

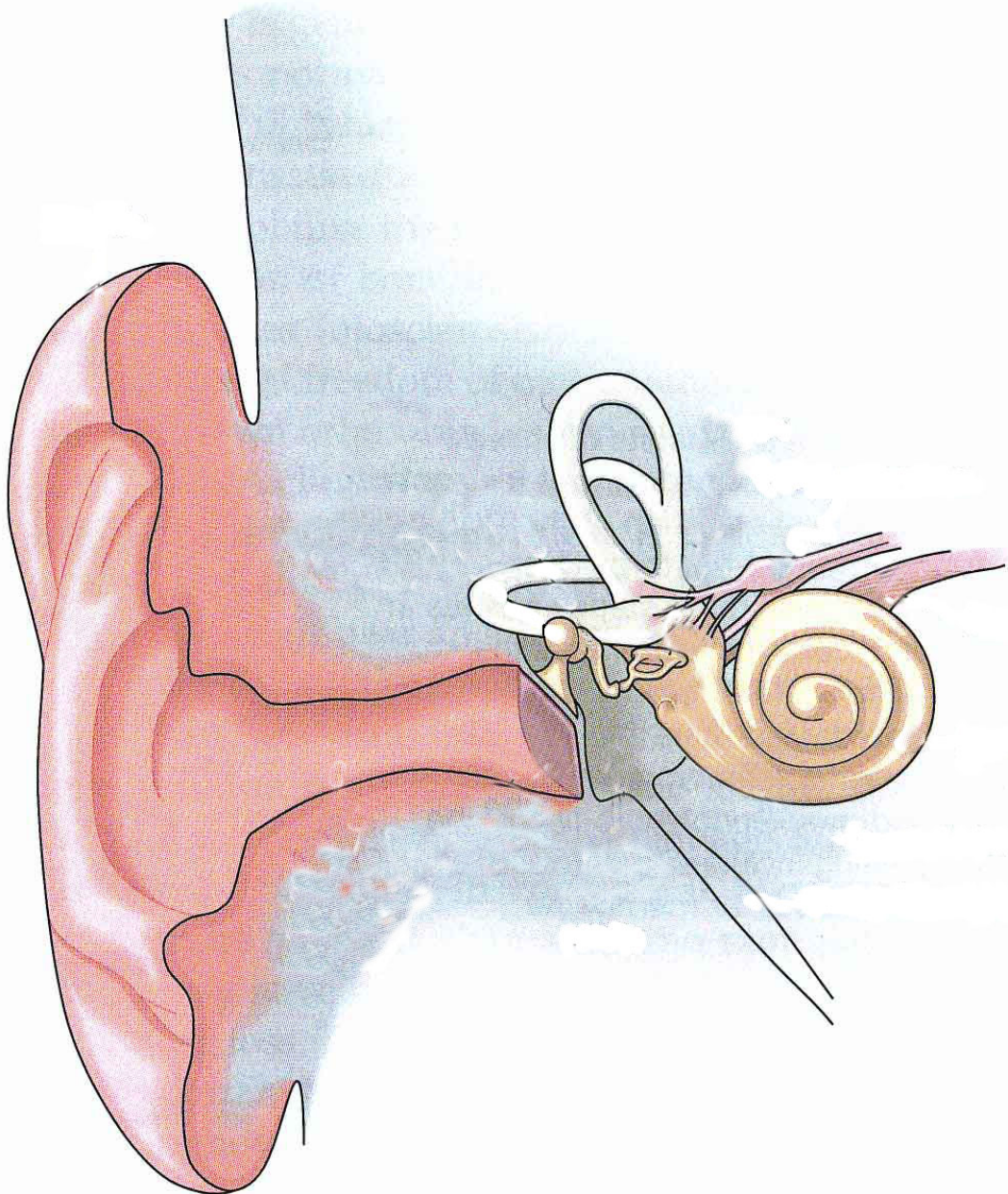
The hair-cell bundle: sensor and amplifier for hearing.

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Hearing specifications

- frequency range (20 Hz - 20 KHz; up to 100 kHz in whale and bats)
- sensitivity (limited by thermal noise)
- frequency selectivity ($\Delta f/f \cong 0.25\%$)
- dynamical range (1 – 1,000,000 ; sound pressure: 20 μ Pa \rightarrow 20 Pa)

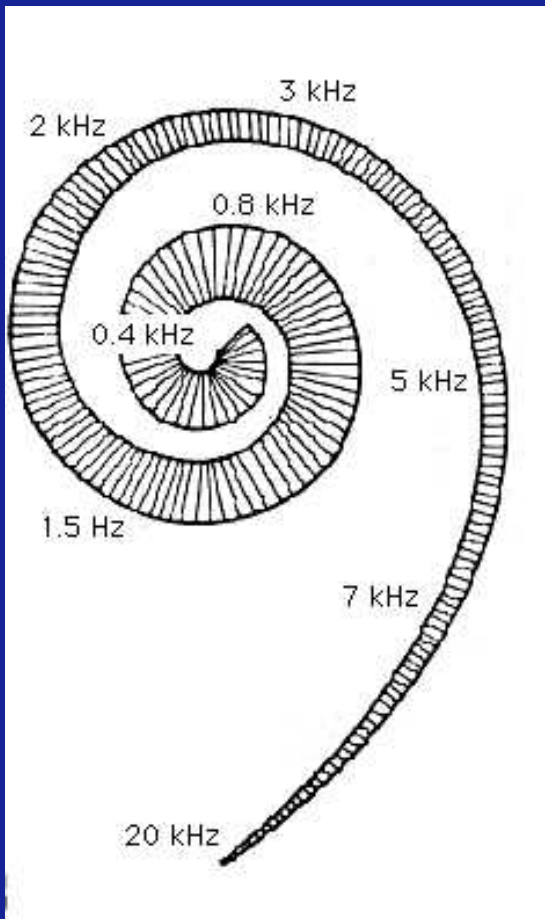
The resonance hypothesis

→ energy accumulation from cycle to cycle of stimulation



« Sympathetic vibration »

Hermann von Helmholtz (1821-1894)



« (...) the radial fibers of the basilar membrane may be approximately regarded as forming a system of stretched strings (...). In that case the laws of their motion would be the same as if every individual string moved independently from the others, and obeyed the influence of the periodically alternating pressure of the fluid (...). Consequently any exciting tone would set that part of the membrane into sympathetic vibration (...). »

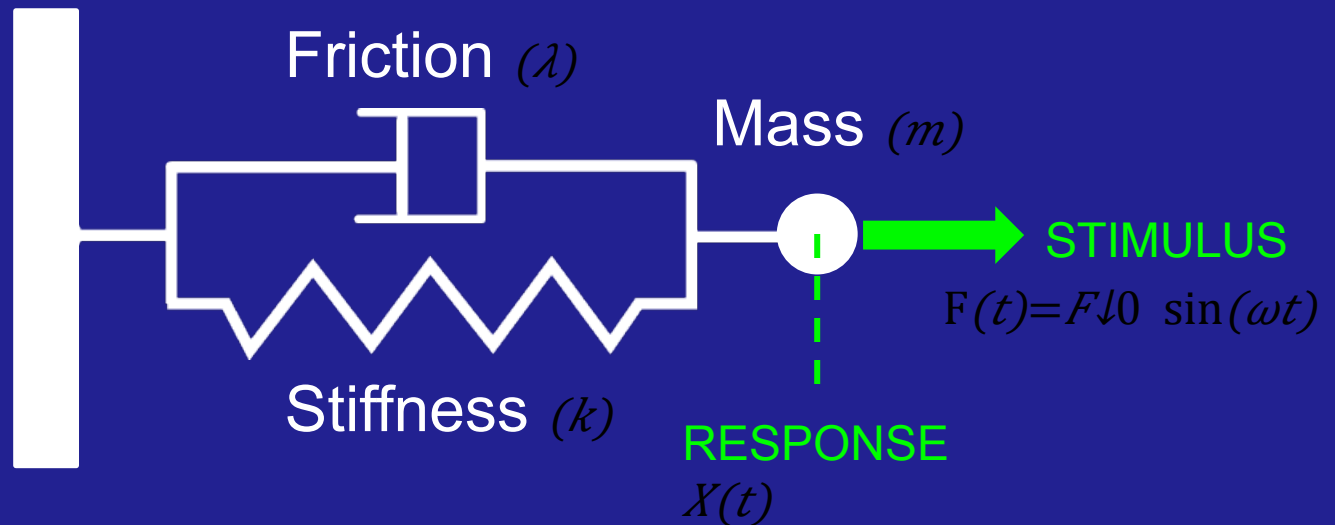
(from “On the sensation of tones”, 1877)

Place of Section	Breadth of Membrane or Length of Transverse Fibres	
	Millimetres	Inches
0.2625 mm. [= 0.010335 in.] from root	0.04125	.00162
0.8626 mm. [= 0.033961 in.] from root	0.0825	.00325
Middle of the first spire	0.169	.00665
End of first spire	0.3	.01181
Middle of second spire	0.4125	.01624
End of second spire	0.45	.01772
At the hamulus	0.495	.01949

The breadth therefore increases more than twelvefold from the beginning to the end.

Harmonic oscillator

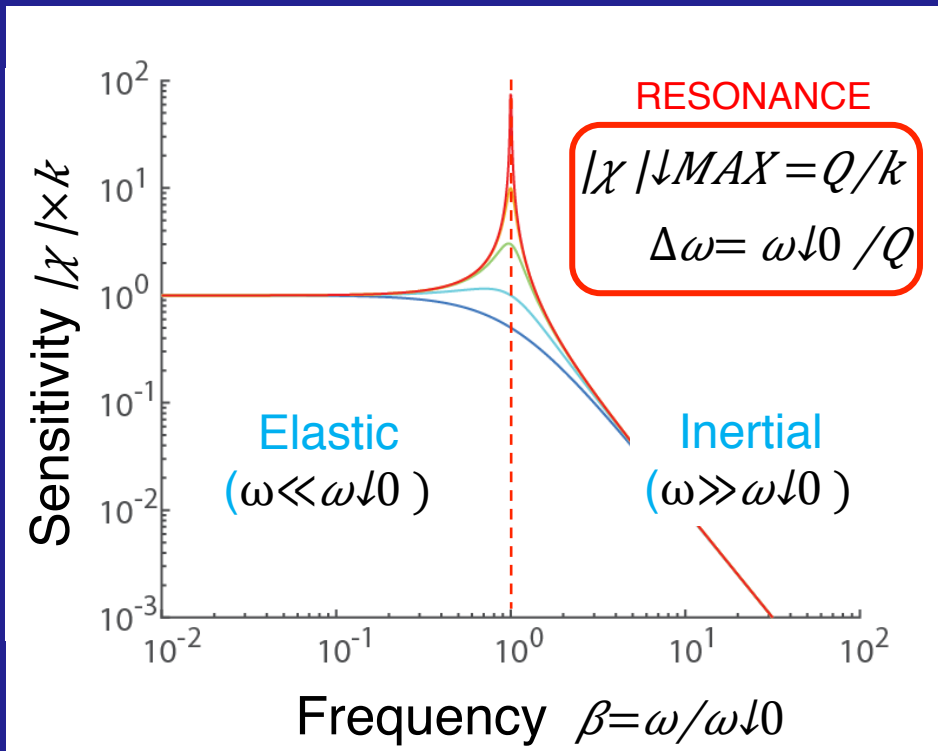
→ passive mechanical properties



Equation
of motion:

$$m \ddot{X} + \lambda \dot{X} + k X = F(t)$$

Mechanical resonance



RESPONSE FUNCTION

$$\chi = 1/k / [1 - \beta^2 + i\beta/Q]$$

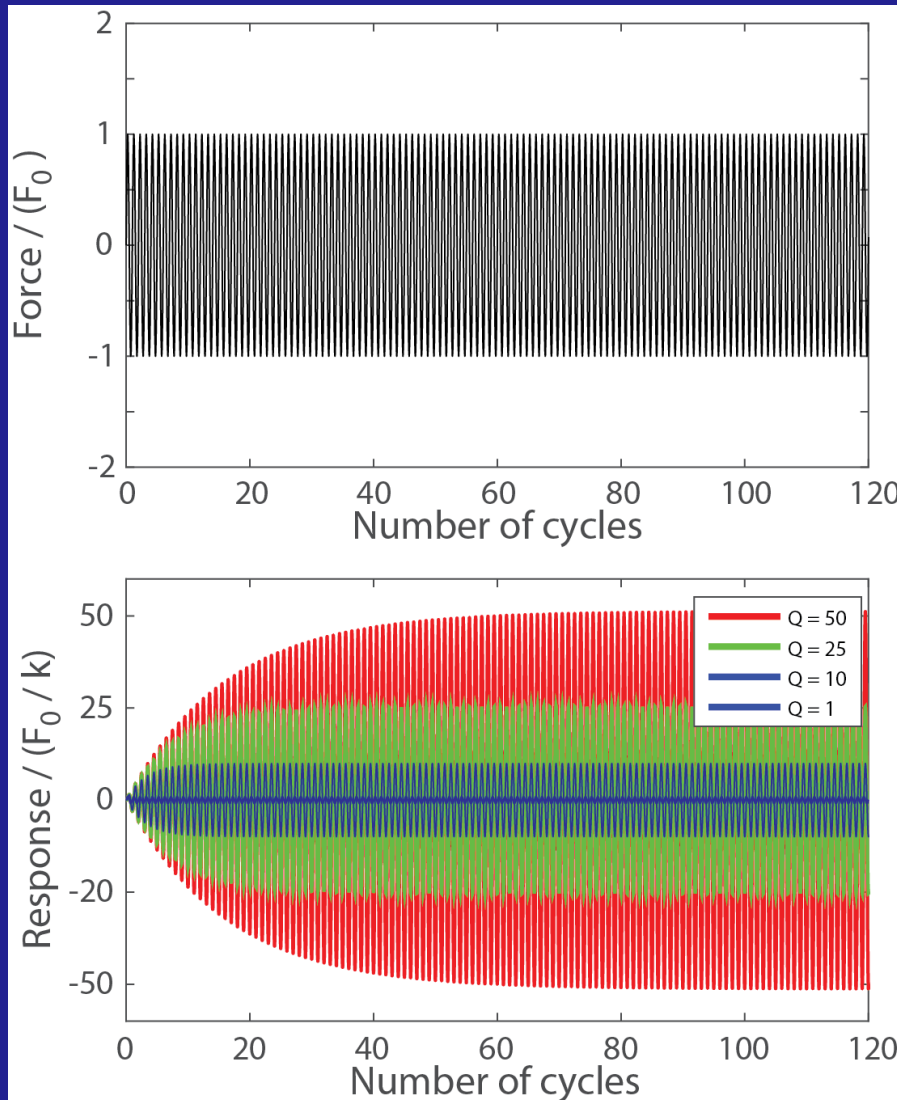
with $\chi = X / F$

$$(F(t) = F e^{i\omega t}; X(t) = X e^{i\omega t})$$

Characteristic frequency: $\omega_0 = \sqrt{k/m}$

Quality factor: $Q = \sqrt{k m} / \lambda = \omega_0 / \Delta\omega$

high sensitivity \leftrightarrow slow response growth



STIMULUS

$$F(t) = F_0 \sin \omega_0 t$$

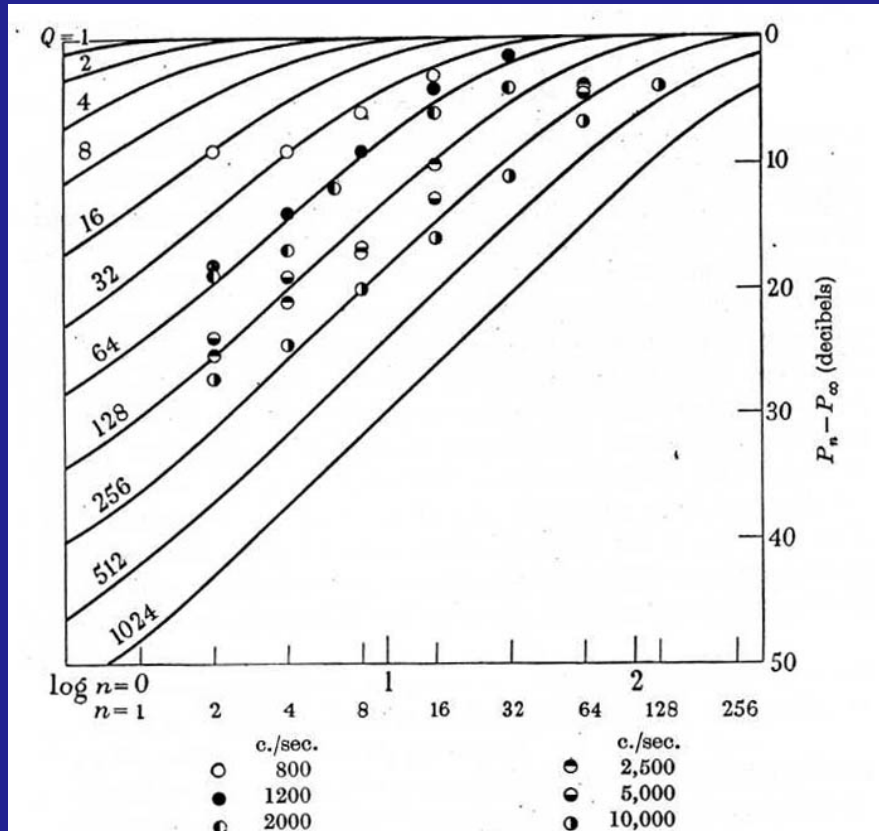
RESPONSE

$$X(t) \cong -Q F_0 / k [1 - \exp(-t/\tau)] \times \cos \omega_0 t$$

response max:
 $Q F_0 / k$

response time:
 $\tau = 2Q / \omega_0$

Sound-pressure level $P \downarrow n = 20 \log(F \downarrow n)$ to get a threshold vibration $X \downarrow \emptyset$ after n cycles of oscillations.



