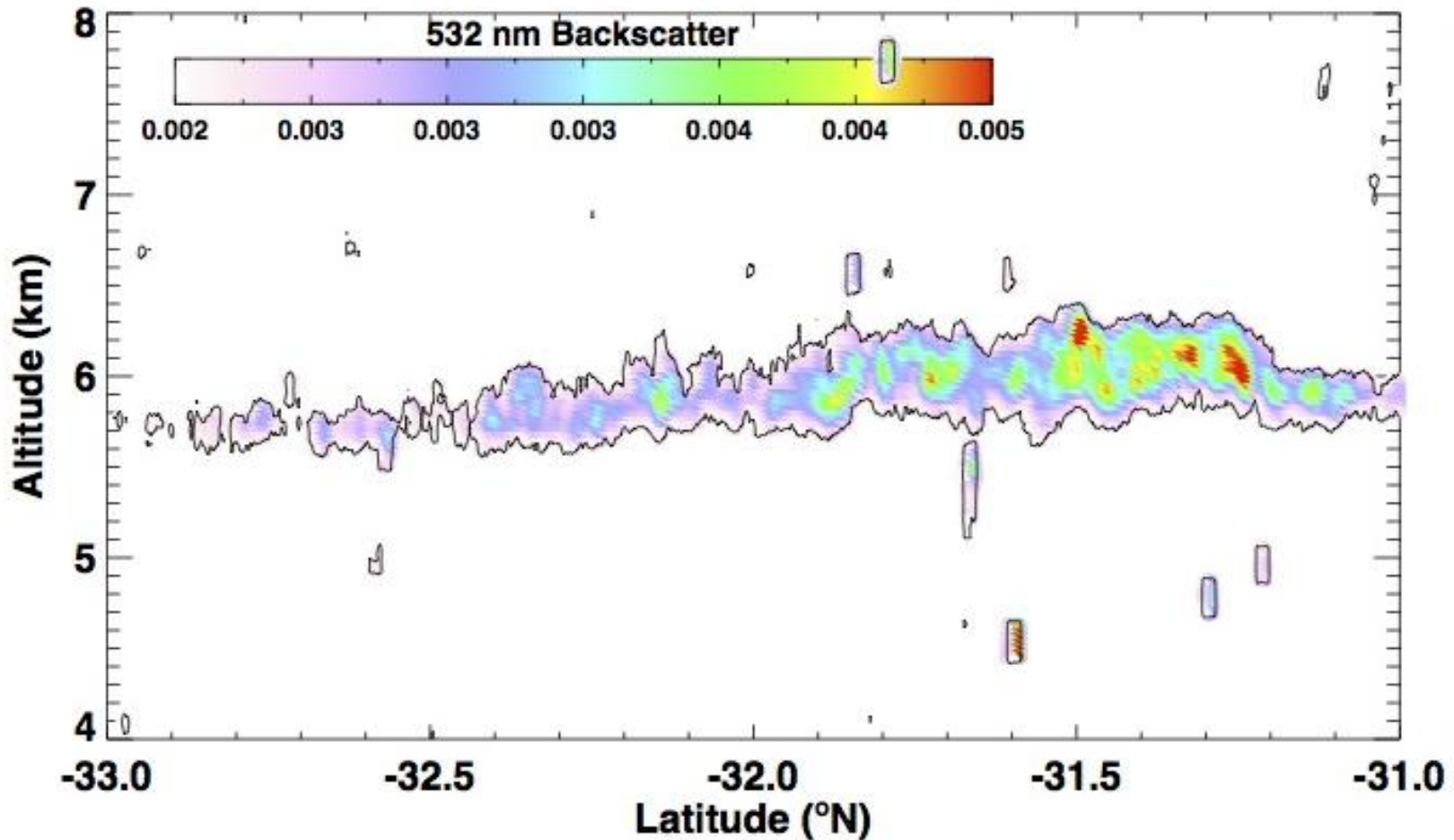


High Intensity eruptions: *weak winds*



- For strong eruptions, wind does not significantly influence near source behaviour.
- *Umbrella cloud* expansion

Satellite images of thin ash layers



Puyehue 24-12-2012 (600 km downwind): *Fred Prata*

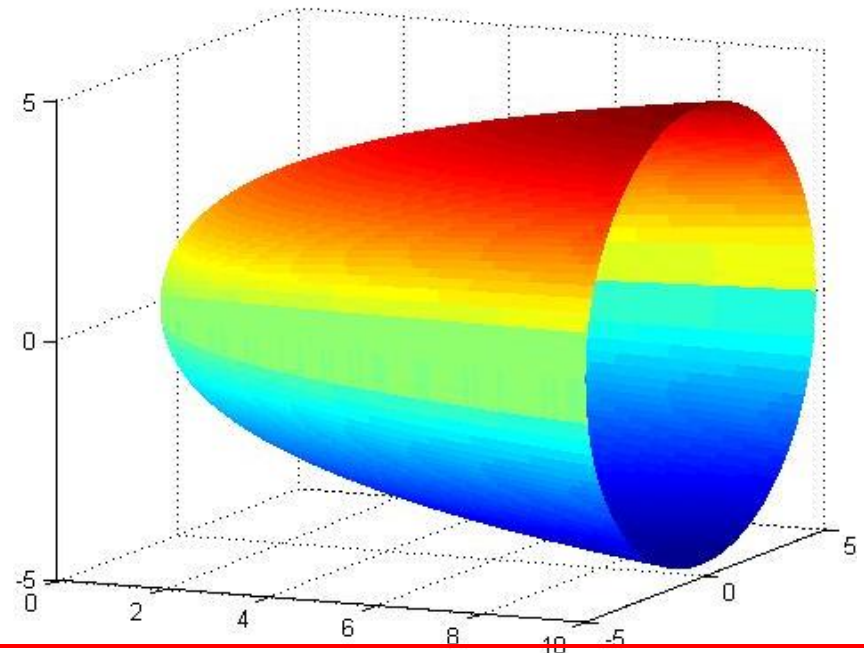
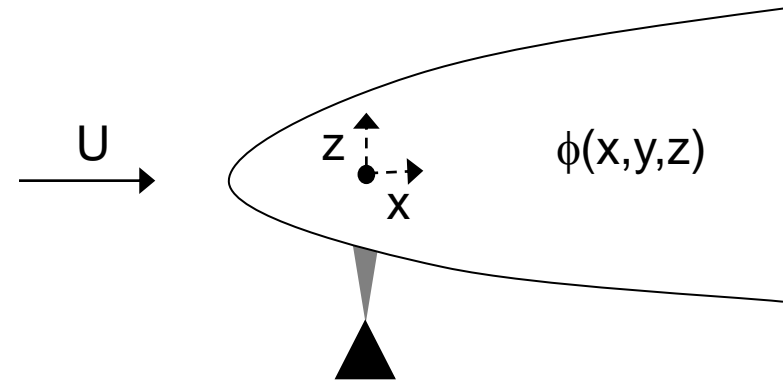


