

# A Variational Multiscale Large Eddy Computational Framework for Numerical Simulations of Turbidity Currents

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COPPE - Federal University of Rio de Janeiro

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# Outline

- Background and Motivation: Turbidity Currents. Sediments and Geological Formations
- Modeling Turbidity Currents : Particle Laden Flows
- Residual Based Variational Multiscale Method LES Formulation for Turbidity Currents
- Computational Simulations
- Final Remarks and Future Steps (*integrating physical models and observational data*)

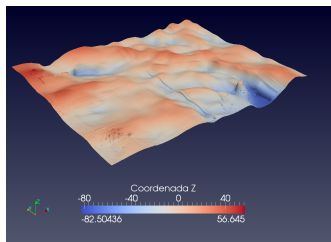
# Background

- Large Scale Algorithms + Petascale Computing push the envelope of Simulation - Based Engineering (SBE) Science
- Confidence (reliability) of simulations predictions make SBE an effective tool
- Uncertainty Quantification + Validation: decision making
- Chain of codes involving high performance computation and a huge amount of data. Need of a efficient control strategy and tools for the analysis of output like provenance catalog and queries within heterogeneous data

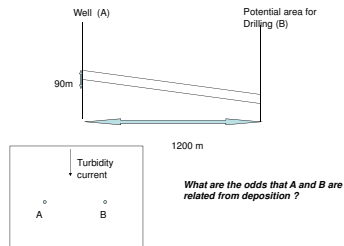
**Our context** : Oil and Gas (and many other) applications: simulation of complex (multiscale - multiphysics) flows

- A large amount of Brazilian oil reservoirs (indeed worldwide) were formed by the action of **Turbidity Currents**;
- Understanding reservoir geological formations may help decision making on reservoir development;
- Most of the studies in this area are still based on experiments or nature observation. Computer simulations might be transformed in an effective tool (at least simulations can help geologists to deeper analyse their theories);
- Highly coupled and non-linear problem: incompressible flow, polydisperse transport, interaction of sand deposition and bottom morphology;
- Room for improvements in turbulence models (RBVMS) and uncertainty quantification (UQ)

# What (oil) Geologists want from simulating turbidity currents?



Deposition map  
sea bottom morphology



Decision about where to drill

# Strategy

We are putting together three pieces:

- High Performance CFD code based on Large Eddy Simulation approach: Residual Based Variational Multiscale Method to model Particle Laden Flows. [Guerra et al, Numerical simulation of particle-laden flows by the residual based variational multiscale method. International Journal for Numerical Methods in Fluids, DOI: 10.1002/flid.3820](#)
- Uncertainty Propagation. Stochastic Collocation [SIAM Conference on Computational Science & Engineering. Boston, 2013](#)
- Scientific Workflows Managing UQ [.Guerra et al.. Uncertainty Quantification in Computational Predictive Models for Fluid Dynamics Using a workflow Management Engine. International Journal for Uncertainty Quantification, v. 2, p. 53-71, 2012.](#)



# NUMERICAL MODEL OF TURBIDITY CURRENTS

## Governing equations

Mathematical setting for the numerical simulation of particle-laden flows within an Eulerian - Eulerian framework:

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} = -\nabla p + \frac{1}{\sqrt{Gr}} \Delta \mathbf{u} + c \mathbf{e}^g \quad \text{in } \Omega \times [0, t_f]$$

$$\nabla \cdot \mathbf{u} = 0 \quad \text{in } \Omega \times [0, t_f]$$

$$\frac{\partial c}{\partial t} + (\mathbf{u} + u_S \mathbf{e}^g) \cdot \nabla c = \nabla \cdot \left( \frac{1}{Sc \sqrt{Gr}} \nabla c \right) \quad \text{in } \Omega \times [0, t_f]$$

where Grashof number expresses the ratio between buoyancy and viscous effects.

$$Gr = \left( \frac{u_b}{\nu H} \right)^2 \quad Sc = \frac{\nu}{\kappa} \quad u_S : \text{settling velocity} \quad c = \frac{C}{C_0} : \text{scaled concentration}$$

boundary condition (bottom) : sediments deposition  $\frac{\partial c}{\partial t} = u_S \frac{\partial c}{\partial z}$   
 and initial conditions  $c(\cdot, 0)$

# Residual Based Variational Multiscale formulation

Differently from traditional LES models, that are built upon spatial filters, RBVMS methods rely on scales splitting of the physical variables combined with variational projections.