Quality factors inferred:

frequency (c./sec.)	Q	time constant $= Q/\pi f_0$ (msec.)
10,000	300	10
5,000	150	10
2,500	150	19
2,000	80	12
1,200	60	16
800	32	13

(Gold and Pumphrey, Proc Roy Soc Lond (1948))

➔ highly tuned resonator

$$X \downarrow \emptyset \cong QF \downarrow n / k [1 - \exp(-\pi n/Q)] = QF \downarrow \infty / k$$

➔

$$P \downarrow n - P \downarrow \infty \cong -20 \log[1 - \exp(-\pi n/Q)]$$

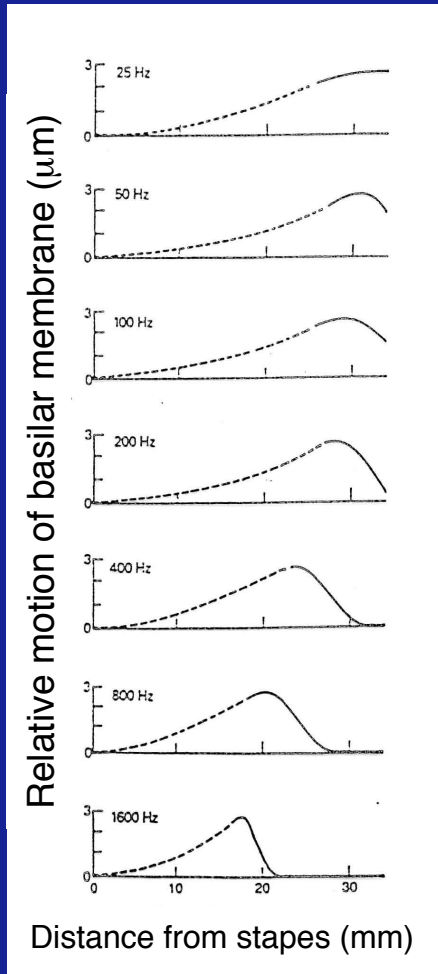
« We would then regard the cochlea no longer as a passive instrument where nerve endings merely record the displacement due to an applied force, but as **an active mechanism** where an applied signal releases a chain of events involving **an additional source of energy**. »

Thomas Gold, 1948

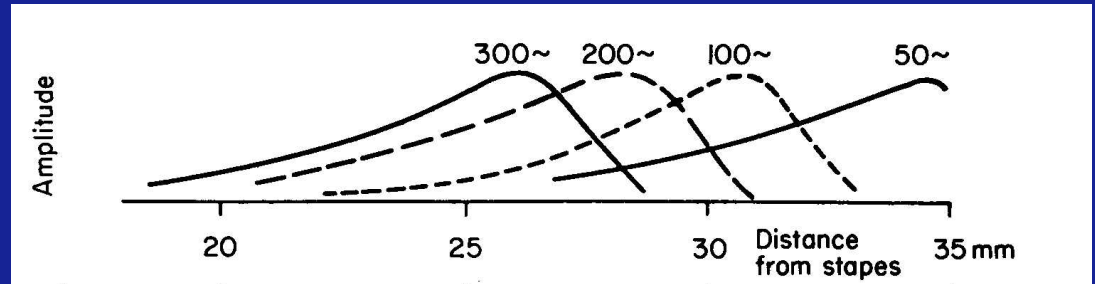


Passive (and broad) resonance

Georg von Békésy (1899-1972)

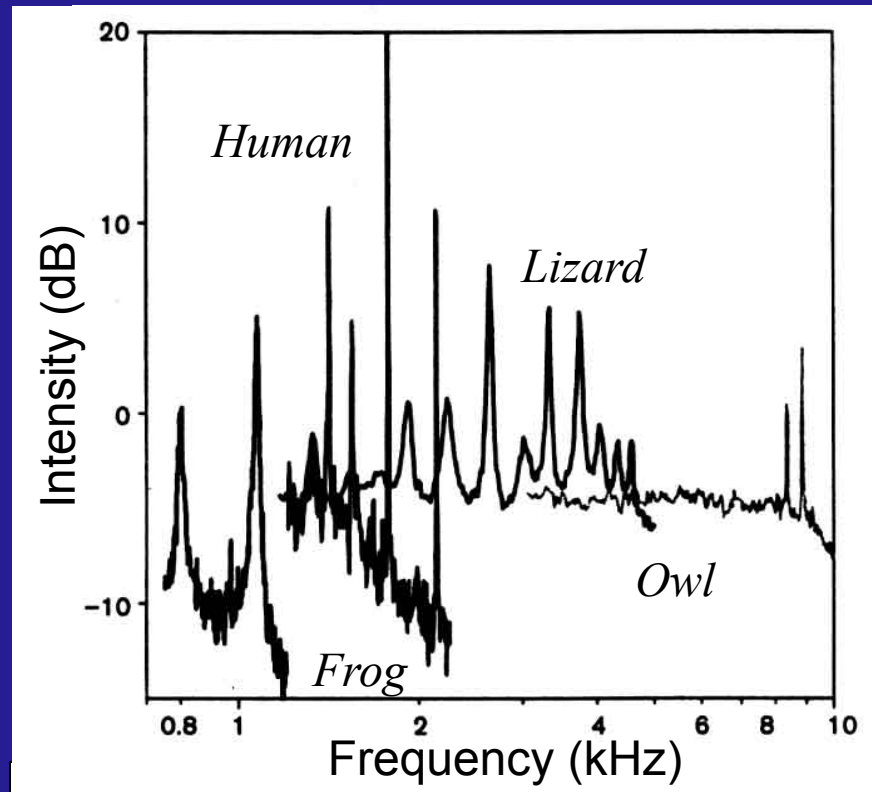


Envelope of basilar-membrane vibration
(in human cadavers...)



The ear can sing!

Spontaneous oto-acoustic emissions (S.O.A.Es)



(G.A. Manley and C. Köppl, 1998)

Not a high-fidelity sound receiver!



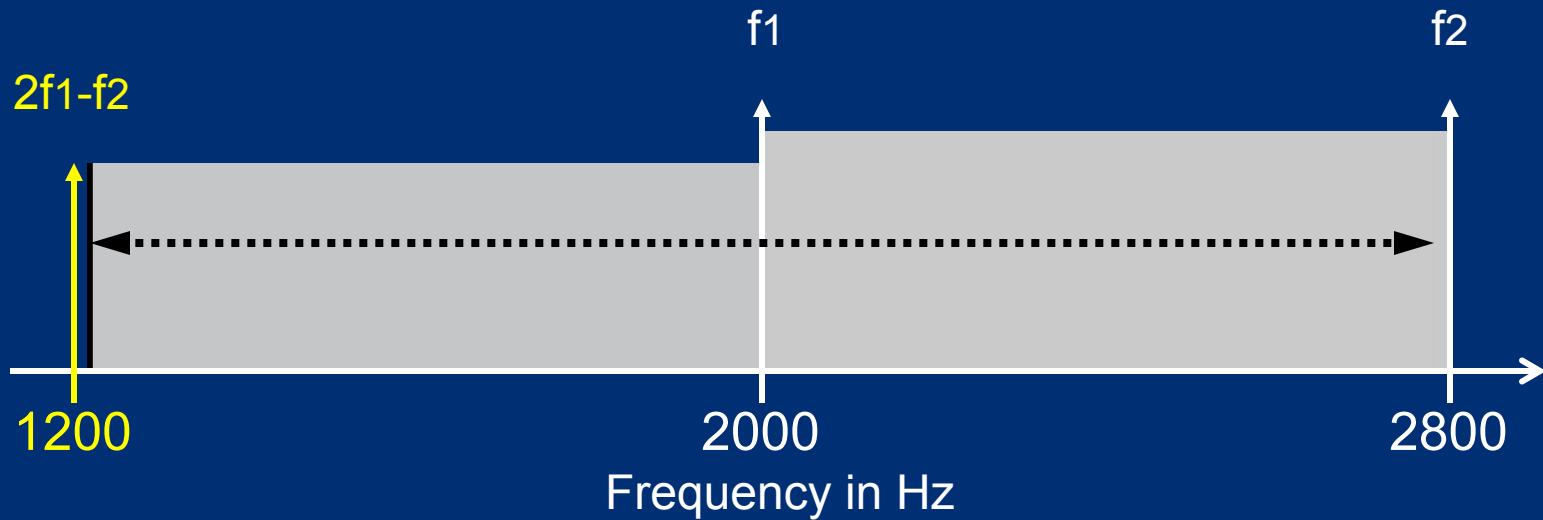
Tartini
(1692-1770)

« Phantom tones »

→ two-tone stimulus:

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t)$$

($f_1 < f_2$)



primary tone f_1



primary chirp f_2



f_1 and f_2

« Phantom tones »

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t)$$

($f_1 < f_2$)

- $f_2 - f_1$ must be small ($f_2/f_1 = 1.1-1.3$)
- perceived even at low levels (threshold $\cong 20$ dB)
- distortion at $2f_1 - f_2$ dominates
- relative level at $2f_1 - f_2$ nearly independent of stimulus level (15-20%)

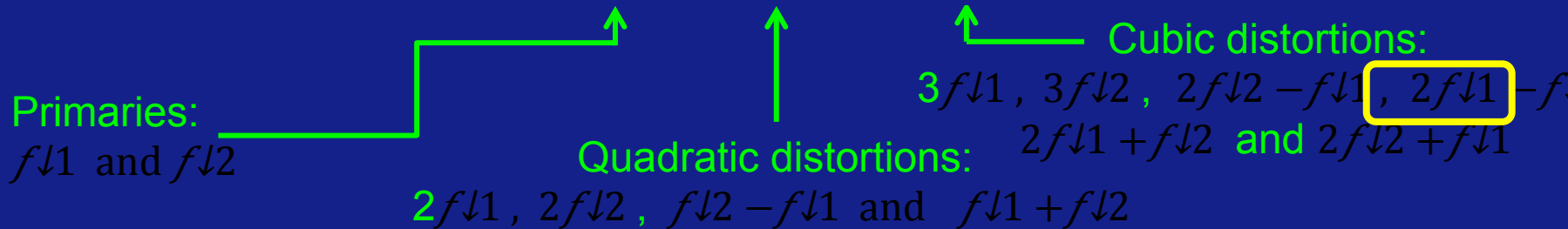
 **Auditory nonlinearity**

(J.L. Goldstein, JASA (1967))

Static nonlinearity

Stimulus: $F(t) = F \sin(2\pi f_1 t) + F \sin(2\pi f_2 t)$

Response: $X(t) \cong \chi F + \alpha F^2$



$$\begin{aligned} X_{f_1} &\propto F; \quad X_{f_2} \propto F \\ X_{2f_1 - f_2} &\propto F^3 \end{aligned}$$

Does NOT explain the auditory nonlinearity!

Relative level of cubic distortion: $X_{2f_1 - f_2} / X_{f_1} \propto F^2$

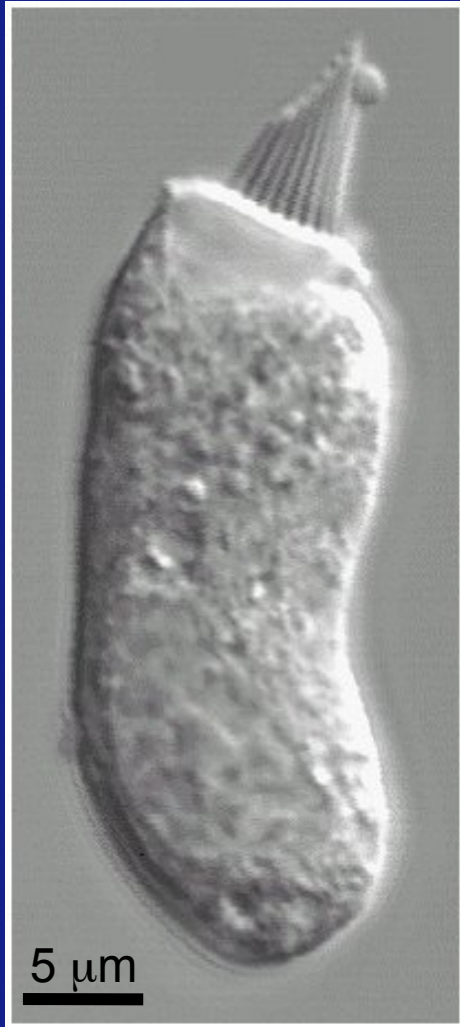
Non-linear interference in hearing

→ **two-tone stimulus:**

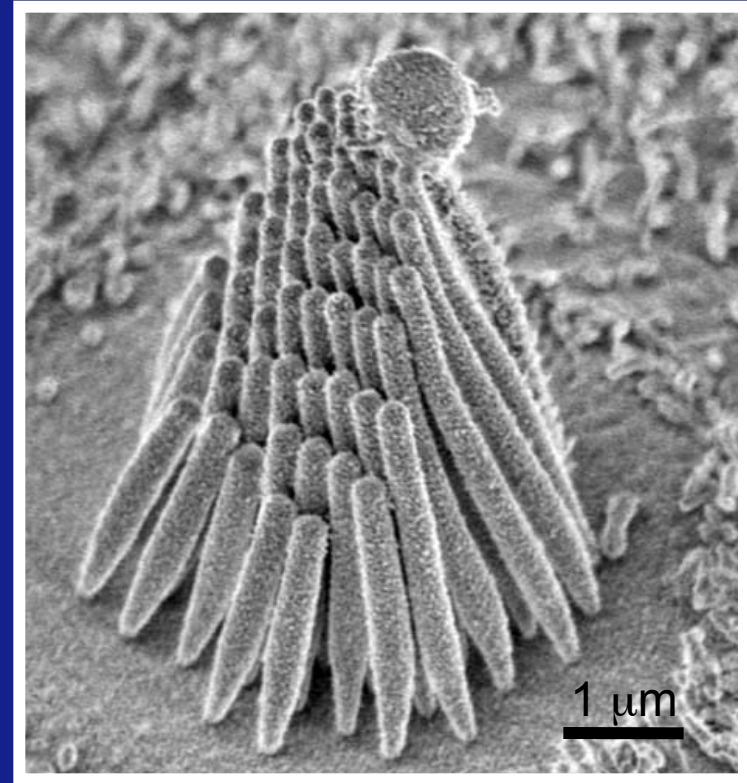
$$F(t) = F_1 \sin(2\pi f_1 t) + F_2 \sin(2\pi f_2 t)$$

- **DISTORTIONS:** tones that are not present in the sound stimulus are perceived.
- **MASKING:** the perceived loudness of a (test) tone diminishes in the presence of a second (masker) tone at a nearby frequency.