A diffusion model

- The concentration of volcanic ash is produced by a sustained source (Q); advected by the wind (U); diffused due to action of turbulence (diffusivity: K); and settles under gravity (v_s)

$$U \frac{\partial \phi}{\partial x} - v_s \frac{\partial \phi}{\partial z} = K \nabla^2 \phi + Q \delta(\mathbf{x})$$

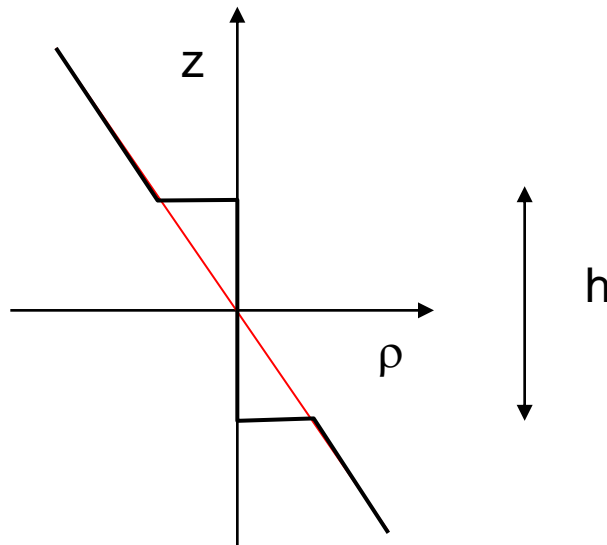
Wind Centreline Settling Diffusion Source
 concentration $\sim 1/x$ cloud width $\sim (Kx/U)^{1/2}$



- But this diffusive model neglects buoyancy-driven motion**

Intrusion dynamics: *buoyancy processes*

Density profile



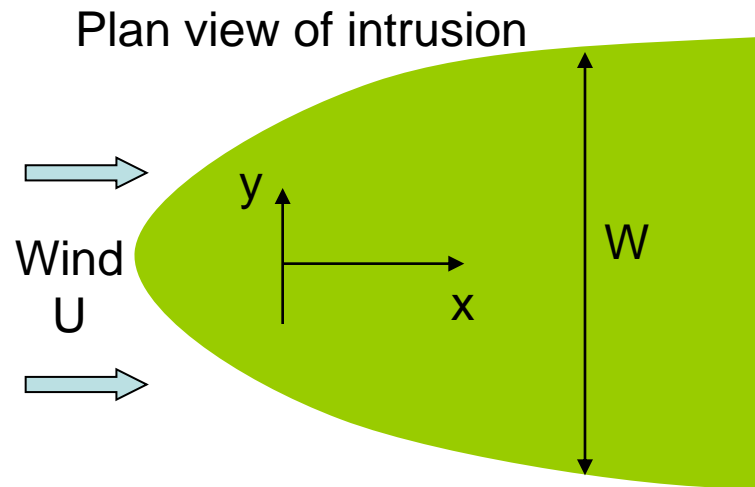
- Plume delivers fluid at neutral buoyancy height, with uniform density
 - Perturbs atmospheric stratification
- Particles do not add significantly to bulk density of intrusion.
- Thickness of intrusion, h , determines pressure excess above hydrostatic balance.
- Gradient of thickness sets up a horizontal pressure gradient

$$\nabla_H P = -\frac{1}{4} N^2 h \nabla_H h$$

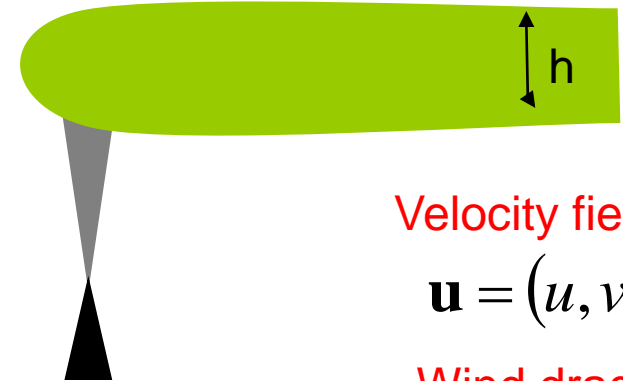
$$N^2 = -\frac{g}{\rho_0} \frac{\partial \rho_a}{\partial z}$$

Buoyancy frequency

Shallow layer model of intrusion



Side view of intrusion



Mass

$$\frac{\partial h}{\partial t} + \frac{\partial}{\partial x}(uh) + \frac{\partial}{\partial y}(vh) = 0$$

$$\boldsymbol{\tau} = \rho C_D (\mathbf{u} - U\hat{\mathbf{x}})|\mathbf{u} - U\hat{\mathbf{x}}|$$

Momentum

$$\frac{\partial}{\partial t}(uh) + \frac{\partial}{\partial x}(u^2h) + \frac{\partial}{\partial y}(uvh) + \frac{1}{4}N^2h^2 \frac{\partial h}{\partial x} = -\tau_x$$

$$\frac{\partial}{\partial t}(vh) + \frac{\partial}{\partial x}(uvh) + \frac{\partial}{\partial y}(v^2h) + \frac{1}{4}N^2h^2 \frac{\partial h}{\partial y} = -\tau_y$$

Radial motion: *unsteady, drag-free*

- Close to the source, the intrusion spreads radially

$$\frac{\partial h}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (r u_r h) = 0$$

$$\frac{\partial}{\partial t} (u_r h) + \frac{1}{r} \frac{\partial}{\partial r} (r u_r^2 h) + \frac{1}{4} N^2 h^2 \frac{\partial h}{\partial r} = 0$$

- Source flux $r h u_r = Q$ at $r=r_0$
- Front condition $u_r = Fr Nh$ at $r=r_f(t)$
- Expectation that $r_f(t) \sim (Q N t^2)^{1/3}$

