

Particle pressure and phase migration in suspensions: *an osmotic approach*

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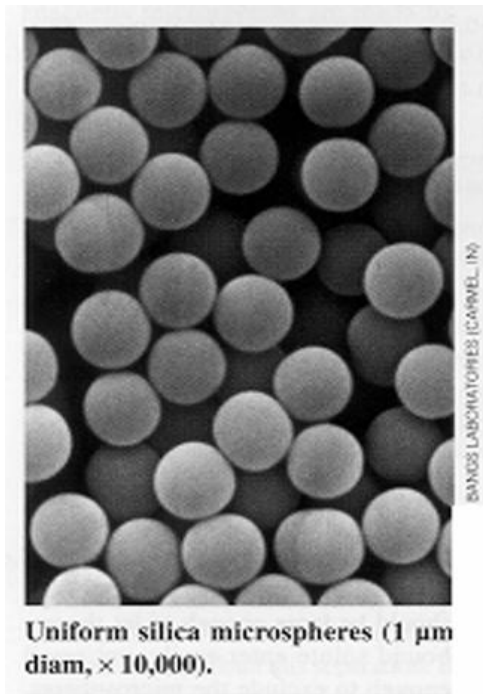
Thanks to

- Ehssan Nazockdast, Yevgeny Yurkovetsky
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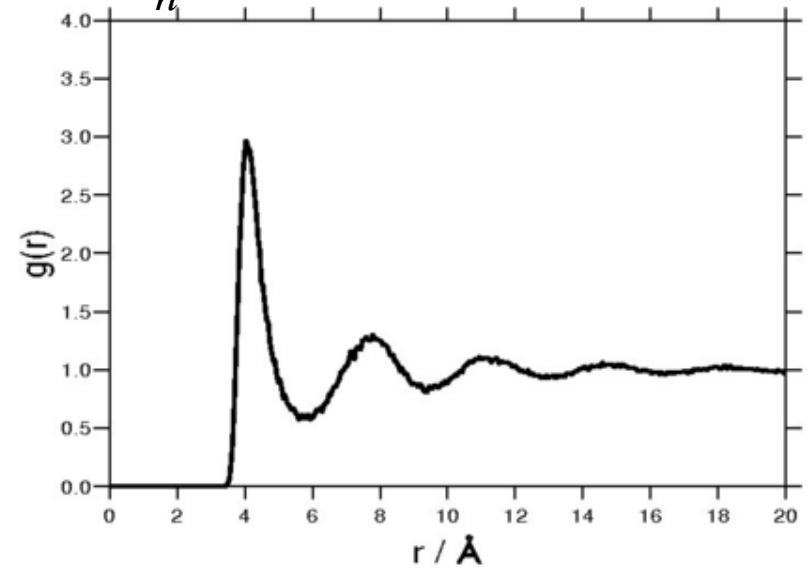
Complex Fluids:

Flow and microstructure are coupled

Hard-Sphere Colloidal Dispersions: Simplest Complex Fluids



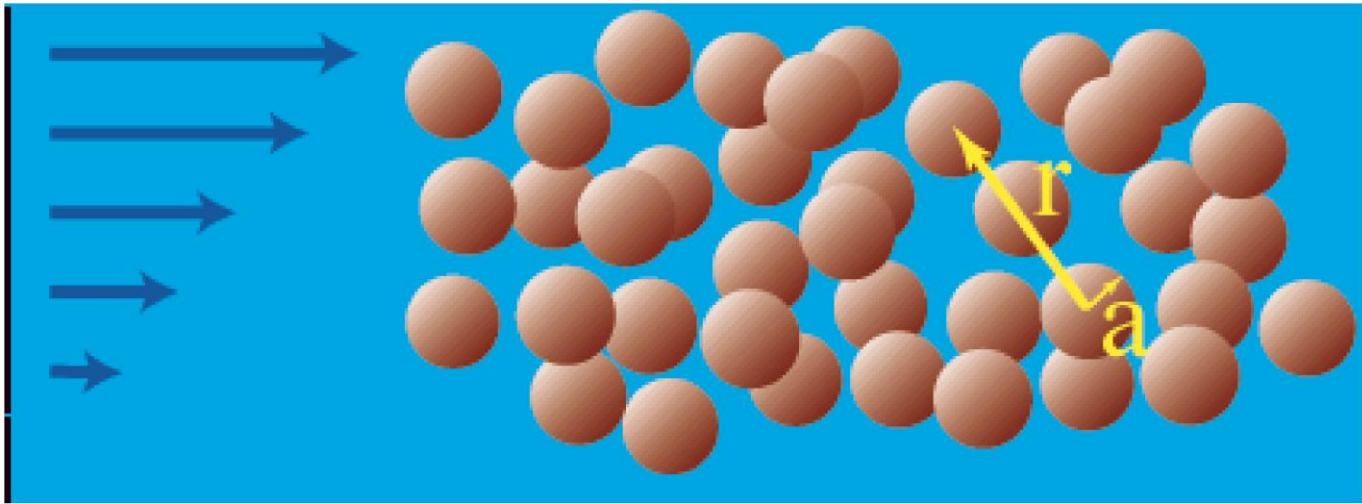
$$g(r) = \frac{P_2(r)}{n^2}, \text{ normalized pair probability}$$



Equilibrium

Pair distribution function:
Agreement of experiment,
simulation and theory
(Percus-Yevick, HNC, ...)

Nonequilibrium dispersions



$$\text{Re}_p \circ \frac{r\dot{\gamma}a^2}{h} \gg 0 \quad (**)$$

$$f = \frac{4pa^3}{3}n, \quad n = \frac{\#}{\text{volume}}$$

Concentration or "loading"

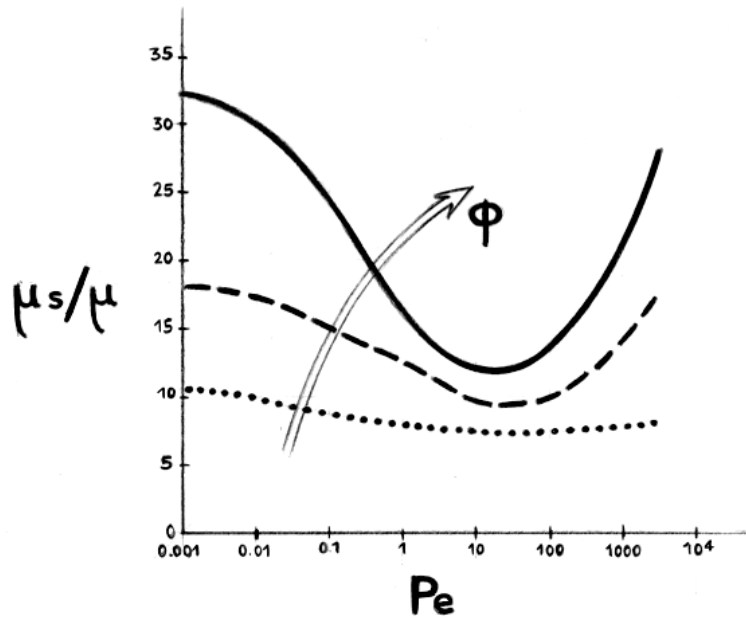
$$\text{Pe} \circ \frac{\dot{\gamma}a^2}{D_0} = \frac{6ph\dot{\gamma}a^3}{kT}$$

D istance from equilibrium

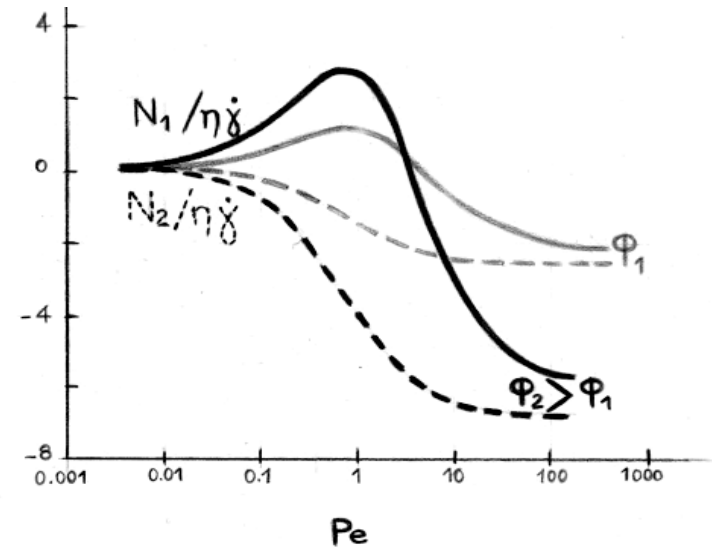
(**) Inertia...Kulkarni & Morris *JFM, PoF* 2008; Humphrey *et al PoF*
Haddadi & Morris submitted *JFM* 2013

Non-Newtonian Rheology

Shear Viscosity



Normal Stress Differences



$$N_1 = \sigma_{xx} - \sigma_{yy}$$

$$N_2 = \sigma_{yy} - \sigma_{zz}$$

ONE GOAL: Microscopic basis for rheology

Flow Kinematics &
Particle loading



Microstructure



Rheology

D. R. Foss & J. F. Brady 2000 *J. Fluid Mech.* 407, 167–200.

I. E. Zarraga, D. A. Hill, & D. T. Leighton 2000 *J. Rheol.* 44, 185.

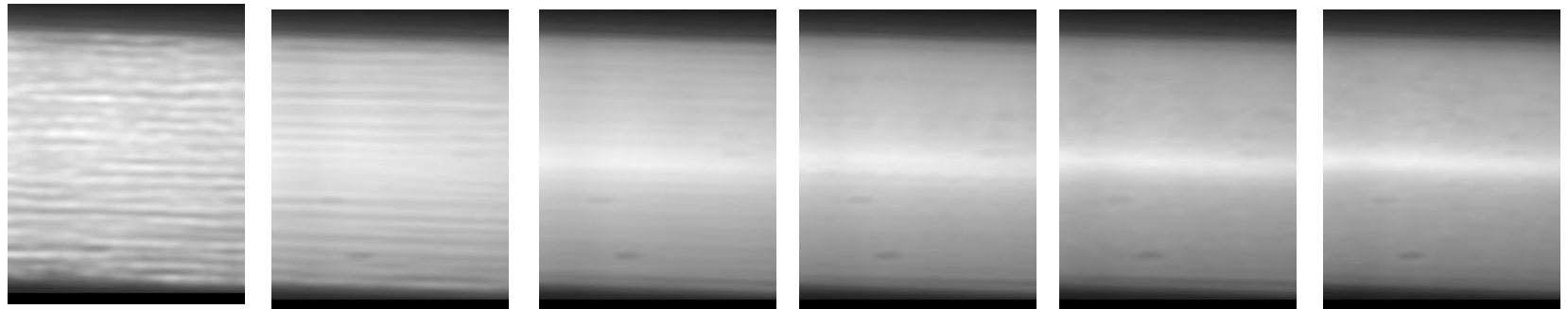
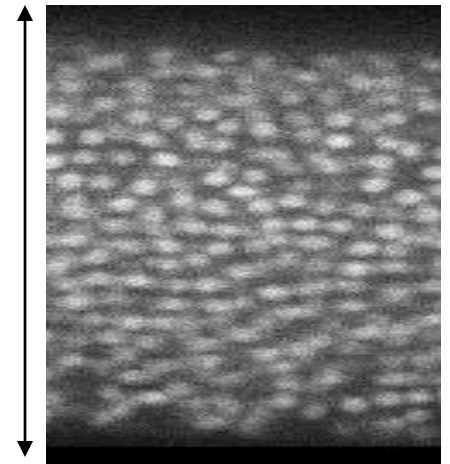
Plots from E. Guazzelli & J. F. Morris 2012 *A Physical Introduction to Suspension Dynamics*, Cambridge.

Macroscopic phenomena by microfluidics

(Confocal microscopy: Eric Weeks lab, Emory Univ.)

Volume fraction $\phi = 0.22$
2 μm diam. PMMA, slight charge

50 μm



0.12 $\mu\text{l}/\text{min}$
Pe ~ 40

Flowrate increasing

10 $\mu\text{l}/\text{min}$
Pe ~ 3400

Frank et al *J. Fluid Mech.* 2003

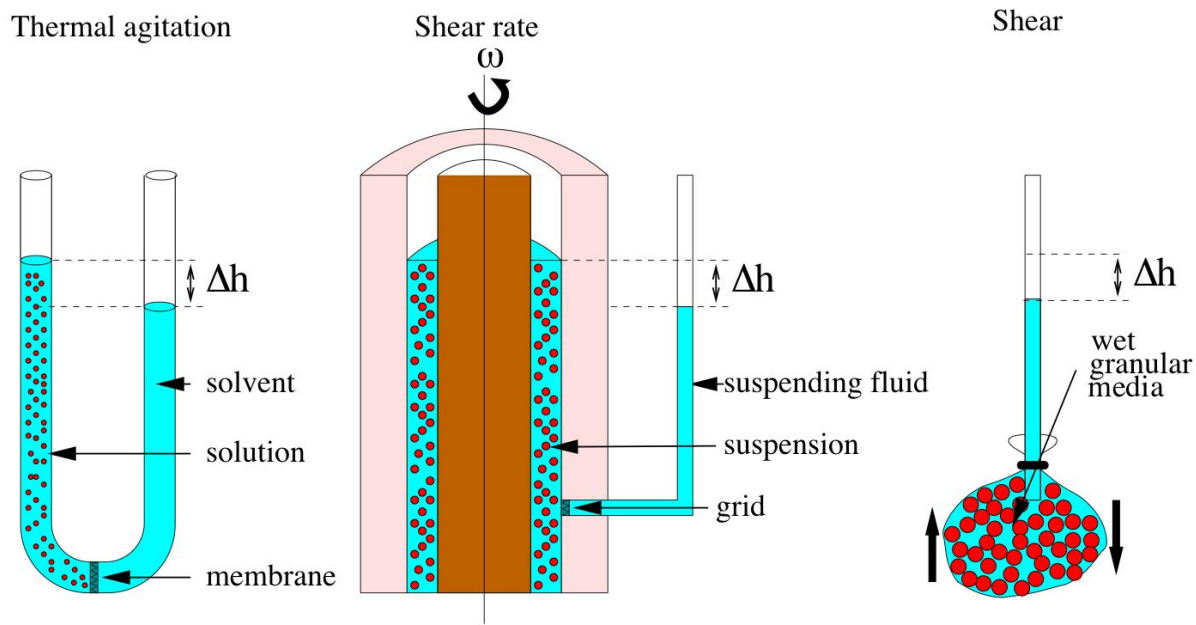
Semwogerere et al. *J. Fluid Mech.* 2007

SECOND GOAL: Coupling migration to rheology

$\mathbf{j} \leftrightarrow \Sigma_{\mathbf{p}}$, particle stress

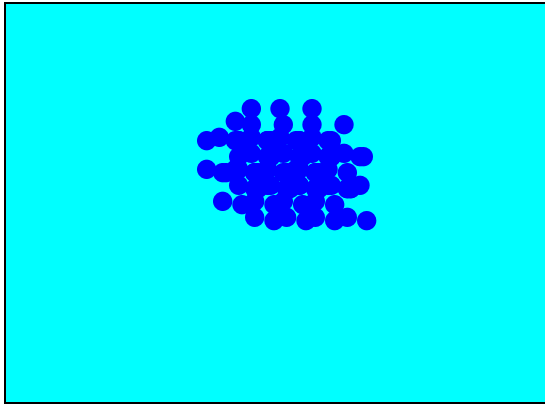
Spreading in particulate mixtures

- Two extremes
 - Osmosis: driven by kT
 - Granular dilation: shear-driven contact stress
- Intermediate conditions...Particle pressure
 - Driven by both kT and shear
 - Contact and noncontact (hydrodynamic) stresses, in principle

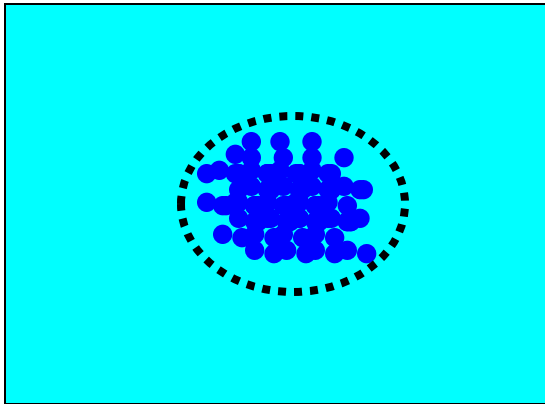
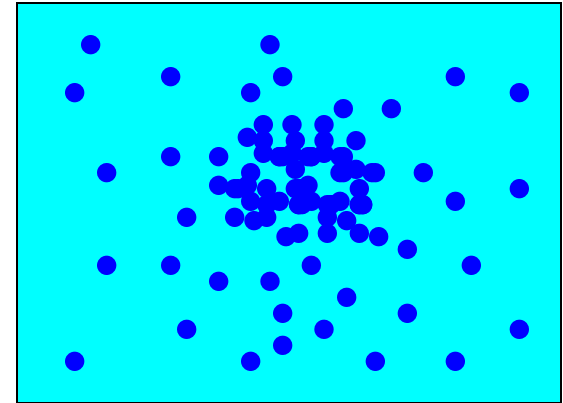


Diffusion and stress

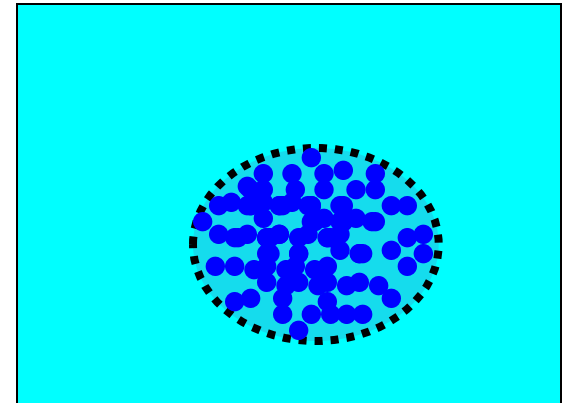
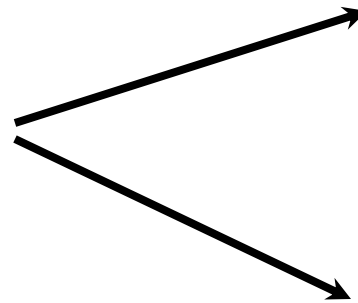
*Constraining diffusion
requires normal stress.*



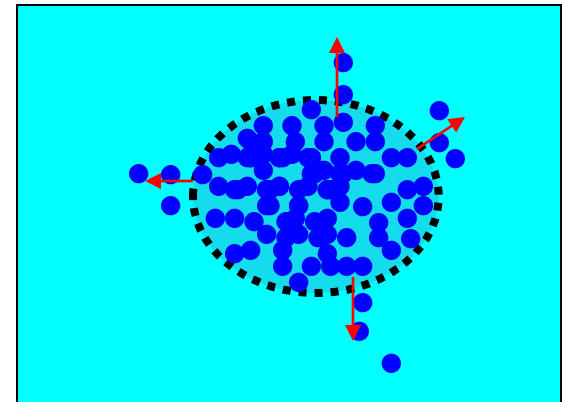
1. Unconfined
Spread with time



2. Confined
Stretch membrane



Burst membrane



$$j = -M\nabla p = -M \frac{\partial p}{\partial f} \nabla f = -D\nabla f$$

Diffusion and stress in dispersions

Pe = 0: Brownian motion & classical osmotic pressure

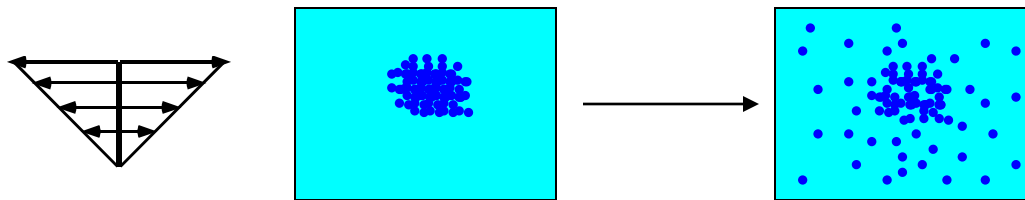
kT drives motion and sets stress scale

$$D \sim \frac{kT}{\eta a} \quad S_{ij}^P = -P d_{ij} \sim nkT$$

Pe >> 1 : Shear-induced diffusion & particle pressure

Shear rate drives motion ... plays *role* of temperature

$$D \sim \dot{\gamma} a^2 \quad \Sigma_{ij}^P \sim (na^3) \eta \dot{\gamma} \sim f(\phi) \eta \dot{\gamma}$$



Pine *et al.* Nature 2005

Suspension stresses: $Pe \gg 1$

Total stress [Batchelor JFM 1970]

$$\Sigma^{\text{Total}} = \Sigma^{\text{F}} + \Sigma^{\text{P}}$$

Shear stress

$$\Sigma_{xy}^{\text{F}} + \Sigma_{xy}^{\text{P}} = (\eta_{Fl} + \eta_P) \dot{\gamma} = \eta_s \dot{\gamma}$$

Normal stresses [Morris & Boulay J. Rheol. 1999]