The hair cell

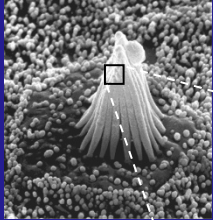


(A.J. Hudspeth)

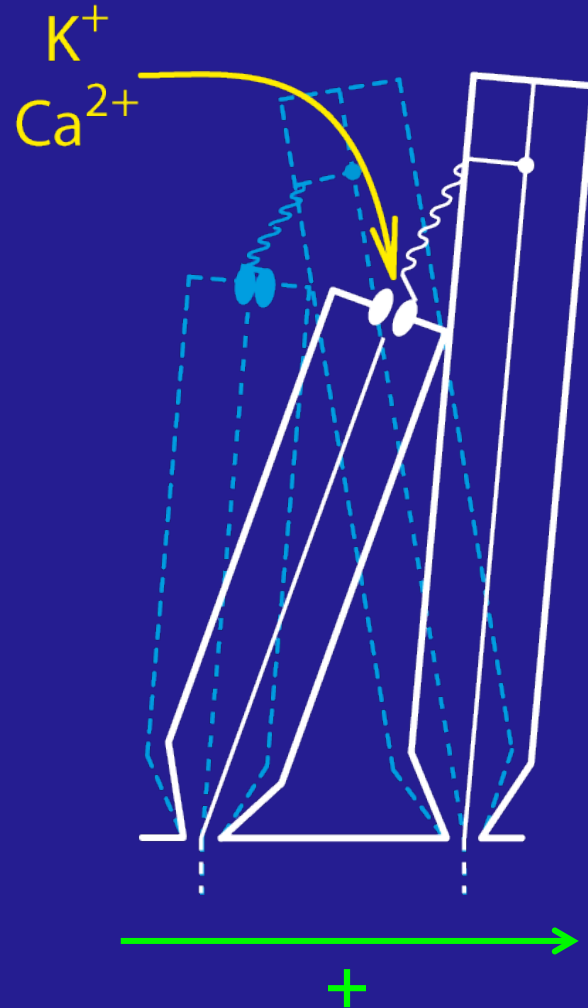


(P. Gillespie)

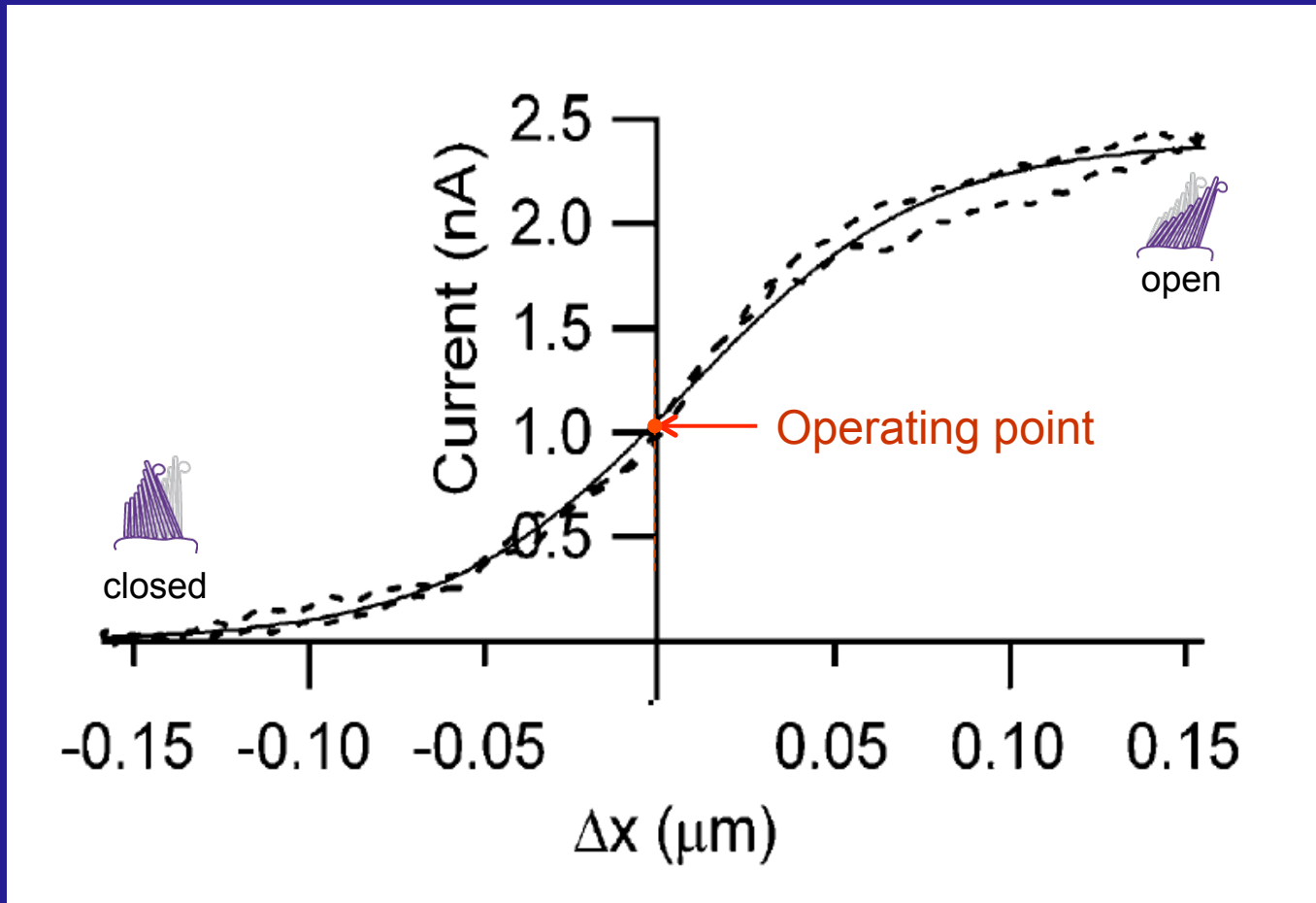
The hair-cell bundle: mechanical antenna



(A.J. Hudspeth)



Transduction current



(Johnson et al, Neuron (2011))

Passive mechanical properties

Mass: $m=60 \times 10^{-15}$ kg

Stiffness: $k=1$ mN/m

Viscous drag: $\lambda=80$ nN·s/m

$$f_0 = 1/2\pi \sqrt{k/m} = 25 \text{ kHz}$$

$$Q = \sqrt{k m} / \lambda = 0.1$$

OVERDAMPED!



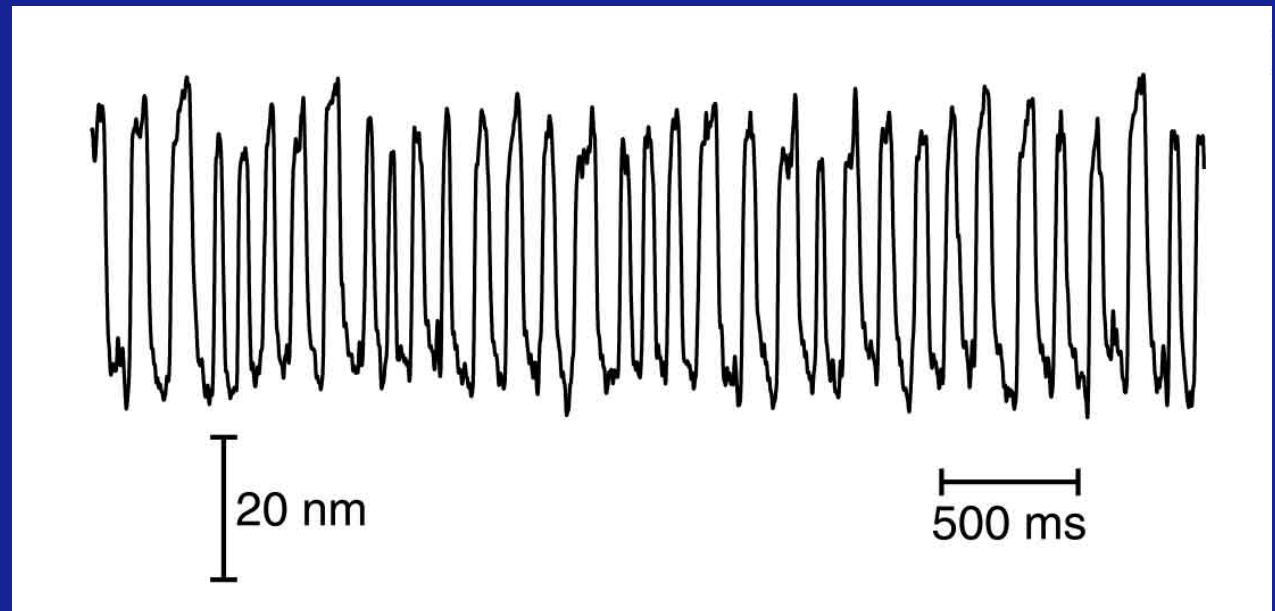
(bullfrog)

The hair-cell bundle → sensory and motile

SPONTANEOUS OSCILLATIONS



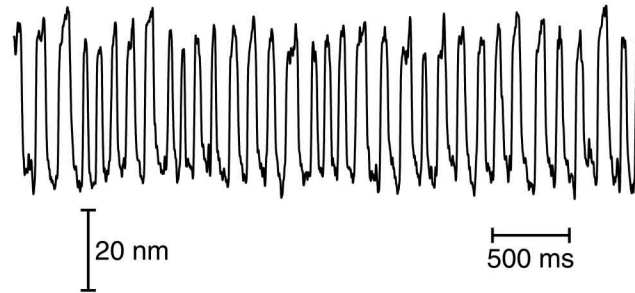
1 μm



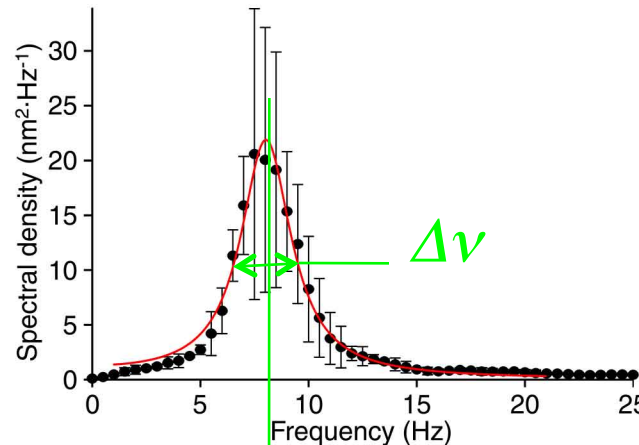
(Martin and Hudspeth, PNAS (1999))

Characteristic frequency

Hair-bundle
position



Spectral
density



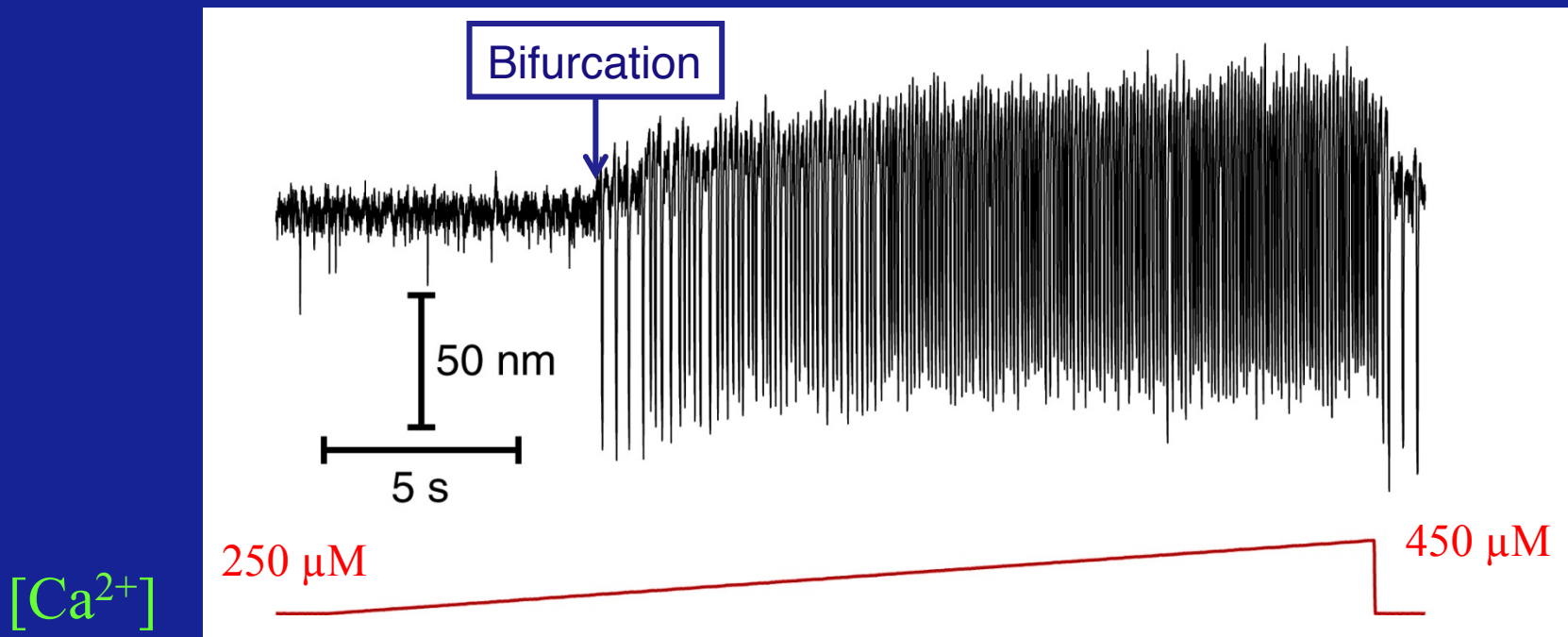
Noisy!

Low quality factor
($Q = \nu_C / \Delta\nu \approx 2$)

characteristic frequency: ν_C (range: 5-50 Hz)

Oscillatory instability

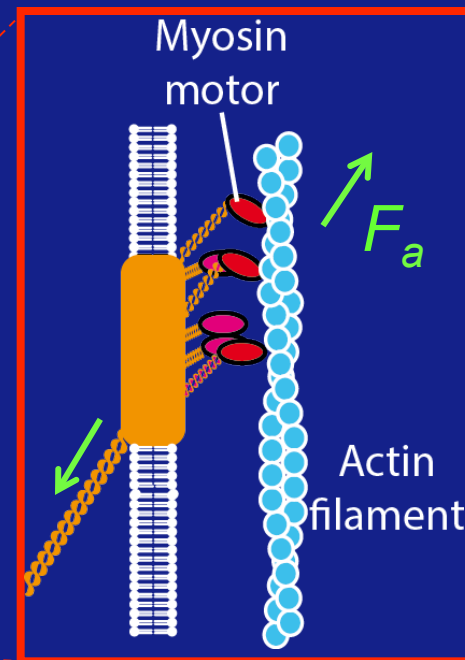
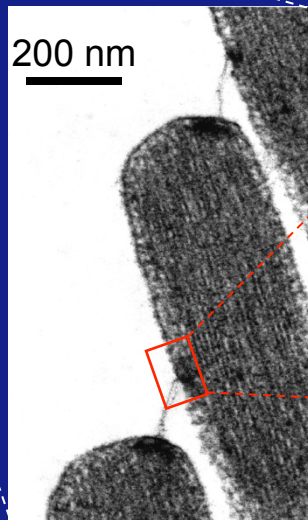
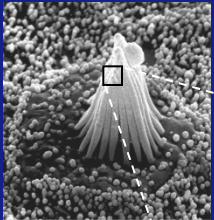
→ calcium = control parameter



(Tinevez, Jülicher and Martin, Biophys J (2007))

Adaptation motors:

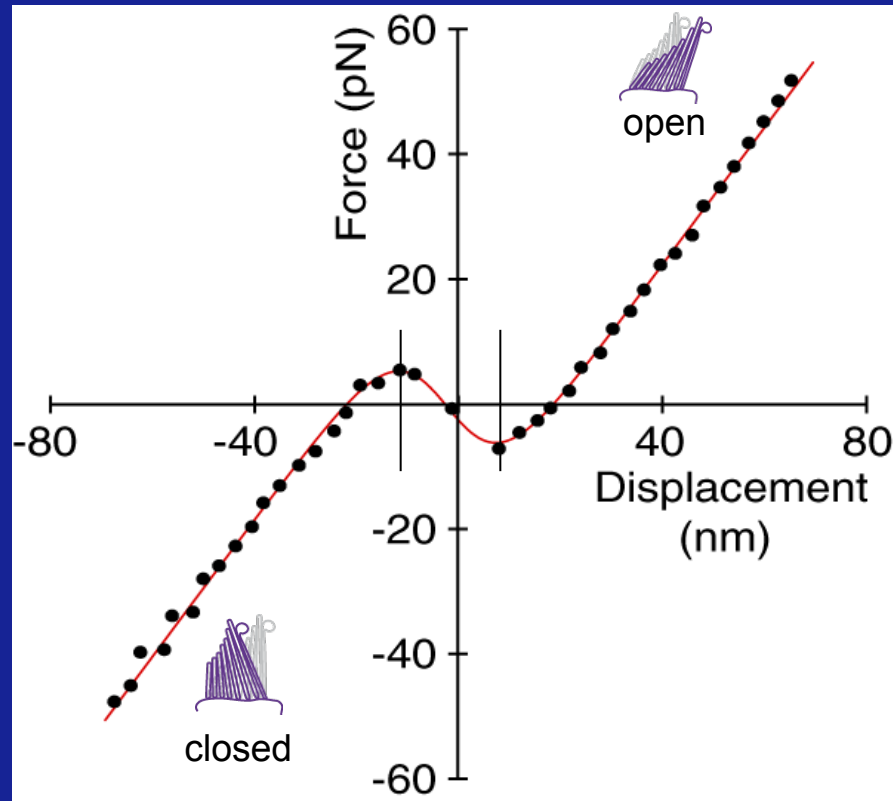
→ set the tip links under tension

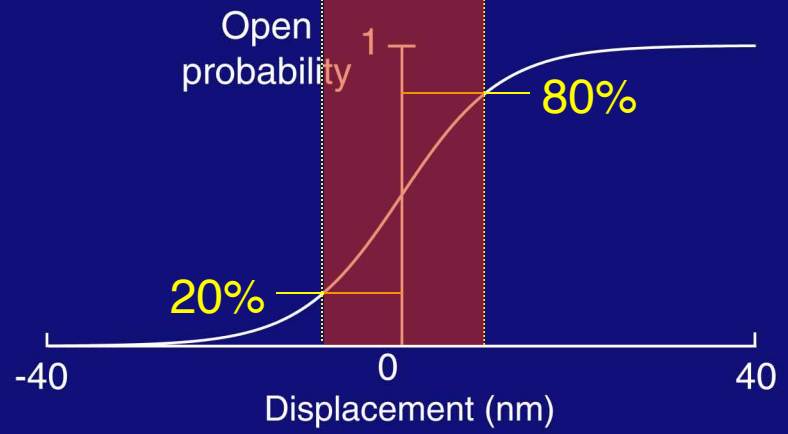
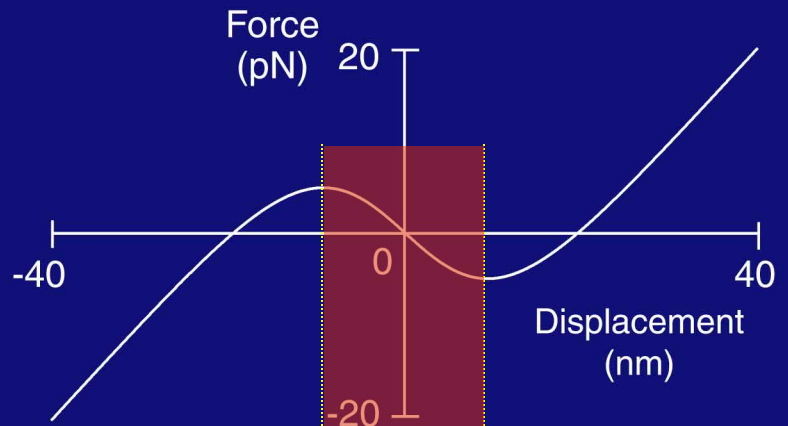


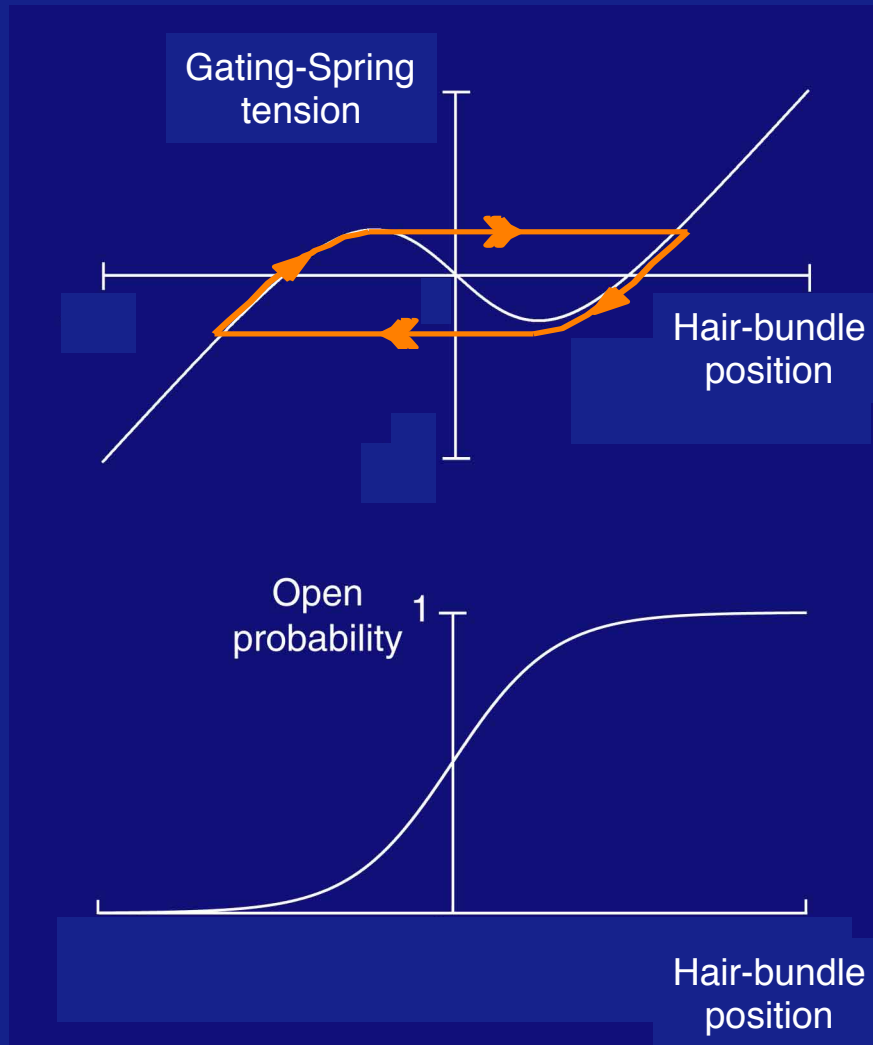
Myosin 1c
(Myosin 7a)

Negative stiffness

→ (passive) mechanical instability







Active dynamical system

$$\left\{ \begin{array}{l} \text{Hair bundle:} \\ \text{Motor:} \end{array} \right. \quad \lambda \frac{dX}{dt} = -\mathbf{K}_{GS}(X - X_a - DP_o) - \mathbf{K}_{SP}X + F_{EXT}$$
$$\lambda_a \frac{dX_a}{dt} = \mathbf{K}_{GS}(X - X_a - DP_o) - F_a$$

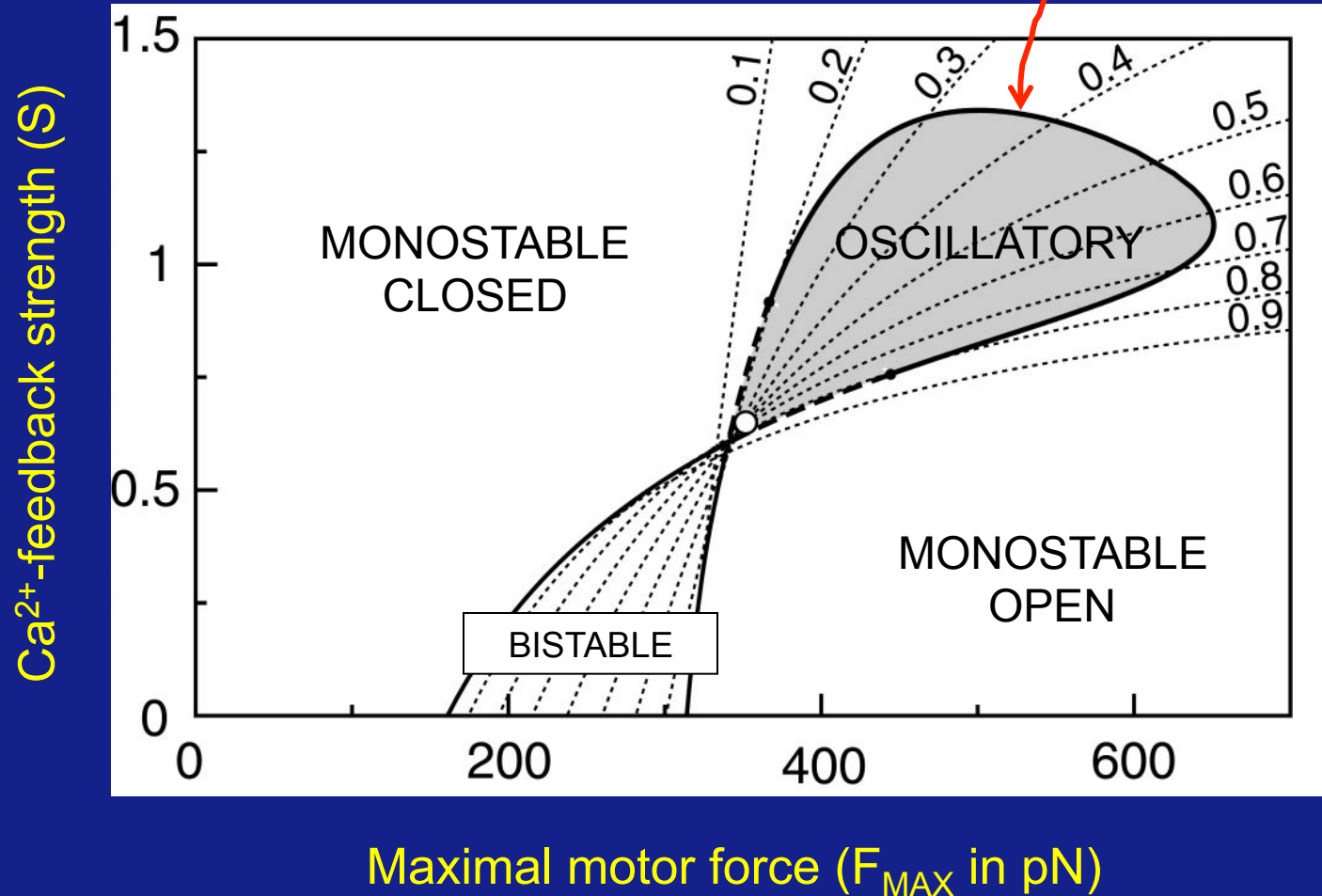
Tip-link
tension

$$\text{Motor force: } F_a = F_{\max} (1 - SP_o)$$

$$\text{Open probability: } P_o = 1 / (1 + A \exp(-(X - X_a) / \delta))$$

Hair-bundle model: state diagram

Hopf bifurcation



A simpler linear model

Bundle position: $\lambda X = -kX + F \downarrow a$

$$k = K \downarrow GS (1 - D P' \downarrow o \uparrow)$$

$$k = k + K \downarrow SP$$

Active force: $\tau \downarrow a F \downarrow a = k X - F \downarrow a$

$$F \downarrow a = k X \downarrow a$$

$$\tau \downarrow a = \lambda \downarrow a / (k + SF \downarrow MAX P' \downarrow o \uparrow)$$



$$(\lambda \tau \downarrow a) X = -(\lambda + k \tau \downarrow a) X - (k - k) X$$

$m \downarrow EFF$

$\lambda \downarrow EFF$

$k \downarrow EFF$

Linear stability analysis

Bundle position: $\lambda X = -kX + F \downarrow a$

Adaptation force: $\tau \downarrow a \quad F \downarrow a = kX - F \downarrow a$



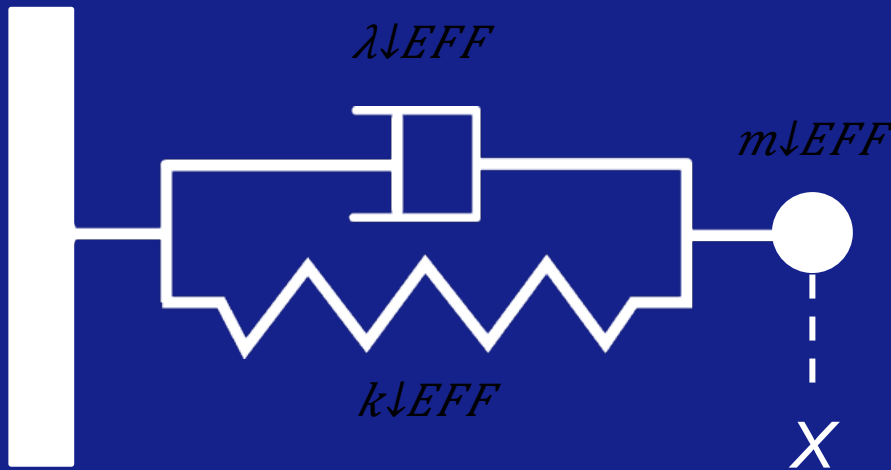
$$(\lambda \tau \downarrow a) X = -(\lambda + k \tau \downarrow a) X - (k - k) X$$

$m \downarrow \text{EFF}$

$\lambda \downarrow \text{EFF}$

$k \downarrow \text{EFF}$

An effective (active) spring-mass system



stiffness: $k \downarrow EFF = k - k$
 « mass »: $m \downarrow EFF = \lambda \tau \downarrow a$
 friction: $\lambda \downarrow EFF = \lambda + k \tau \downarrow a$

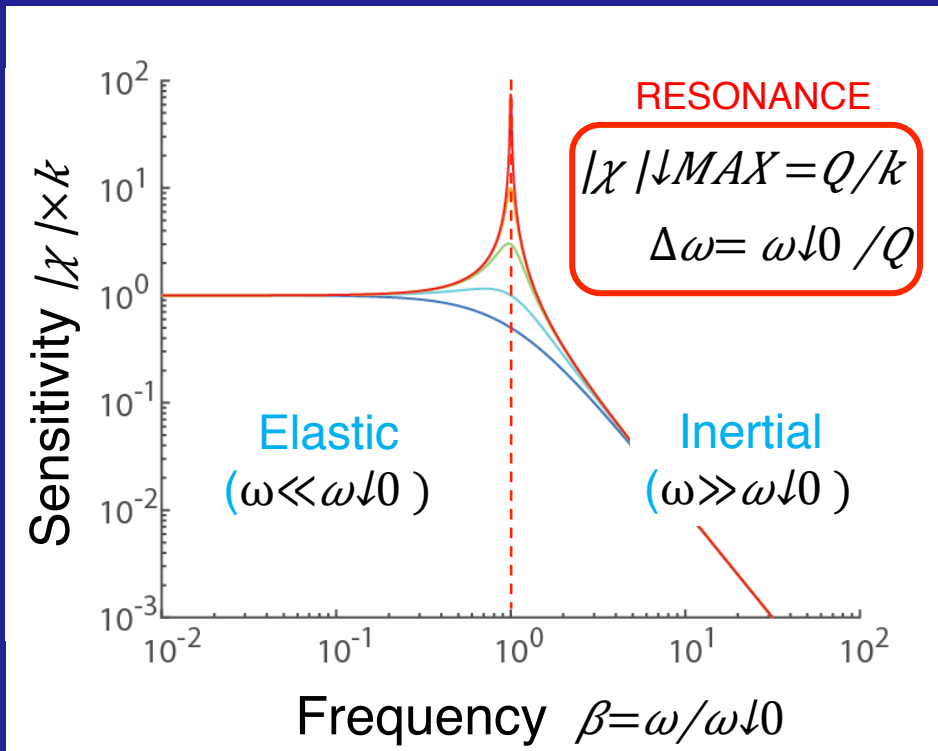
if $k > 0$, $\lambda \downarrow EFF > \lambda$: increased damping

if $k < 0$, $\lambda \downarrow EFF < \lambda$: reduced damping

Resonant behavior if $Q = \sqrt{k \downarrow EFF / m \downarrow EFF} / \lambda \downarrow EFF > 1$