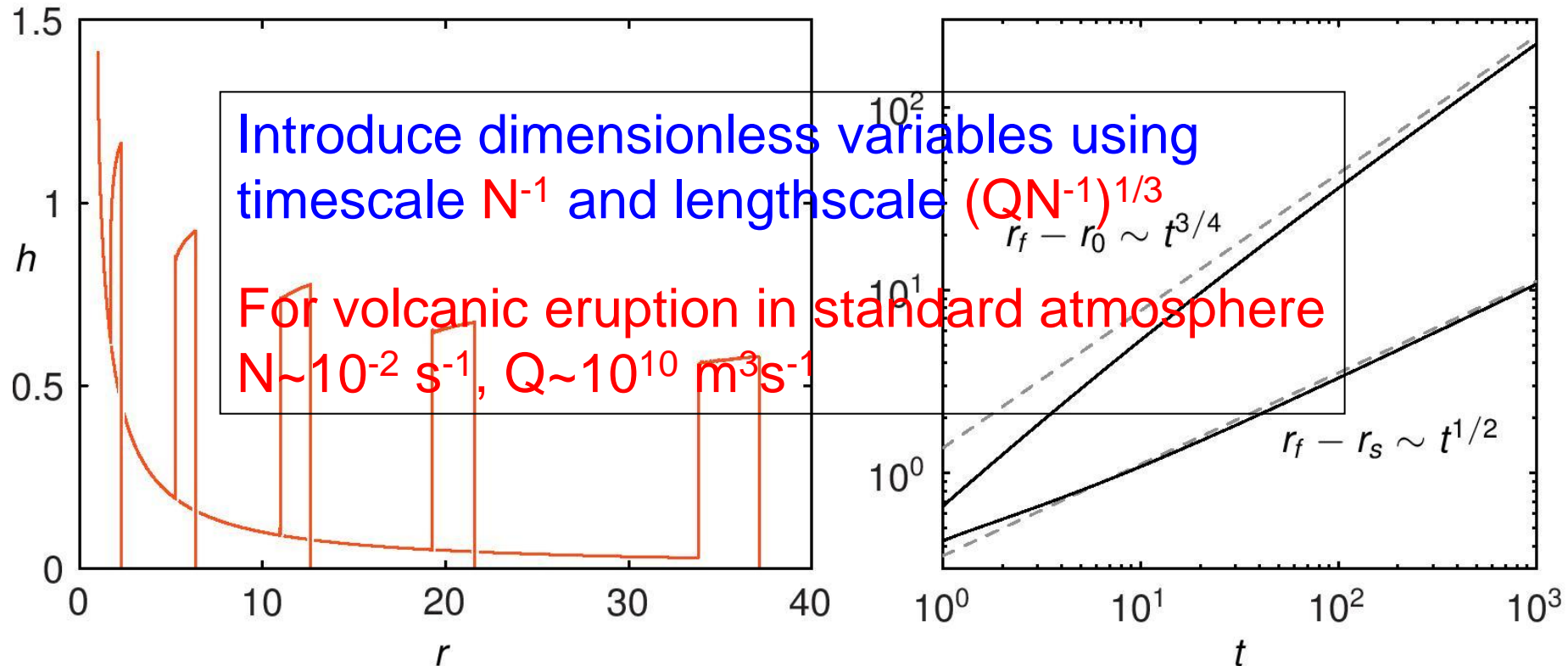
mass: $r h u_r \sim Q$

dynamics: $u_r \sim N h$

kinematics: $u_r \sim r/t$

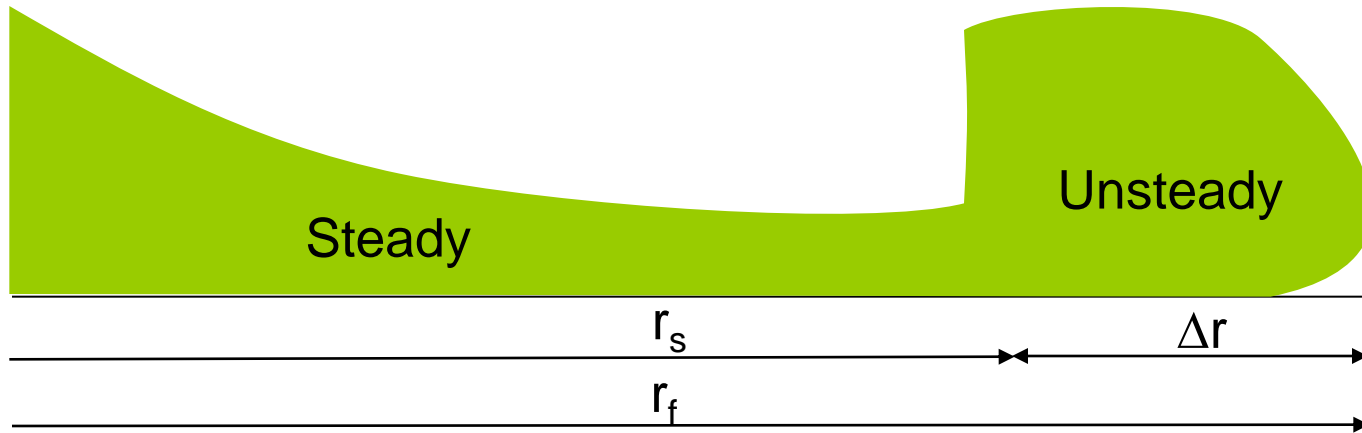
$$r^3 \sim Q N t^2$$

Numerical solution of shallow layer model



- The front: $r_f \sim t^{3/4}$
- Height & velocity fields are not time-dependent throughout
 - Time dependence in frontal region; steady-state in tail.