The splitting involving the large scales and the fine scales for the present problem are:

$$\begin{aligned}\mathbf{u} &= \mathbf{u}_h + \mathbf{u}' \\ \mathbf{p} &= \mathbf{p}_h + \mathbf{p}' \\ \mathbf{c} &= \mathbf{c}_h + \mathbf{c}'\end{aligned}$$

where the subscript  $h$  denotes the large scale and the superscript  $'$  refers to the subgrid complement.

# Residual Based Variational Multiscale Formulation

Explicit Scales Splitting

$$\mathbf{u} = \mathbf{u}_h + \mathbf{u}' \quad \mathbf{p} = \mathbf{p}_h + \mathbf{p}' \quad \mathbf{c} = \mathbf{c}_h + \mathbf{c}'$$

Weak Form

$$\begin{aligned} & \left( \rho \frac{\partial \mathbf{u}^h}{\partial t}, \mathbf{w}^h \right)_{\Omega} + \left( \rho (\mathbf{u}^h + \mathbf{u}') \cdot \nabla \mathbf{u}^h, \mathbf{w}^h \right)_{\Omega} + (2\mu \varepsilon(\mathbf{u}^h), \varepsilon(\mathbf{w}^h))_{\Omega} - (\tilde{p}_h, \nabla \cdot \mathbf{w}^h)_{\Omega} \\ & \left( \rho \frac{\partial \mathbf{u}'}{\partial t}, \mathbf{w}^h \right)_{\Omega} - \left( \rho \mathbf{u}', (\mathbf{u}^h + \mathbf{u}') \cdot \nabla \mathbf{w}^h \right)_{\Omega} - (2\mu \mathbf{u}', \underbrace{\nabla_h \cdot \varepsilon(\mathbf{w}^h)}_{=0 \text{ for linear elements}})_{\Omega} \\ & + \left( \nabla \cdot \mathbf{u}^h, q^h \right)_{\Omega} - \left( \mathbf{u}', \nabla q^h \right)_{\Omega} - (\rho', \nabla \cdot \mathbf{w}^h)_{\Omega} \\ & \left( (\mathbf{c}_h + \mathbf{c}')(\rho_p - \rho) \mathbf{g}, \mathbf{w}^h \right)_{\Omega} + \left( \mathbf{t}, \mathbf{w}^h \right)_{\Gamma_h} \end{aligned} \tag{1}$$

$$\forall (\mathbf{w}^h, q^h) \in W^h \times P^h$$

# Transport Equation

$$\begin{aligned}
 & \left( \frac{\partial c_h}{\partial t}, v_h \right)_\Omega + ((\mathbf{u}_h + \mathbf{u}' + u_s e^{\mathcal{E}}) \cdot \nabla c_h, v_h)_\Omega + (\tilde{\kappa} \nabla c_h, \nabla v_h)_\Omega \\
 - & \sum_{e=1}^{Nel} (\nabla \cdot (u_h + u' + u_s e^{\mathcal{E}}) c', v_h)_{\Omega_e} + \underbrace{(u_h + u' + u_s e^{\mathcal{E}}) \cdot \nabla v_h, c'}_{\text{SUPG like}}_{\Omega_e} \\
 & + \sum_{e=1}^{Nel} \underbrace{(\tilde{\kappa} c', \Delta v_h)_{\Omega_e}}_{\text{vanishes for linear elements}} = 0
 \end{aligned}$$

## Sub-grid Modeling (designed based on numerics reasoning)

Fine Scale Approximation (static hypothesis - residuals of the balance equations)

$$\rho' = \tau_c \rho R_c = \nabla \cdot \mathbf{u}^h$$

$$u' = \frac{\tau_m}{\rho} R_m = -\rho \frac{\partial \mathbf{u}^h}{\partial t} - \rho (\mathbf{u}^h + \mathbf{u}') \cdot \nabla \mathbf{u}^h + \nabla \cdot (2\mu \varepsilon(\mathbf{u}^h)) - \nabla \tilde{p}_h + c(\rho_p - \rho) \mathbf{g}$$