Hopf bifurcation at $\lambda \downarrow EFF = 0$ with frequency $\sqrt{k \downarrow EFF / m \downarrow EFF}$

Mechanical resonance



RESPONSE FUNCTION

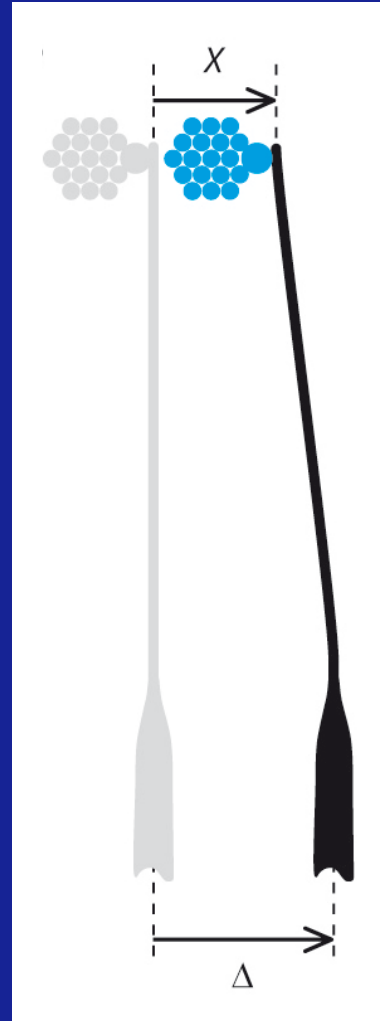
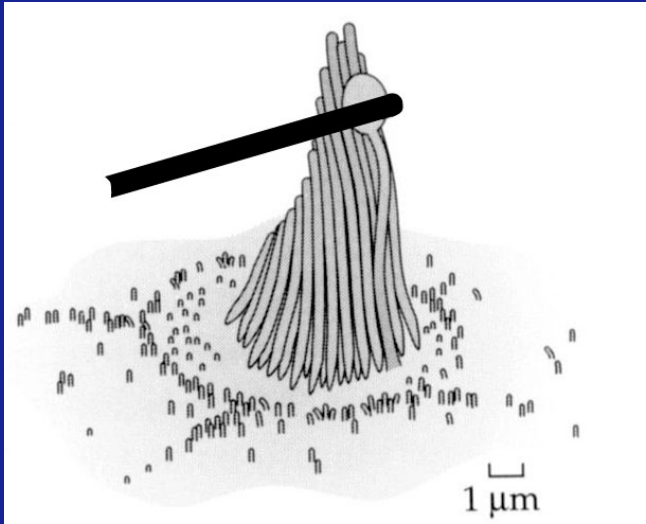
$$\chi = 1/k / [1 - \beta^2 + i\beta/Q]$$

with $\chi = X/F$

$$(F(t) = F e^{i\omega t}; X(t) = X e^{i\omega t})$$

Characteristic frequency: $\omega_0 = \sqrt{k/m}$

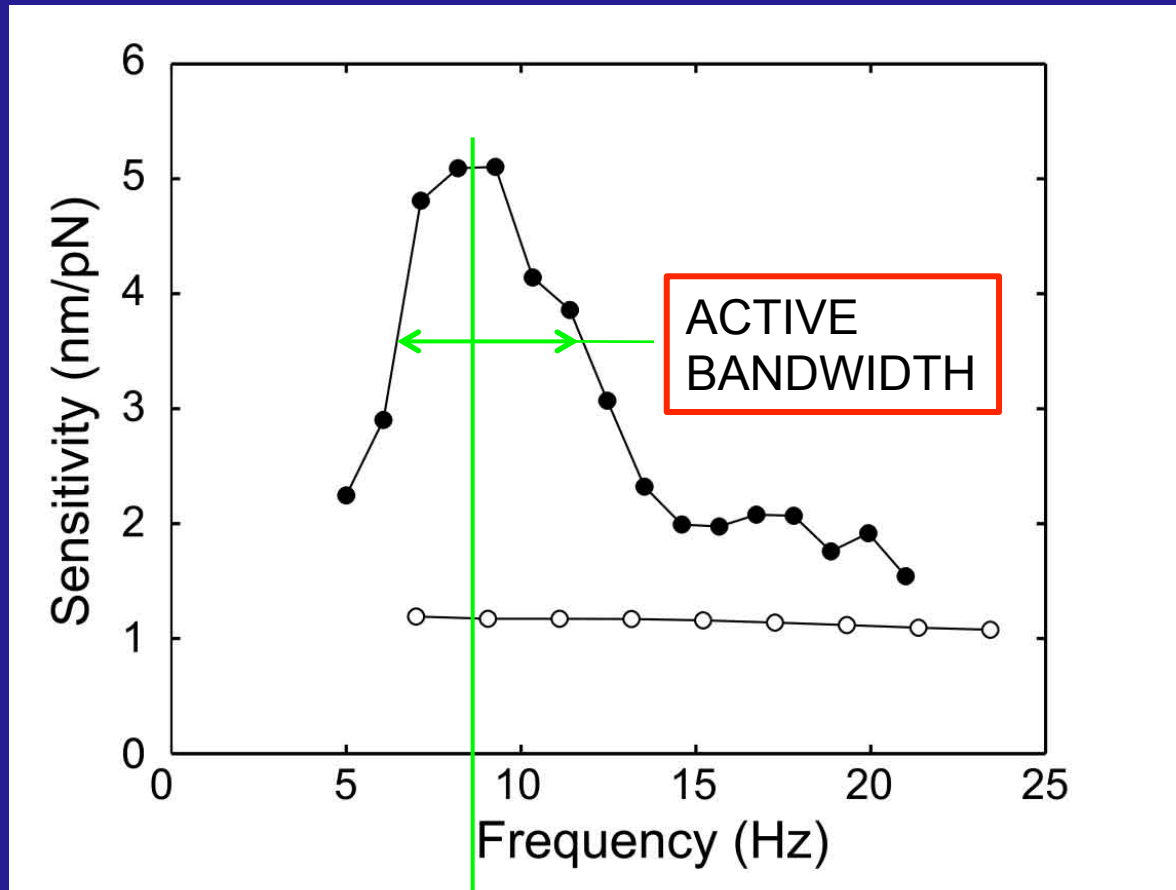
Quality factor: $Q = \sqrt{k m} / \lambda = \omega_0 / \Delta\omega$



Active resonance

$(F_1 \cong 5 \text{ pN})$

STIMULUS: $F(t) = F_1 \sin(2\pi f_1 t)$

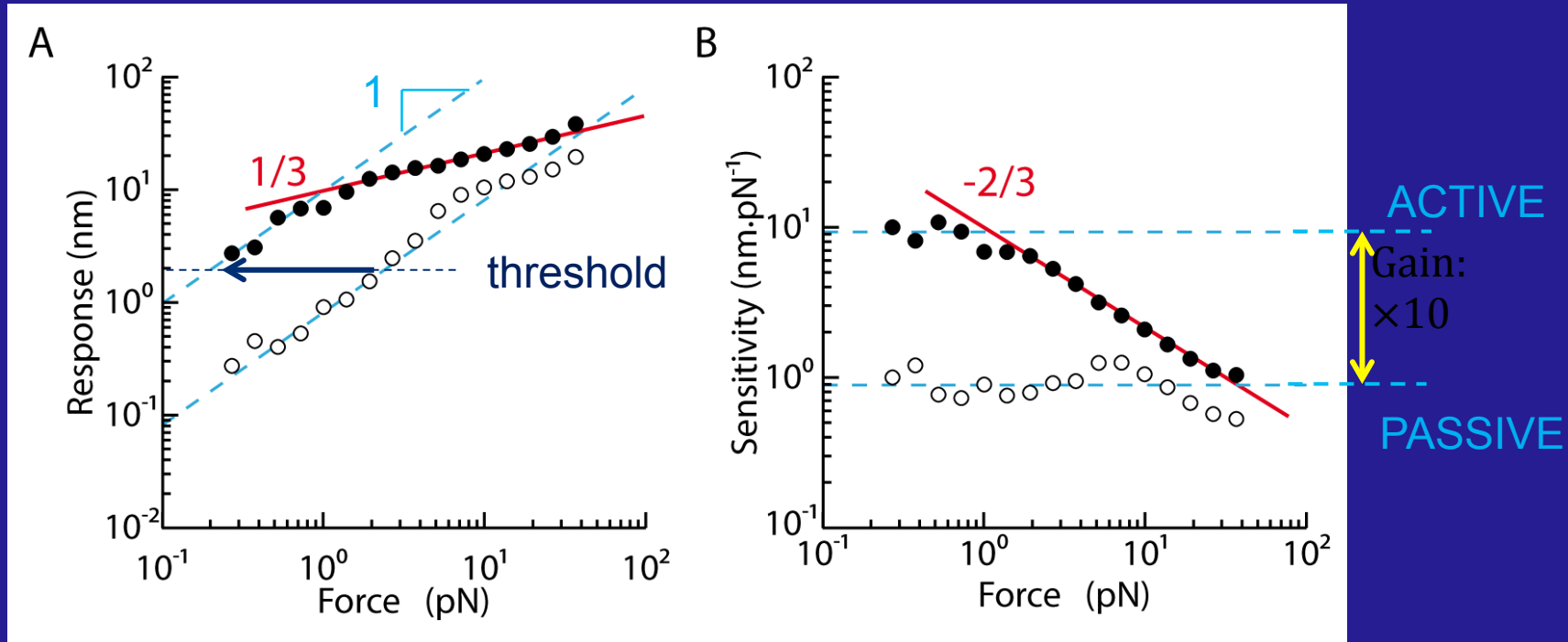


- Oscillatory ($\sim 8 \text{ Hz}$)
- Non oscillatory

f_c

Dynamic non-linearity

STIMULUS: $F(t) = F_0 \sin(2\pi f_0 t)$



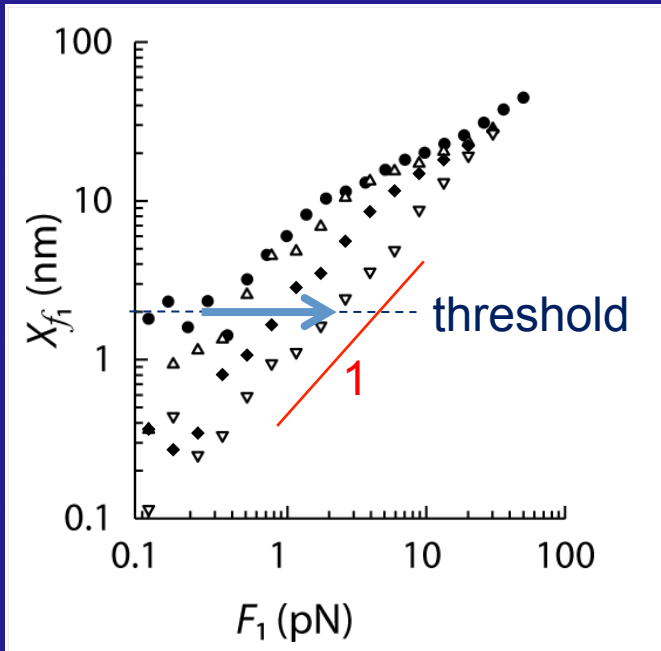
- at resonance ($f_1 = 9$ Hz)
- off resonance ($f_1 = 180$ Hz)

(Martin and Hudspeth, PNAS (2001))

Two-tone response

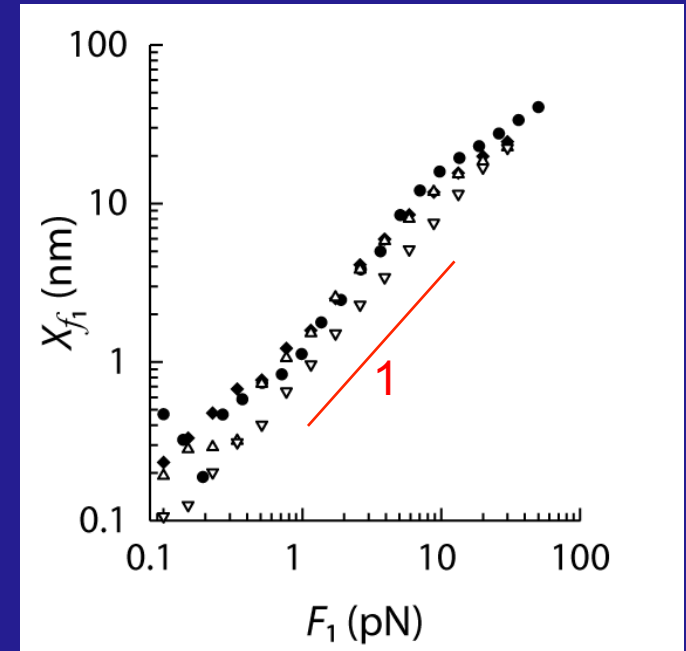
$$F(t) = \underbrace{F_1 \sin(2\pi f_1 t)}_{\text{test tone}} + \underbrace{F_2 \sin(2\pi f_2 t)}_{\text{masker tone}} \quad (f_2 / f_1 = 1.1)$$

At resonance
($f_1, f_2 \approx f_c$)



- $F_2 = 0$ pN
- △ $F_2 = 2$ pN
- ◆ $F_2 = 5$ pN
- ▽ $F_2 = 20$ pN

Off resonance
($f_1, f_2 \gg f_c$)

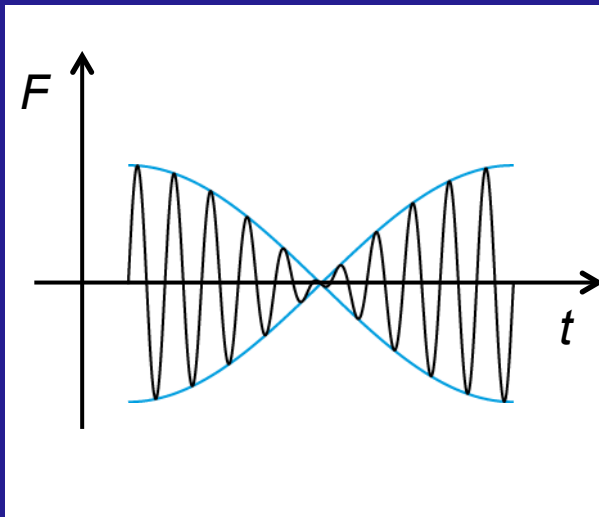


➔ Frequency-specific masking

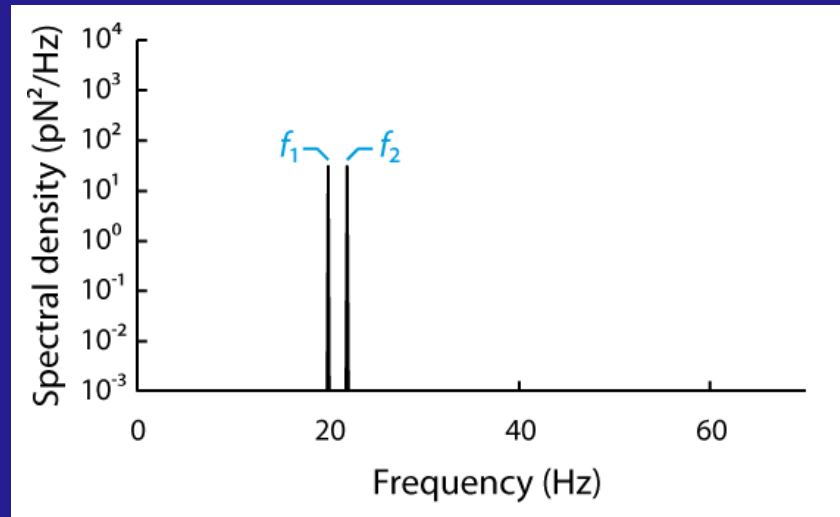
Two-tone stimulus

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t) \quad (f_2 / f_1 = 1.1)$$

Beating pattern



Power spectrum



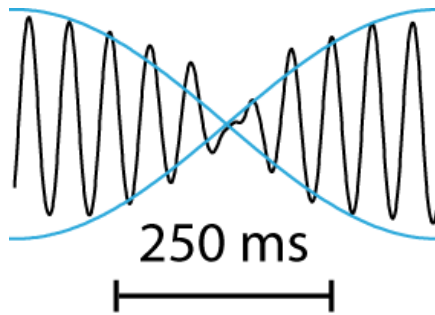
High-fidelity amplifier?