Differences

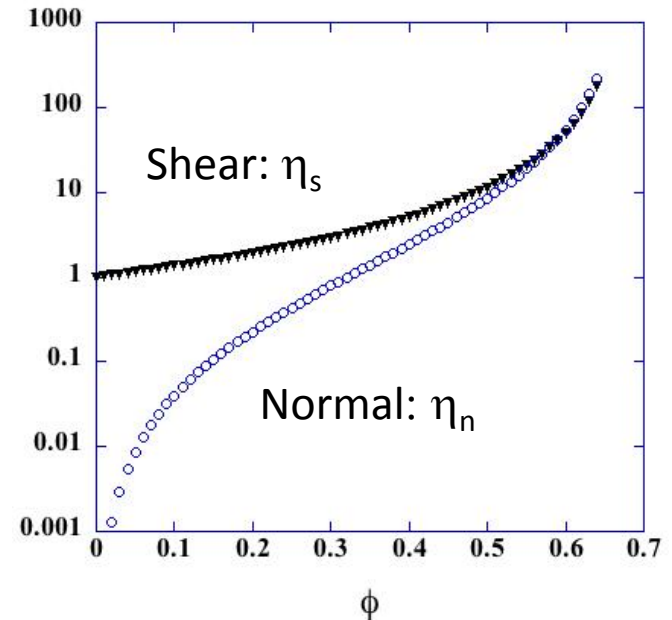
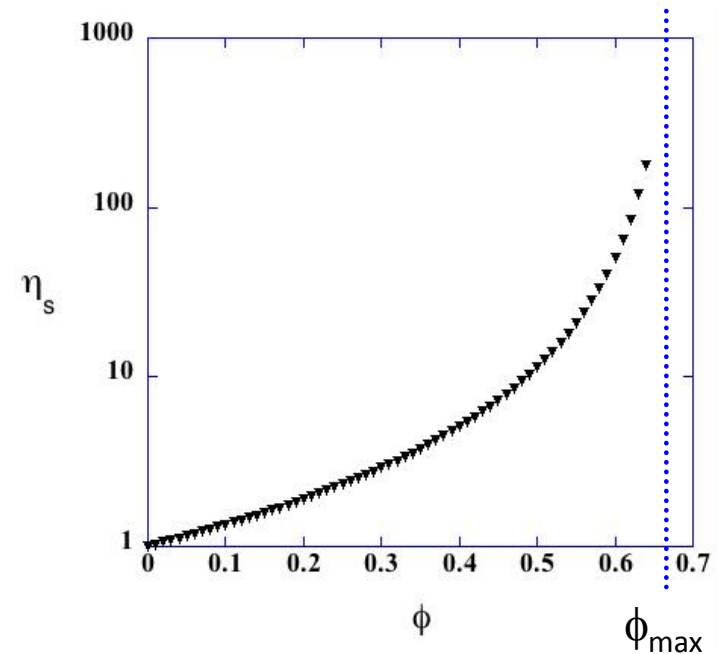
$$\mathbf{N}_1 = \Sigma_{11}^P - \Sigma_{22}^P \quad \mathbf{N}_2 = \Sigma_{22}^P - \Sigma_{33}^P$$

Particle pressure

$$\Pi = -\frac{1}{3} \mathbf{I} : \Sigma^P = -\frac{1}{3} [\Sigma_{11}^P + \Sigma_{22}^P + \Sigma_{33}^P]$$

$$\Pi, \mathbf{N}_1, \mathbf{N}_2 \sim \eta_n \dot{\gamma}$$

$$\Rightarrow \nabla \Pi(\phi, \dot{\gamma}) = \frac{\partial \Pi}{\partial \phi} \nabla \phi + \frac{\partial \Pi}{\partial \dot{\gamma}} \nabla \dot{\gamma}$$



Two-fluid model and particle migration

Particle conservation:
$$\frac{\partial f}{\partial t} + \langle \mathbf{u} \rangle \cdot \nabla f = -\nabla \cdot \mathbf{j}_\wedge$$

General momentum balance:
$$\rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} \right) = \nabla \cdot \Sigma$$

Average over particles ($\text{Re} \ll 1$):
$$0 = \nabla \cdot \Sigma^{\mathbf{P}} + \mathbf{F}_{\text{drag}}$$

$$\mathbf{F}_{\text{drag}} \approx -\frac{9\eta_c}{2a^2} f(\phi)^{-1} \phi (\mathbf{U} - \langle \mathbf{u} \rangle)$$

$\mathbf{j}_\wedge \circ f (\mathbf{U} - \langle \mathbf{u} \rangle)$ migration flux

$$= \frac{2a^2}{9\eta_0} f(\phi) \nabla \cdot \Sigma^{\mathbf{P}}$$

Viscous suspensions:

Jenkins & McTigue 1990

Nott & Brady 1994

Morris & Boulay 1999

Similarly in polymeric fluids:

Onuki & Doi 1991

Mavrantzas & Beris 1994

MacDonald & Muller 1996

Two-fluid modeling

$$\mathbf{j}_\perp = \frac{2a^2}{9\eta_c} f(\phi) \nabla \cdot \Sigma^{\mathbf{P}} \sim -\nabla \Pi$$

$$\frac{\partial \phi}{\partial t} + \langle \mathbf{u} \rangle \cdot \nabla \phi \approx \frac{2a^2}{9\eta_0} f(\phi) \nabla^2 \Pi$$

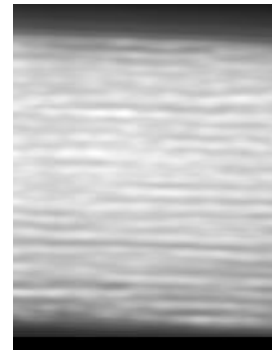
Bulk mixture motion

$$\nabla \cdot \langle \mathbf{u} \rangle = 0$$

$$\nabla \cdot \Sigma = \nabla \cdot \Sigma^{\mathbf{F}} + \nabla \cdot \Sigma^{\mathbf{P}} = 0$$

$$\Rightarrow \nabla \cdot \Sigma^{\mathbf{F}} = -\nabla \cdot \Sigma^{\mathbf{P}}$$

**$\Sigma^{\mathbf{P}}$ (and Π) has hydrodynamic (H) and Brownian (B) terms:
roughly speaking balance two osmotic contributions**



A

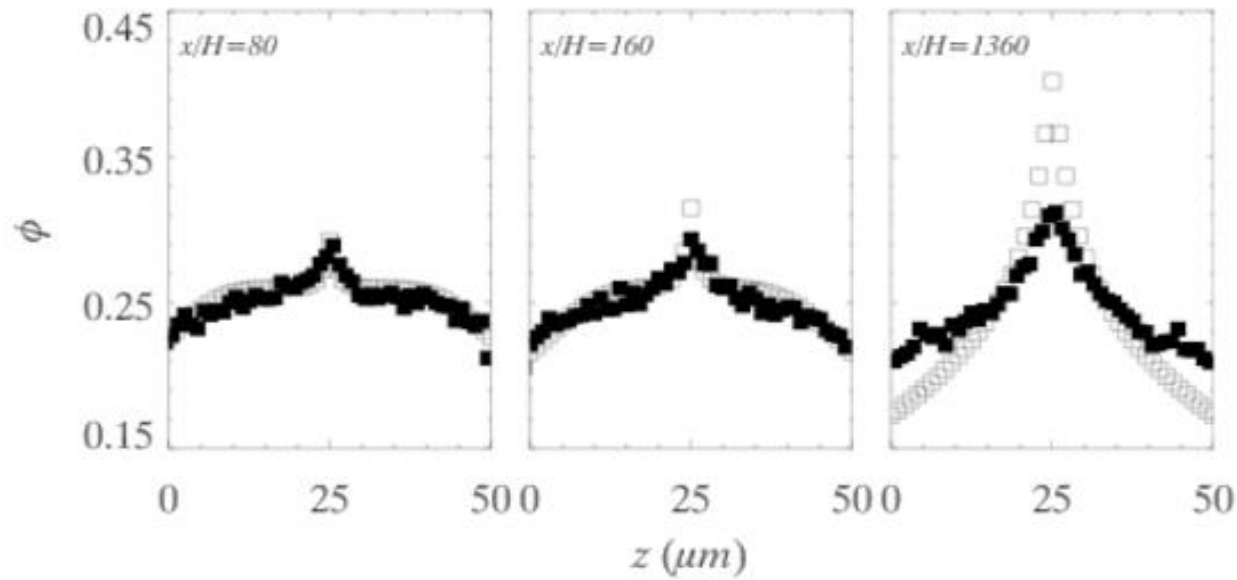
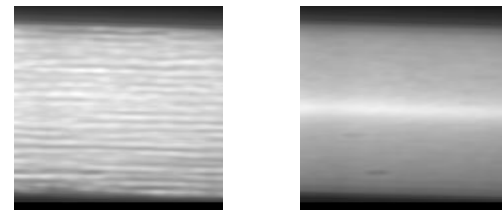


B

A. Low flowrate = small Pe:
Brownian stress – particles dispersed

B. High flowrate = large Pe:
Hydrodynamic stress drives migration

Axial evolution



experiment (solid)
model (open)
 $\phi = 0.26$
 $Pe = 130$

So particle pressure is
useful for modeling ...
but is it real (= measurable)?

Suspension stresses: $Pe \gg 1$

Total stress [Batchelor JFM 1970]

$$S^{\text{Total}} = S^{\text{F}} + S^{\text{P}}$$

Shear stress

$$S_{xy}^{\text{F}} + S_{xy}^{\text{P}} = (h_{Fl} + h_P)\dot{g} = h_s\dot{g}$$

Normal stresses [Morris & Boulay J. Rheol. 1999]

Differences

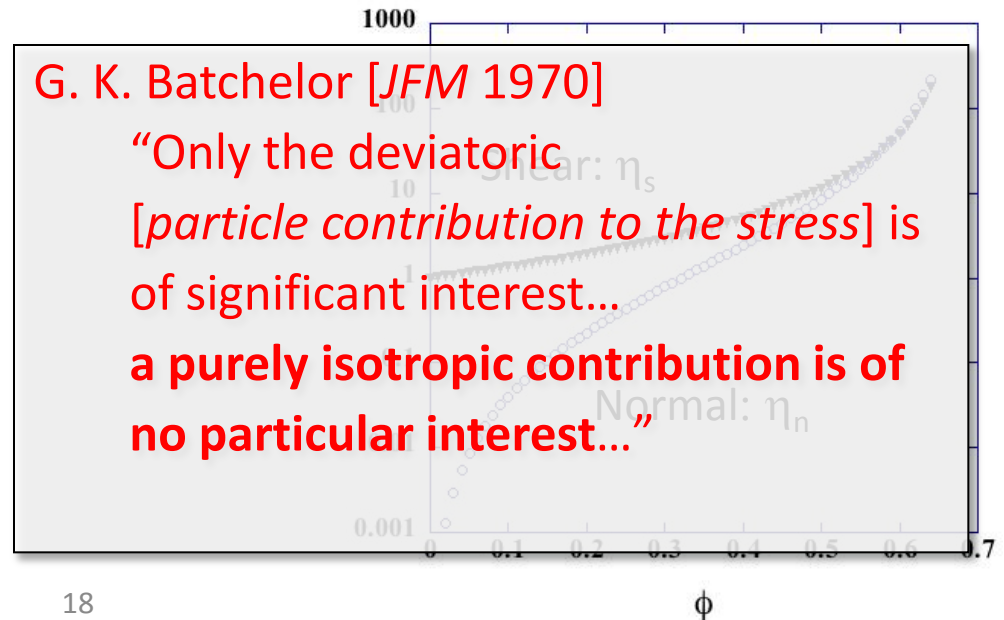
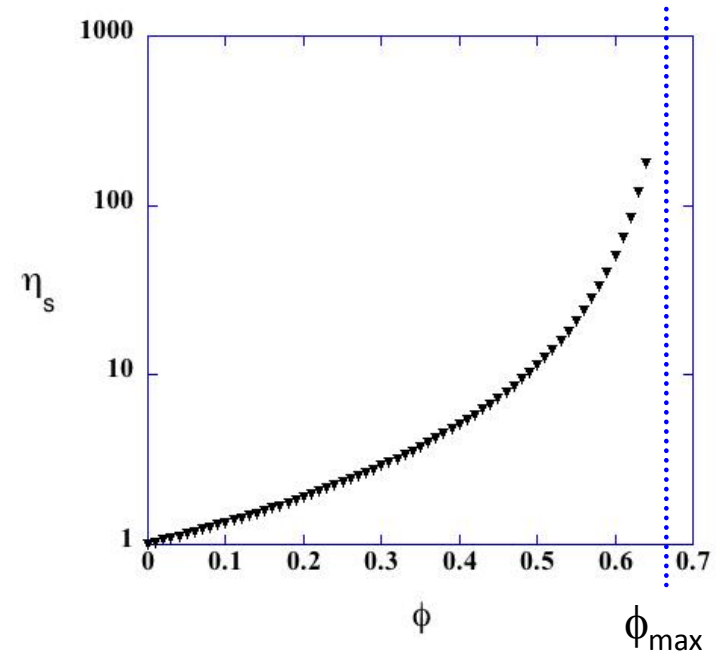
$$N_1 = S_{11}^P - S_{22}^P \quad N_2 = S_{22}^P - S_{33}^P$$

Suspension pressure

$$P = -\frac{1}{3} \mathbf{I} : S^P = -\frac{1}{3} [S_{11}^P + S_{22}^P + S_{33}^P]$$

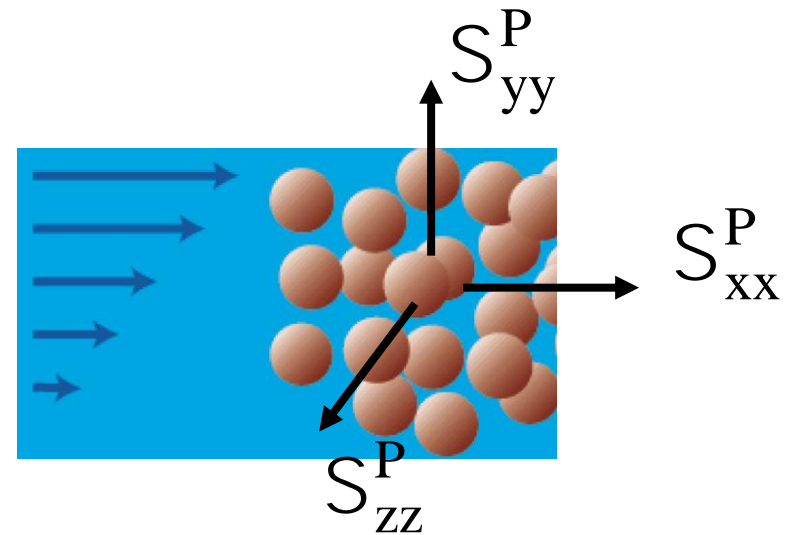
$$P, N_1, N_2 \sim h_n \dot{g}$$

$$\Rightarrow \nabla P(f, \dot{g}) = \frac{\partial P}{\partial f} \nabla f + \frac{\partial P}{\partial \dot{g}} \nabla \dot{g}$$



Rheometry:

Incompressibility constraint



$$S^{Total} = S^F + S^P \quad \text{⊢}$$

$$P^{Total} = P^{Fluid} + P = \text{confining pressure, } P^0 \text{ (reference level } P^0 = 0)$$

$$P = - \frac{S_{xx}^P + S_{yy}^P + S_{zz}^P}{3}$$

$$\text{⊢ } P^{Fluid}(\dot{\gamma}) = - P(\dot{\gamma})$$

\ Summation obscures : need to discriminate particles & fluid.

Yurkovetsky & Morris *J. Rheol.* 2008

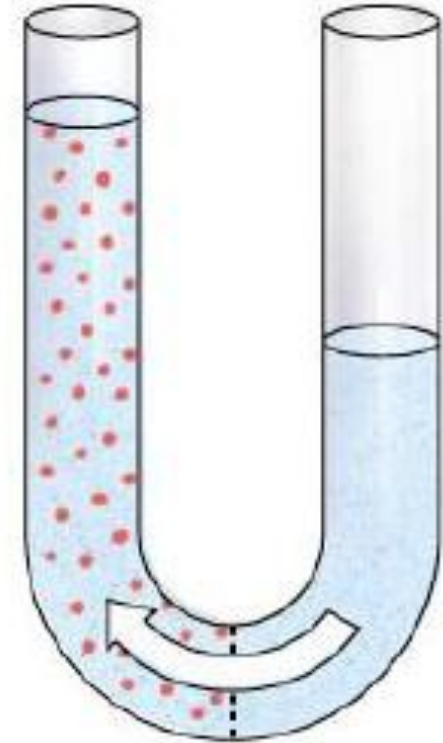
See also : Prasad & Kytomaa *Int. J. Multiphase Flow* 1995

Suction into a mixture...osmosis

Osmotic pressure, Π

$$\text{Thermodynamics: } P = - \left. \frac{\partial A}{\partial V} \right|_{T,N}$$

A = Helmholtz energy

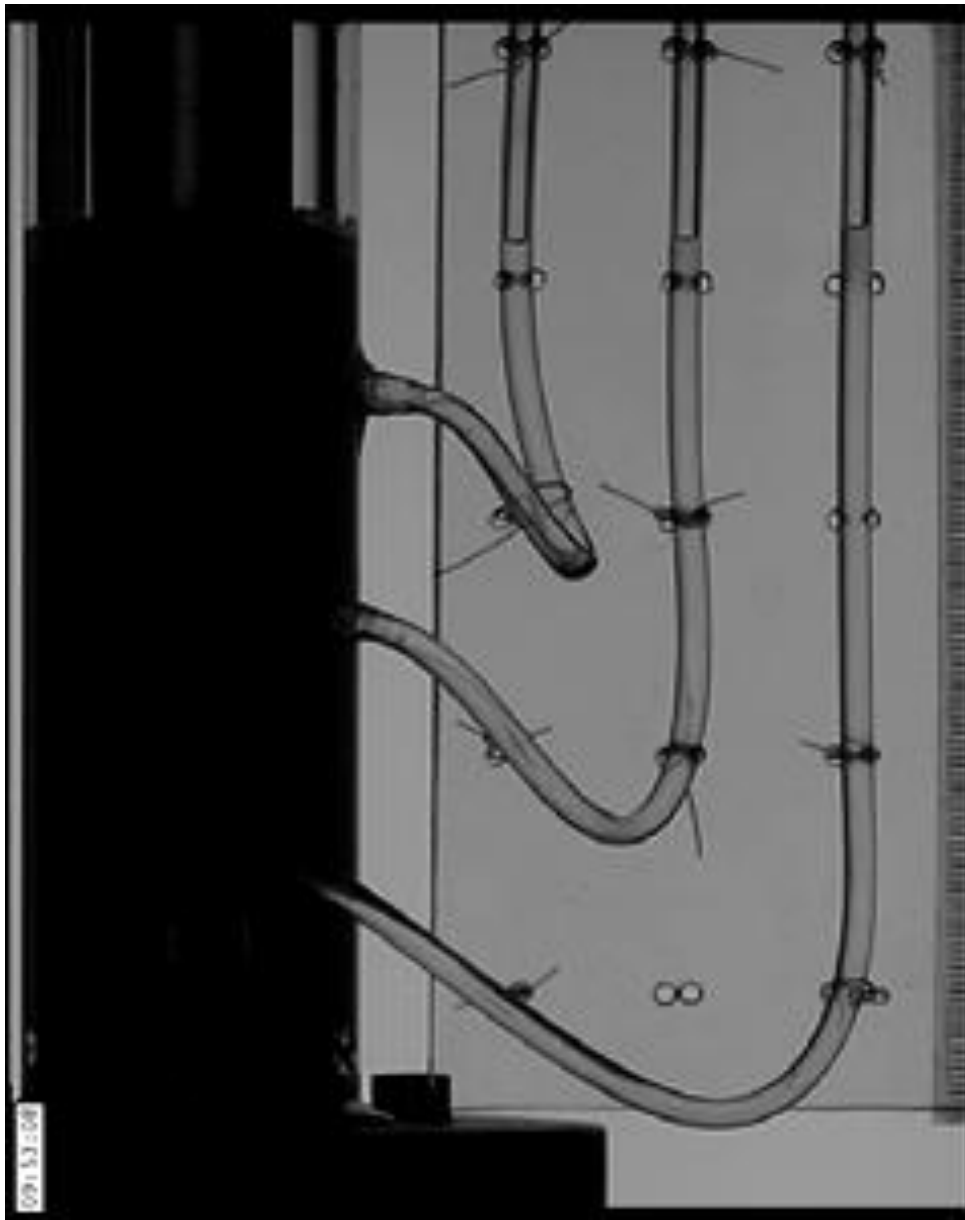


Colloidal dispersions [Russel *et al.* 1989] :

$$f = Nv_1 / V = nv_1 \quad \text{solid fraction}$$

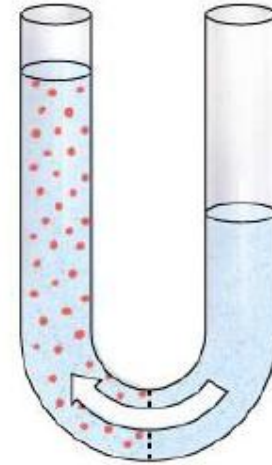
$$P = - \left. \frac{\partial A}{\partial V} \right|_{T,N} = \frac{f}{V} \left. \frac{\partial A}{\partial j} \right|_{T,N}$$

