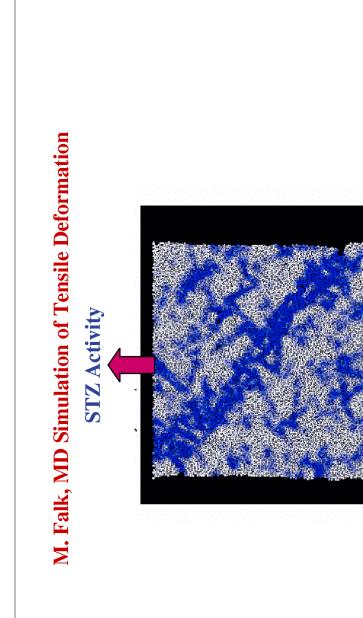
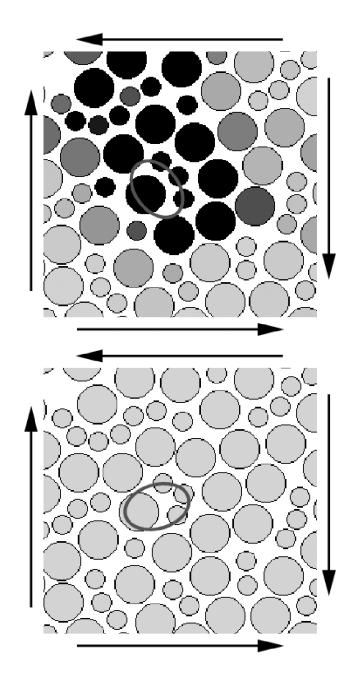
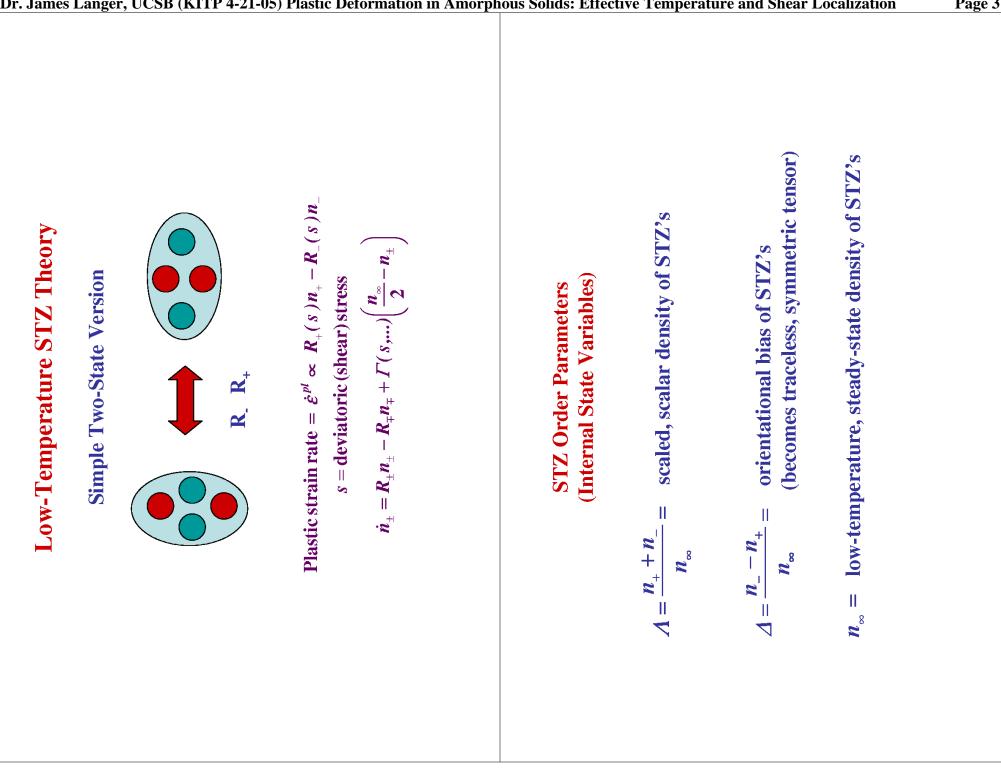
Plastic Deformation in Amorphous Solids: Effective Temperature and Shear Localization J.S. Langer, UCSB J.S. Langer, UCSB KITP Granular Materials Seminar April 21, 2005	Fundamental Puzzles in Solid Mechanics	• How can we understand brittle and ductile behaviors – especially in noncrystalline solids?	• What is the origin of memory effects in simple noncrystalline solids?	• What is the origin of dynamic instabilities in brittle fracture?