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t) \quad (F = 2 \text{ pN})$$

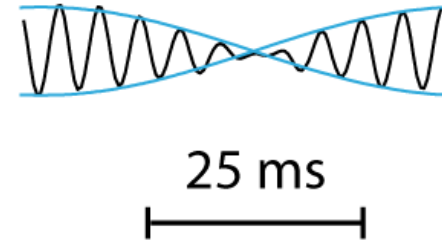
At resonance
($f_1, f_2 \approx f_c$)

Off resonance
($f_1, f_2 \gg f_c$)

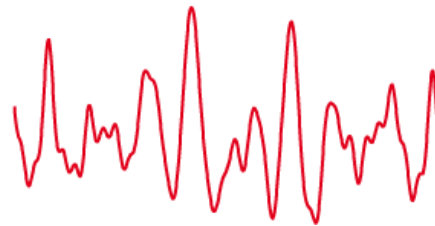
HB motion



40 nm



Distortions
(primaries
filtered out)



5 nm



$f_1 = 20 \text{ Hz}$
 $f_2 = 22 \text{ Hz}$

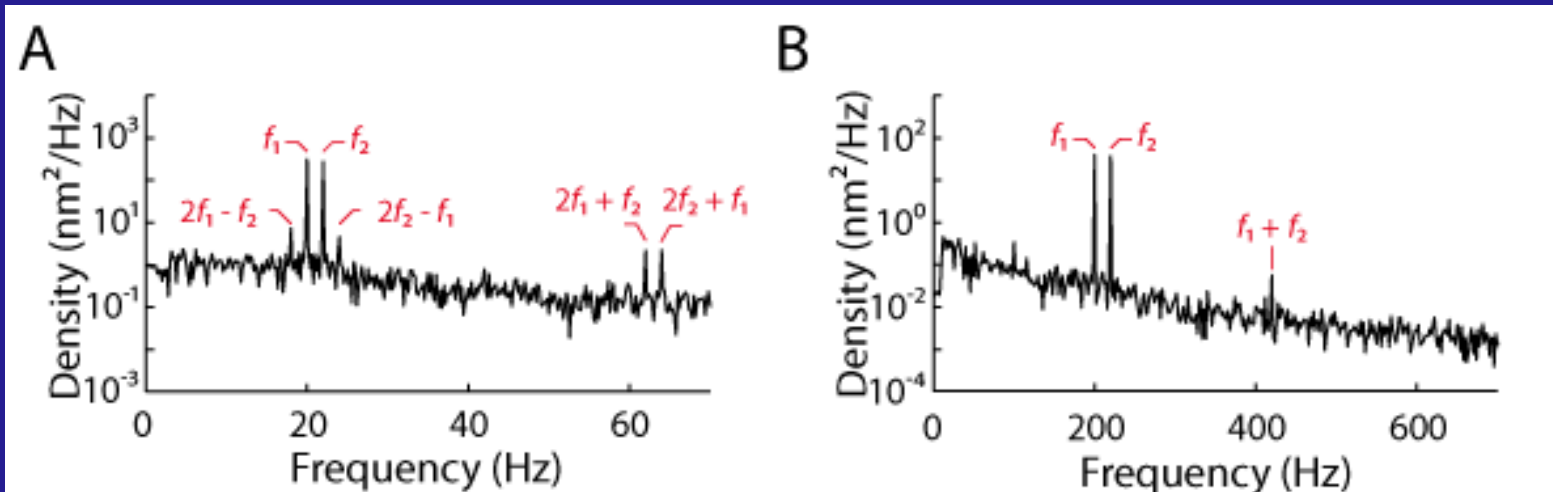
$f_1 = 200 \text{ Hz}$
 $f_2 = 220 \text{ Hz}$

Distortion products

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t) \quad (F = 2 \text{ pN})$$

At resonance
($f_1, f_2 \approx f_c$)

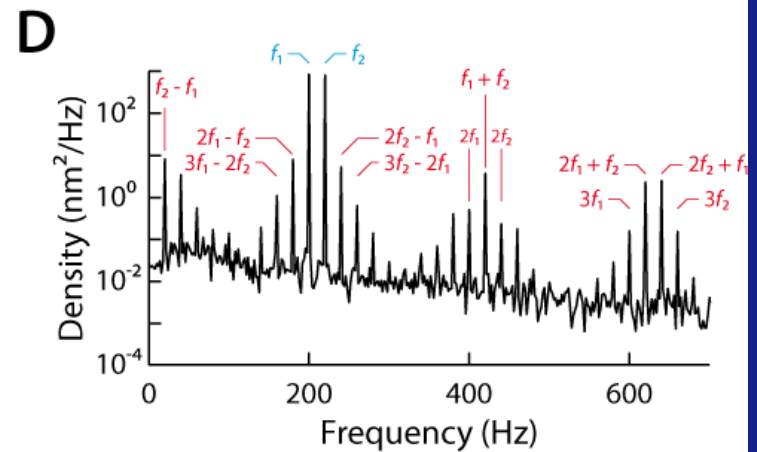
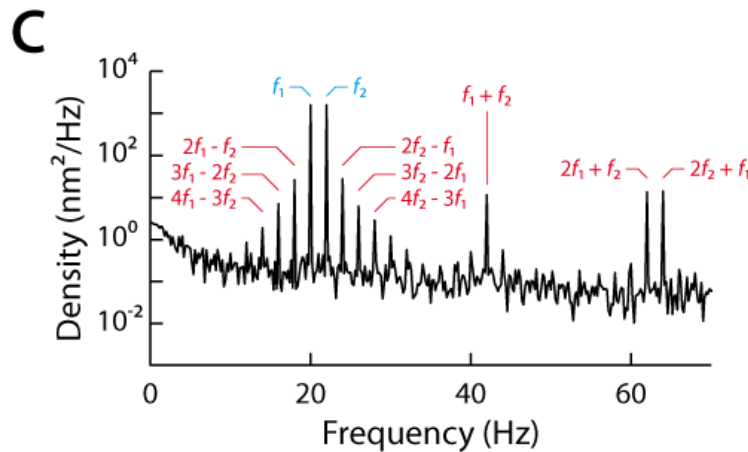
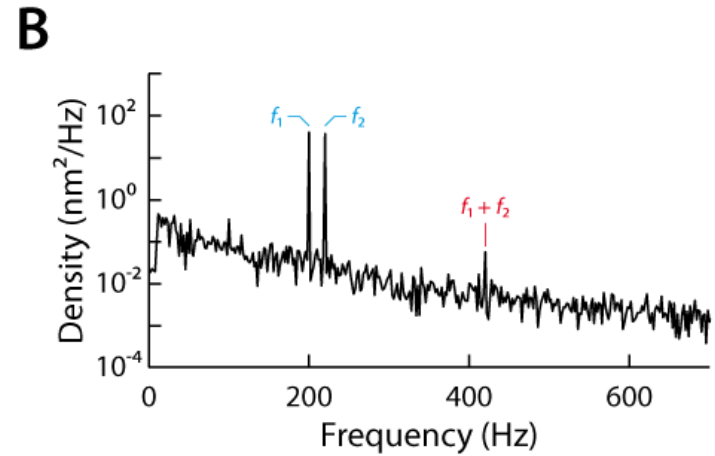
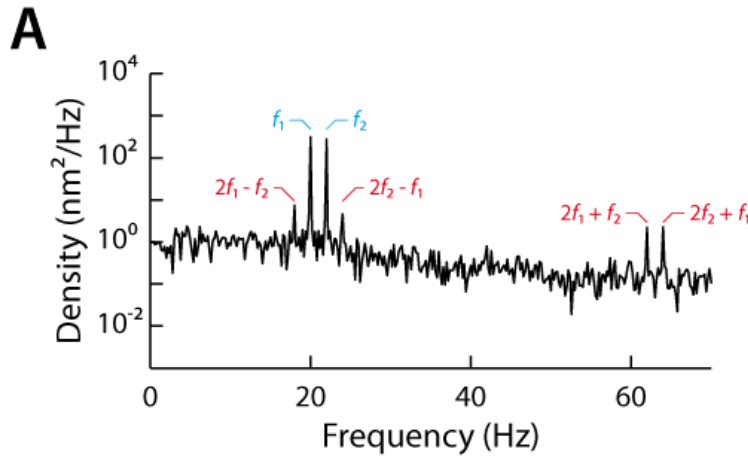
Off resonance
($f_1, f_2 \gg f_c$)



At resonance
 $(f_1, f_2 \approx f_c)$

Off resonance
 $(f_1, f_2 \gg f_c)$

2 pN

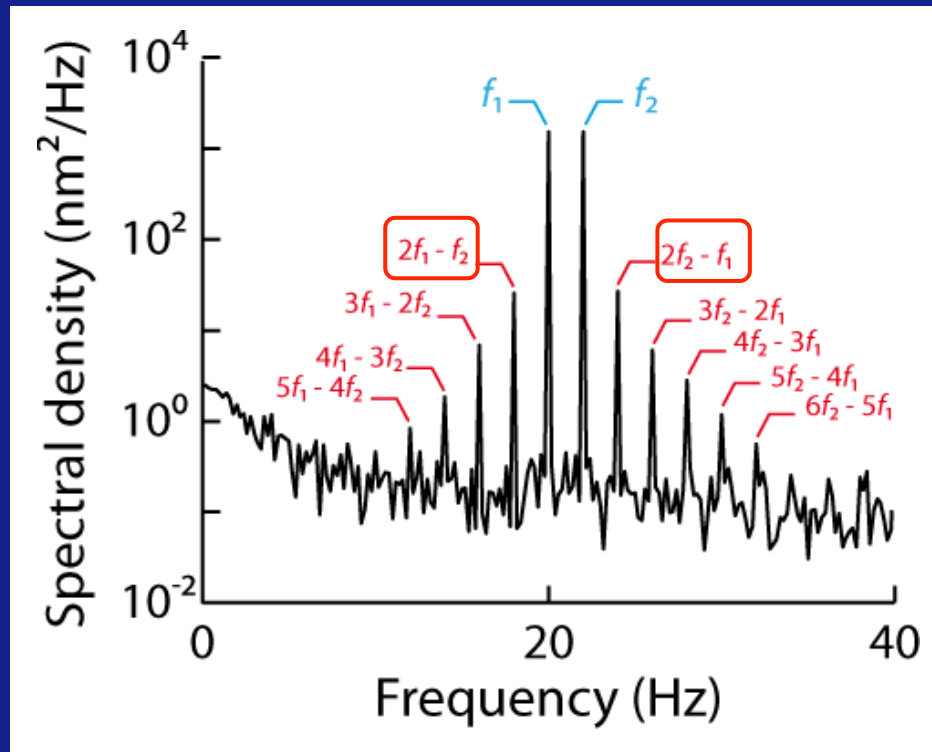


10.1 pN

“Colored” response

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t)$$

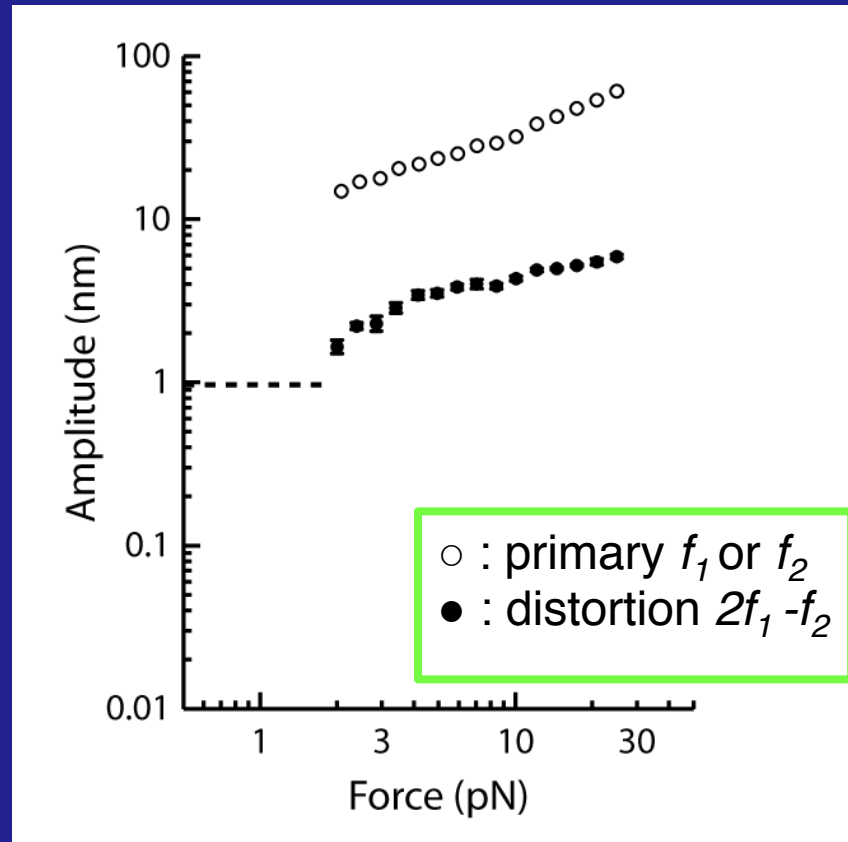
($F = 10.8 \text{ pN}$)



CUBIC
DISTORTIONS

Distortion $2f_1 - f_2$ at resonance

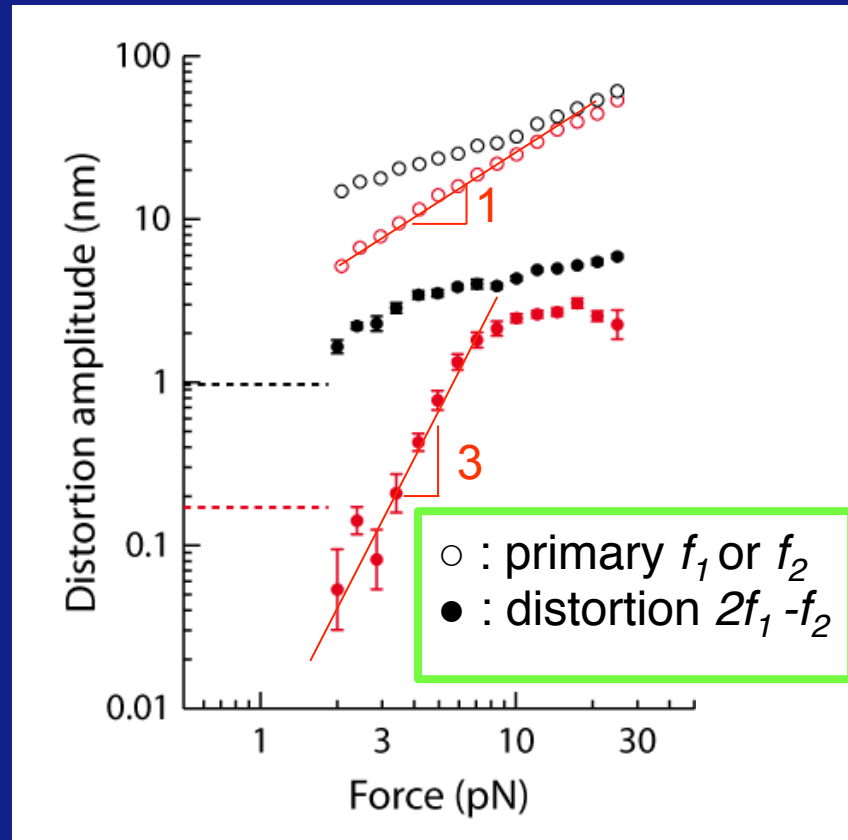
$(f_1, f_2 \approx f_c)$



CONSTANT RELATIVE LEVEL (~15%)!

