

On the physical limit of hair- bundle mechanosensitivity: friction, noise, coupling.

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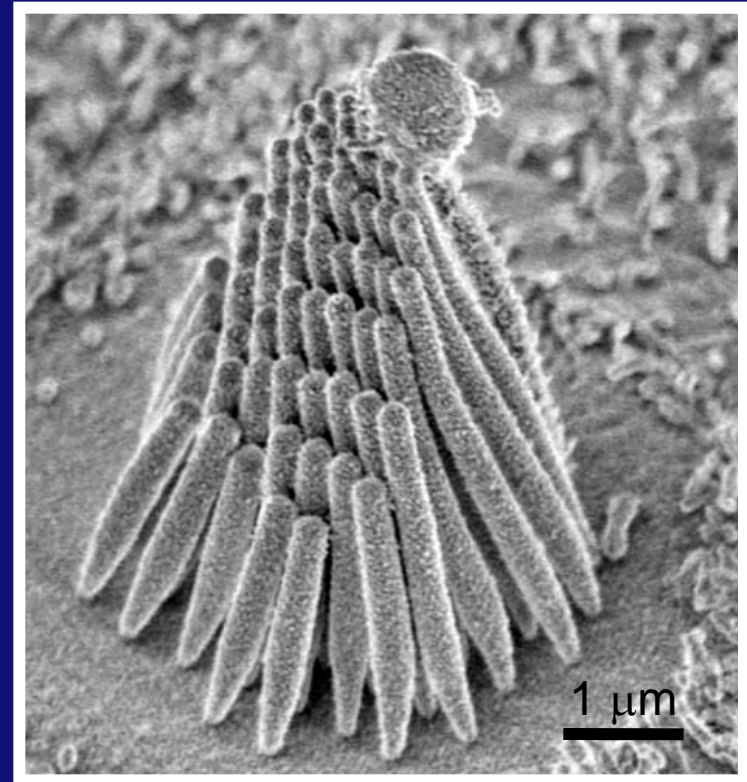
pascal.martin@curie.fr



The hair cell

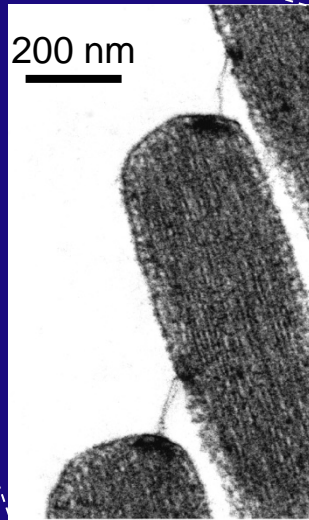
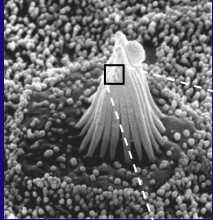


(A.J. Hudspeth)

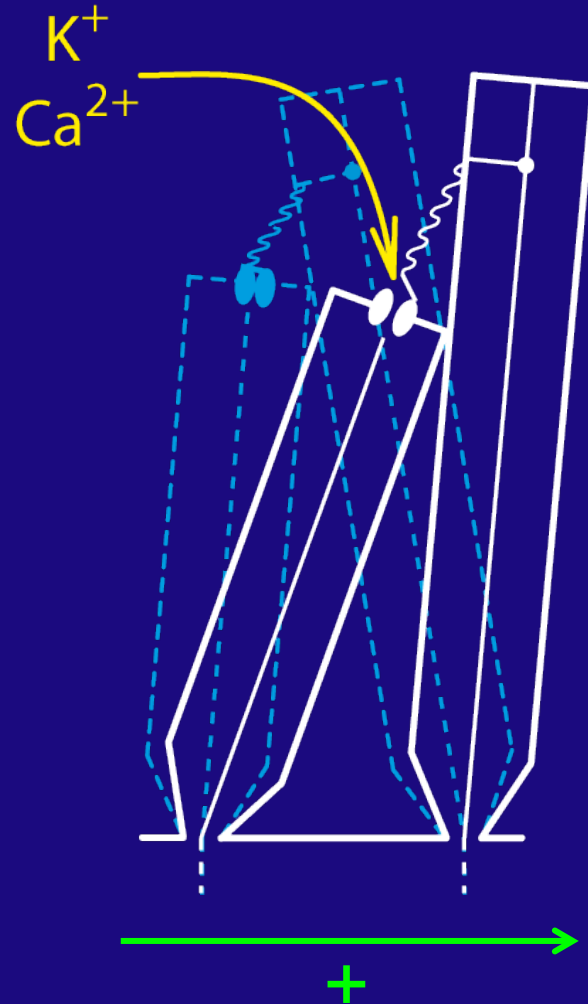


(P. Gillespie)