$$c' = \tau_t R_t = -\frac{\partial c_h}{\partial t} - (u_h + u' + u_s \mathbf{e}^g) \cdot \nabla (c_h) + \tilde{\kappa} \nabla^2 (c_h)$$

$$\tau_m = \left( \left( \frac{2}{\Delta t} \right)^2 + \left( c_1 \frac{\|u^h\|}{h_e} \right)^2 + \left( c_2 \frac{\nu}{h_e^2} \right)^2 \right)^{-\frac{1}{2}} \quad \tau_c = \frac{h_e}{3} \|u^h\|$$

$$\tau_t = \left( \left( \frac{2}{\Delta t} \right)^2 + \left( c_1 \frac{\|u^h\|}{h_e} \right)^2 + \left( c_2 \frac{k}{h_e^2} \right)^2 \right)^{-\frac{1}{2}}$$

# Our Software Playground

EdgeCFD is a parallel and general purpose CFD solver developed at UFRJ with the following main characteristics:

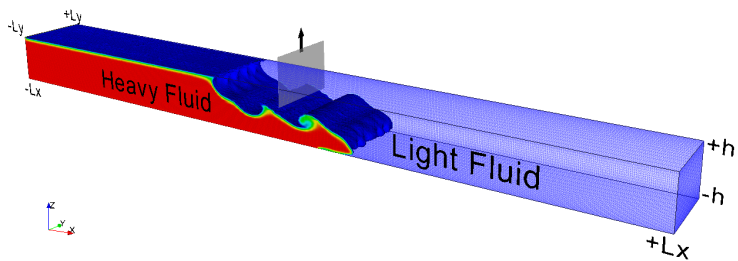
- Edge-based data structure;
- Hybrid parallel (MPI, OpenMP or both);
- Low Order Finite Elements; Unstructured Meshes
- Staggered Multiphysics solver strategies;
- SUPG/PSPG/LSIC FEM formulation for incompressible flow;
- RBVMS or Smagorinsky turbulence treatment;
- u-p fully coupled solver;
- RB-VMS + shock capturing for multiple advection-diffusion eq.;
- Free-surface flows (VOF and Level Sets);
- Adaptive time step control;
- Inexact-Newton solvers;

R.N.Elias, P.L.B. Paraizo and A.L.G.A. Coutinho. *Stabilized edge-based Finite element computation of gravity currents in lock-exchange configurations*. International Journal for Numerical Methods in Fluids, 2008.

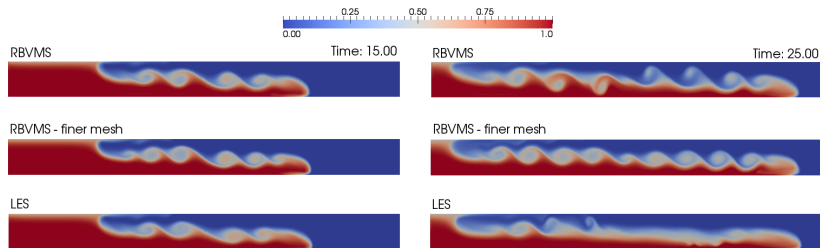
## COMPUTATIONAL SIMULATIONS



# Lock-Exchange Scenario



# Lock-Exchange



**Figure:** Side view: Concentration field at  $t = 15$  and  $t = 25$  for different spatial discretizations for  $Gr = 1.5 \times 10^6$ .

# Lock-Exchange

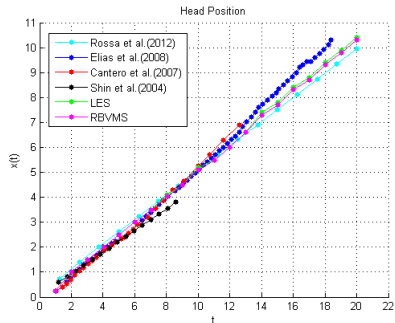
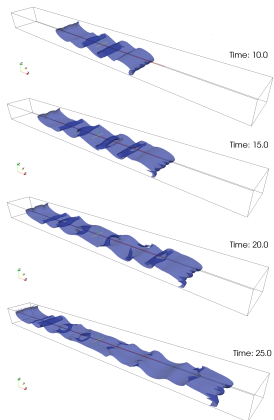