Structure of unsteady solution



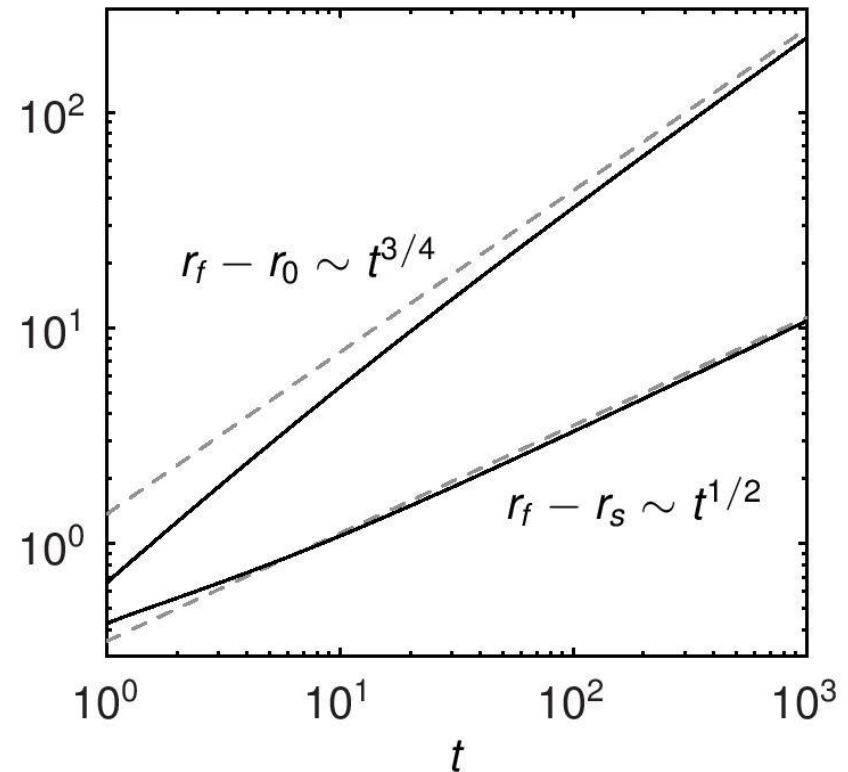
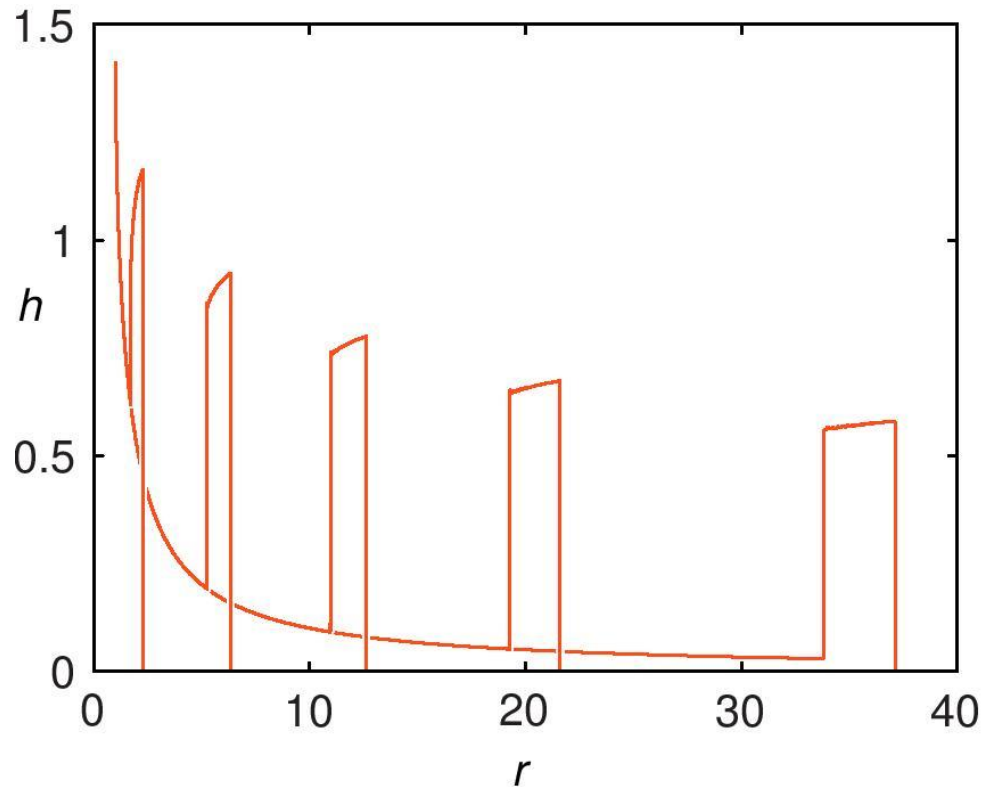
- Within tail, motion is steady: $ru_r h = 1$ $u_r^2 + h^2/4 = \text{const}$ $h \sim 1/r$ $u_r \sim 1$

- Connected to unsteady front via a shock:

$$\begin{aligned} [(u-c)h]_{-}^{+} &= 0 & \xrightarrow{r \gg 1} & c = u_f & h_f^3 &\sim \frac{1}{r_f} & r_f &\sim t^{3/4} \\ [(u-c)^2 h + \frac{1}{12} h^3]_{-}^{+} &= 0 & \xrightarrow{\text{red arrow}} & u^2 h|_{-} = \frac{1}{12} h_f^3 & u_f &\sim h_f \end{aligned}$$

- Mass conservation $\Delta r r_f h_f \sim t$ $\Delta r \sim t^{1/2}$

Numerical solution: *radial, drag-free*



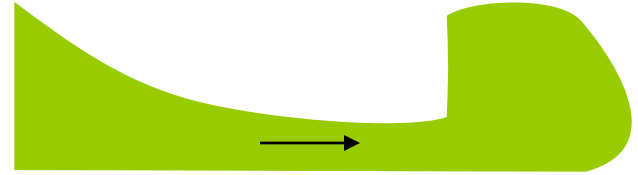
Aside: constant flux, radial gravity currents through uniform environments

- For currents of excess density ($\Delta\rho$), moving through a uniform environment

Mass
$$\frac{\partial h}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (ru_r h) = 0$$

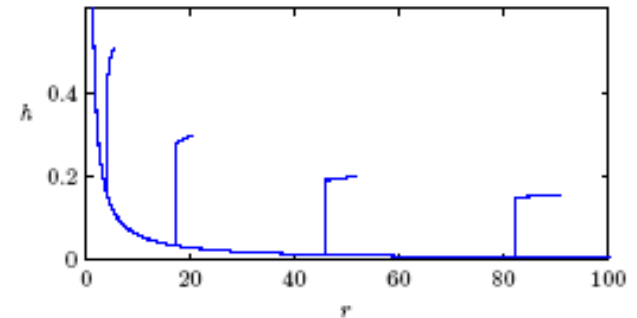
Momentum
$$\frac{\partial}{\partial t} (u_r h) + \frac{1}{r} \frac{\partial}{\partial r} (ru_r^2 h) + g'h \frac{\partial h}{\partial r} = 0$$