Distortion $2f_1 - f_2$

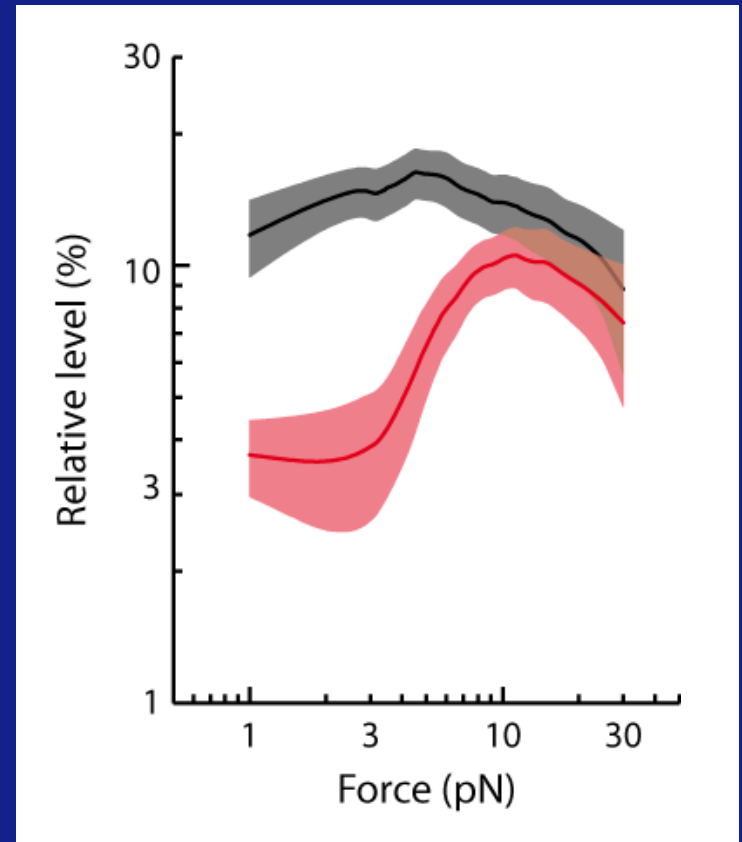
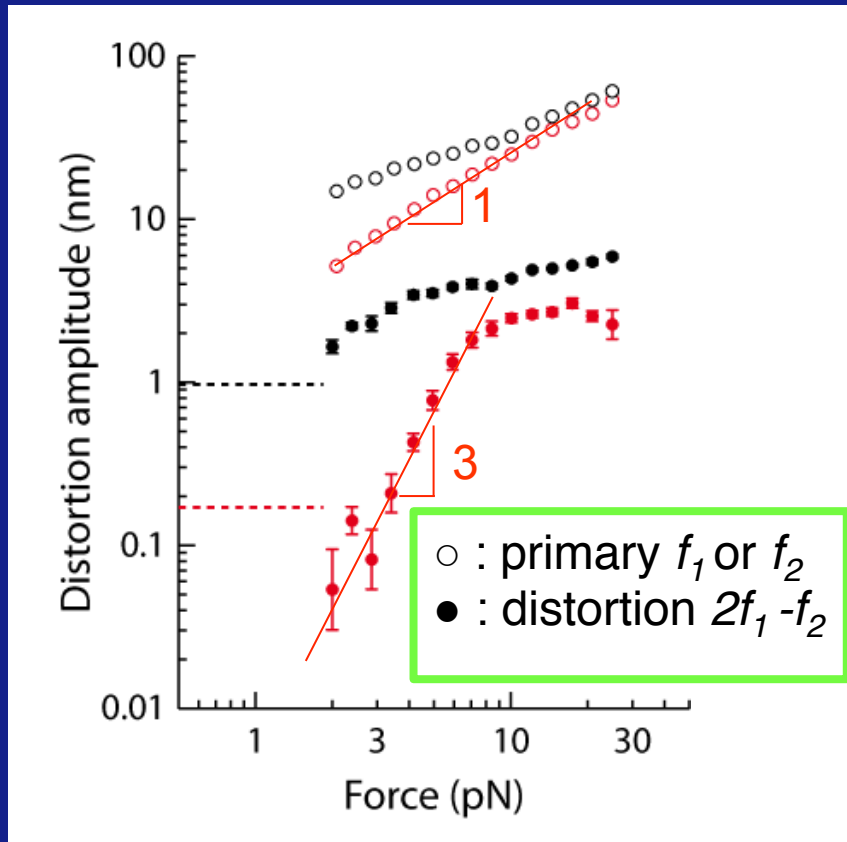
At resonance – Off resonance



ACTIVE MECHANICS ↔ PASSIVE MECHANICS
(black) (red)

Distortion $2f_1 - f_2$

At resonance – Off resonance



ACTIVE MECHANICS ↔ PASSIVE MECHANICS
(black) (red)

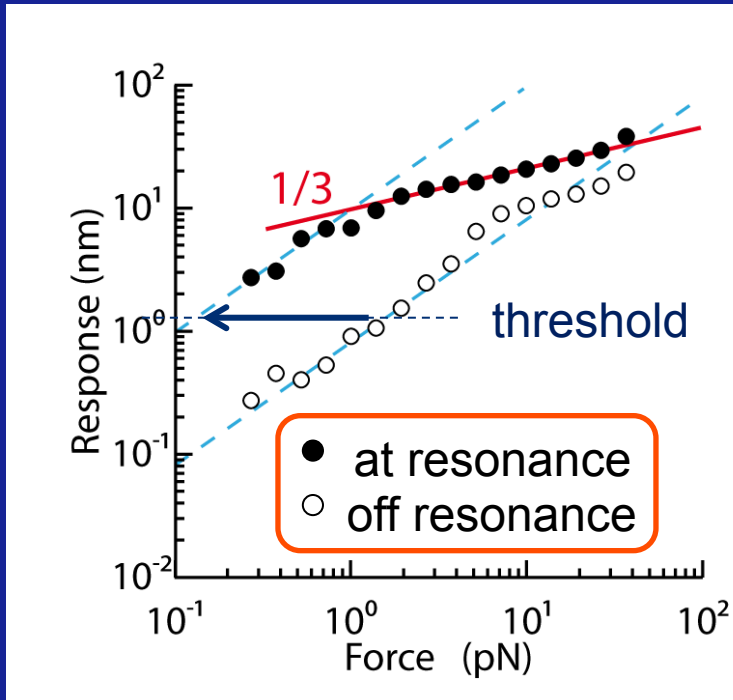
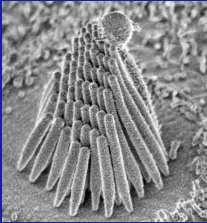
« Phantom tones » from a single oscillatory hair bundle

$$F(t) = \bar{F} \cos(2\pi f_1 t) + \bar{F} \cos(2\pi f_2 t)$$

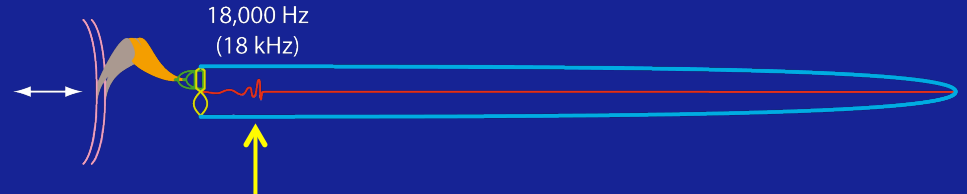
- cubic distortion dominates ($2f_1-f_2$, $2f_2-f_1$)
- appear at low stimulation levels ($F \geq 1$ pN)
- relative level at $2f_1-f_2$ nearly independent of stimulus level (15-20%)
- inherent frequency specificity (f_1 and f_2 must be near f_c)

→ because of nonlinear amplification from active oscillation!

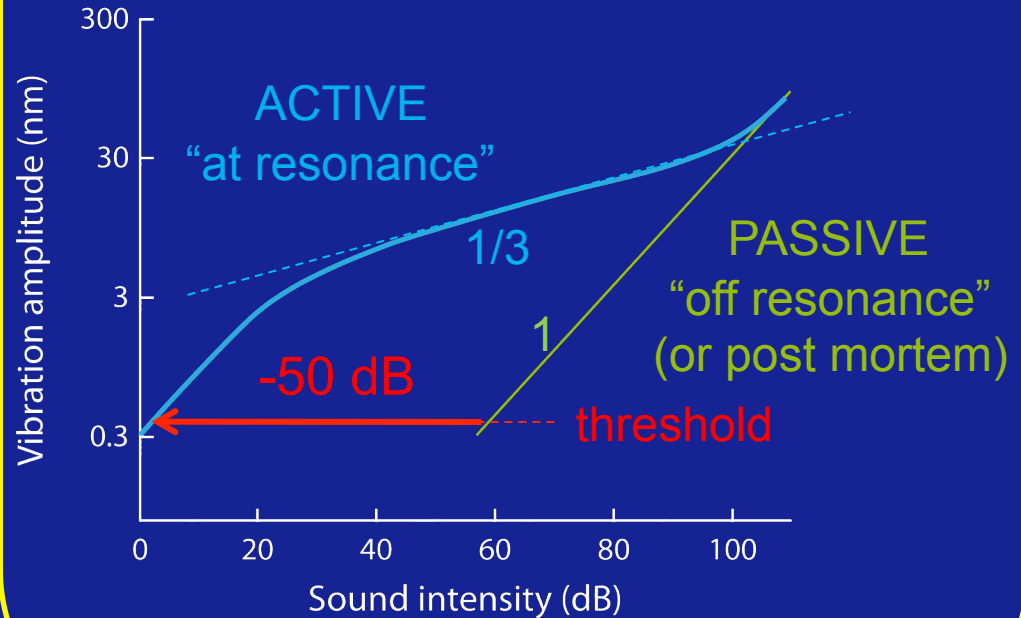
SINGLE HAIR-BUNDLE



COCHLEA IN VIVO



⇒ Same physics!



(inspired by: Ruggero et al., JASA (1997))

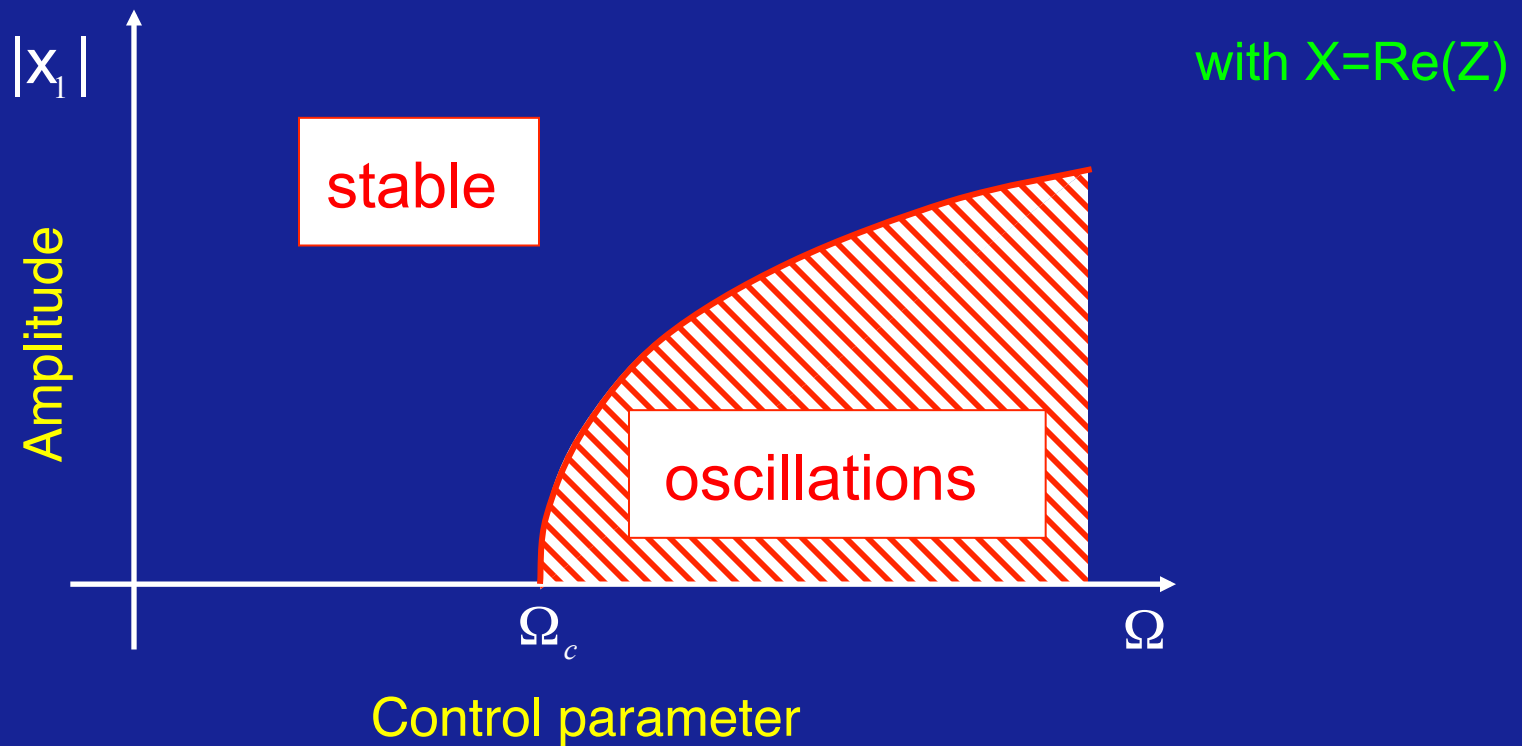
A useful concept: the « critical » oscillator

*(Choe, Magnasco, Hudspeth, PNAS (1998); Camalet, Duke, Jülicher, Prost, PNAS (2000)
Eguíluz, Ospeck, Choe, Hudspeth, Magnasco, Phys. Rev. Lett. (2000);
Jülicher, Andor and Duke, PNAS (2001))*

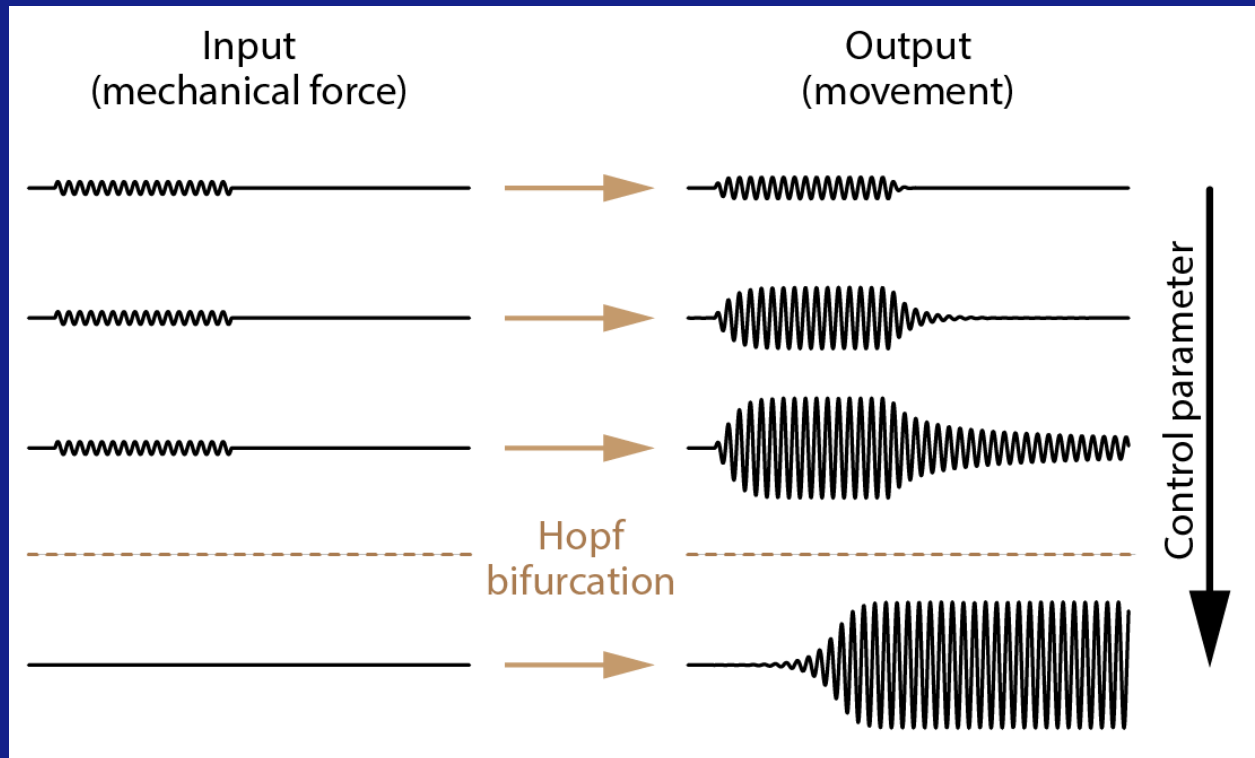
Hopf bifurcation

→ « Normal form »

$$dZ/dt \cong -(\Omega_c - \Omega - i 2\pi f_c) Z - B|Z|^2 Z + F/\Lambda$$



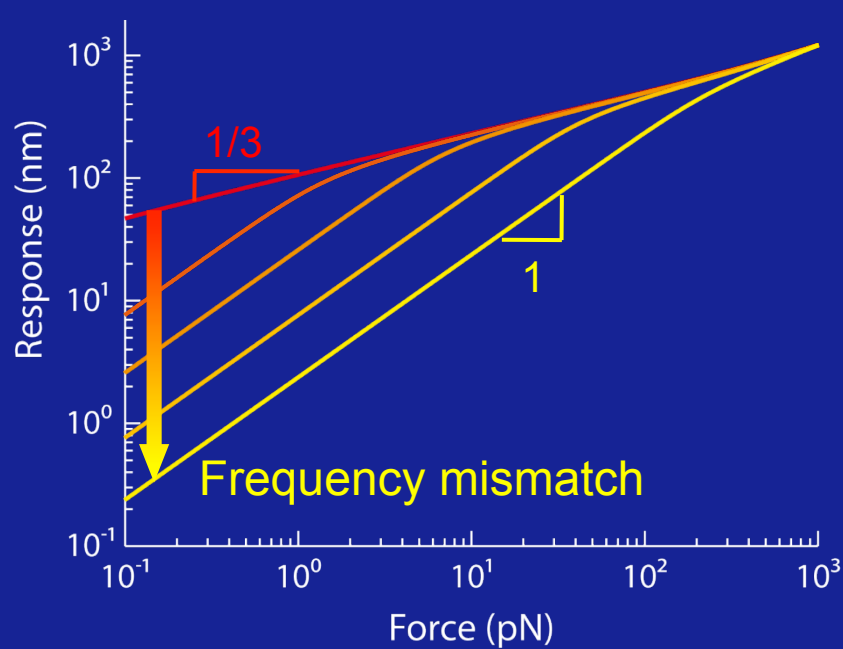
Critical point: $\Omega = \Omega_c$



(Hudspeth, Nat Neurosci (2014))