Figure: Evolution of the fluids interface

# Lock-Exchange

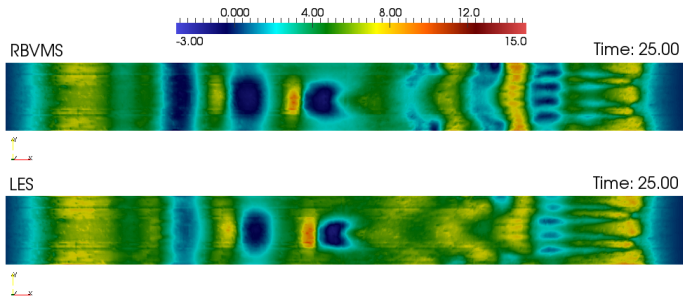
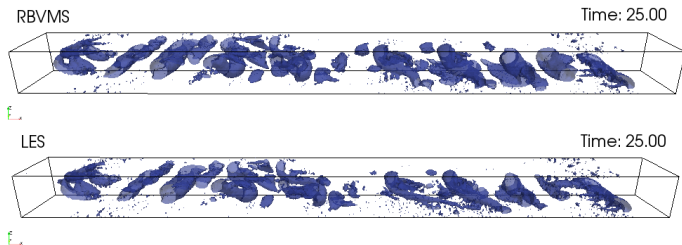


Figure: Non-dimensional shear stress at the bottom

# Lock-Exchange



**Figure:** View of vortical structures, Q-criterion iso-surfaces ( $Q=0.3$ ).

# Lock-Exchange $Gr = 9.0 \times 10^7$

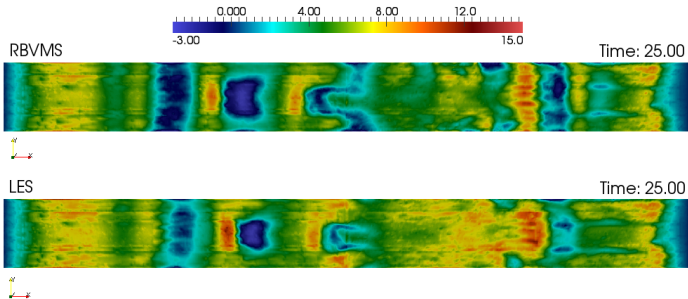


Figure: Top view: shear stress distribution at the bottom

# Lock-Exchange ( deposition) $Gr = 1.0 \times 10^8$

Time evolution of the concentration field

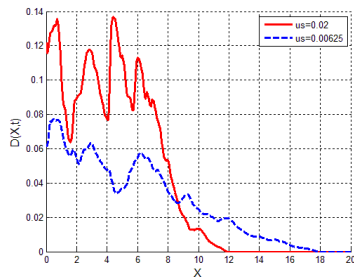
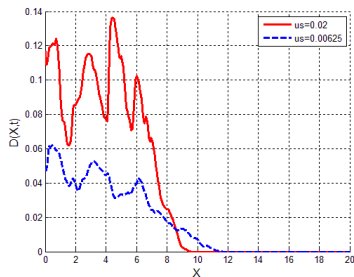
Lock-Exchange –  $Gr = 1.0 \times 10^8$ 

Figure: Deposit profile at the middle plane:  $t=25$  (left) and  $t=50$  (right)



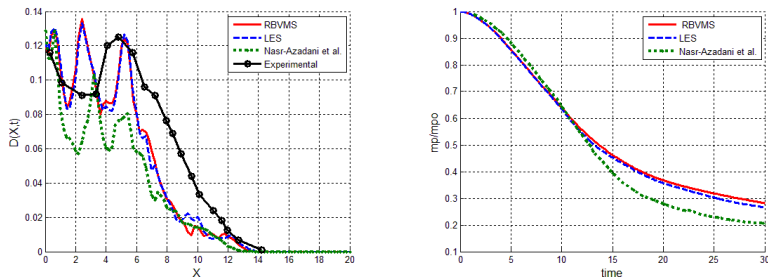
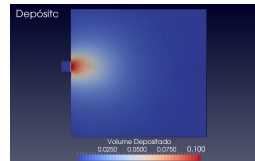
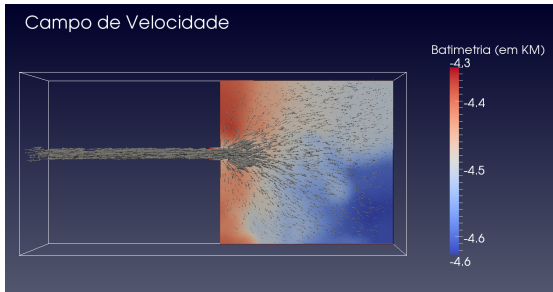
Lock-Exchange –  $Gr = 1.0 \times 10^8$ 