Reduced gravity
 $g' = \Delta\rho g / \rho_0$

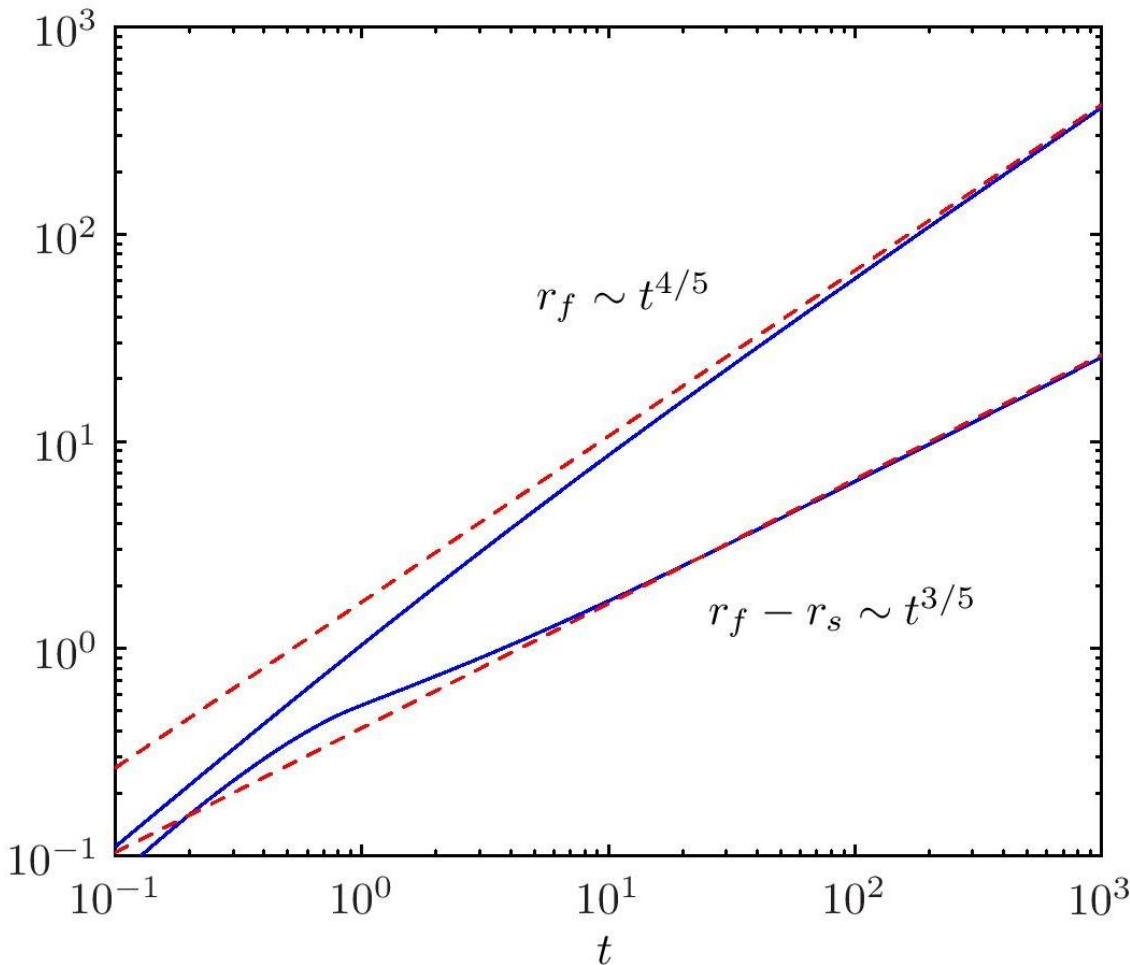


- A similarity scaling would indicate that $r_f \sim (g'Qt^3)^{1/4}$

- But this is not realised from numerical solutions of the governing equations.



Numerical solution



- Within tail, motion is steady: $ru_r h = 1$
 $u_r^2 + h = \text{const}$
- Connected to front via a shock:

$$[(u-c)h]_{-}^{+} = 0$$

$$\left[(u-c)^2 h + \frac{1}{2} h^2 \right]_{-}^{+} = 0$$

$r \gg 1$
 \longrightarrow

$$c = u_f$$

$$u^2 h \Big|_{-} = \frac{1}{2} h_f^2$$

$$h_f^2 \sim \frac{1}{r_f}$$

$$u_f \sim \sqrt{h_f}$$

$$r_f \sim t^{4/5}$$

Radial motion: *unsteady, drag-influenced*

- The motion becomes influenced by atmospheric drag, here modelled $C_D \rho u_r |u_r|$

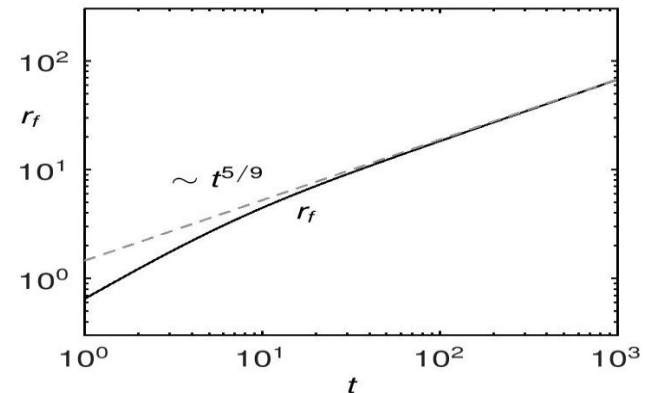
$$\frac{\partial h}{\partial t} + \frac{1}{r} \frac{\partial}{\partial r} (r u_r h) = 0$$

$$\frac{\partial}{\partial t} (u_r h) + \frac{1}{r} \frac{\partial}{\partial r} (u_r^2 h) + \frac{1}{4} N^2 h^2 \frac{\partial h}{\partial r} = -C_D u_r |u_r|$$

- At long times: **pressure gradient** ~ **drag** [*inertia negligible*]

mass: $r h u_r \sim Q$ **dynamics:** $N^2 h^3 / r \sim C_D u_r^2$ **kinematics:** $u_r \sim r/t$