Hard or repulsive particles--
 $\Pi > 0$:
Free energy minimized at $\phi = 0$

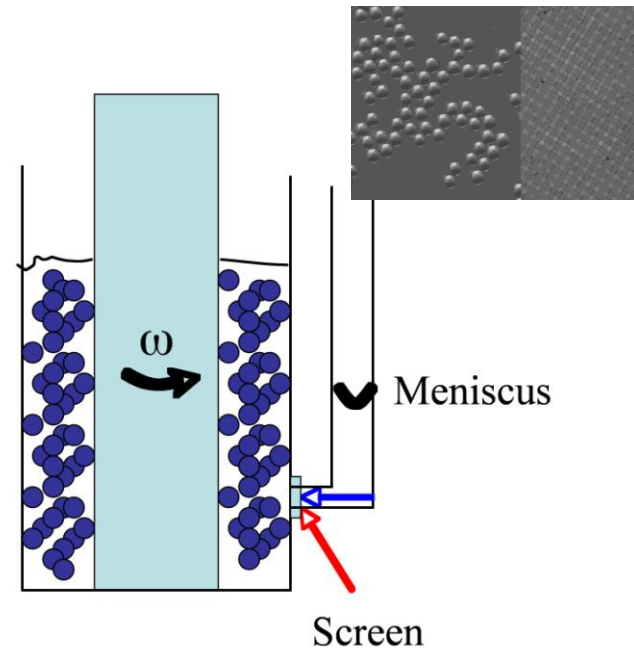


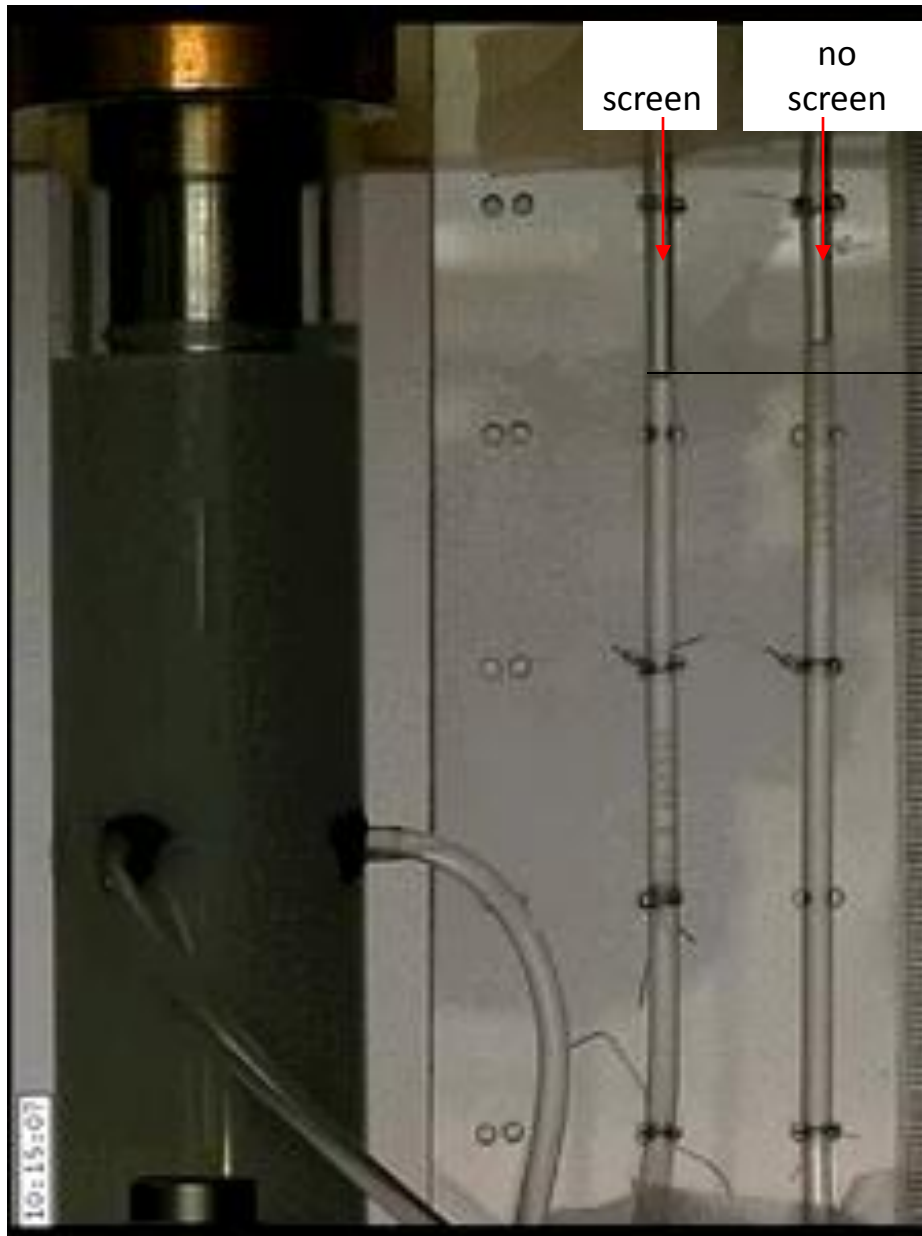
Concentrated suspension / 3 mm gap
 $Re \ll 1, Pe \gg 1, \phi = 0.45$

Osmosis - classical

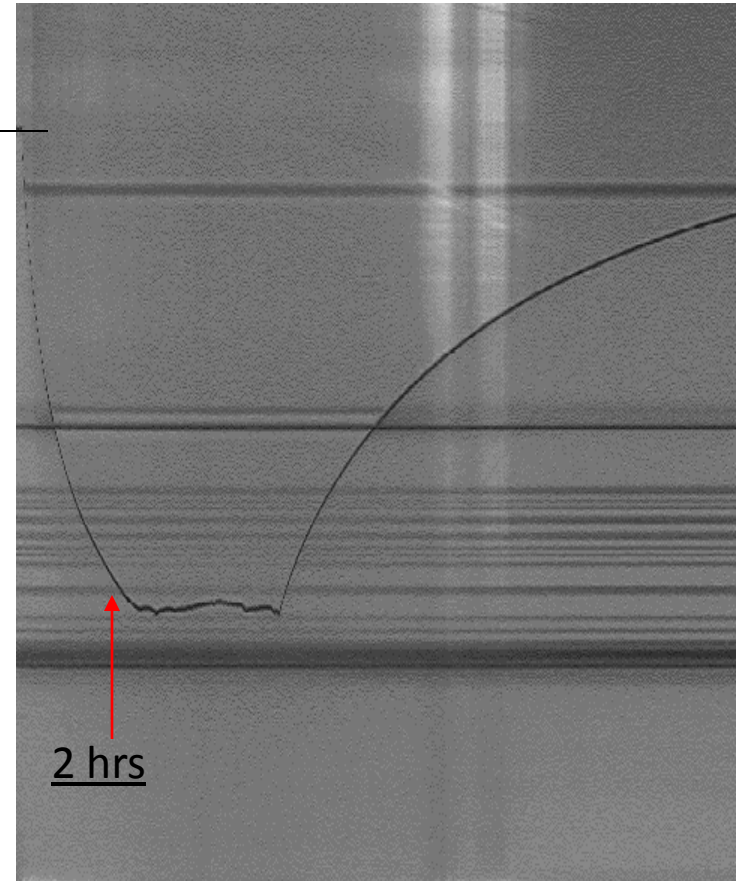


Osmosis - shear-induced?





Deboeuf *et al.* *Phys. Rev. Lett.* 2009



$$\bar{f} = 0.45$$

$$\dot{g} = 20 \text{ s}^{-1}$$

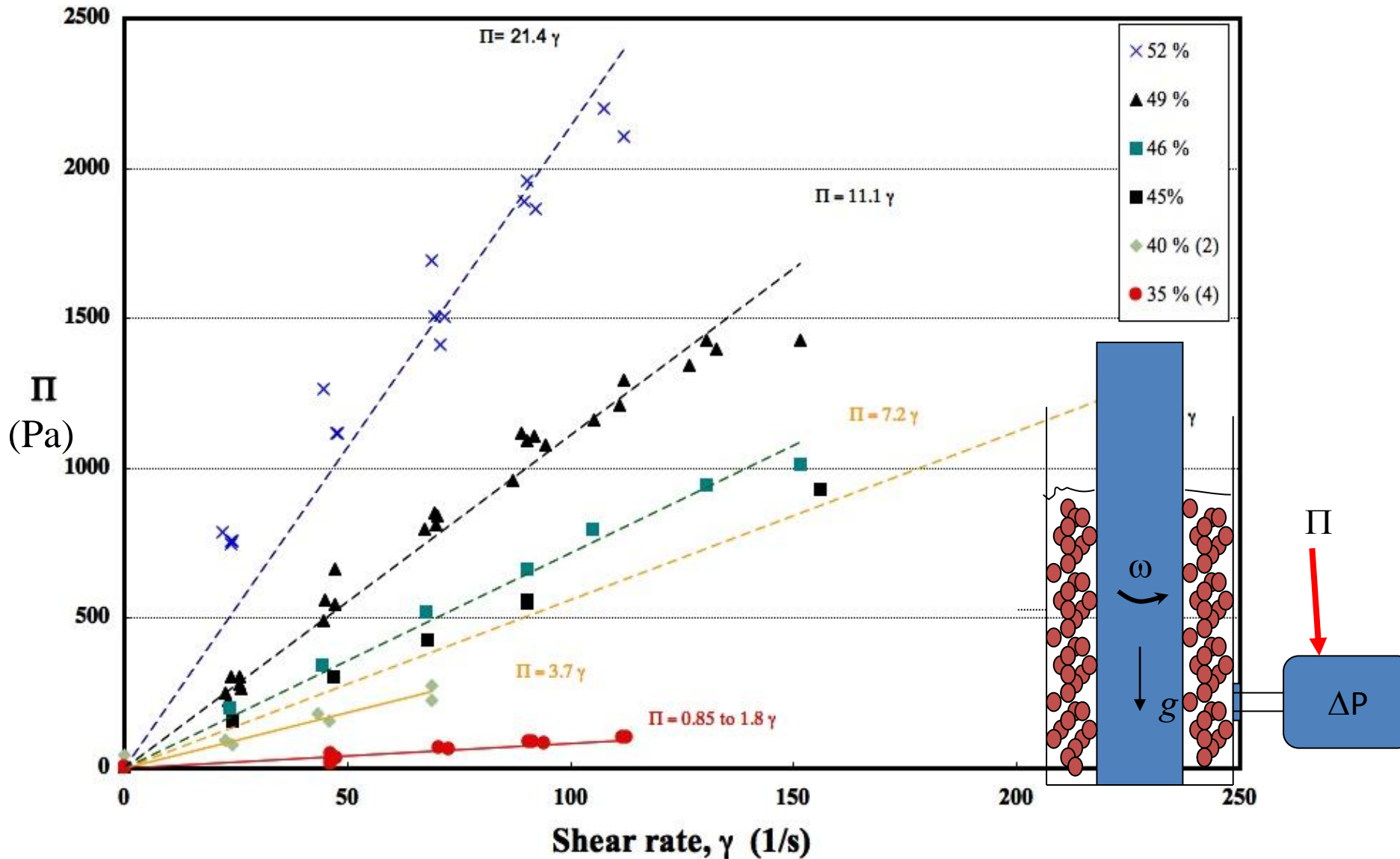
Neutrally - buoyant, $d = 80 \text{ mm}$

fluid viscosity: $\eta_0 = 2000 \text{ cP}$

Quantitative rheology

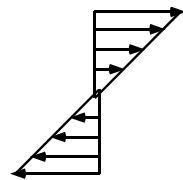
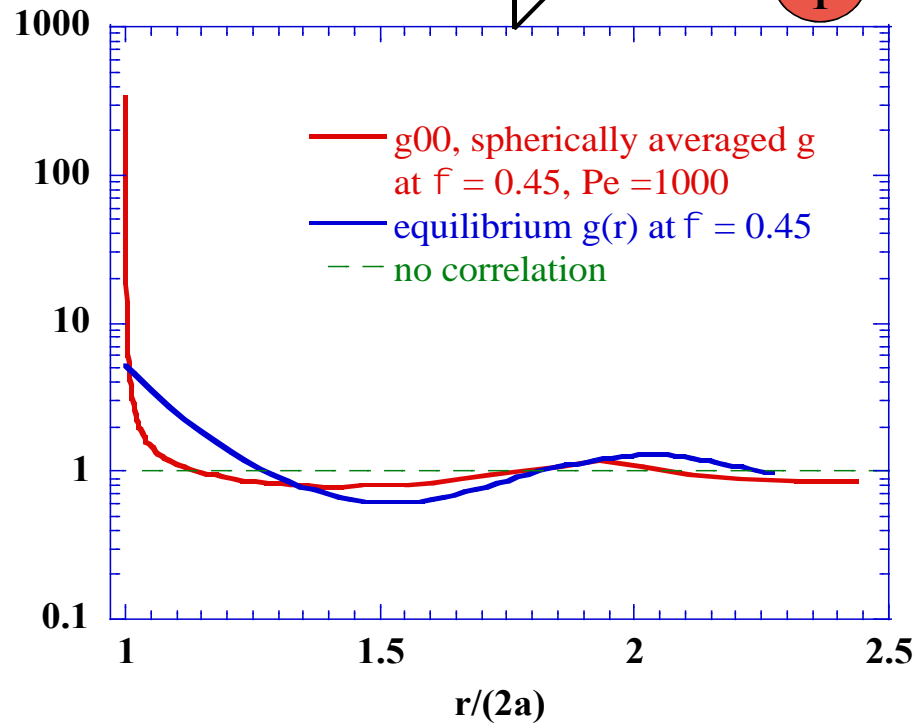
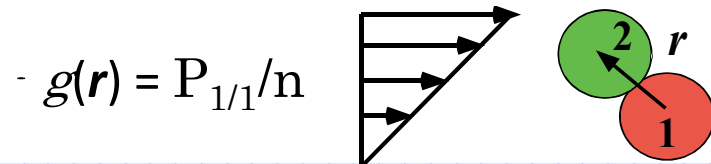
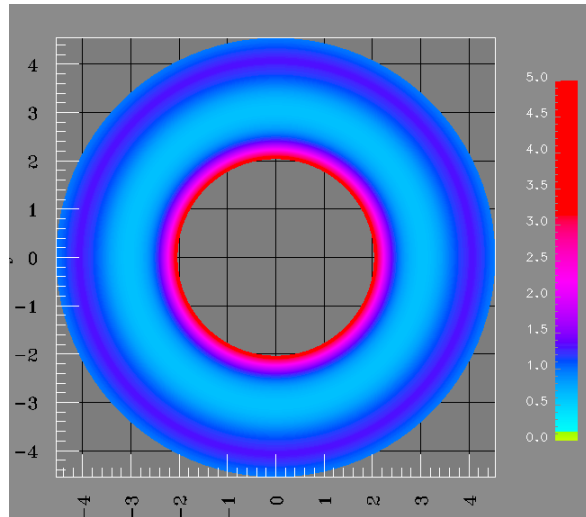
Deboeuf *et al.* PRL 2009

Details: Garland *et al.* J Rheol. 2013 (extension to $\phi = 0.2$)

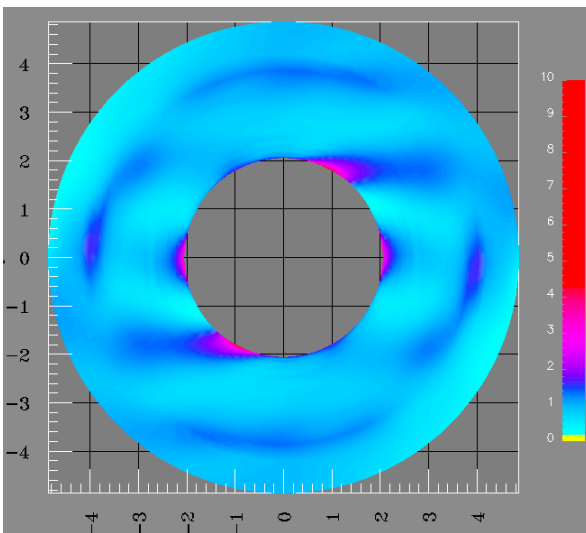


Π : the role of microstructure

$Pe = 0$
(eqm)

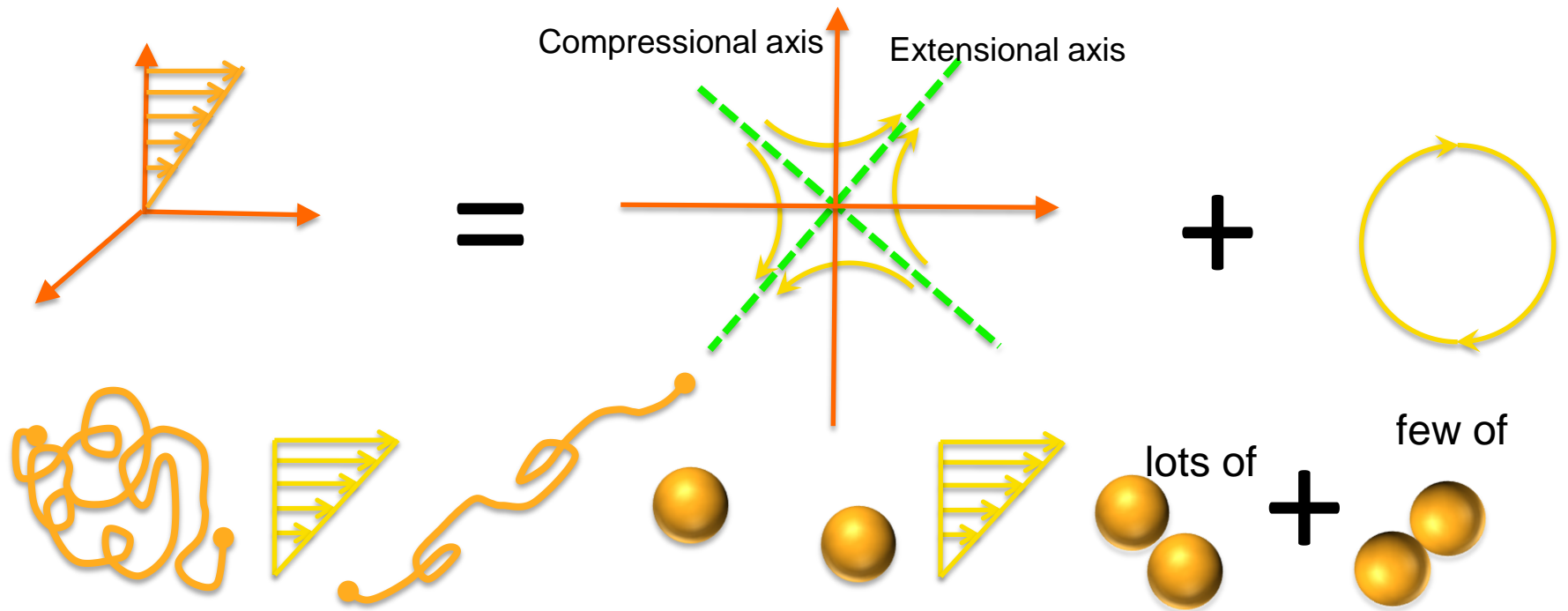


$Pe = 10^3$
(strong shear)



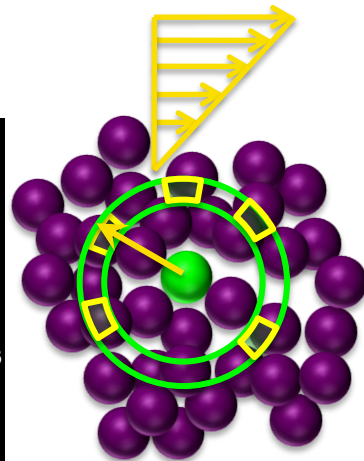
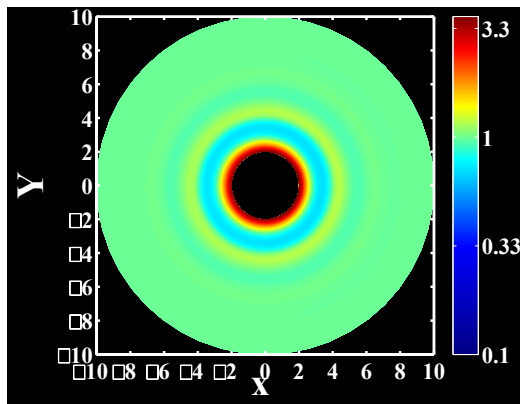
Configurational sampling from Stokesian Dynamics simulations.
 [Morris & Katyal *Phys. Fluids* 2002
 Kulkarni & Morris *J. Rheol.* 2009]