The hair-cell bundle: mechanical antenna



(A.J. Hudspeth)



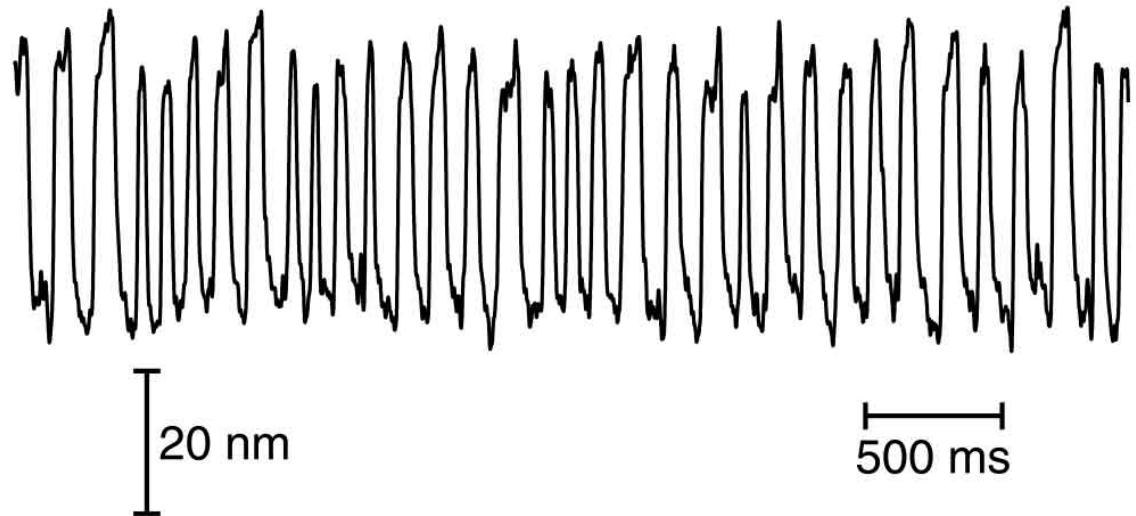


(bullfrog)

The hair-cell bundle

→ sensory and motile

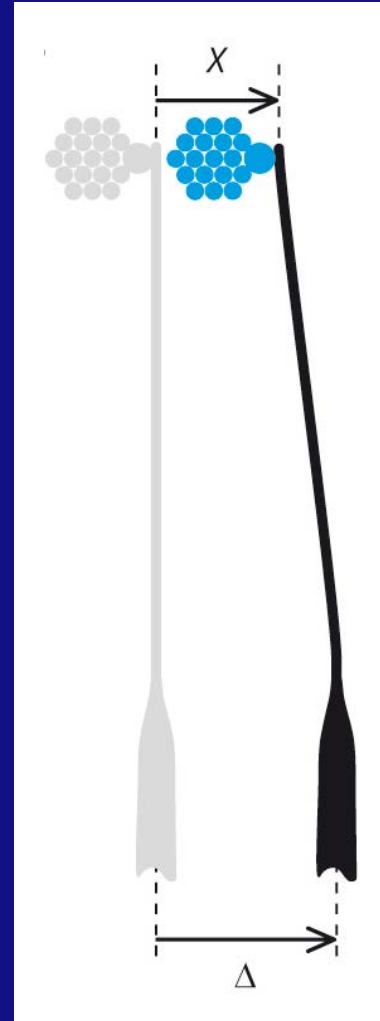
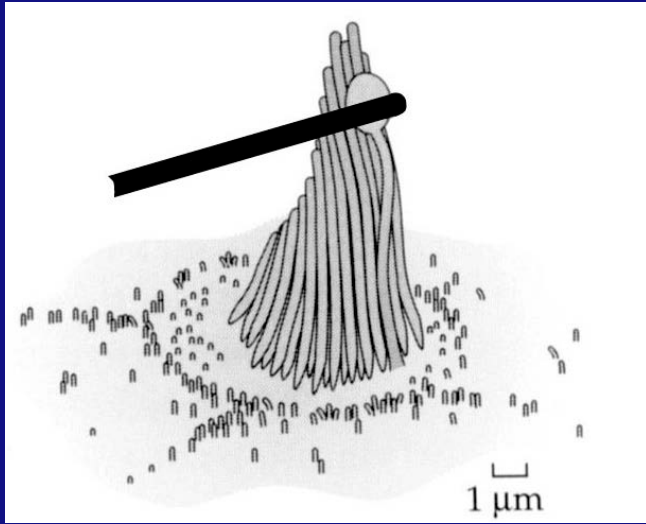
SPONTANEOUS OSCILLATIONS