Figure: Deposit map profile (left) and mass along time (right), comparison among experiments and numerical simulations

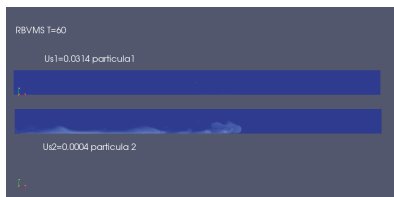
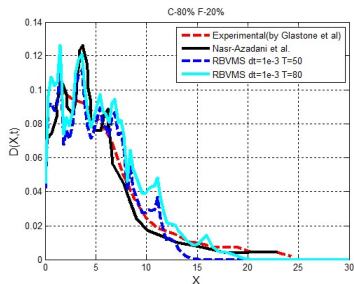
# Subgrid Modeling

# Sustained Flow and Complex Bottom Topography (prelimary results)



## POLYDISPERSE FLOWS

# Polydisperse flow: Coarse 80% and Fine 20%



**Figure:** Depositon map profile (left) and mass along time (right), comparison among experiments and numerical simulations

Ref.: M.M. Nasr-Azadani, B.Hall, E.Meiburg. Polydisperse turbidity currents propagating over complex opography: Comparison of experimental and depth-resolvedsimulation results. *Computer & Geosciences* (53), 141 – 153, 2013.

Tank Configuration –  $Gr = 1.0 \times 10^8$  (preliminary results)

## ALE (FSI) FORMULATION FOR MORPHODYNAMICS





## UNCERTAINTY QUANTIFICATION

# General Aspects

- Model uncertainty (epistemic), numerical errors, uncertainty in parameters (initial conditions, physical constants...), all of them interacting and compromising the simulations reliability
- Verification and Validation (V&V) and Uncertainty Quantification (UQ)
- Probabilistic Perspective : parameters modeled as random variables or fields. Looking for a PDF instead of a point solution
- Governing Equations represented by Stochastic Partial Differential Equations

# Mathematical Preliminaries

To quantify the uncertainty in a system of differential equations we adopt a probabilistic approach.

Definition: Complete probability space  $(\Omega, \mathcal{F}, \mathcal{P})$

- $\Omega$  is a event space,
- $\mathcal{F} \subset 2^\Omega$  is the  $\sigma$ -algebra of subsets in  $\Omega$
- $\mathcal{P} : \mathcal{F} \rightarrow [0, 1]$  is the probability measure

In this framework, the uncertainty in a model is introduced by representing the input data (parameters, geometry, boundary and initial condition) as random fields.

# Mathematical Preliminaries

For a general differential equation defined on  $\mathcal{D} \subset \mathbb{R}^d$ ,  $d = 1, 2, 3$  with boundary  $\partial\mathcal{D}$ . The problem consists on find a stochastic function,  $\mathbf{u} \equiv \mathbf{u}(\omega, \mathbf{x}) : \Omega \times \mathcal{D} \longrightarrow \mathbb{R}$ , such that, for everywhere  $\omega \in \Omega$ , (**Main idea: uncertainty as an extra stochastic dimension**)

## Governing Stochastic Equations

$$\begin{aligned}\mathcal{L}(\omega, \mathbf{x}; \mathbf{u}) &= f(\omega, \mathbf{x}) & \mathbf{x} \in \mathcal{D} \\ \mathcal{B}(\omega, \mathbf{x}; \mathbf{u}) &= g(\omega, \mathbf{x}) & \mathbf{x} \in \partial\mathcal{D}\end{aligned}$$

with  $\mathbf{x} = (x_1, \dots, x_d) \in \mathbb{R}^d$ ,  $d \geq 1$ , the space coordinates.