Flow-induced microstructure

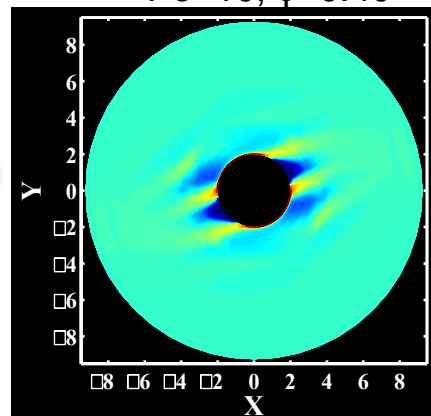


Sheared Anisotropic Structure

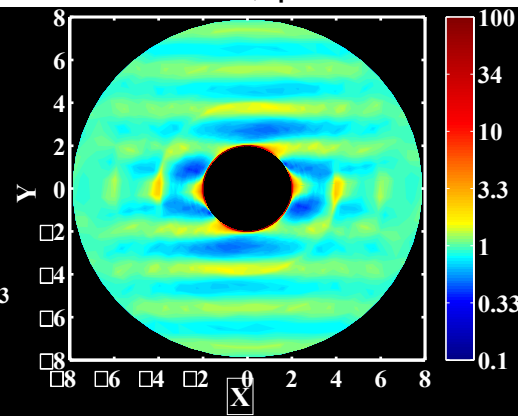
$Pe=0, \phi=0.40$



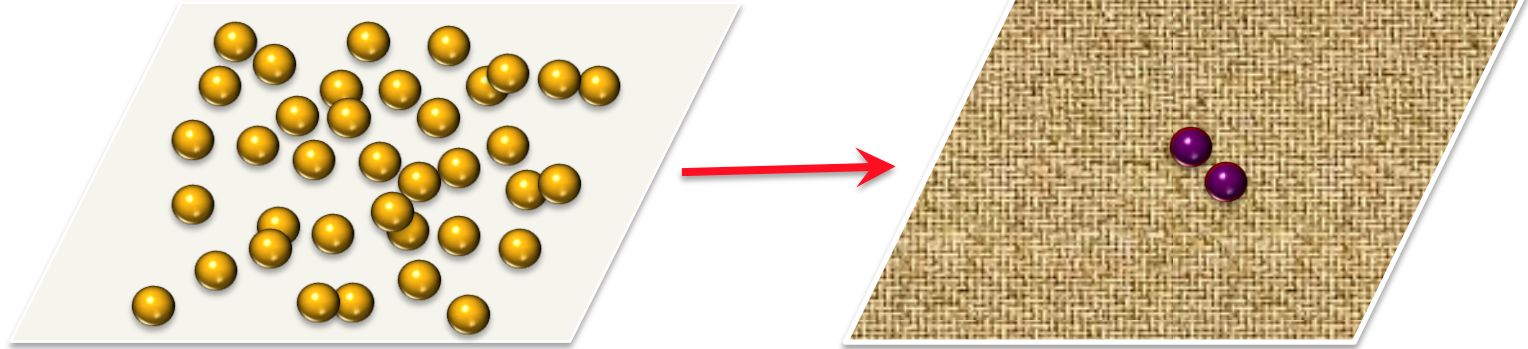
$Pe=10, \phi=0.40$



$Pe=10, \phi=0.50$



N - Body \longrightarrow 2 - Body



$$\nabla \cdot [Ug(\mathbf{r}) - \mathbf{D} \cdot \nabla g(\mathbf{r})] = 0$$

$\mathbf{U}(\mathbf{r})$: Relative pair velocity

$\mathbf{D}(\mathbf{r})$: Relative pair diffusivity

Boundary Conditions:

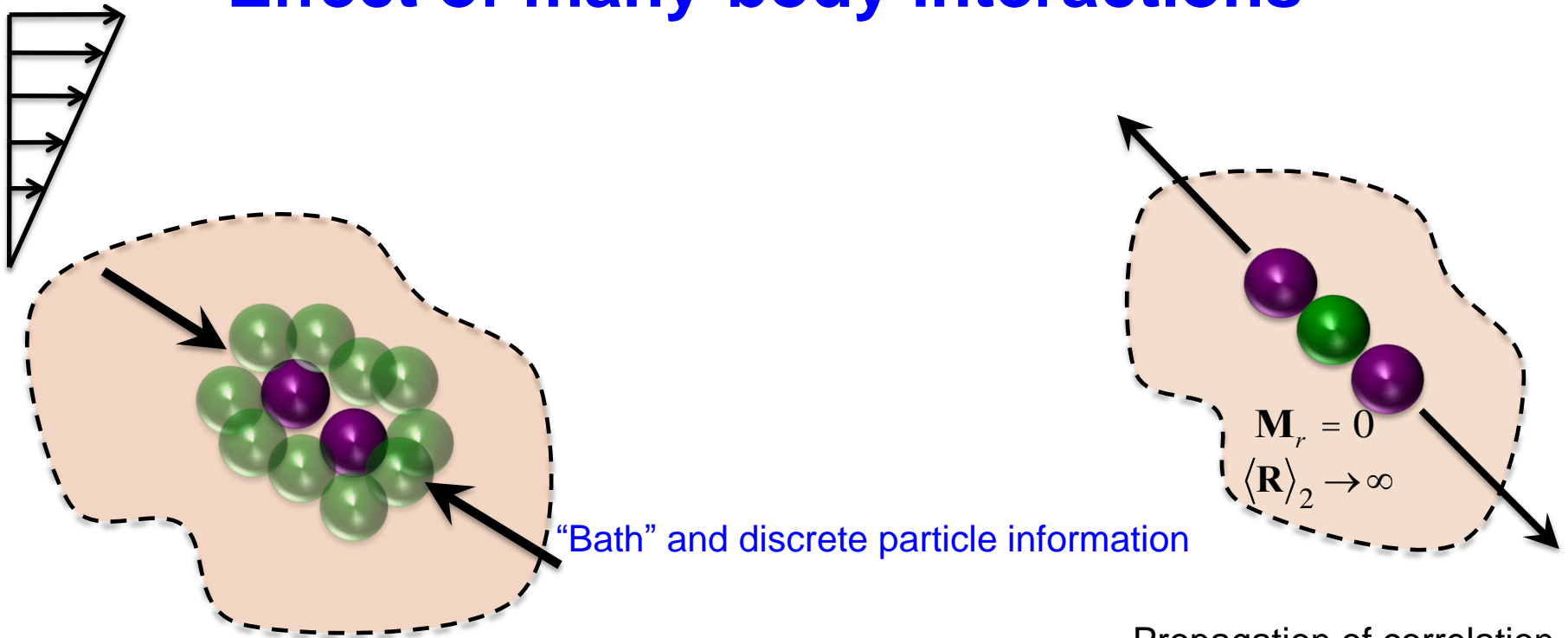
$$j_r = 0 \text{ at } r=2a$$

Zero radial flux at contact

$$g(r) = 1 \text{ at } r/a \gg 1$$

Two particles become de-correlated

Effect of many-body interactions

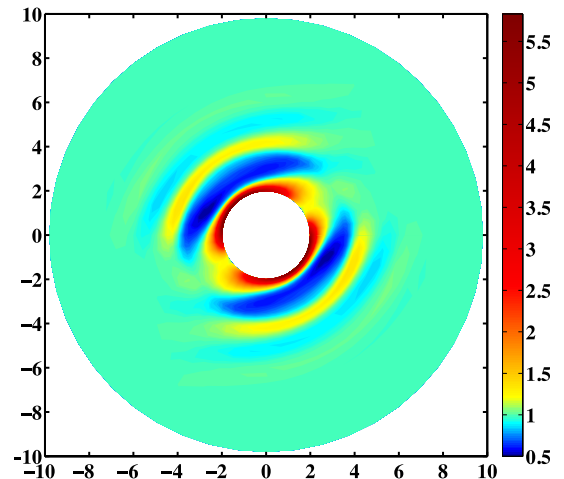


Generates correlation and shear-induced diffusion

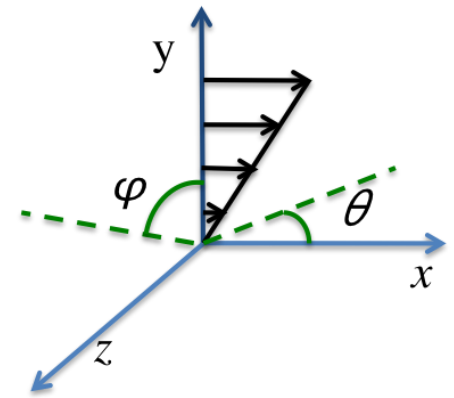
Details:

E. Nazockdast & J. F. Morris *JFM* 2012

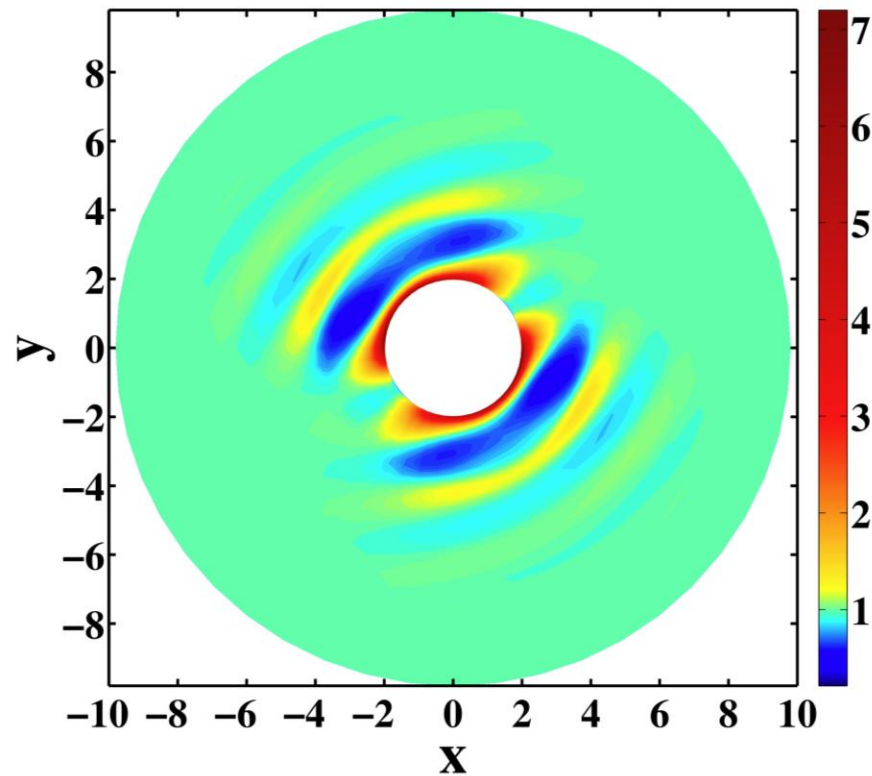
Propagation of correlation



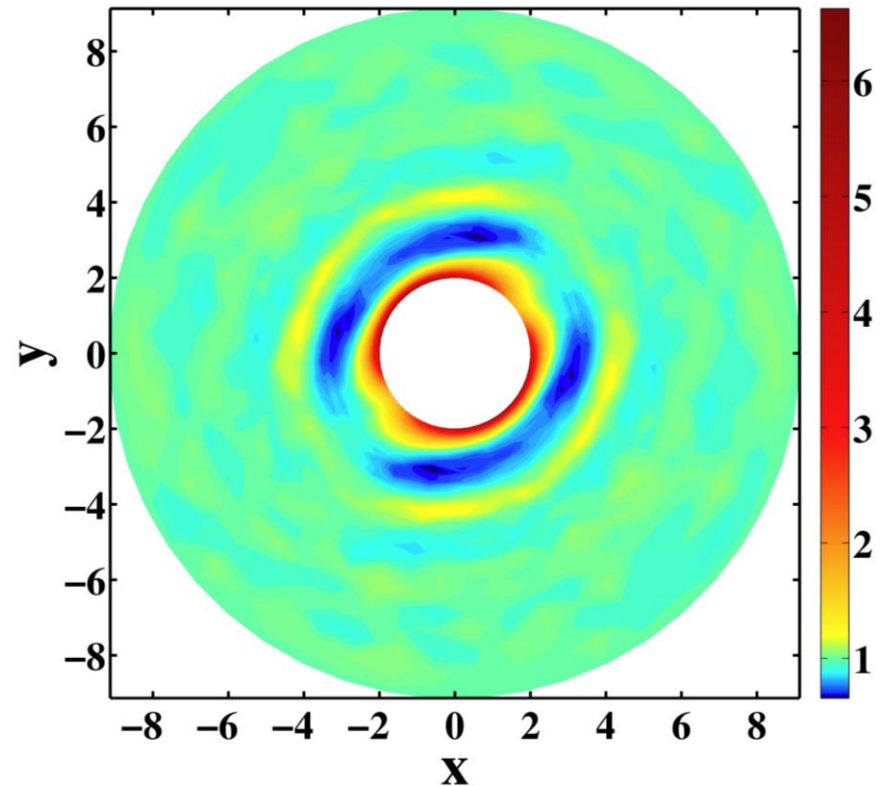
Microstructure



Theory, $\phi=0.40$, $Pe=1$

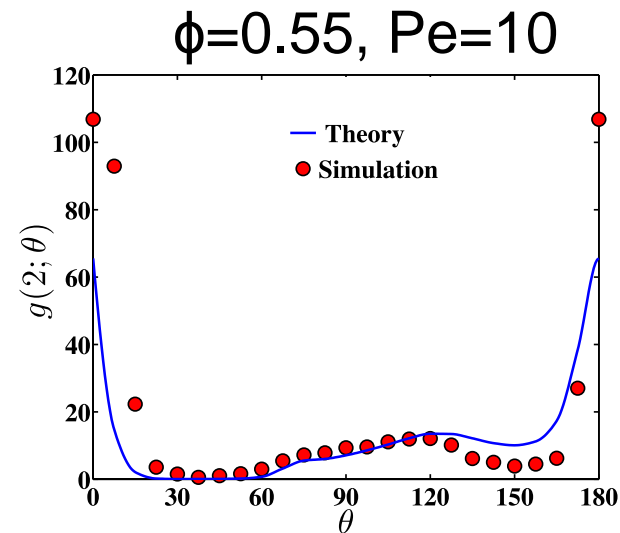
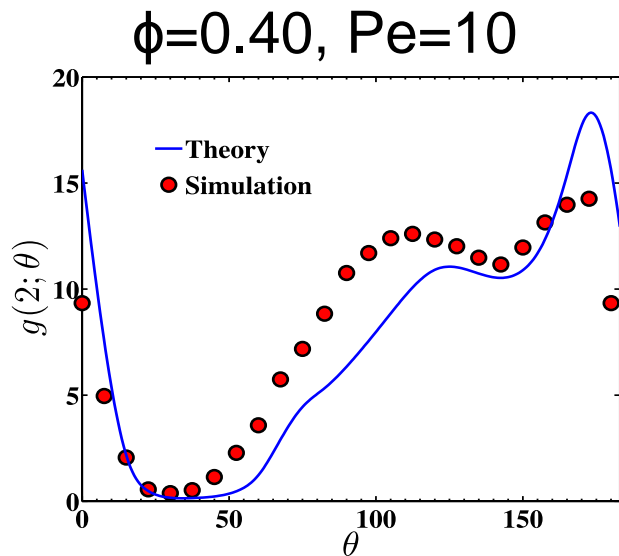
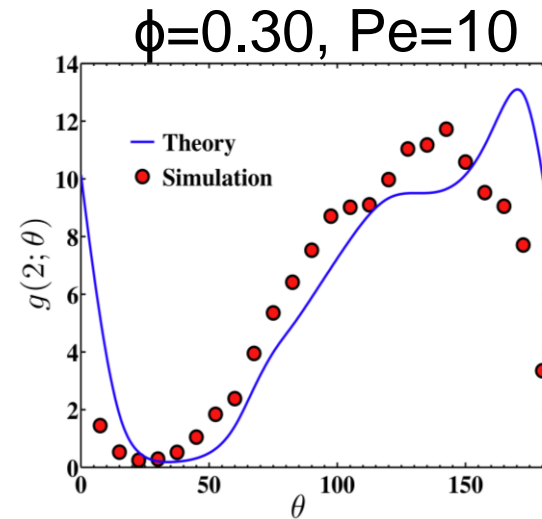
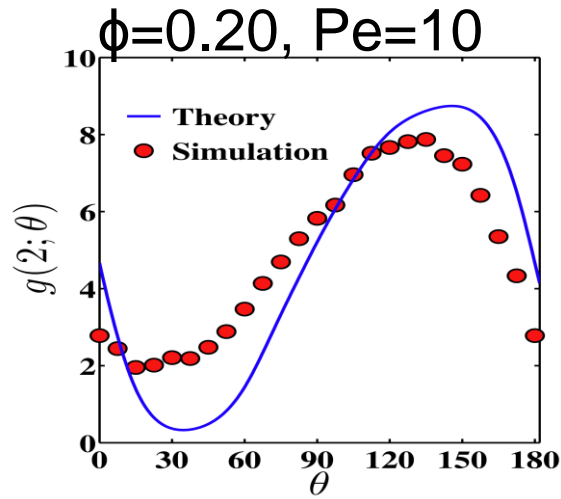
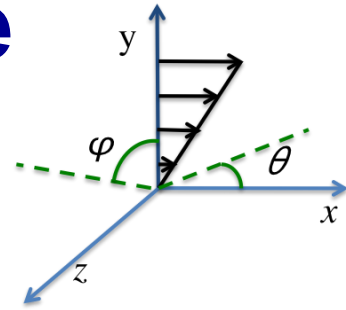


Simulation, $\phi=0.40$, $Pe=1$



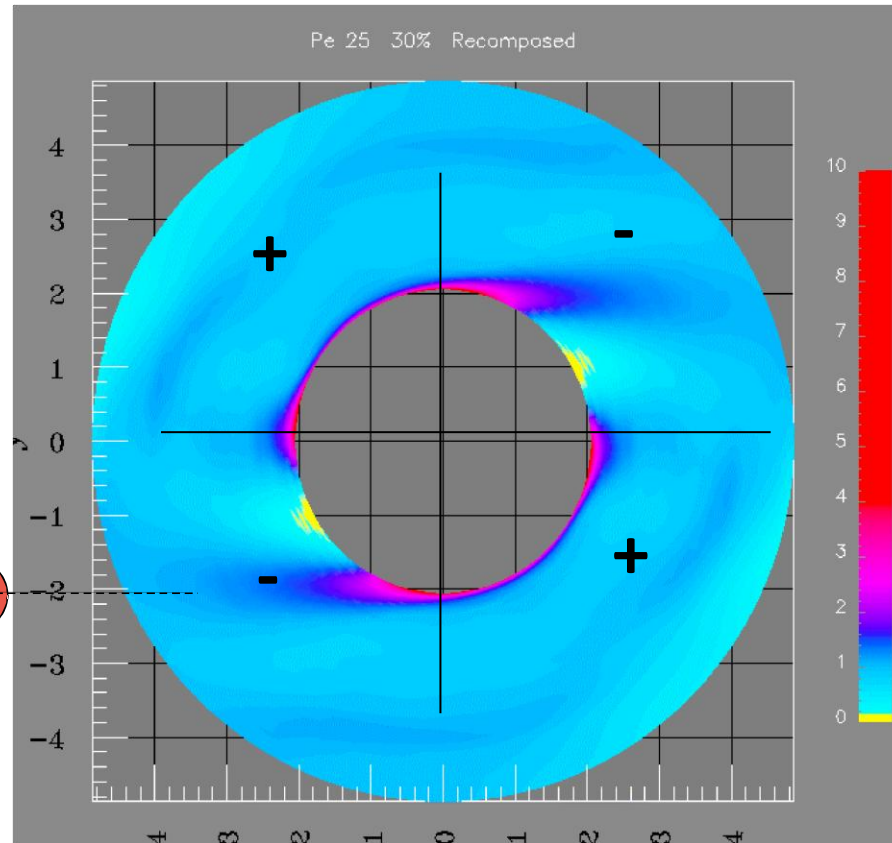
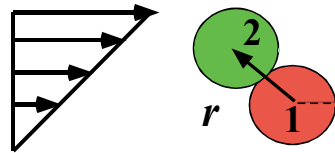
Simulation: Accelerated Stokesian Dynamics
Banchio & Brady *J Chem Phys* 2003