$$r^9 \sim Q^3 N^2 t^5 / C_D$$

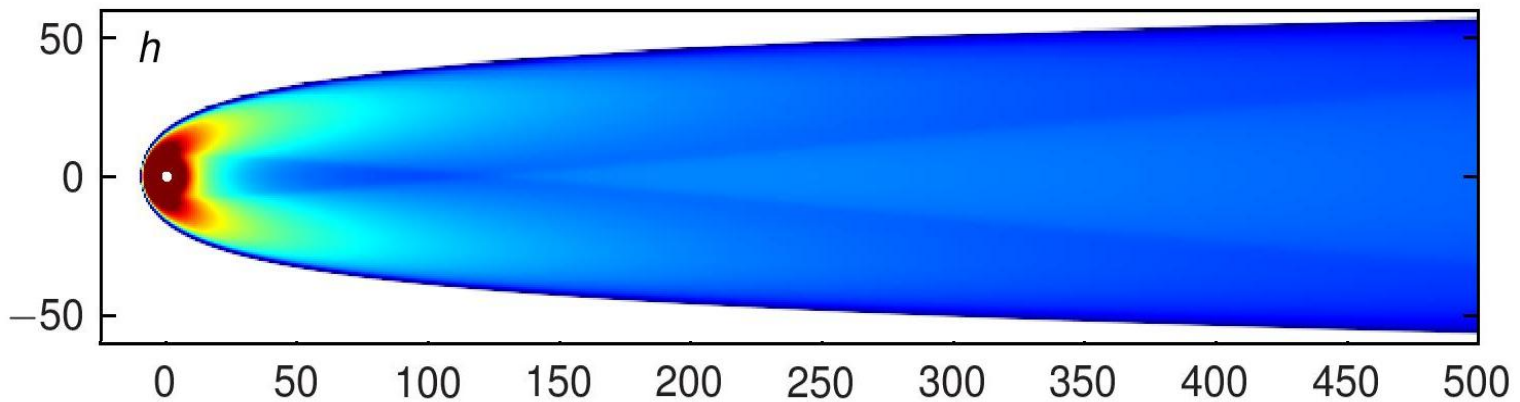


Steady evolution with wind: *Numerical solutions*

$Q=10^{10} \text{ m}^3\text{s}^{-1}$, $N = 0.01 \text{ s}^{-1}$,
Wind speed 30 ms^{-1}

Dimensionless wind speed
 $U=0.3$

$$\frac{\partial}{\partial x}(uh) + \frac{\partial}{\partial y}(vh) = 0$$
$$\frac{\partial}{\partial x}(u^2h) + \frac{\partial}{\partial y}(uvh) + \frac{1}{4}h^2 \frac{\partial h}{\partial x} = -\tau_x$$
$$\frac{\partial}{\partial x}(uvh) + \frac{\partial}{\partial y}(v^2h) + \frac{1}{4}h^2 \frac{\partial h}{\partial y} = -\tau_y$$



Plan views of the height of an intrusion from a sustained source

Far-field form of intrusion

- When width of intrusion $W \ll$ streamwise length L

$$\frac{\partial}{\partial x}(u^2 h) + \frac{\partial}{\partial y}(uvh) + \frac{1}{4} h^2 \frac{\partial h}{\partial x} = -\tau_x \quad \Rightarrow u = U$$

$$\frac{\partial}{\partial x}(uvh) + \frac{\partial}{\partial y}(v^2 h) + \frac{1}{4} h^2 \frac{\partial h}{\partial y} = -\tau_y = -C_D v^2$$

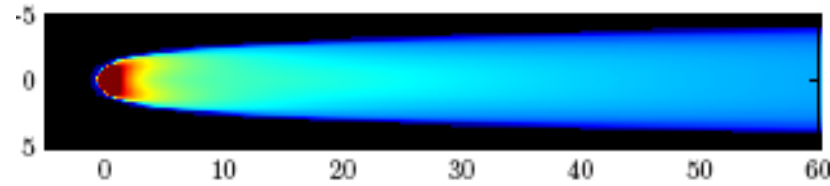
- Fluid conservation $\frac{\partial}{\partial x}(uh) + \frac{\partial}{\partial y}(vh) = 0 \quad \int_0^W uh = \frac{1}{2}$

Solution:

$$v = \frac{y}{3x} \quad h(x, y) = \frac{1}{x^{1/3}} \frac{2^{2/3} C}{3^{2/3}} \left(1 - \frac{y^3}{Cx}\right)^{1/3} \quad W = Cx^{1/3} \quad \begin{array}{l} \text{Constant} \\ C = 0.884 \end{array}$$



Far downwind of source

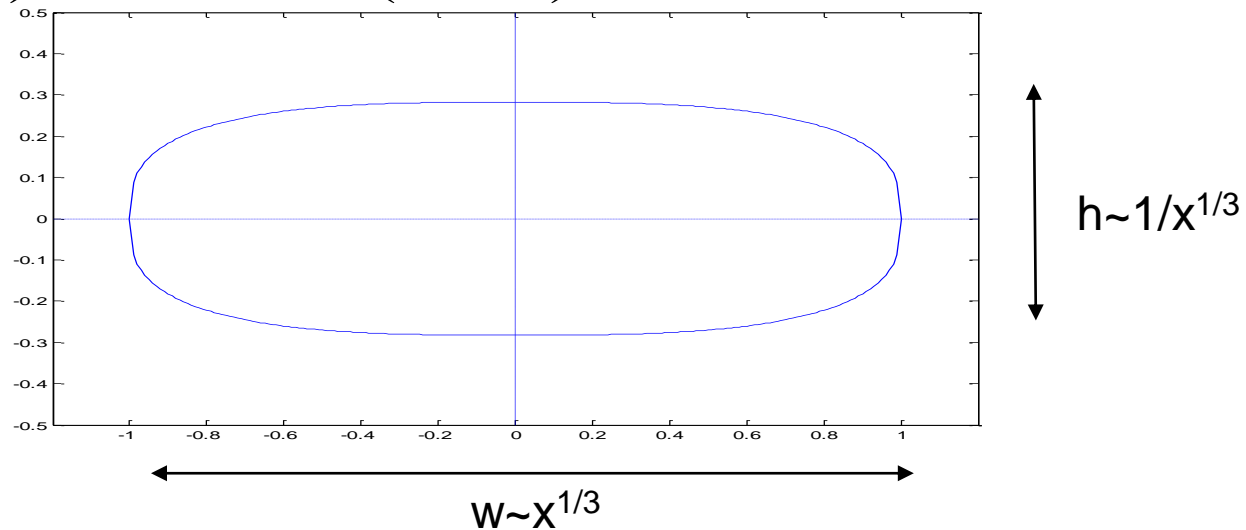


- Far from source the intrusion tends to the downwind velocity ($u \sim U$), but continues to spread laterally
- Height of intrusion: *similarity solution far downwind*