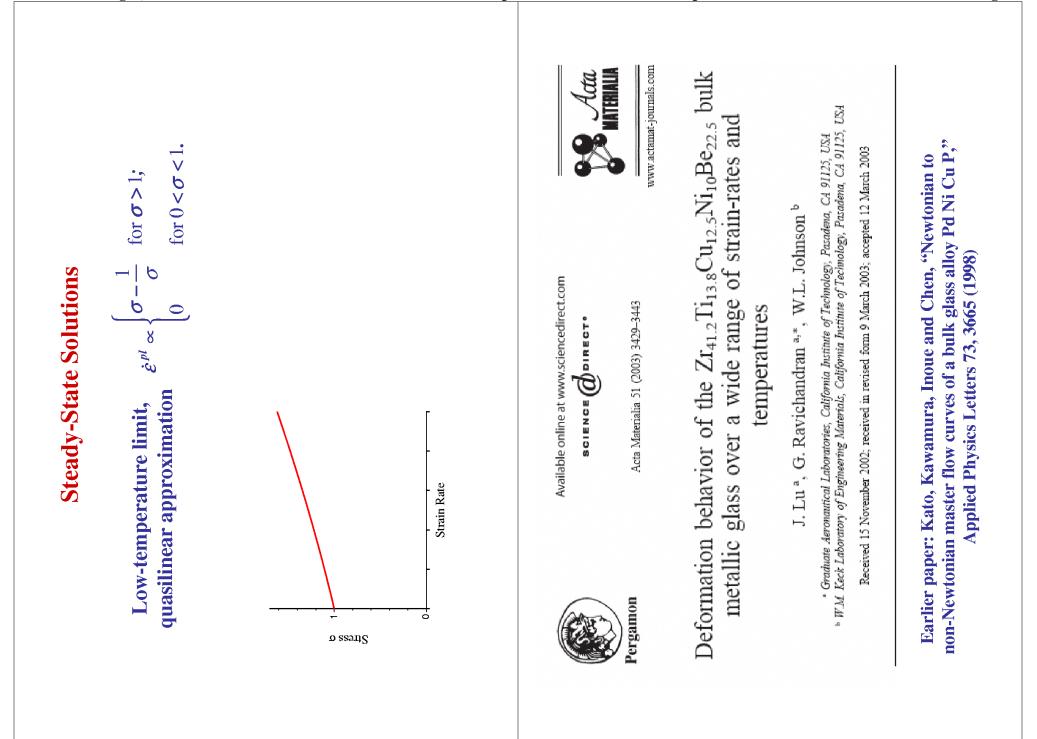


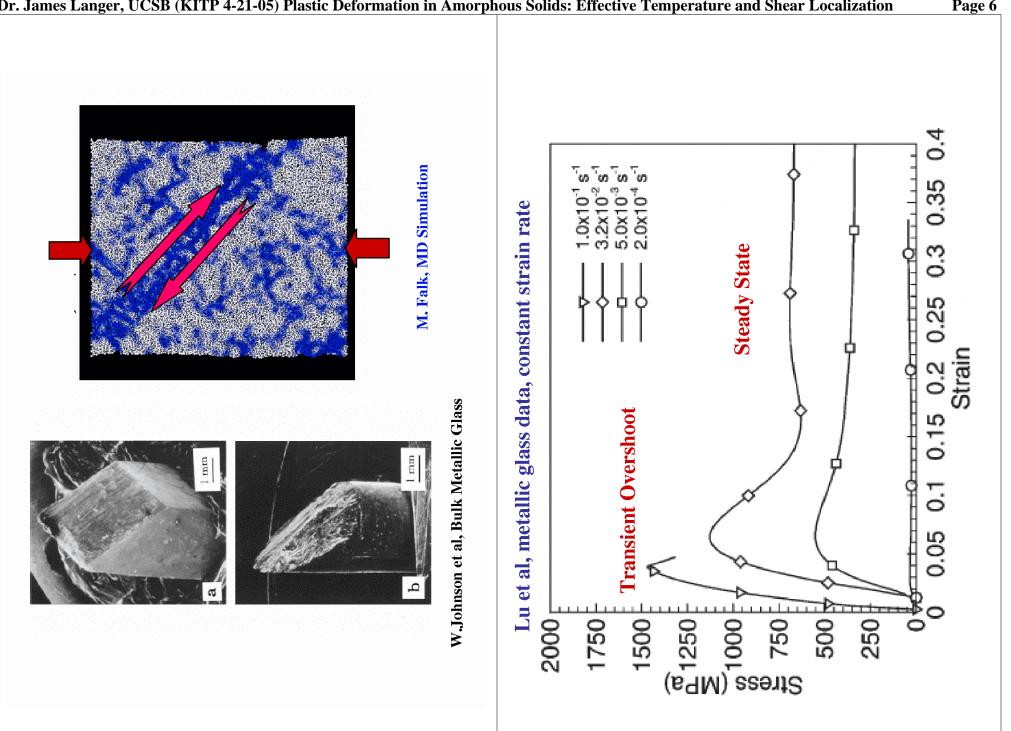


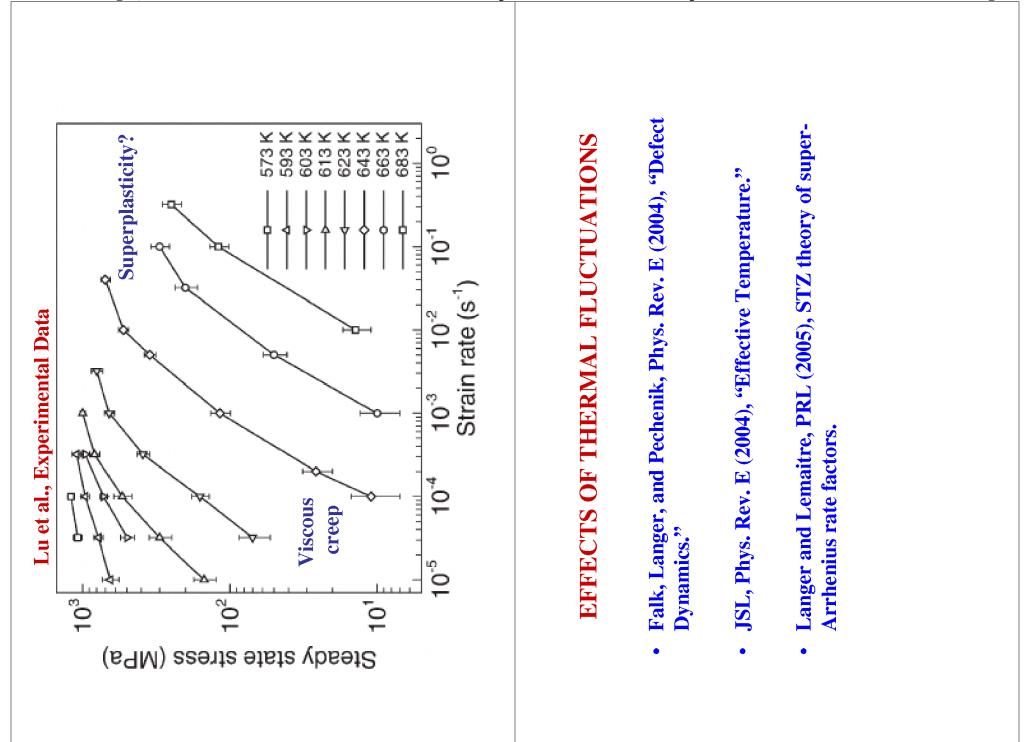


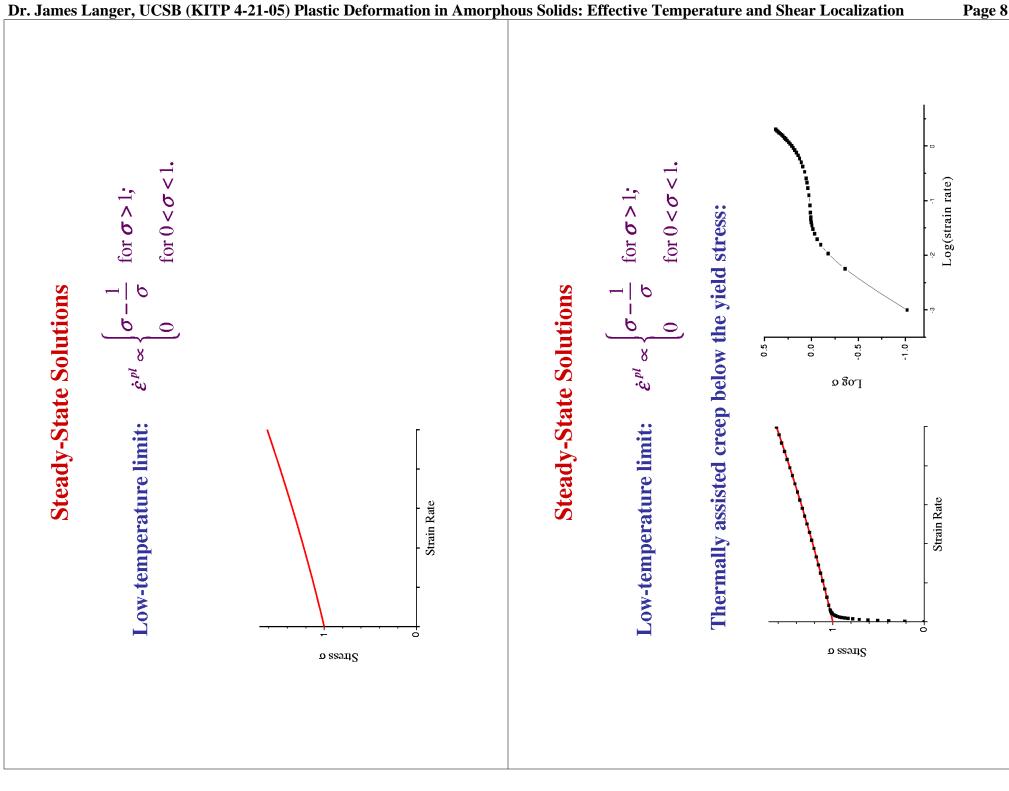


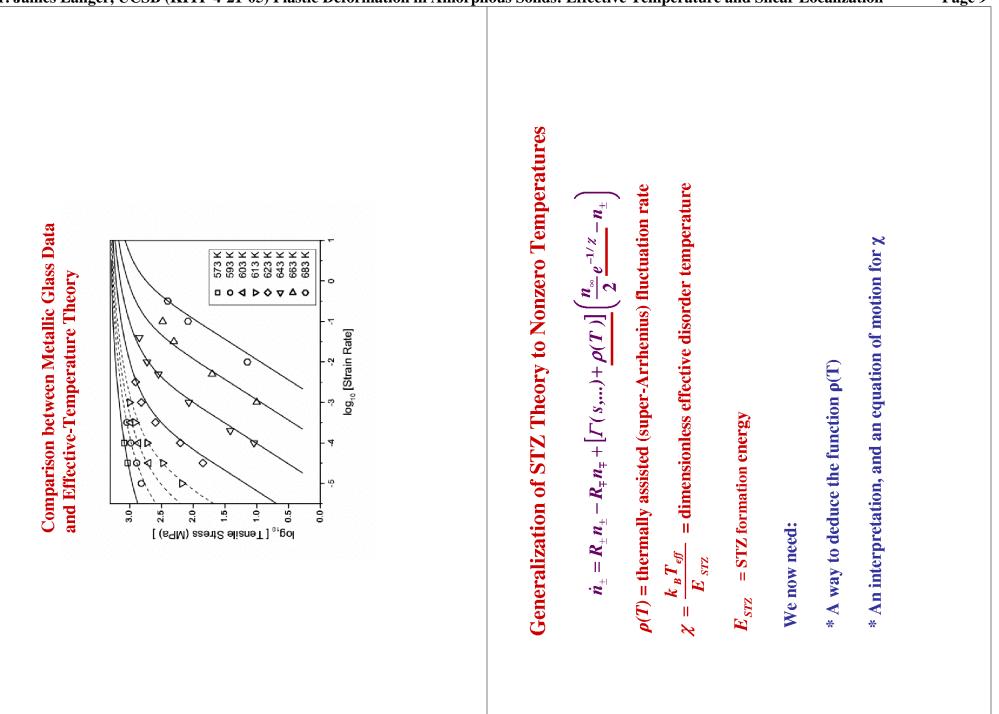
<b>Dissipation (Production) Rate</b> <b>Energy balance:</b> $2\varepsilon^{pt}s = \frac{d}{dt}\psi(\Lambda, \Delta) + Q$ <b>Energy balance:</b> $2\varepsilon^{pt}s = \frac{d}{dt}\psi(\Lambda, \Delta) + Q$ $2\varepsilon^{pt}s = \text{ rate at which work is done}$ $\psi = \text{ recoverable energy}$ Q =  dissipation rate > 0 (second law) <b>Chenik's conjecture:</b> $Q \sim \Lambda \Gamma(s, \Lambda, \Delta)$ Use equations of motion and second law to solve for $\Gamma$ and $\Psi$ $\Gamma = \frac{4\Lambda(\Lambda s - \Delta)^2}{(1 + \Lambda)(\Lambda^2 - \Lambda^2)};  \Psi = \frac{\Lambda}{2} \left( 1 + \frac{\Lambda^2}{\Lambda^2} \right)$	) Equations of Motion $\Delta \int_{a=s/s}^{2} \int_{a=s/s}^{b=0} \int_{a=1/s}^{b=0} \int_{a=1/s}^{b=0} \int_{a=1/s}^{b=0} \int_{a=1/s}^{b=0} \int_{a=1/s}^{a=1/s} \int_{a=1/s}^{a=1/s}$
<b>Dissipation (Production) Ra</b> <b>Energy balance:</b> $2\hat{\varepsilon}^{pl}s = \frac{d}{dt}\Psi(\Lambda, \Delta) + Q$ $2\hat{\varepsilon}^{pl}s = \text{rate at which work is done}$ $\Psi = \text{recoverable energy}$ Q = dissipation rate > 0 (second