Microstructure – contact surface



Hydrodynamic theory (contact is not essential)
of particle pressure, Π

Π sign map



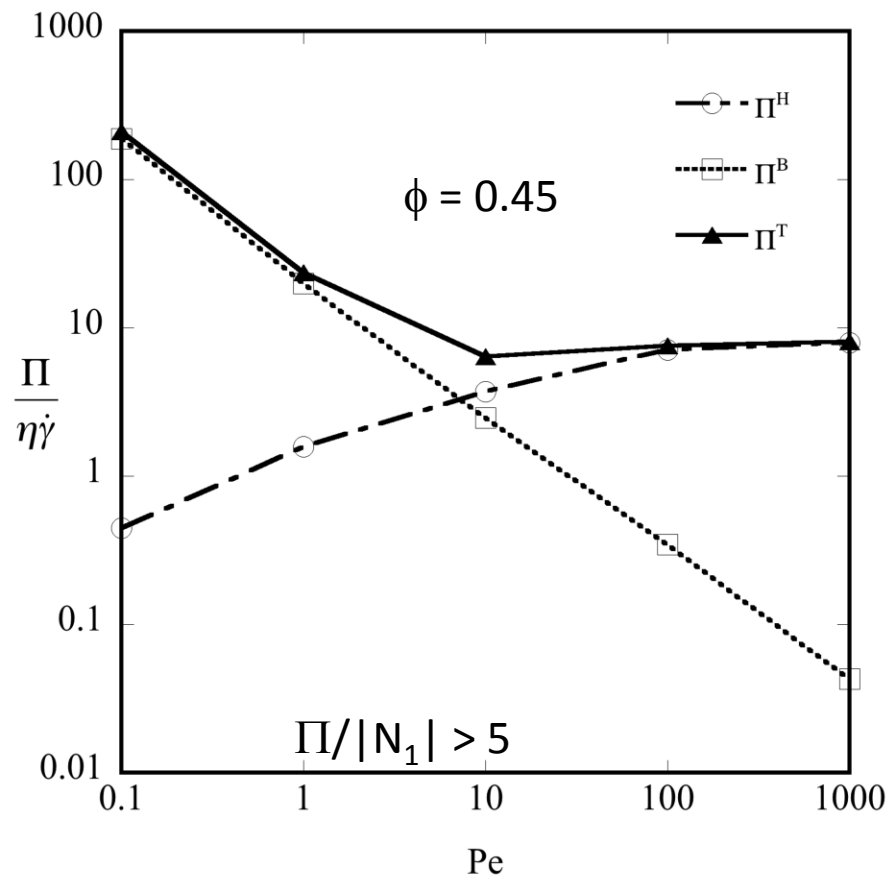
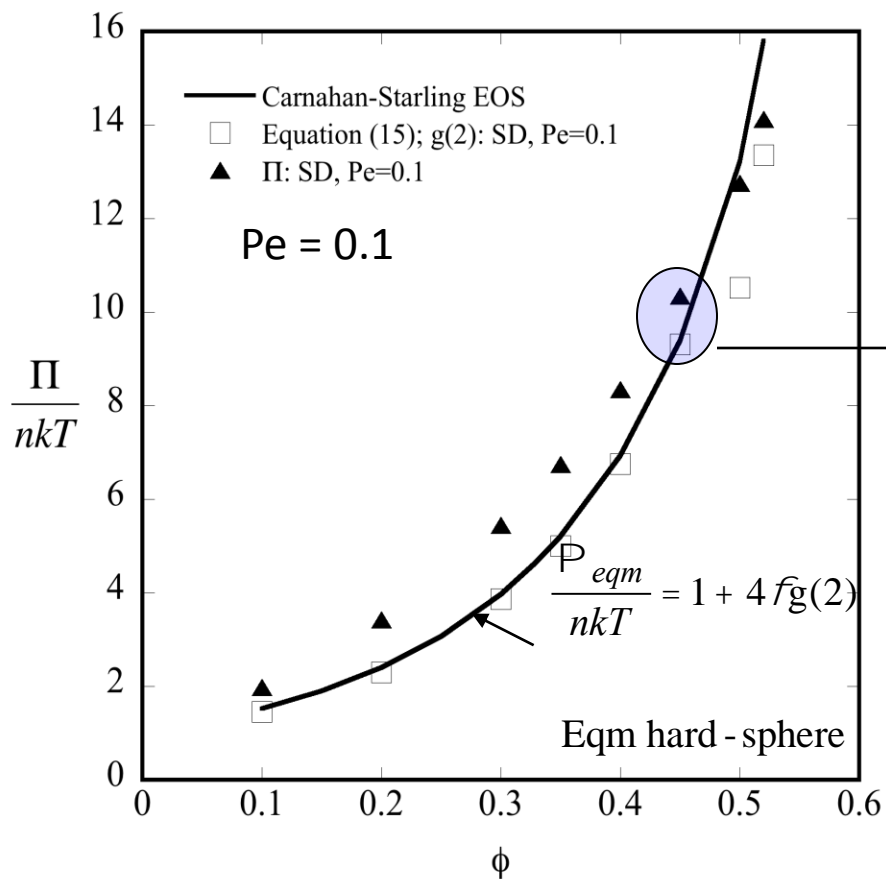
Jeffrey, Morris & Brady *Phys Fluids* 1993

Morris & Katyal *Phys Fluids* 2002

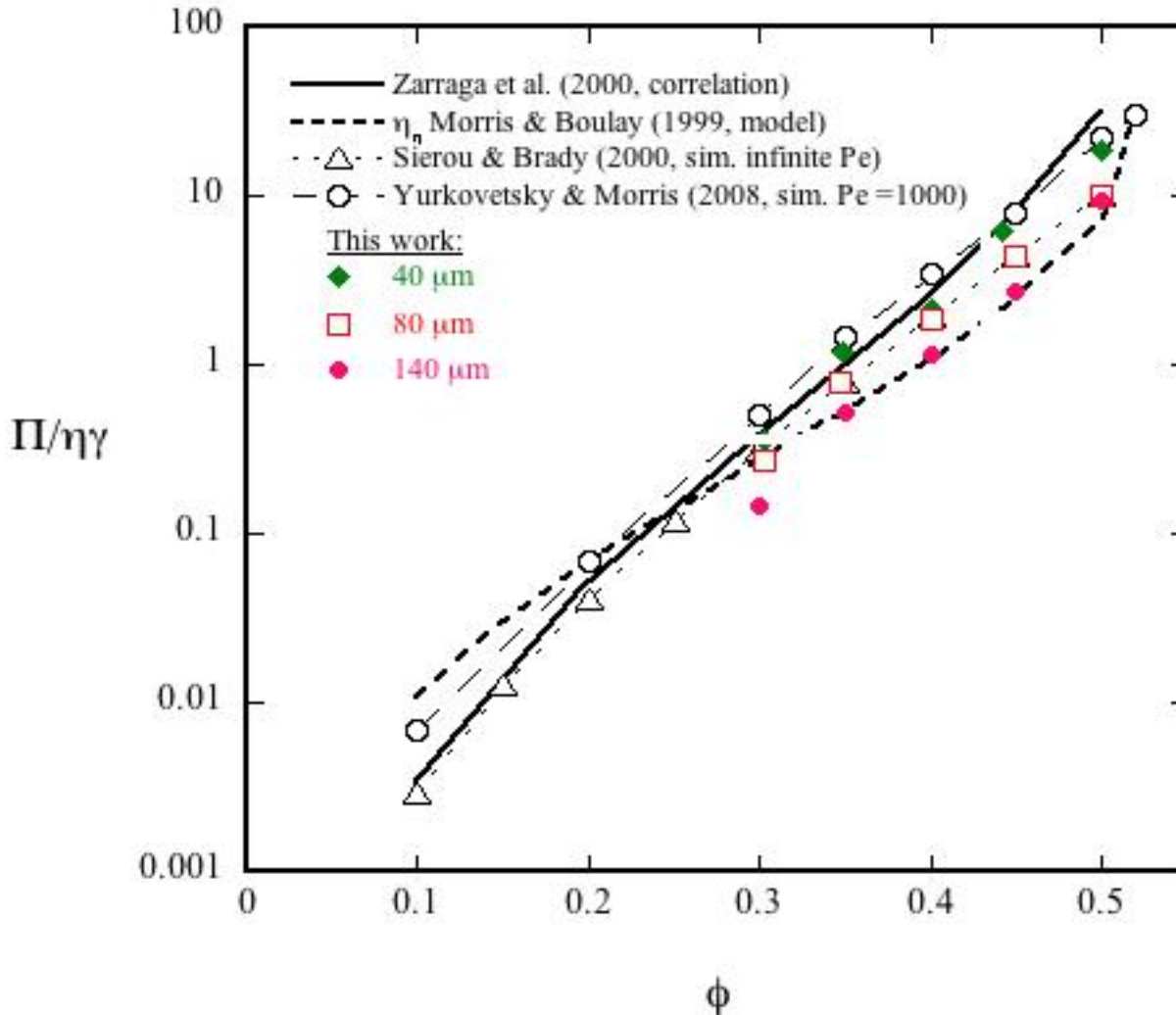
Melrose & Ball *J. Rheol* 2004

Simulation (Stokesian Dynamics) for varying Pe: *osmotic pressure to “viscous dilation”*

Bagnold *Proc. Roy. Soc.* 1954



Simulated and experimental Π



Size dependence:
 due to capillary force limitation:
 Garland *et al. J. Rheol* 2013

$$\Pi_{\max} \approx \frac{\sigma}{a}, \quad \sigma : \text{surface tension}$$

Contact is not essential for particle pressure –
but **it happens

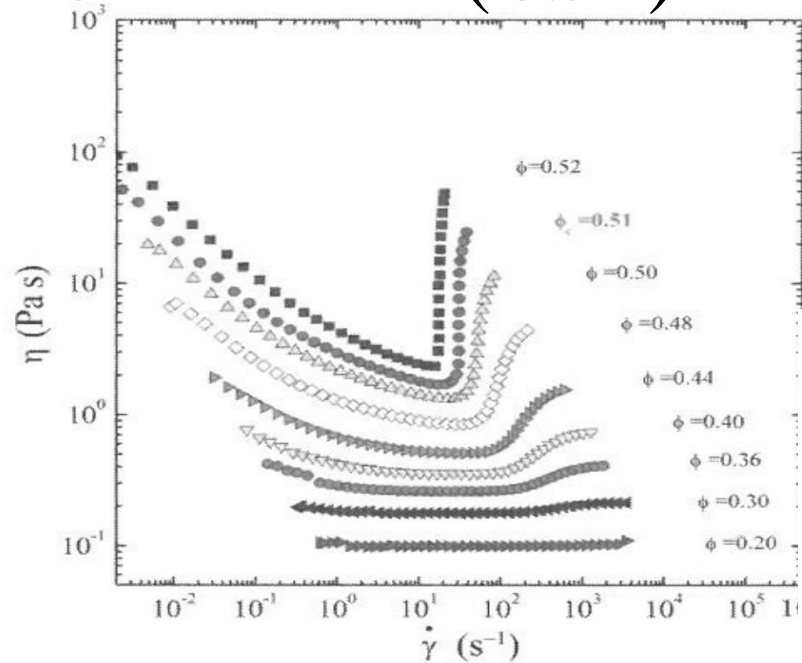
Discontinuous Shear Thickening in frictional particle suspensions

with Ryohei Seto, Romain Mari, Mort Denn

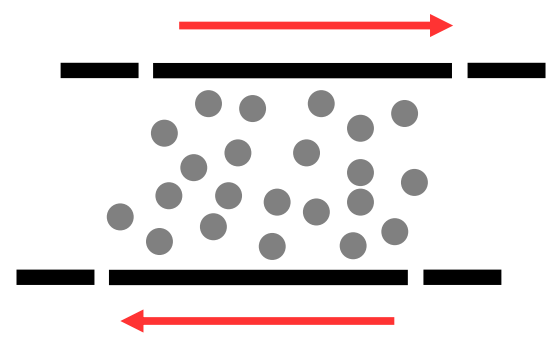
Levich Institute, City College of New York

R. Seto, R. Mari, J. F. Morris & M.M. Denn *PRL* Nov. 2013 (available at ArXiv now)

Shear Thickening: Discontinuous (DST) vs Continuous (CST)

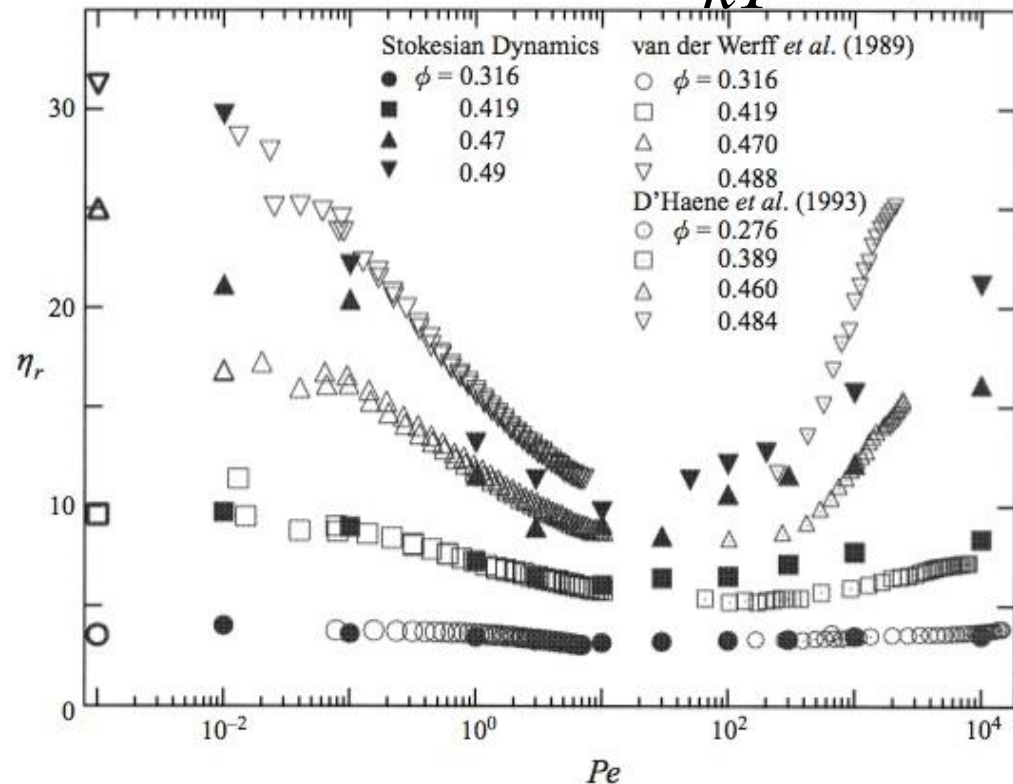


R. Egres, U Delaware



$$\eta(\dot{\gamma}, \phi)$$

$$\eta(Pe \sim \frac{\eta_0 \dot{\gamma} a^3}{kT}, \phi)$$



Foss & Brady *JFM* 2000

Simulation of friction + hydrodynamics

Stokes hydrodynamics

Bidisperse (radius 1 and 1.4)

Short-range HI: lubrication

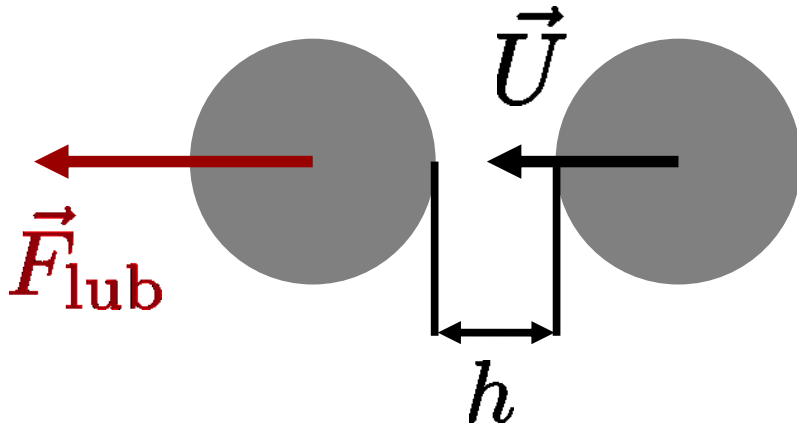
Electrostatic forces

▫ Frictional hard sphere contacts

▫ Roughly speaking--

our model = Stokesian Dyn. - long-range HI + contacts

Contacts?

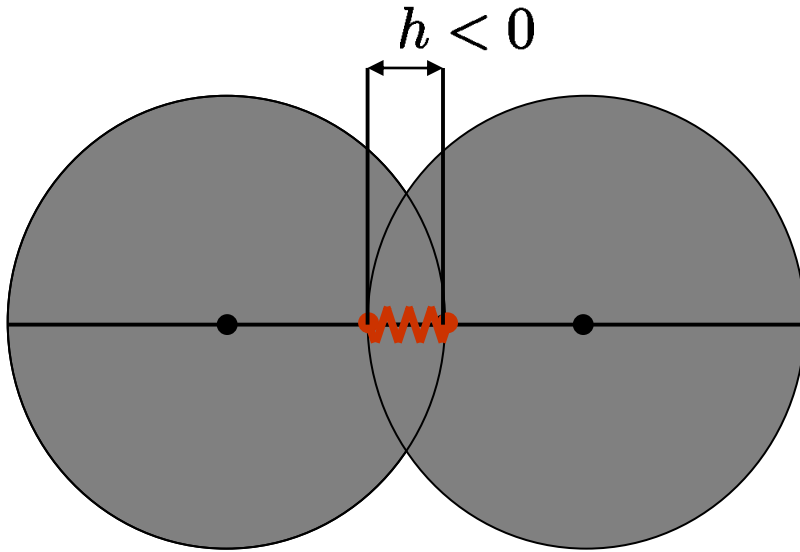


$$\vec{F}_{\text{lub}} = \frac{C}{h + \delta} (\vec{U} \cdot \vec{n}) \vec{n}$$

$$\delta = 10^{-3} \times \text{radius}$$

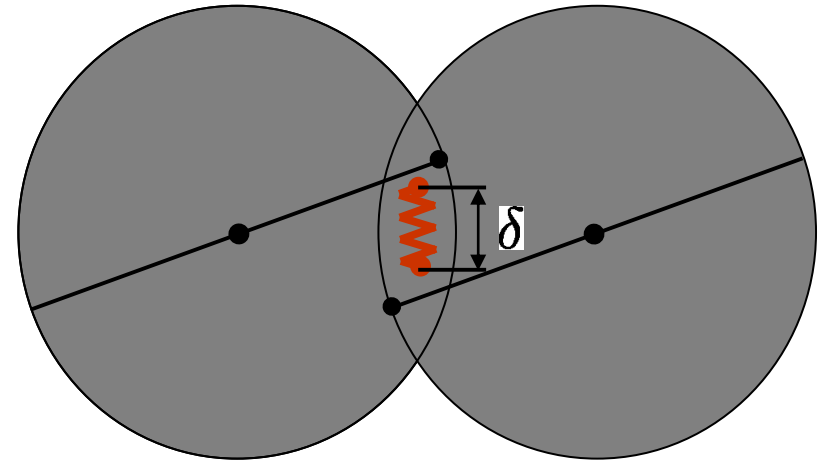
Contacts expected at this scale:
nm physics for micron-scale particles