« Critical » oscillator: generic properties

$$F(t) = F_0 \sin(2\pi f_0 t) \rightarrow X(t) = \sum_n X_n e^{i n \omega t}$$



$f_c = 100$ Hz

- $f_l = 100$ Hz
- $f_l = 99$ Hz
- $f_l = 97$ Hz
- $f_l = 90$ Hz
- $f_l = 70$ Hz

$$F_0 \cong A(f_l) X_0 + B |X_0|^2 X_0$$

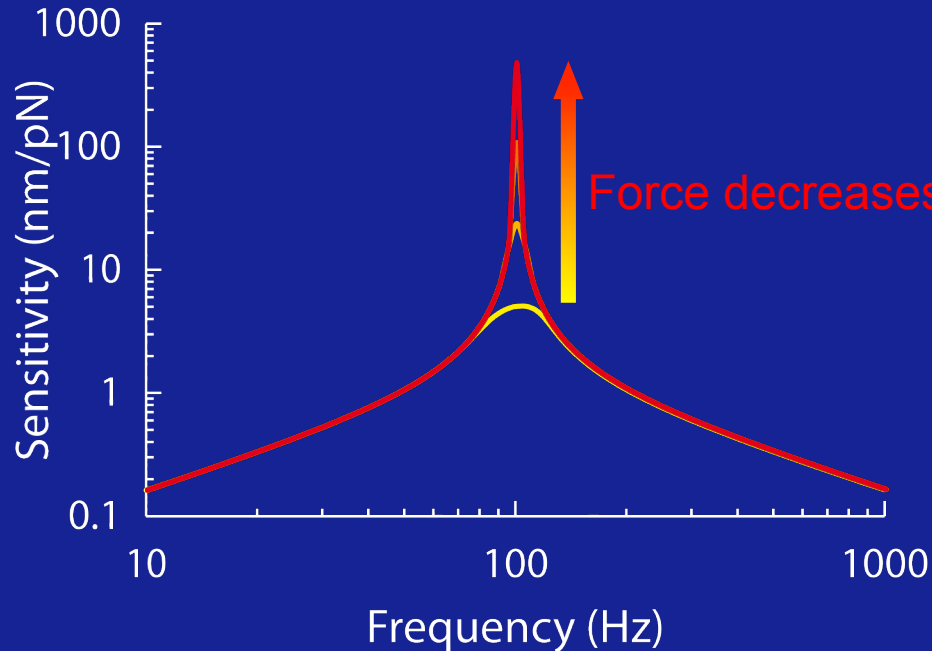
with: $A(f_l = f_c) = 0!$

(Choe, Magnasco, Hudspeth, PNAS (1998); Camalet, Duke, Jülicher, Prost, PNAS (2000)
Eguíluz, Ospeck, Choe, Hudspeth, Magnasco, Phys. Rev. Lett. (2000))

« Critical » oscillator: generic properties

$$F(t) = F_1 \sin(2\pi f t) \rightarrow X(t) = \sum_n \hat{X}_n e^{i n 2\pi f t}$$

$(f_c = 100 \text{ Hz})$



$F_1 = 100 \text{ pN}$

$F_1 = 10 \text{ pN}$

$F_1 = 1 \text{ pN}$

$F_1 = 0.1 \text{ pN}$

$$F_1 \cong A(f) X_1 + B |X_1|^2 X_1$$

with: $A(f = f_c) = 0 !$

(Choe, Magnasco, Hudspeth, PNAS (1998); Camalet, Duke, Jülicher, Prost, PNAS (2000)
Eguíluz, Ospeck, Choe, Hudspeth, Magnasco, Phys. Rev. Lett. (2000))

Two-tone distortions

(simulations)

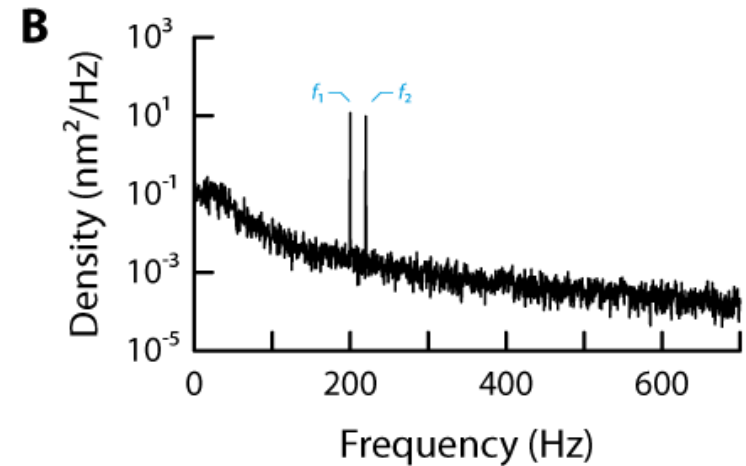
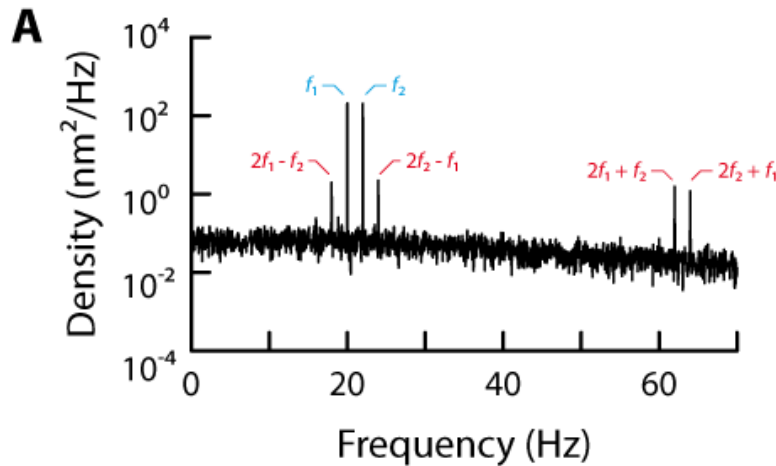
At resonance

$$(f_1, f_2 \approx f_c)$$

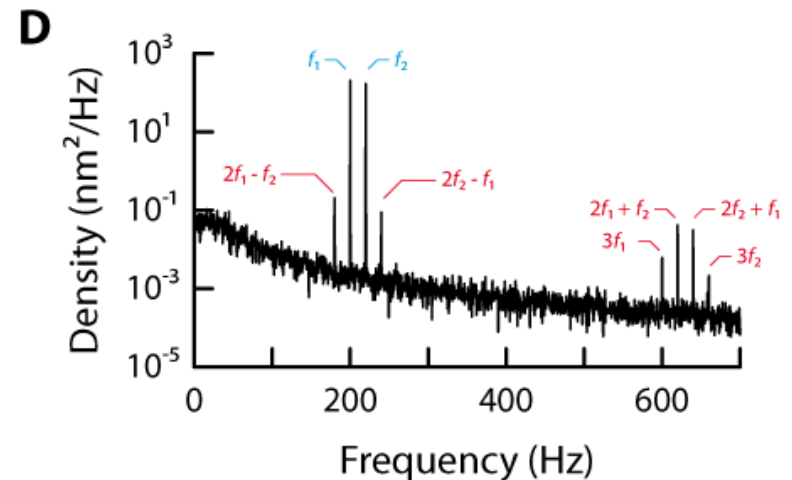
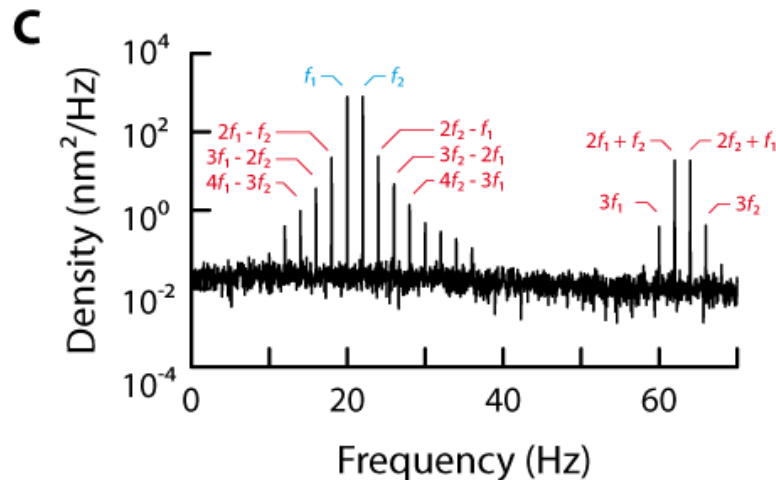
Off resonance

$$(f_1, f_2 \gg f_c)$$

0.9 pN



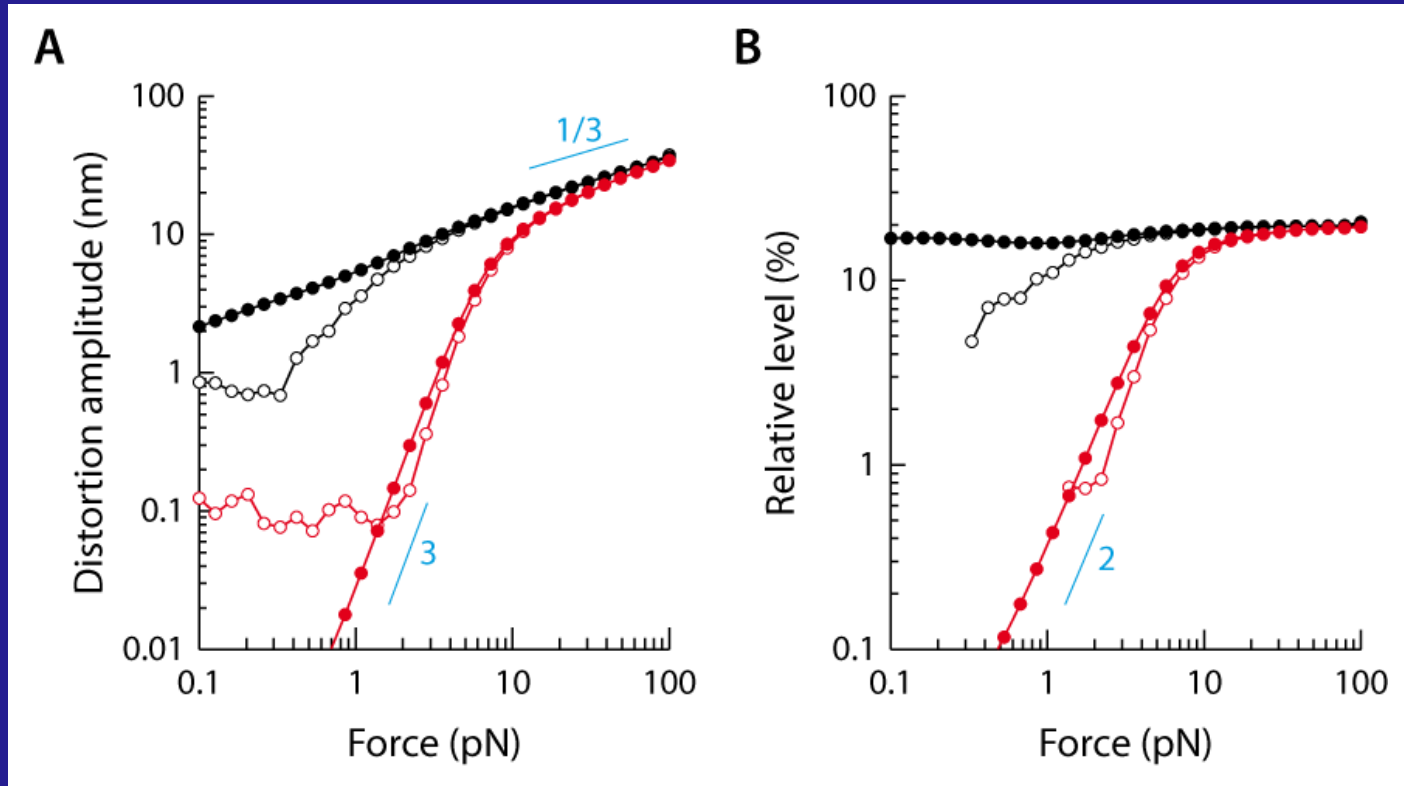
3.6 pN



Distortion $2f_1 - f_2$: level functions

$$F(t) = \bar{F} \sin(2\pi f_1 t) + \bar{F} \sin(2\pi f_2 t)$$

(simulations)



No noise

With noise

● : at resonance
● : off resonance

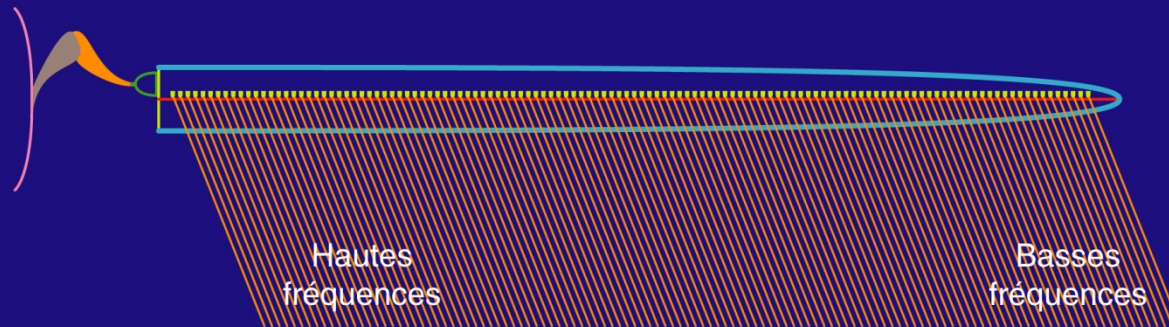
○ : at resonance
○ : off resonance

Critical oscillators: nonlinear amplifiers for hearing

1. Amplified movements for small stimuli
2. Extended dynamic range of responsiveness
3. Increased frequency selectivity
4. « Essential » compressive nonlinearity: **prominent masking and cubic distortions within the active bandwidth.**

Outlook:

tonotopic organisation of critical oscillators



Acknowledgments:



Jérémie Barral and his princess



Frank
Jülicher
(MPIPKS, Dresden)



Coming next:

1. The physical limit to mechanosensitivity of a single hair cell: **noise and friction**
2. Teaming-up to boost mechanosensitivity: **the effects of mechanical coupling.**
3. Mechanical gradients to tune the characteristic frequency of a hair cell