law) <b>Pechenik's conjecture:</b> $Q \sim \Lambda \Gamma(s, \Lambda, \Delta)$ Use equations of motion and second law to solv $\Gamma = \frac{4\Lambda(\Lambda s - \Delta)^2}{(1 + \Lambda)(\Lambda^2 - \Lambda^2)};  \Psi = \frac{\Lambda}{2}\left(1 + \frac{\Lambda^2}{\Lambda^2}\right)$	Quasilinear (Approximate) Equations of Motion $A \rightarrow 1; s / s_{yield} \rightarrow \sigma$ $A \rightarrow 1; s / s_{yield} \rightarrow \sigma$ $A \rightarrow 1; s / s_{yield} \rightarrow \sigma$ $\delta^{nl} \approx \sigma - \Delta$ (effective stress) $\delta^{nl} \approx \sigma - \Delta$ (effective stress) $\Gamma \propto \frac{(\sigma - \Delta)^2}{1 - A^2}$ (dissipation rate) $\dot{\Delta} \propto \frac{(\sigma - \Delta)(1 - \sigma \Delta)}{1 - A^2}$ $\dot{\Delta} \propto \frac{(\sigma - \Delta)(1 - \sigma \Delta)}{1 - A^2}$ Exchange of stability a between jammed state and flowing states ( $\Delta$