Contact model



normal:

$$\vec{F}_C^{\text{norm}} = k_n h \vec{n}$$



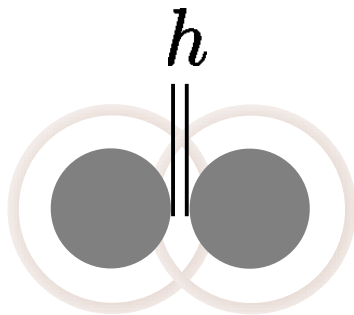
tangential:

$$\vec{F}_C^{\text{tan}} = k_t \delta \vec{t}$$

$$|\vec{F}_C^{\text{tan}}| \leq \mu |\vec{F}_C^{\text{norm}}|$$

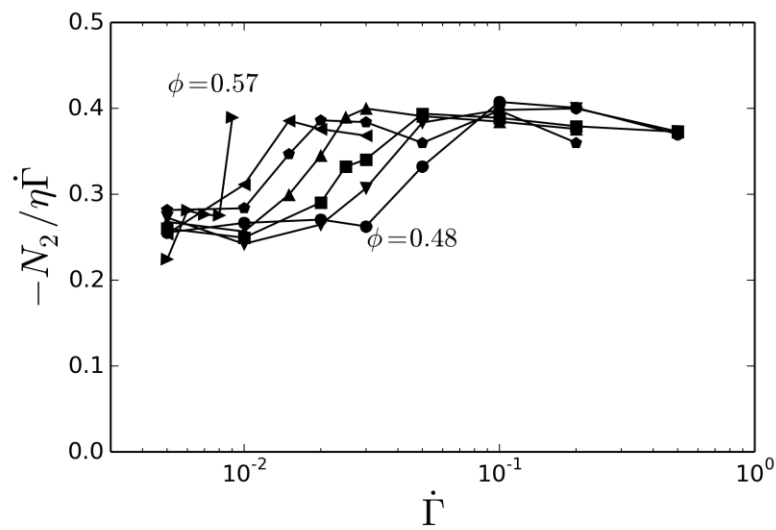
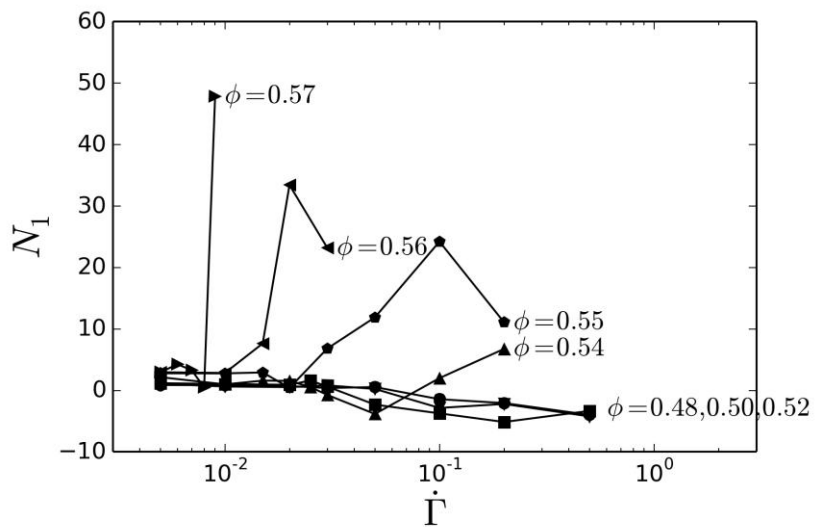
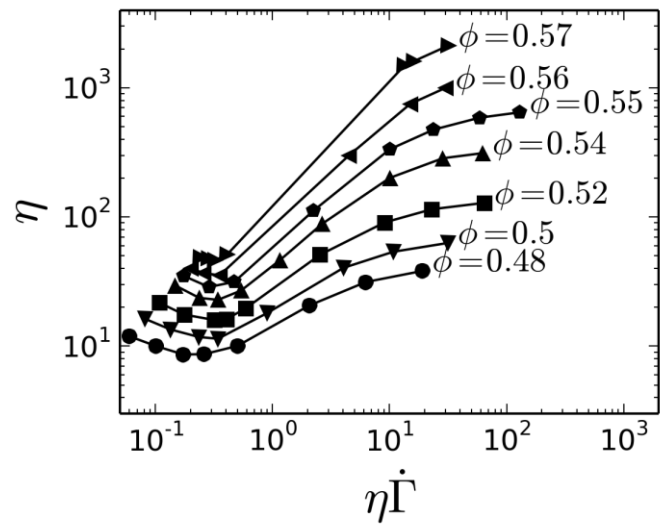
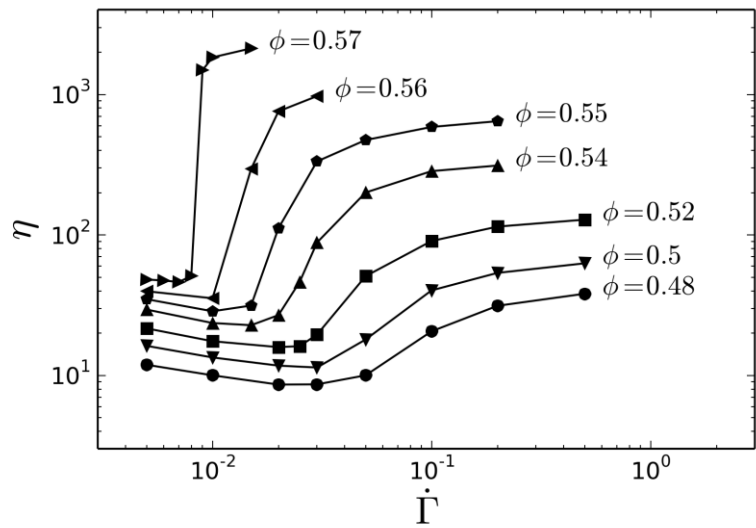
Electrostatic interaction: stabilization

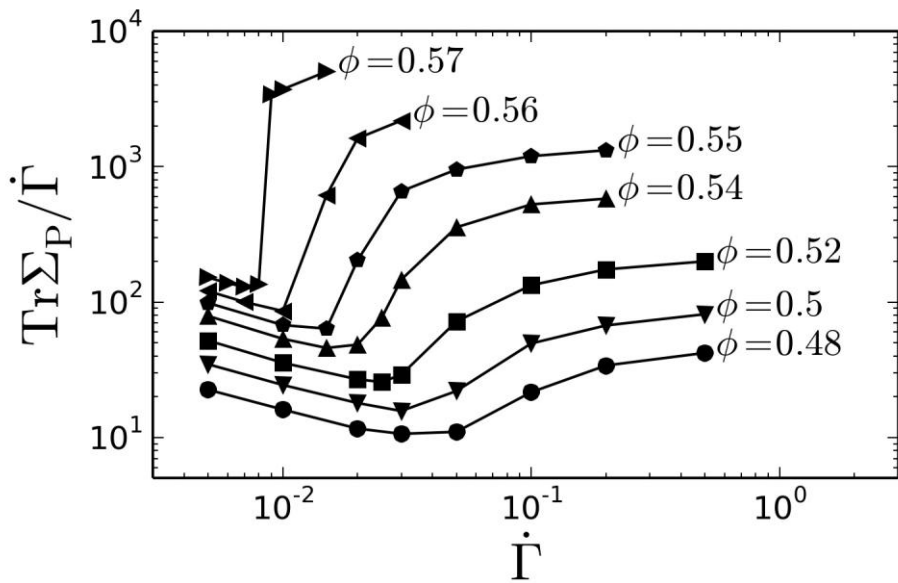
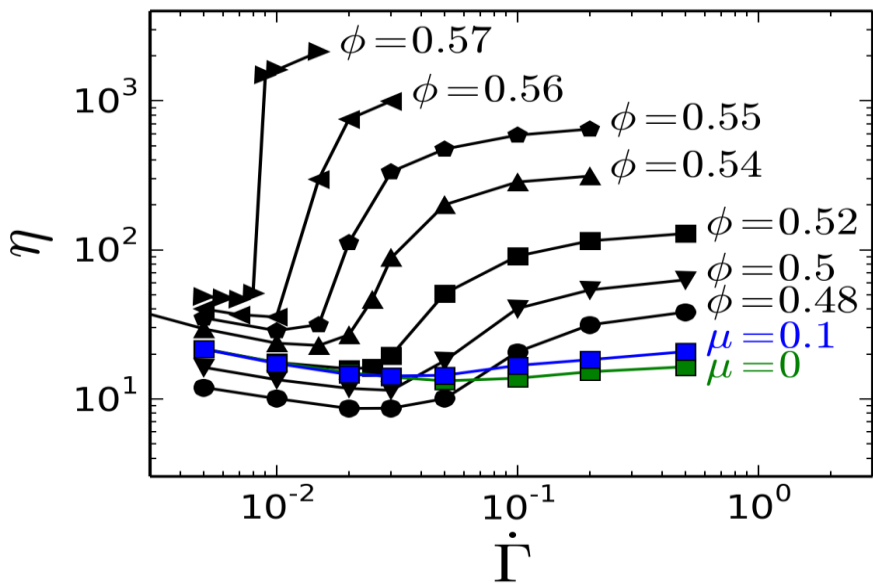
- Stokes hydrodynamics + hard spheres:
- no shear rate dependence
- electrostatic double layer repulsion (colloidal particle model):



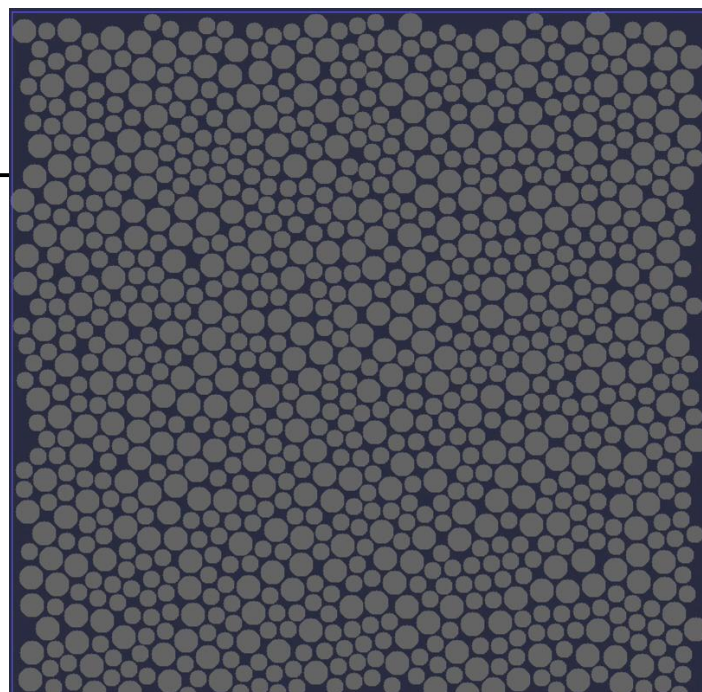
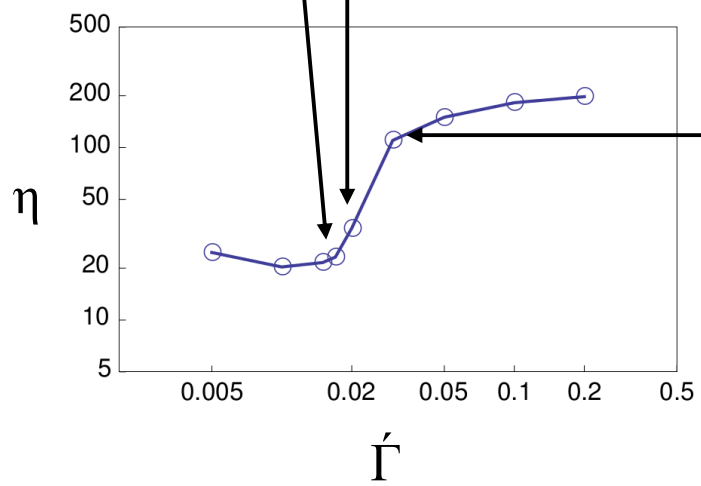
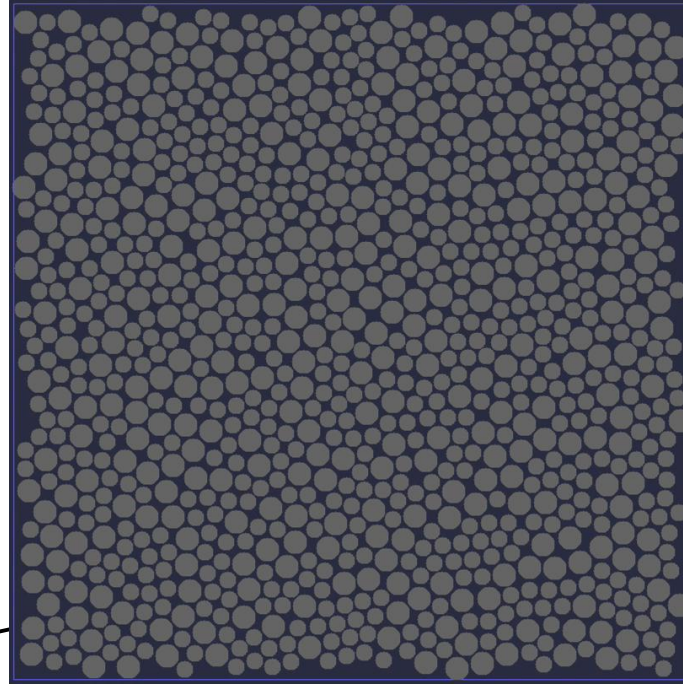
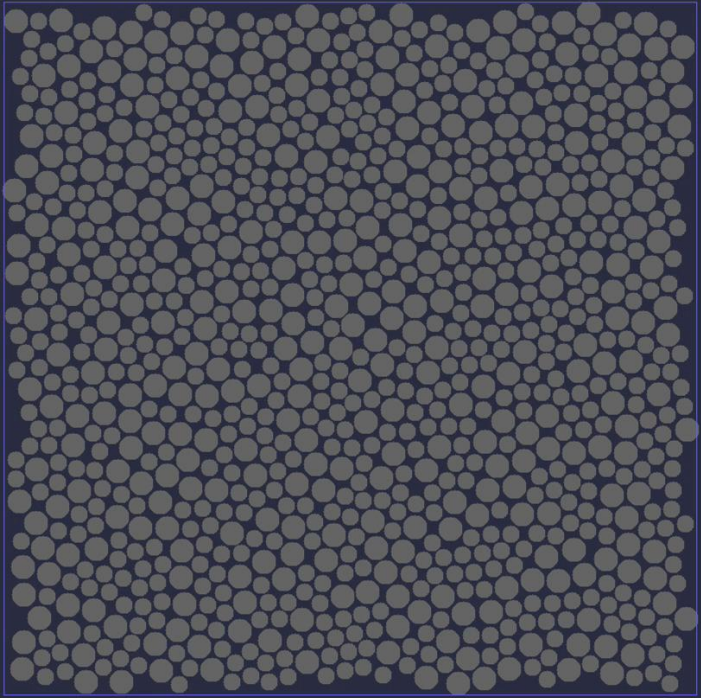
$$F_{\text{el}} = A_{\text{D}} e^{-h/\kappa}$$

$$\dot{\Gamma} = \frac{6\pi\eta_0 a^2 \dot{\gamma}}{A_{\text{D}}}$$



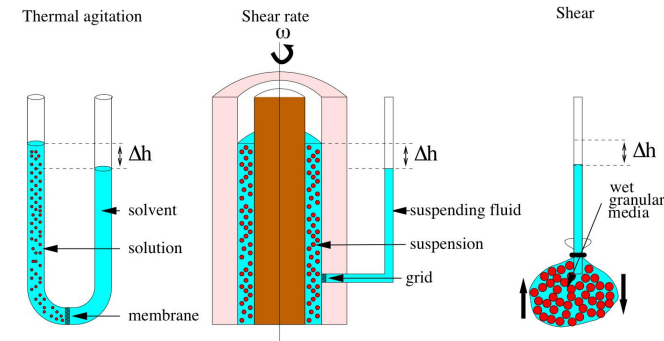


$$\Pi/\dot{\Gamma} = -\text{Tr}\Sigma_p/3$$



SUMMARY

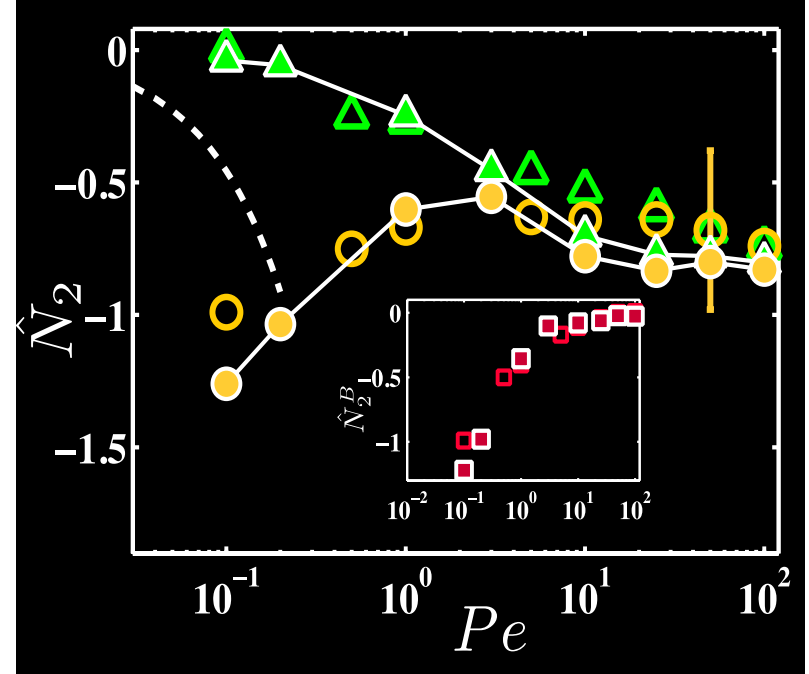
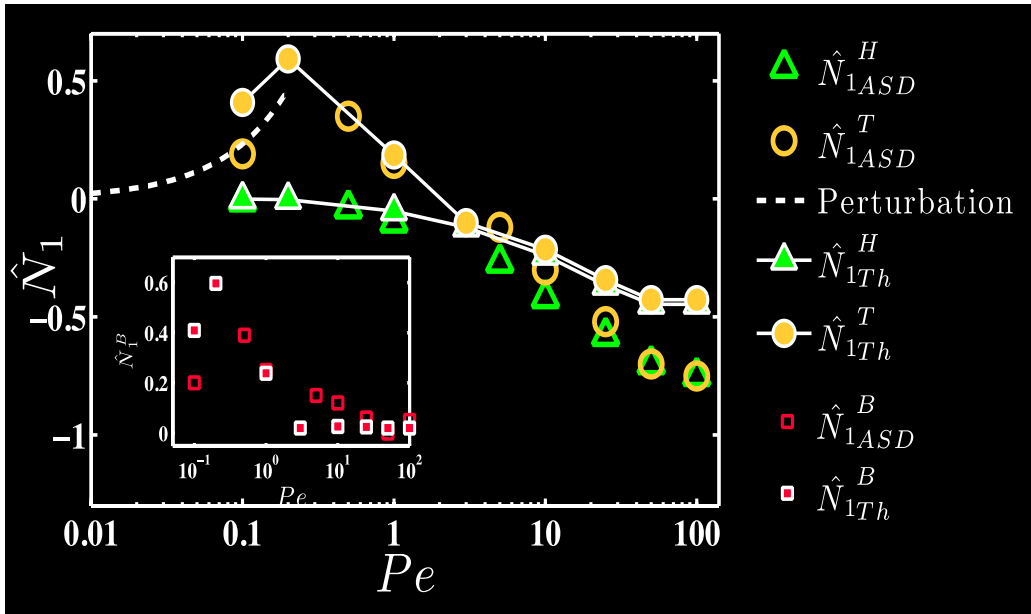
- Two phase mixtures
 - stress active objects (e.g. particles, polymers, ...) migrate
 - driving force can be related to normal stresses
 - two phases are in very different (normal) stress states
- Normal stress plays a key role
 - **Particle pressure**
 - Not an analog of osmotic pressure, but a generalization
 - Connection to granular pore pressure established
 - Feedback to fluid mechanics (through ϕ)
 - **Normal stress differences**
 - velocity effects (secondary flows)
 - Zreben & Ramachandran *PRL* 2013
- **Role of contact forces with hydrodynamics**
 - Simulations show phenomena seen experimentally
 - Next question: what about large-scale flows, with gradients in Π ?



CHALLENGES

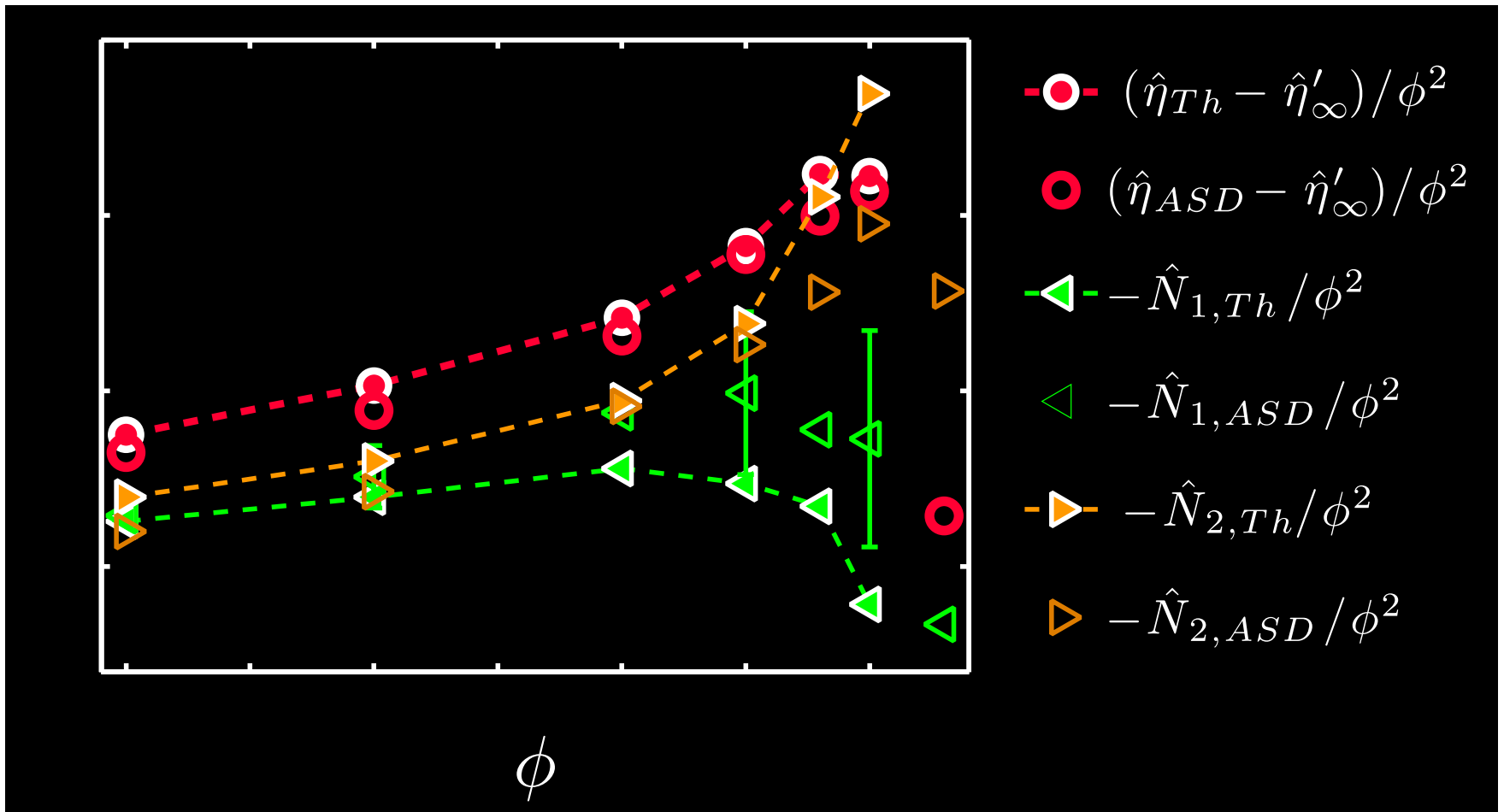
- *Complex geometries*: rheology in general flows
 - Proposed frame-invariant rheology (Miller, Singh & Morris *CES* 2009)
 - More experiments !!
 - Need to explore algorithms
 - Micro-macro coupling (with S. Marenne)