# Numerical methods

## ■ Intrusive Methods

- Polynomial Chaos + Galerkin Formulation

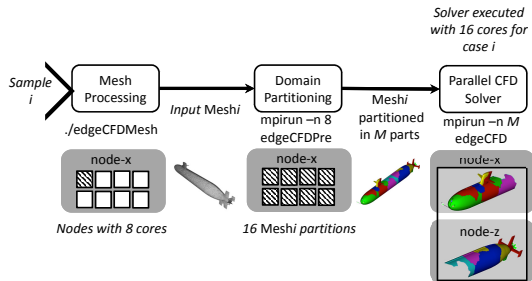
## ■ Non-Intrusive Methods

- Sampling: Monte Carlo, Quasi MC, LHS
- **Stochastic Collocation** : Polynomial Chaos, Quadratures or Polynomial interpolation
- Bayesian Surrogates and Gaussian Process Modeling

# Scientific Workflows supporting High Performance Computing

- Scientific/Engineering Computational Experiments Modeled as Scientific Workflows
- Simulations generate a lot of data: understanding how to manage and query simulation data in runtime
- Track who performed the computational experiment and who is responsible for its results Provenance data is automatically registered by SWfMS

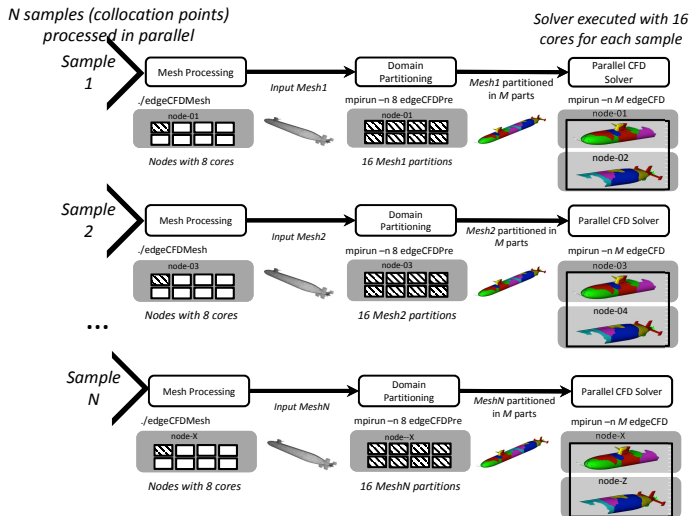
# Provenance



Chiron is running in each core of each node: managing scheduling, fault-tolerance, provenance data gathering

Typical queries : check for convergence of the deterministic solver ; computation on the fly of high order statistics (two point correlation represents important Qol) for checking convergence regarding stochastic components

# Edge-CFD + CHIRON : Two level parallelism



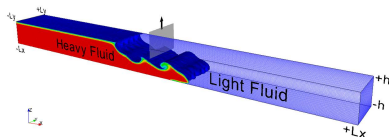


## Proof of Concept Prototype (ongoing research and implementation)

- Non-intrusive UQ strategies : Edge-CFD not to be recoded
- Stochastic Collocation : low stochastic dimension
- Double level parallelization: exploring the stochastic space ; exploring built-in parallel Edge-CFD features
- Still more: space-time-stochastic adaptivity (provenance data and online queries); computing solution statistics (post-processing)
- Uncertainty on the initial conditions (initial scenario of the currents – Lesshaff et al. . Towards inverse modeling of turbidity currents: The inverse lock-exchange problem. *Computer & Geosciences*, 37(4): 521-529,2011 ) and on settling velocity

# Lock Exchange Configuration

$Gr = 2.5 \times 10^6$  and 320,000 tetrahedra



**Example 1:** Homogeneous uncertain initial condition  $c = \bar{c} + \sigma_c \phi$  with mean and variance given by  $(\bar{c}, \sigma_c) = (1, 0.2)$ . No sediments deposition ( $u_S = 0$ )

**Example 2:** Non uniform initial condition  $c(x, y, 0; \phi) : c(x, y, \phi) = c_0 + \sum_1^2 \phi_n \sqrt{\lambda_n} f_n(x, y)$ , where

$$\lambda_n = \frac{4\eta_1\eta_2\sigma_Y^2}{[\eta_1^2(w_i^{(1)})^2+1][\eta_2^2(w_j^{(2)})^2+1]} \quad \text{with} \quad (\eta^2 w^2 - 1)s(wL) = 2\eta wc(wL) \quad \text{and}$$

$f_n(x) = \frac{1}{\sqrt{(\eta^2 w_n^2 + 1)L/2 + \eta}} [\eta w_n \cos(w_n x) + \sin(w_n x)]$ . The random variables  $\phi$  with support  $[-1, 1]$  are assumed independent and uniformly distributed.