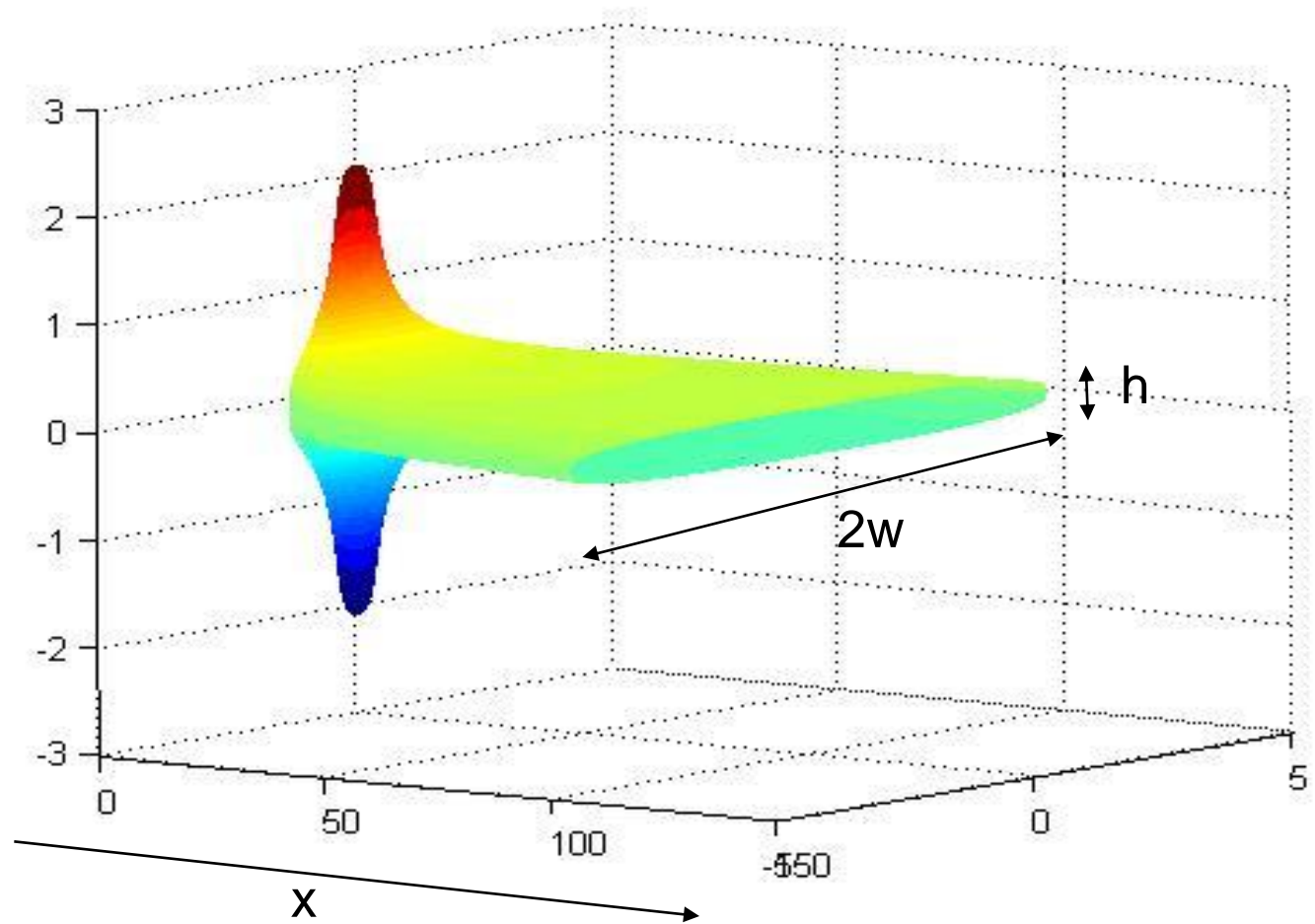
Height $h(x, y) = \left(\frac{Q^3 C_D}{N^2 U} \right)^{1/6} \frac{1}{x^{1/3}} \frac{2^{2/3} C}{3^{2/3}} \left(1 - \frac{y^3}{w^3} \right)^{1/3}$ Width $w = C \left(\frac{Q^3 N^2}{U^5 C_D} \right)^{1/3} x^{1/3}$

Lateral Velocity $v = \frac{Uy}{3x}$

Constant $C = 0.884$

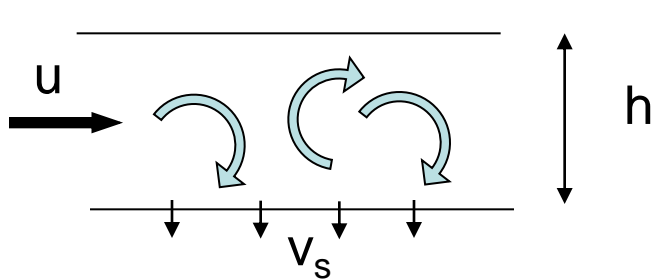


Shape of intrusion



Particle transport

- The concentration of suspended particles, ϕ , within a turbulent layer satisfies: (*Hazen's Law*)



$$\frac{\partial}{\partial t}(h\phi) + \frac{\partial}{\partial x}(hu\phi) + \frac{\partial}{\partial y}(hv\phi) = -v_s\phi$$

↑
↑
Advection with wind
Settling

- Steady, radially symmetric intrusion at neutral buoyancy height (u_r =radial velocity)

Particle transport:

$$\frac{1}{r} \frac{\partial}{\partial r} (ru_r h \phi) = -v_s \phi$$

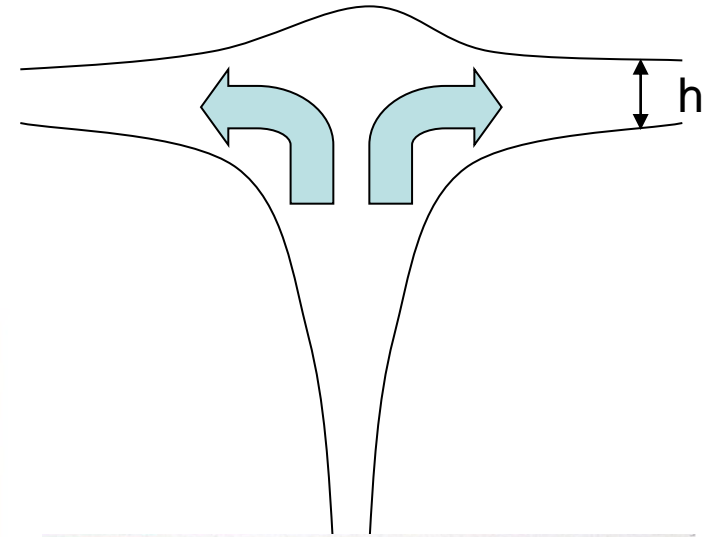
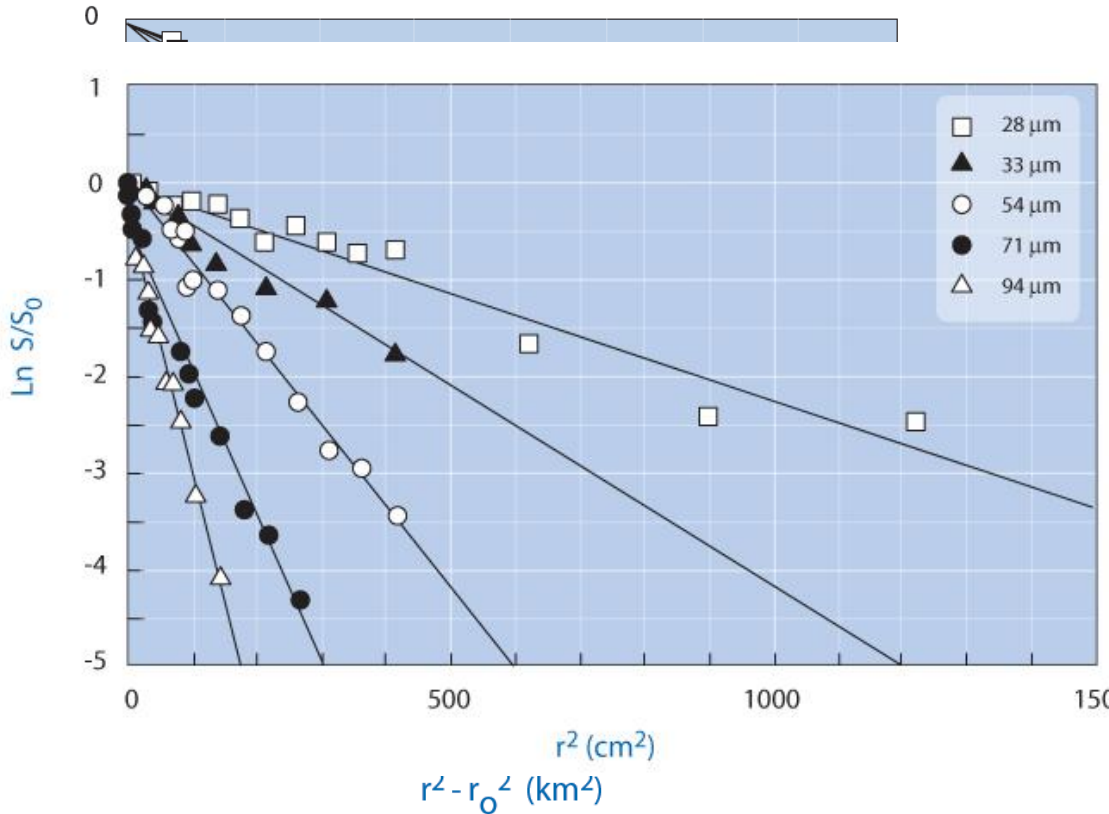
Volume flux: $Q = ru_r h$

$$\phi = \phi_0 \exp\left(-\frac{v_s r^2}{2Q}\right)$$

Distribution of deposit: *observations*

- Measure deposit from umbrella clouds

Field data from Fogo Volcano (Azores)
Laboratory experiments



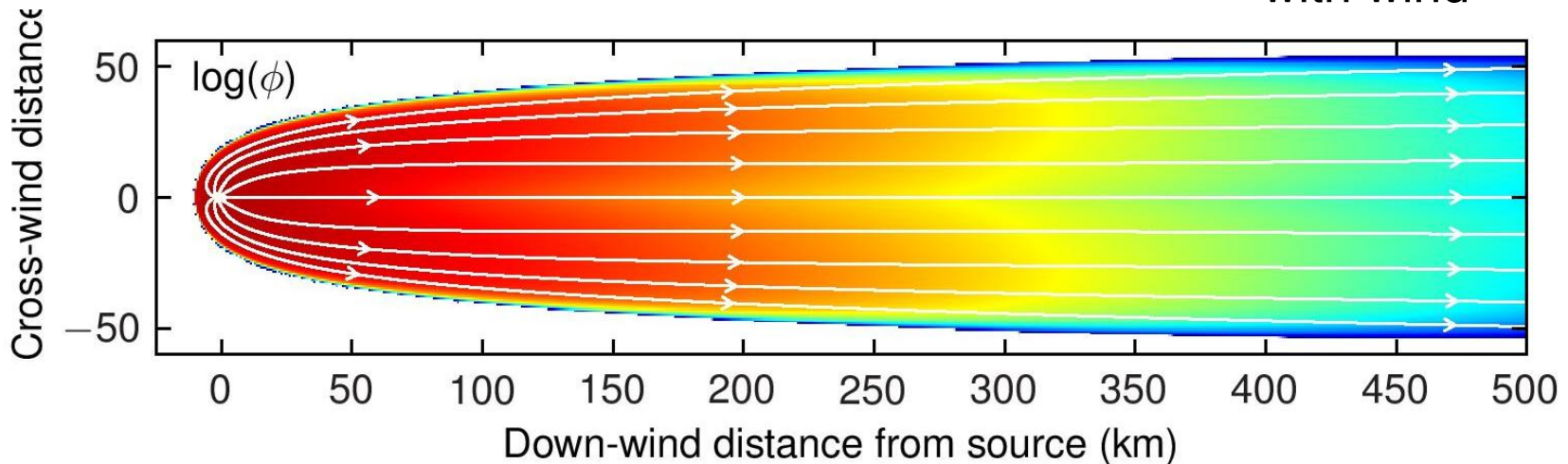
Ash transport in wind

- The concentration of particles satisfies:

$$\frac{\partial}{\partial x} (u\phi) + \frac{\partial}{\partial y} (v\phi) = -\frac{v_s\phi}{h}$$

↑
Advection
with wind

↑
Settling



$$\phi(x, y) = \phi_0 \exp \left(-\frac{3^{5/3}}{C2^{8/3}} \left(\frac{v_s N^{1/3}}{U^{5/6} Q^{1/2}} \right) \frac{x^{4/3}}{(1 - y^3 / w^3)^{1/3}} \right)$$

Conclusions

- Plume rise heights are reduced by atmospheric winds
- Estimates of source mass flux from height of rise need to be derived from models that account for wind
 - Revised empirical formulae accounting for wind
- Intruding ash clouds are partly driven by buoyancy forces.
- Buoyancy processes lead to progressively thinning layers of ash in the atmosphere [*contrast to diffusive thickening*].
- Down wind the ash cloud moves with the atmospheric wind but continues to spread laterally,
- Ash is suspended in a well-mixed turbulent fluid layer and settles from its base.