Normal stress differences, $\phi=0.40$



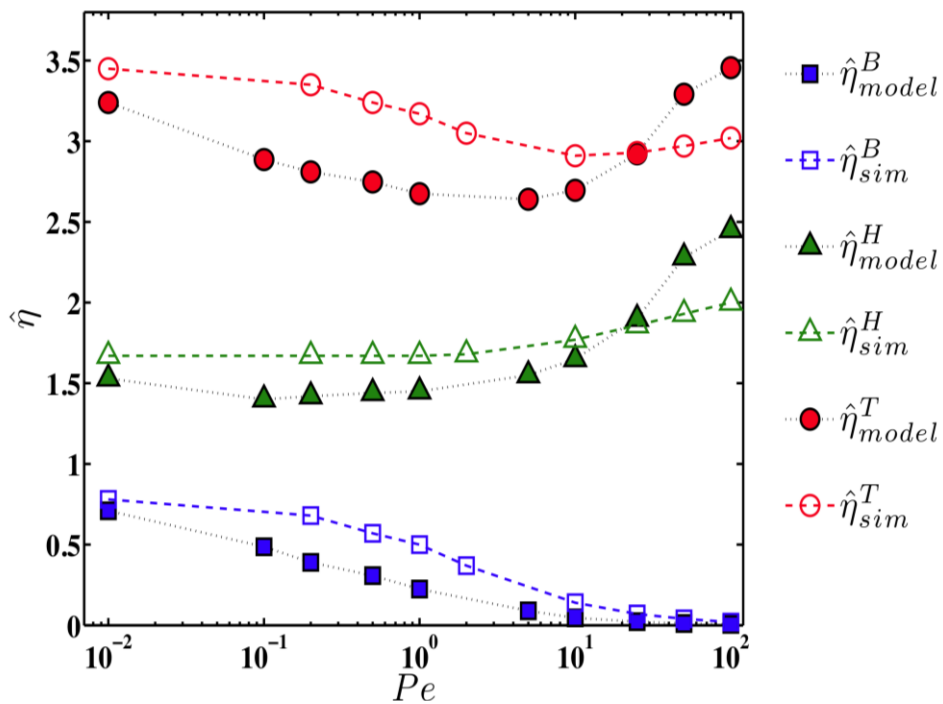
Normalized by $\eta \gamma$

Non-Newtonian Rheology at $Pe = 270$

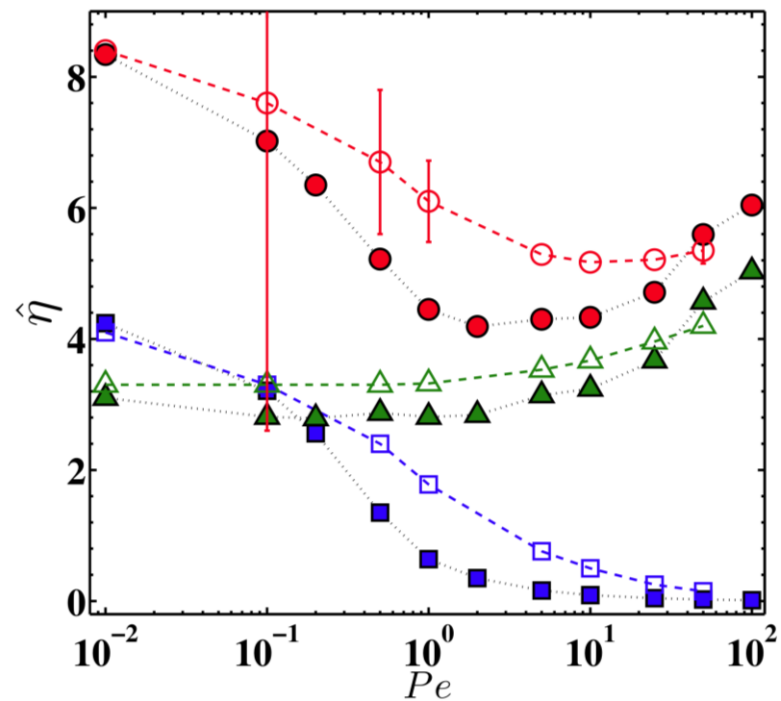


Shear Viscosity

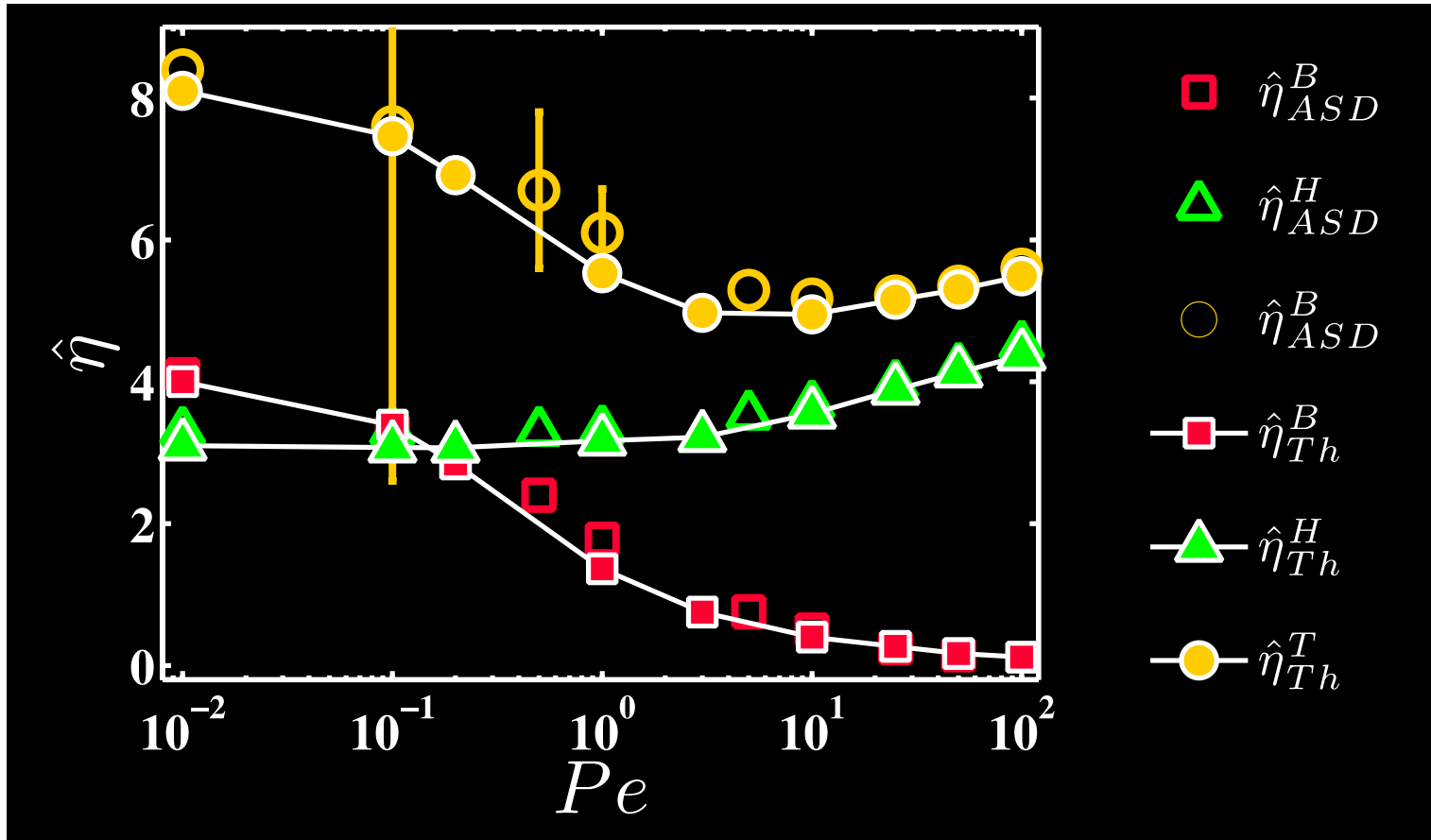
$\phi=0.30$



$\phi=0.40$

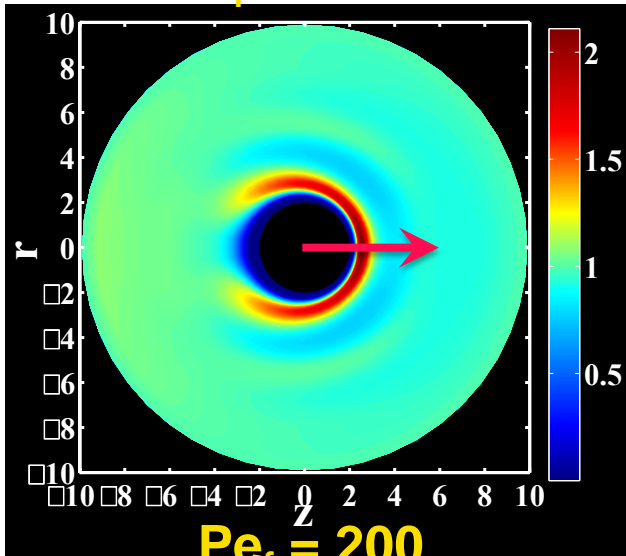


Shear Viscosity, $\phi=0.40$

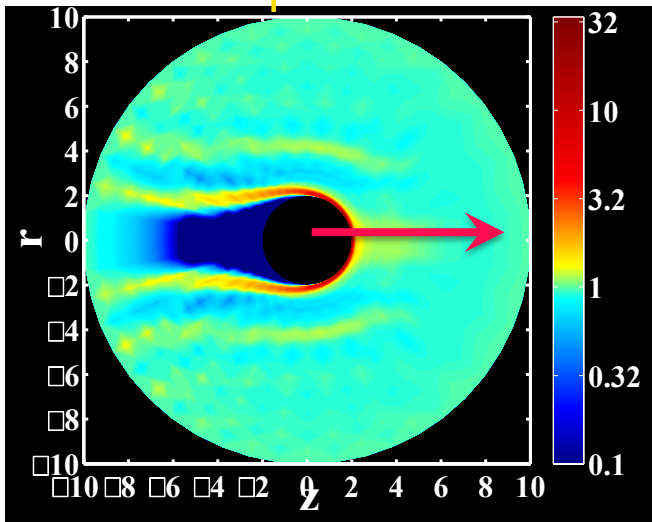


Soft Colloids, Comparison with experiments

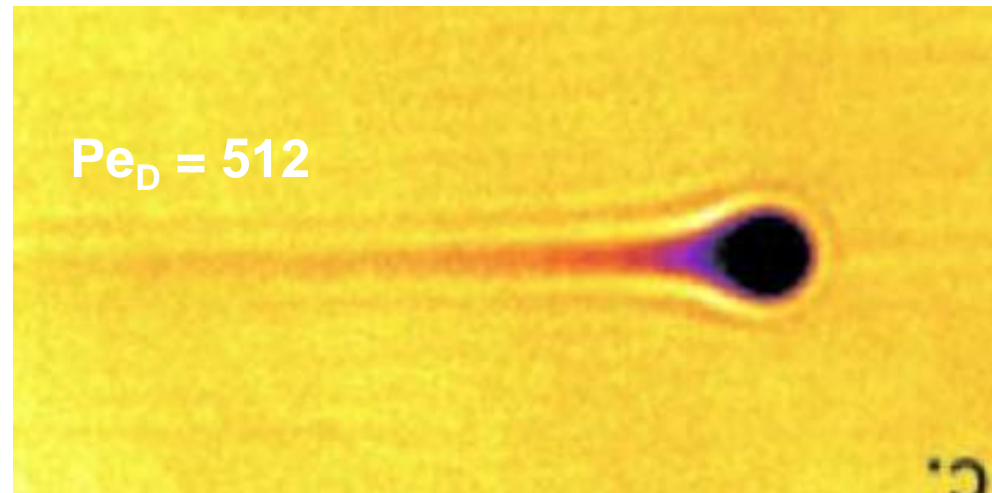
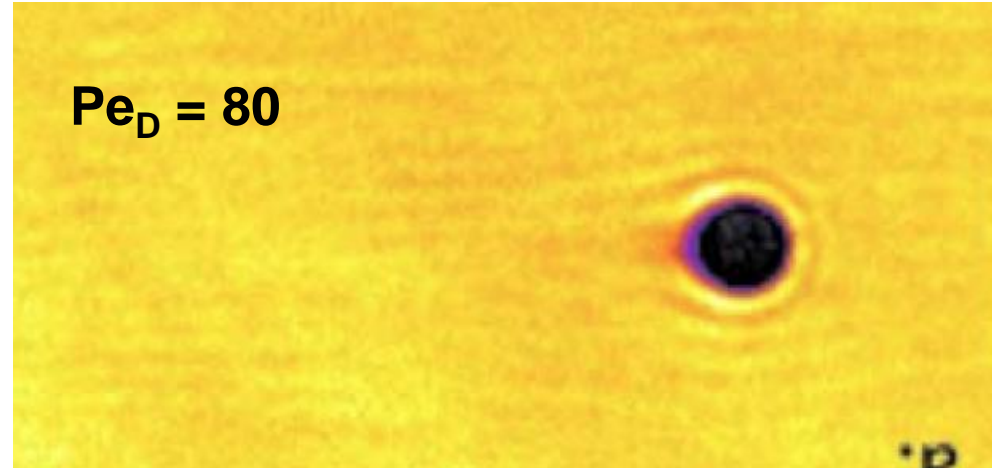
$Pe_f = 25$



$Pe_f = 200$



$2.67Pe_f \approx Pe_D$

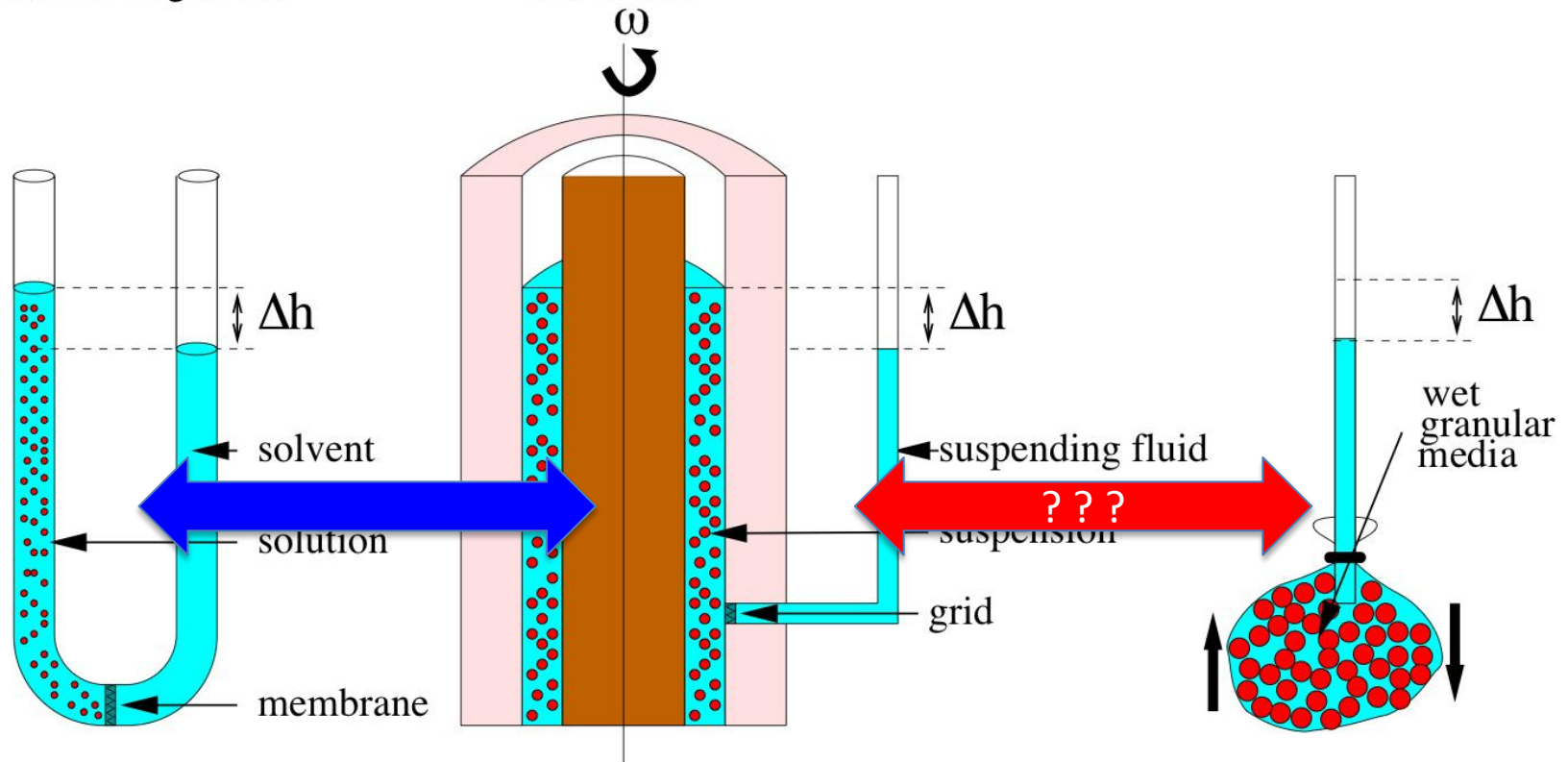


Osmotic pressure to athermal shear-induced particle pressure

Thermal agitation

Shear rate

Shear



Dense suspension flow through a contraction

Noncolloidal suspension :

380-500 μm PS spheres UCON 50-HB-660

Density matched $h_f = 300 \text{ cP}$ at 23°C

→ Very low Reynolds number

Contraction ratio: $\frac{w}{W} = 1/6$ (also $1/3$)

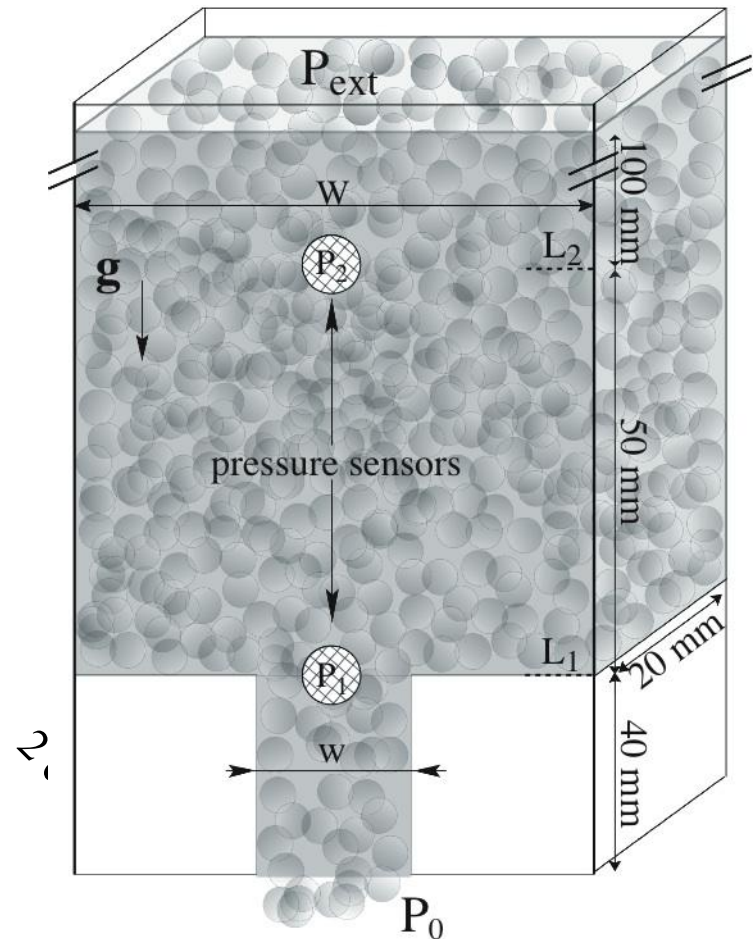
$w/d \sim 10$ (also 20)

Experiments:

Flow visualization at the wall

Liquid pressure measured

Impose ϕ_{in} ; measure effluent ϕ_{out}



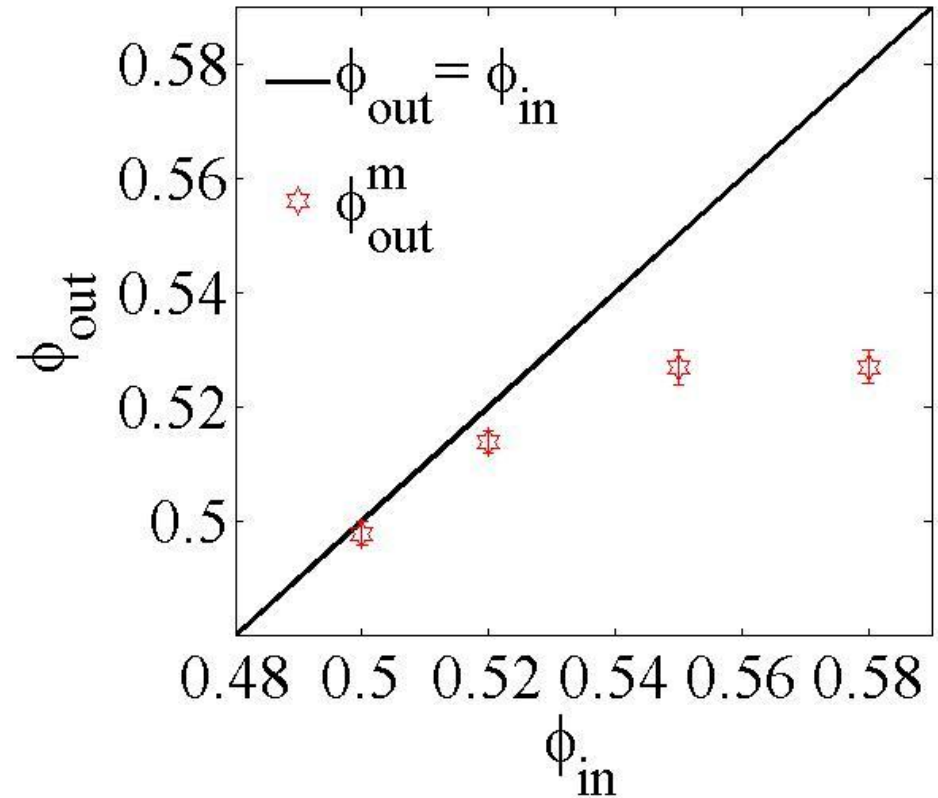
Self-filtration*

$$f_{out}^m < f_{in}$$

$(f_{in} - f_{out}^m) - \text{as } f_{in} -$

Saturation :

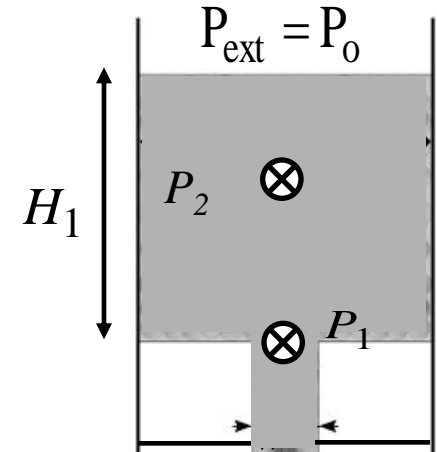
$$f_{in} \approx 0.55, \quad f_{out}^m \approx 0.527 \pm 0.003$$



*Haw *Phys. Rev. Lett.* (2004)

Viscous liquid flow (*sans* particles)

liquid X ($\eta_s = 36.5 \text{ Pa}\cdot\text{s}$), liquid Y ($\eta_s = 7 \text{ Pa}\cdot\text{s}$)



❖ Stokes flow

$$P_1 = \rho g H_1 - \Delta P_1$$

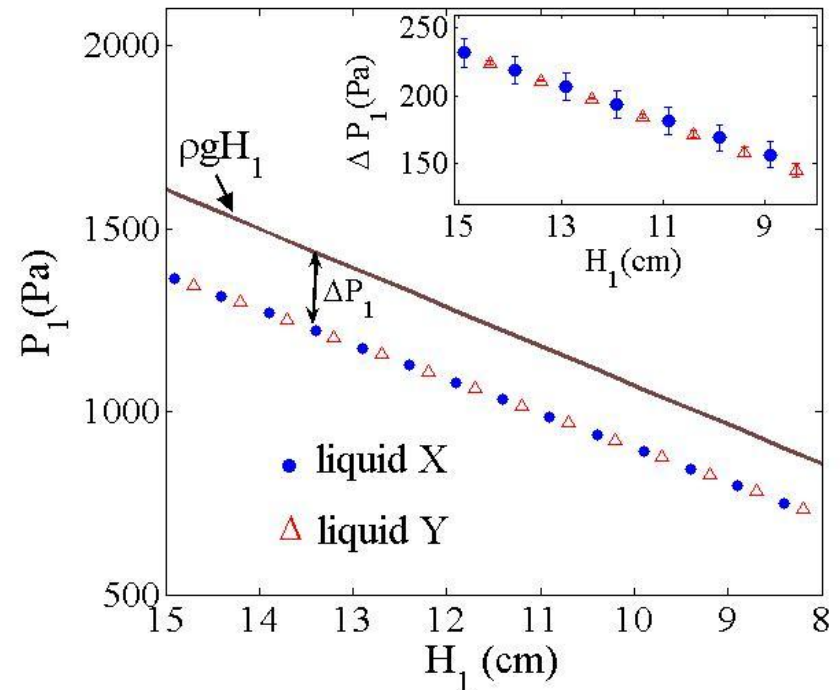
ΔP_1 is independent of the material viscosity

$$\Delta P_1 \propto \eta_s \dot{\gamma} \propto \rho g H_1$$

$$\Delta P_1 = 0.16 r g H_1$$

Likewise:

$$\Delta P_2 = 0.030 r g H_1$$

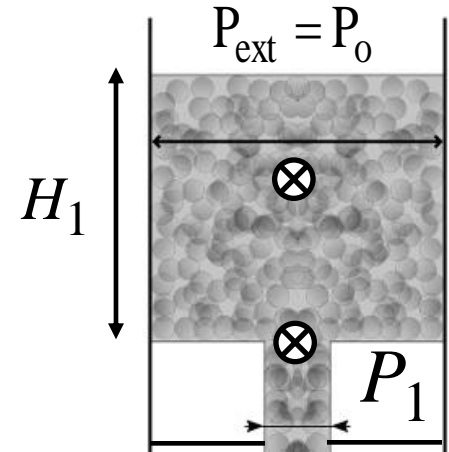


Suspension flow

Experiment:

Liquid pressure *alone* is measured across a screen

For $\phi = 0.50 - 0.58$, $P_1 \downarrow$ as $\phi \uparrow$



ΔP_1 is independent of material viscosity \rightarrow
decrease in P_1 is a two-phase flow phenomenon.

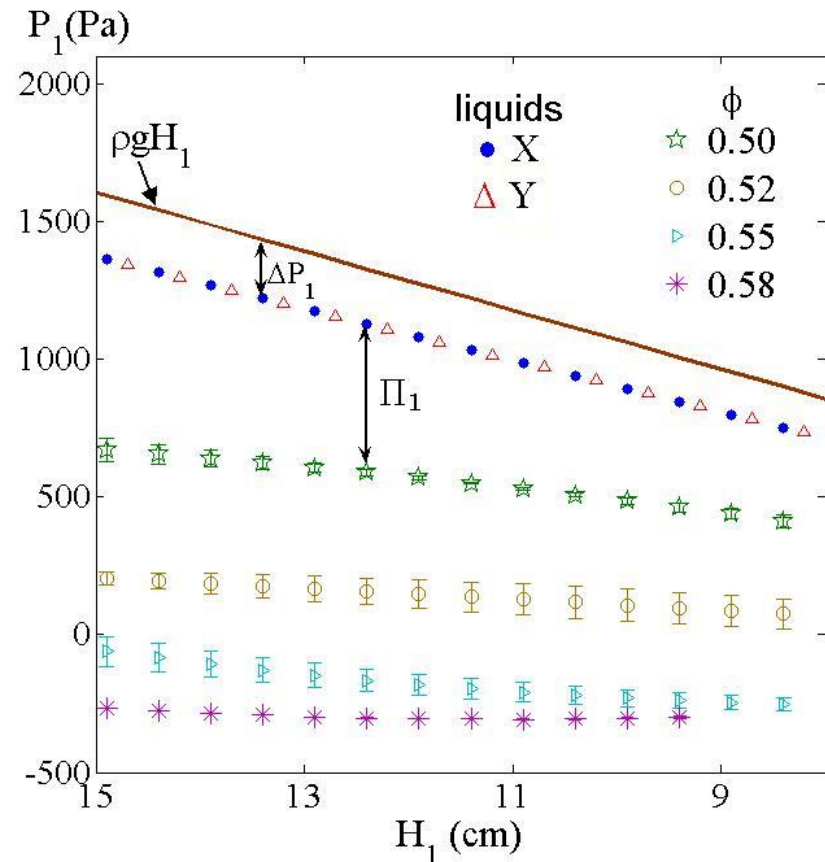
❑ Shearing of suspensions generates suction pressure in the suspending liquid

$$\Pi_{liq} = -\Pi(\dot{\gamma}, \phi)$$

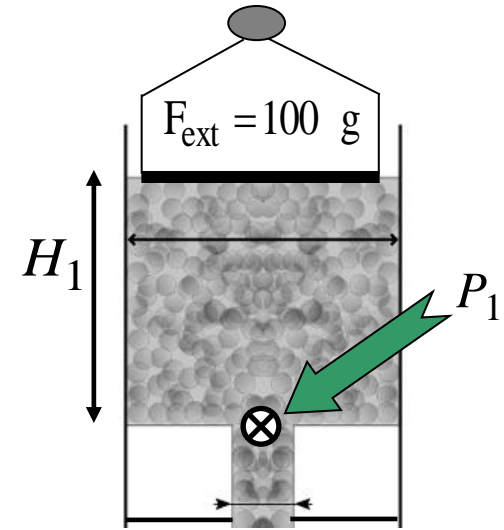
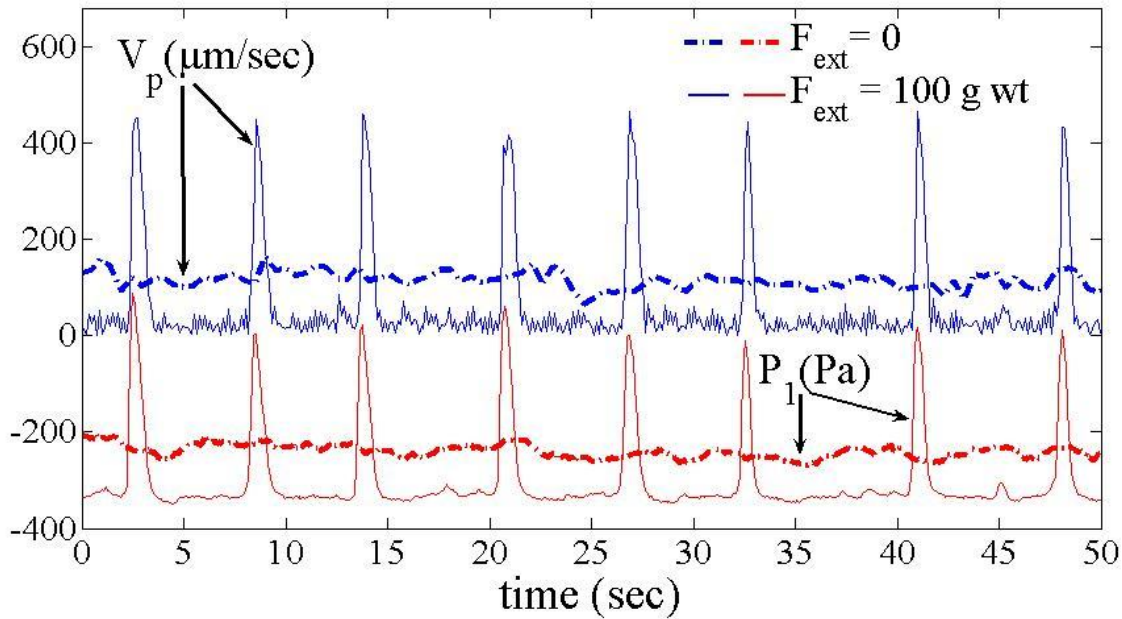
[Yurkovetsky and Morris (2008), Deboeuf *et al.* (2009)]

❑ The expression for P_1 (similarly P_2) is modified:

$$P_1 = \rho g H_1 - \Delta P_1 - \Pi_1$$



Suspension flow under external load



$$f_{in} = 0.58$$

$$f_{out}^m = 0.527 \pm 0.003$$

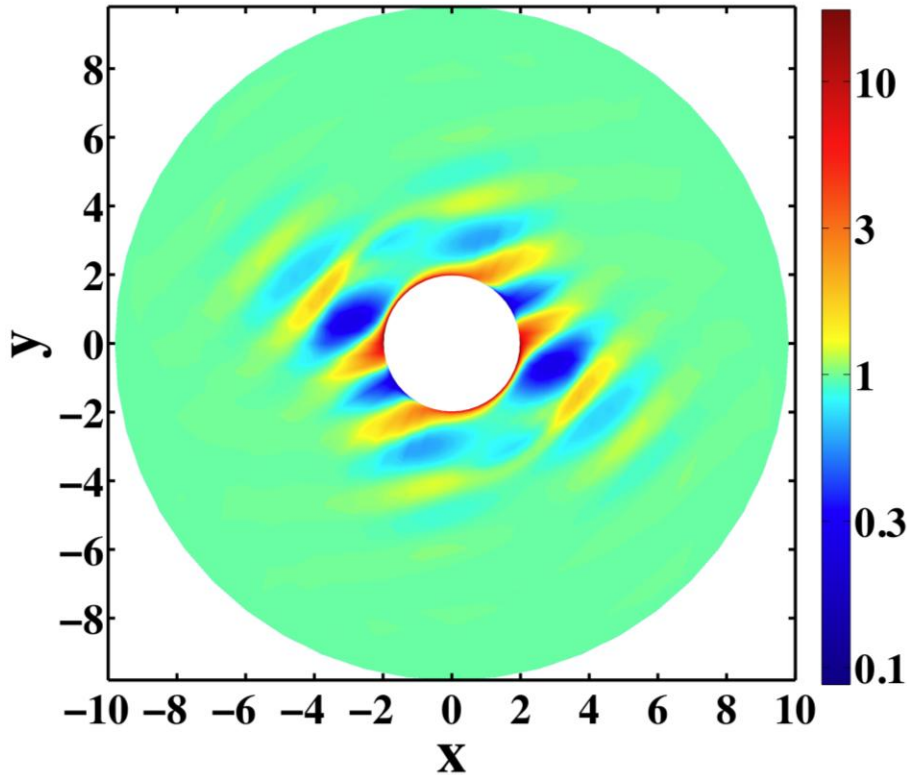
Periodic flow with alternating “fast” and “slow” motions.

V^p in “slow” motion under 100 g load < V^p under no external load.

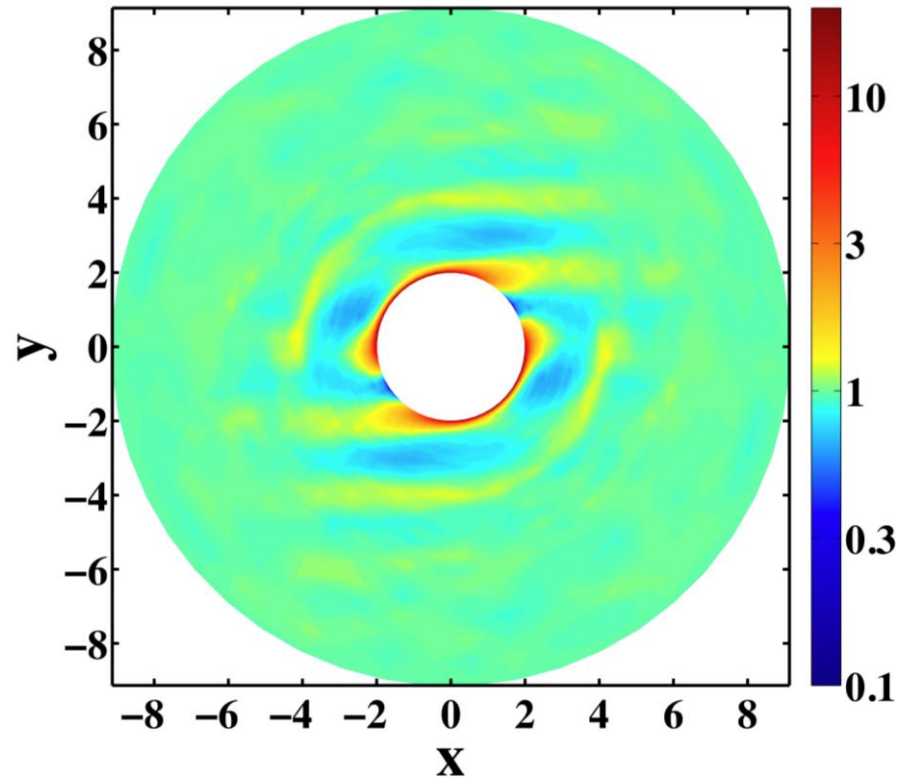
“Slow” motion \leftrightarrow <i>deforming granular network</i>	(decrease in P_1)
“Fast” motion \leftrightarrow <i>suspension flow</i>	(pressure peaks)

Microstructure

Theory, $\phi=0.40$, $Pe=10$



Simulation, $\phi=0.40$, $Pe=10$

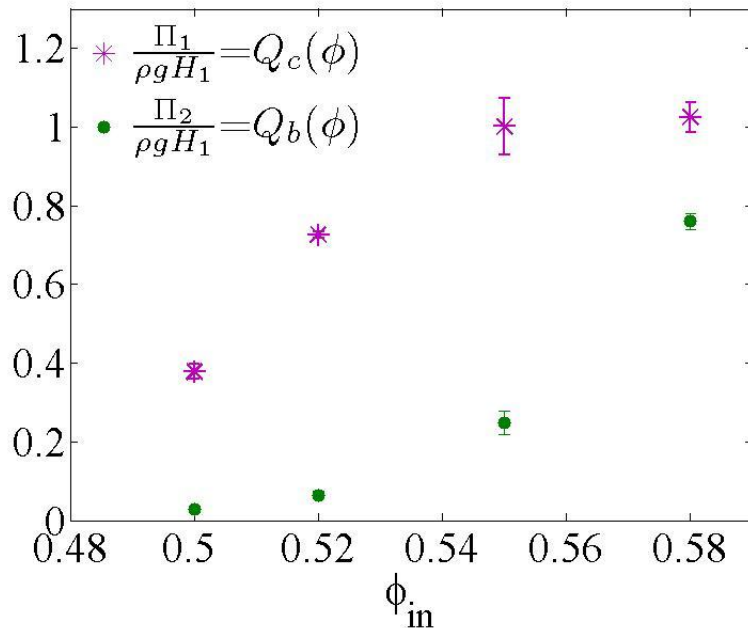


Relating liquid pressure to self-filtration

Combining local rheology $P \propto h_n \dot{\gamma}$ with head dependence $P \propto r g H_1$

$$\frac{P}{r g H_1} = Q(f, x) = K(x) \frac{h_n(f)}{h_s(f)}$$

Specific to geometry

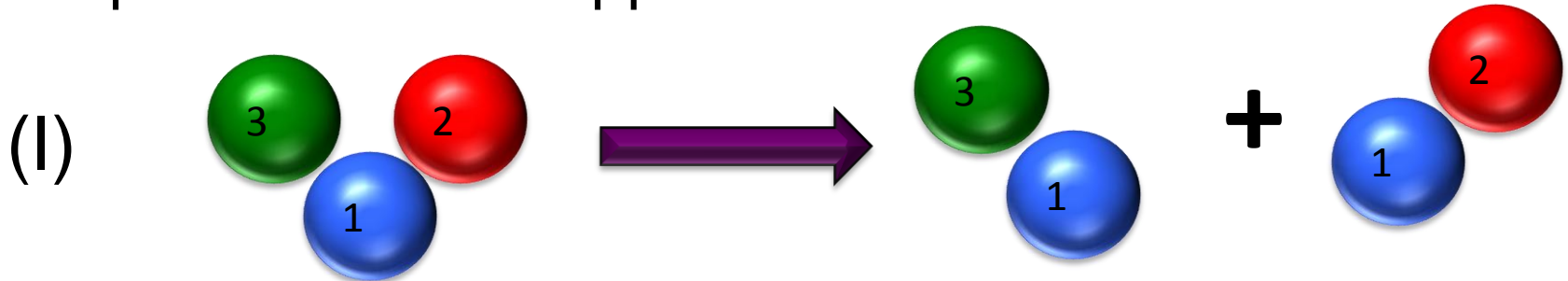


Q_c flattens at high $f_{in} \propto f_c^{-1} f_{in}$

Liquid suction ahead of the particles into contraction.

$f_c (< f_{in})$ remains constant for $f_{in} \gtrsim 0.55$

Simplifications and approximations



Hydrodynamic interactions are summation of pairs near contact

(II) $F^H = F^{\text{EXT}} + F^{\text{HD}} = 0$

F^{EXT} External force driving particles with mean flow

F^{HD} Hydrodynamic/lubrication force imposing the excluded volume