# Uncertainty Propagation - Homogeneous Initial Conditions

# Propagation of uncertainties in the Qols: deposition map

# Multipoint Statistics – Spatial Correlation

## Final Remarks and Next Steps

- RB-VMS as LES model for Turbidity Currents. Room for improvement in the subgrid modeling
- FSI - ALE formulation for handling bed form evolution
- We have made progress on exploring Chiron ( Scientific Workflow Management Systems) capabilities for UQ analysis - two level paralelism and first steps towards adaptivity. More to come.
- Characterization of  $c(x, 0)$  through inverse stochastic algorithms (again Chiron has a role to play)

# Future Trends

Bayesian Analysis of Turbidity Currents Deposition

# A question raised by a geologist

Imaginemos que no eixo do escoamento, ao longo da linha central, exista um poço (posição XX). À cerca de 1139 metros afastado dele, existe um outro poço (posição YY), conforme o esquema abaixo. O poço na posição YY está mais alto cerca de 90m em relação ao poço XX.

A pergunta é a seguinte. Uma corrente, entrando pelo eixo, vai depositar na posição XX. Essa mesma corrente tem condições de depositar também na posição YY, apesar do mesmo estar mais alto ??

Penso que poderíamos variar o número de Reynolds dessa corrente, e ver se em alguma condição, ela consegue deixar sedimento no poço mais alto.

Isso teria um grande interesse, pois nos ajudaria a entender se as areias que observamos nos dois poços tem alguma chance de estarem conectadas, uma informação muito relevante para o desenvolvimento dessa área.



## A response (in elaboration)...

- Integrating (well log from XX) data with the numerical model
- Robust predictions relying upon taking into consideration uncertainties (measurements + numerical inputs)
- Probabilistic framework: odds to reach YY translated into joint probabilities ( $p(\mathbf{D}_{XX}, \mathbf{D}_{YY})$ )
  - Flow driven by spatial distribution in the beginning of the flow (initial conditions (scenario). It is not known!! Inversion (quite expensive).
  - Initial conditions modeled as random (uncertain) fields (sensitivity analysis) - Uncertainty Quantification
  - Different scenarios must be analyzed. Physical experiments would help a lot.
  - Results might be (easily) integrated in a decision making framework (risk analysis)

# Bayesian Analysis Framework

*Stochastic framework - parameters or (and) physical quantities are modeled as random variables (fields).*

*Physics - based models phrased as stochastic partial differential equations (SPDE).*

*Bayesian techniques emerging as leading tools for analysis*

Analysis Bayesian workflow (inspired in Bayesian modeling of air-sea interaction. Berliner et. al., Journal of Geophysical Research, 2003.)

$$\pi_{post} := \pi(\mathbf{D}, \mathbf{m} | \mathbf{d}) \propto [\mathbf{d} | \mathbf{D}] L(\mathbf{D} | \mathbf{m}) \pi_{prior}(\mathbf{m}) \quad (2)$$

$\mathbf{d}$  ... well log data : deposits heights and sediments distribution.

$\mathbf{m}$  . . . initial conditions (initial scneario) and settling velocity

$[\mathbf{d} | \mathbf{D}]$  ... data model (measurements error)

# Analysis

- Equation (2) is often not amenable to be treated by analytical means
- Indeed, one might want only to compute quantiles...  
 $P(D_j \leq \bar{D})$  or analyse plausible scenarios. Sampling will do.
- Sampling from  $\pi_{post}$  is not a trivial task... Markov Chain Monte Carlo algorithms represent a good option. But they will be quite expensive (a forward problem is to be solved for each sample (accepted or not))
- Computational Surrogates : I. Bilionis, N. Zabaras, B. A. Konomi, G. Lin. Multi-output separable Gaussian process: Towards an efficient fully Bayesian paradigm for uncertainty quantification. *Journal of Computational Physics* 241 (2013) 212–239.