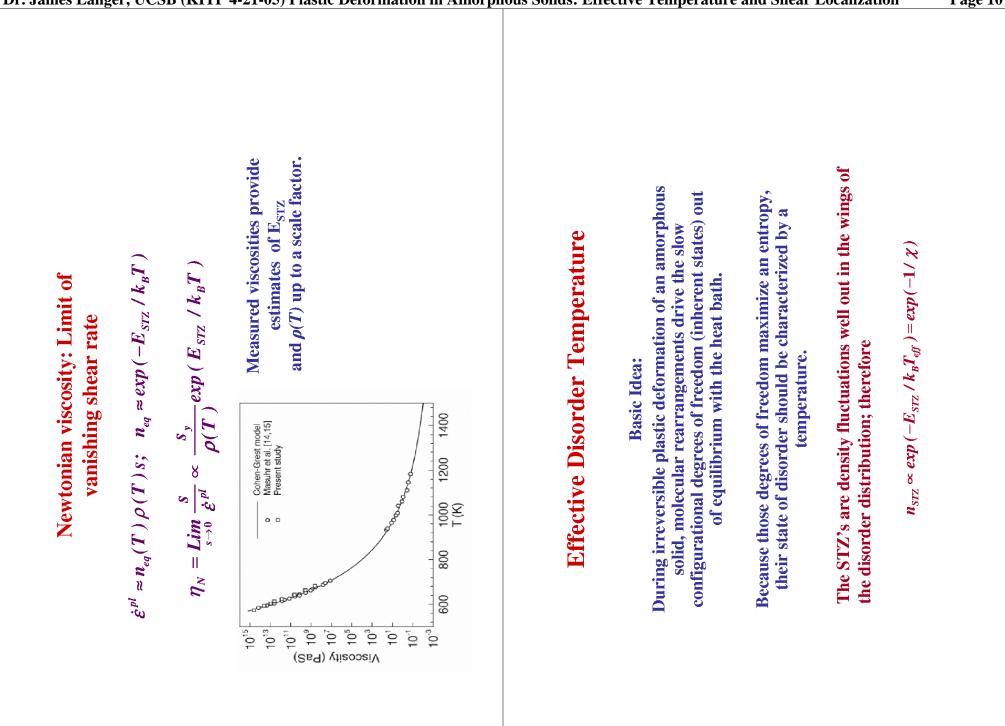


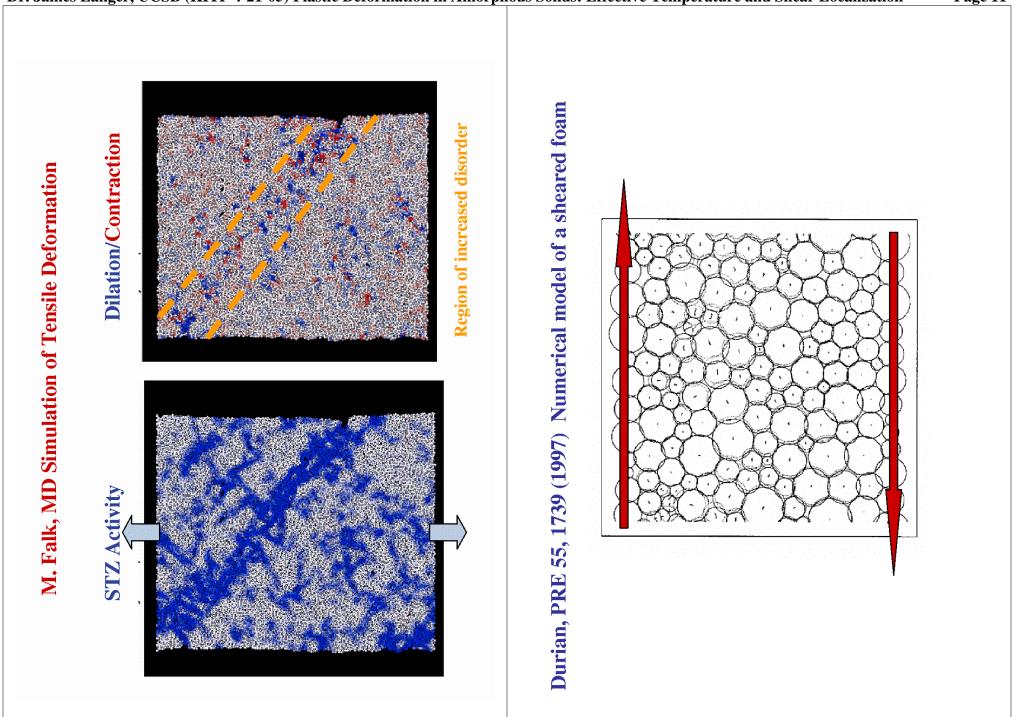


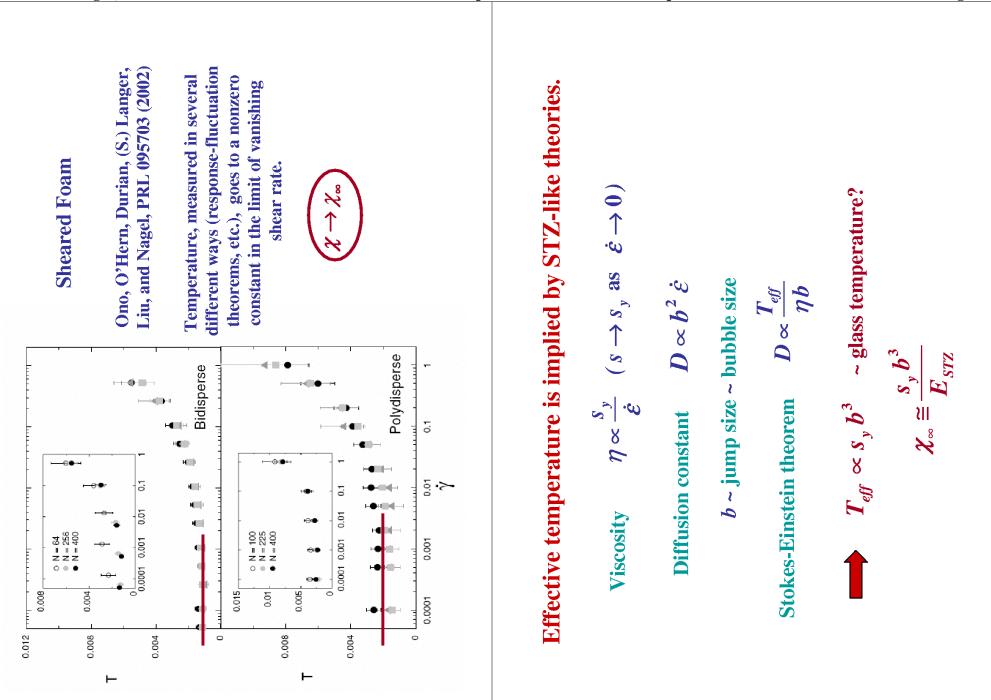


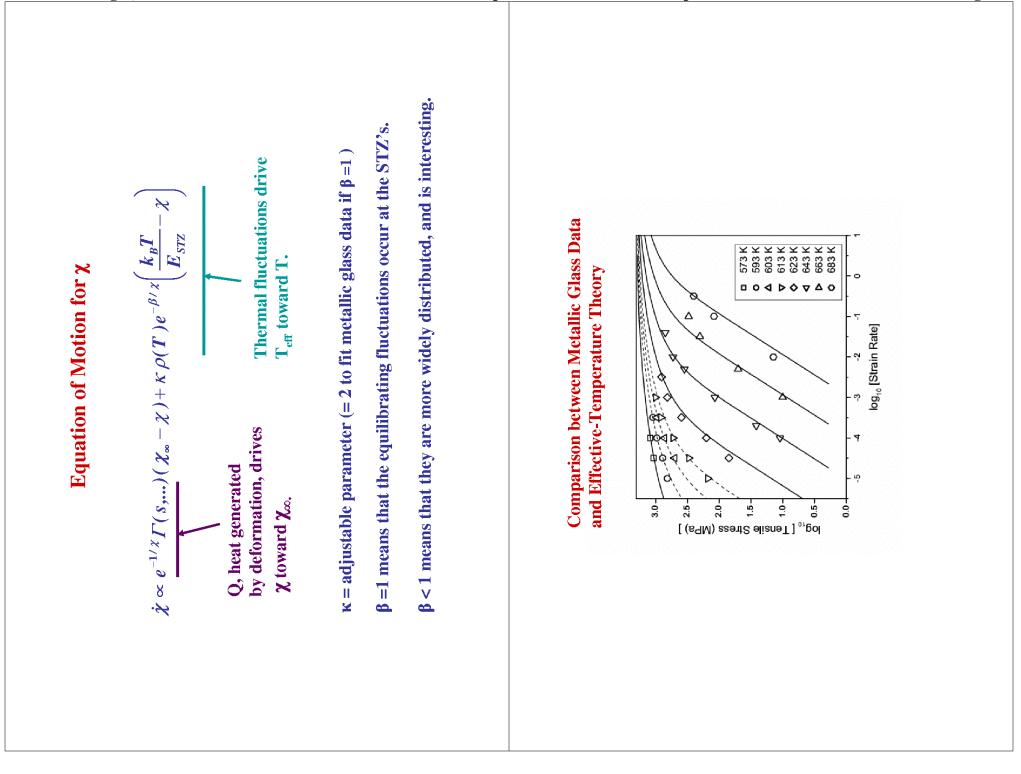


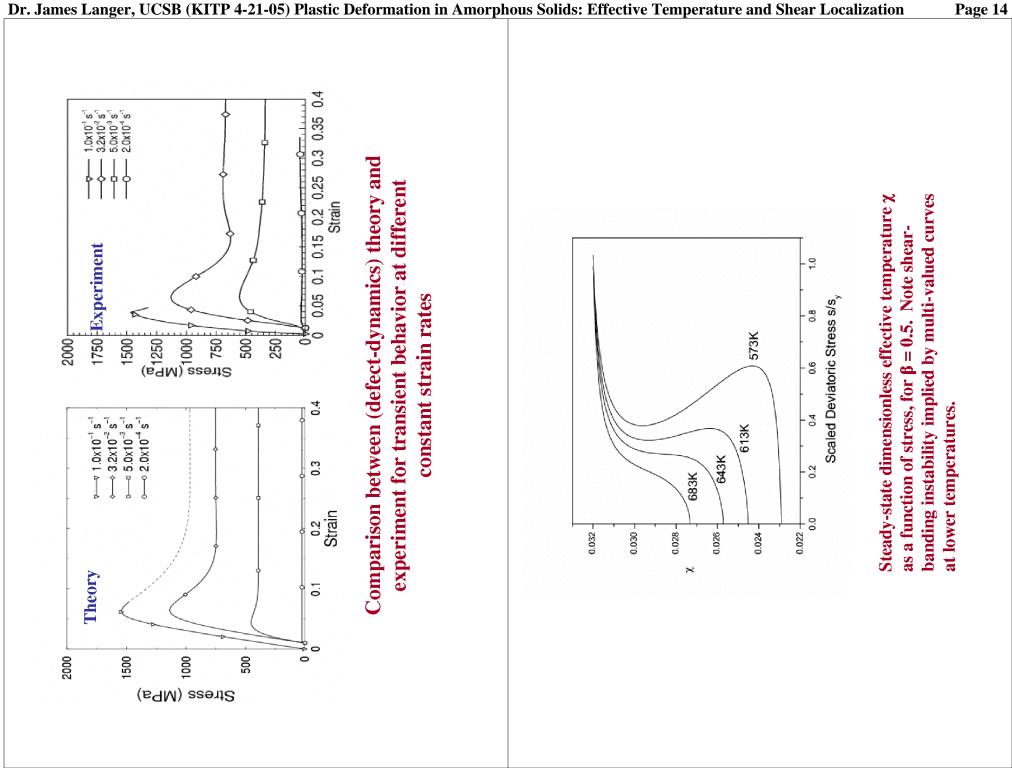


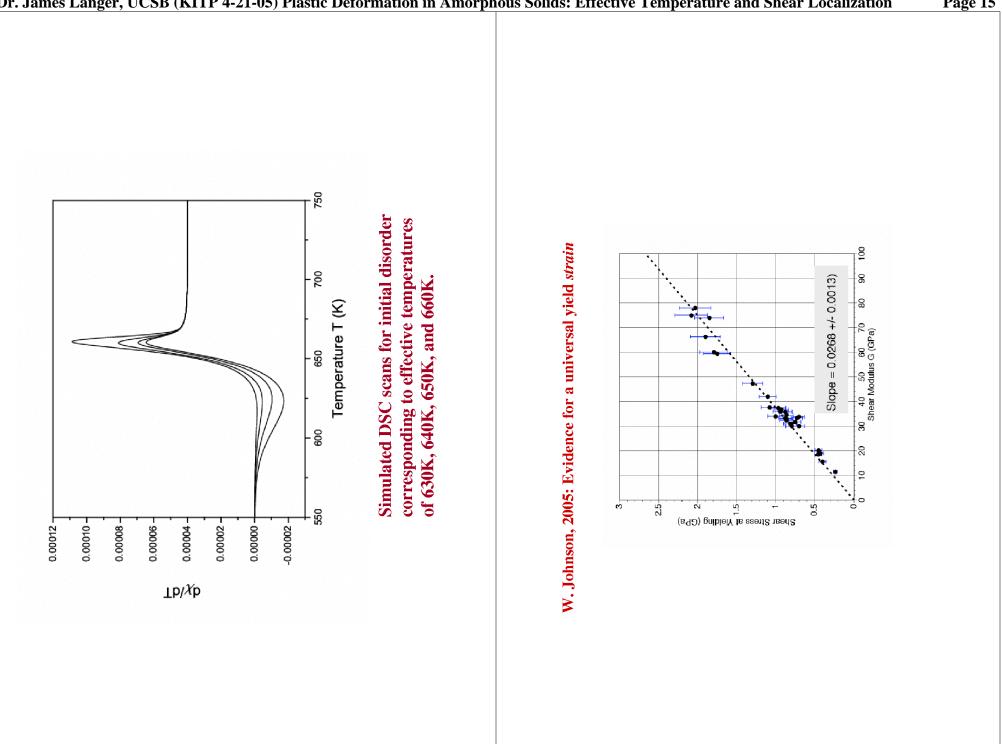


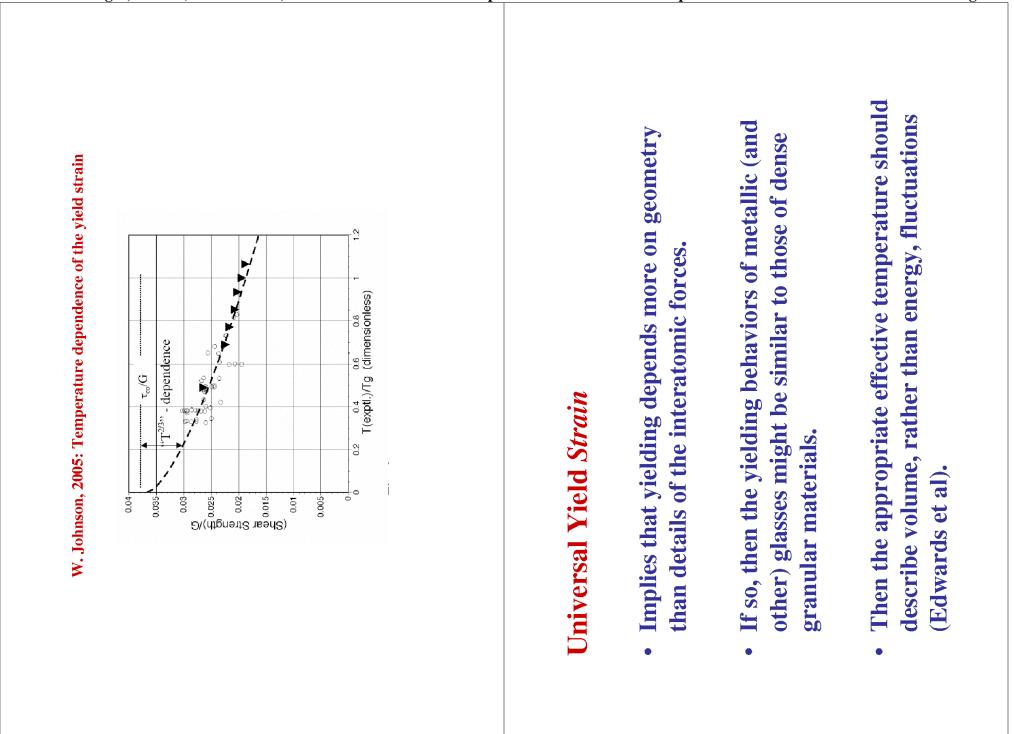












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<ul> <li>Concluding Remarks</li> <li>The effective-temperature theory seems to work well, but needs to be developed further and tested by experiments.</li> <li>The deepest outstanding problem is to find a theory for the super-Arrhenius fluctuation rate p(T). The STZ picture should give us clues about possible – intrinsically dynamic – mechanisms. (Langer and Lemaitre, PRL in press)</li> <li>Extension of STZ theory to (from) granular materials?</li> </ul>	Ide 3	