(Martin and Hudspeth, PNAS (1999))



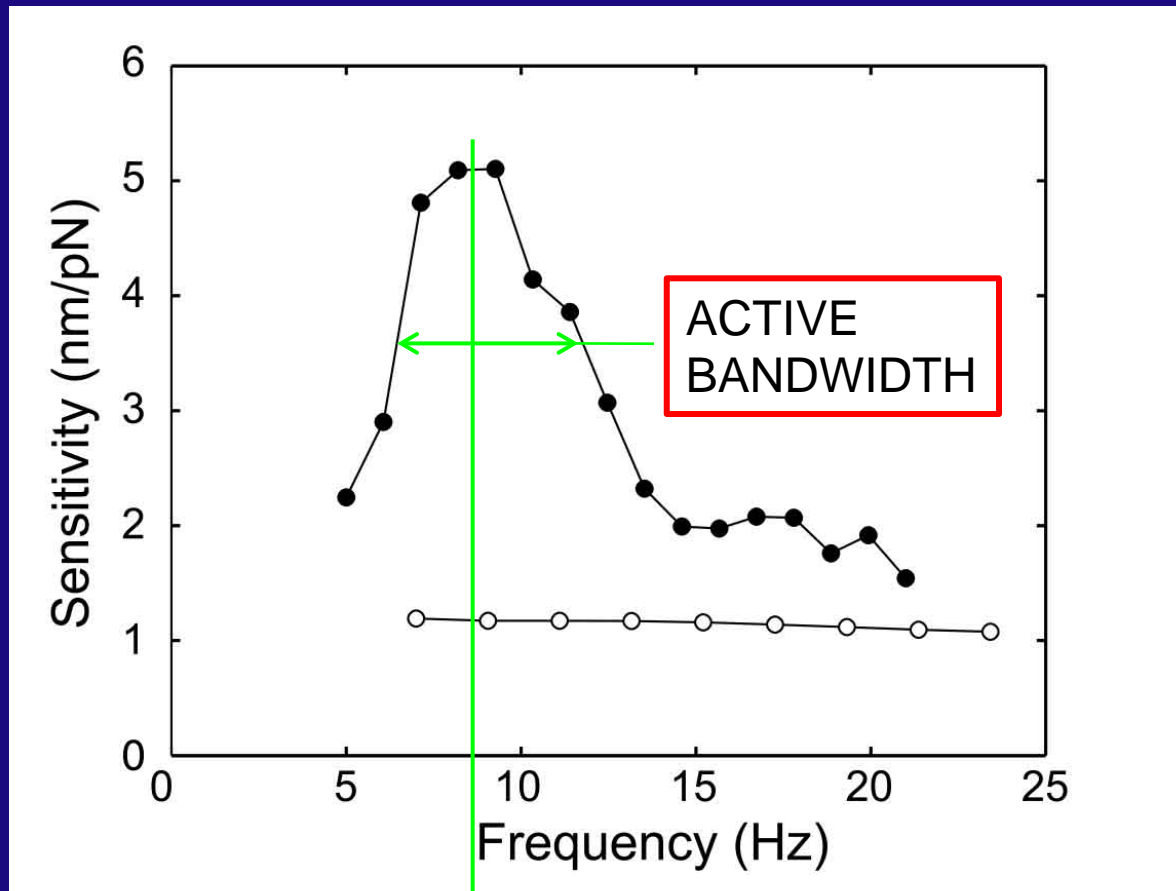
1 μm



Active resonance

($F_1 \cong 5$ pN)

STIMULUS: $F(t) = F_1 \sin(2\pi f_1 t)$

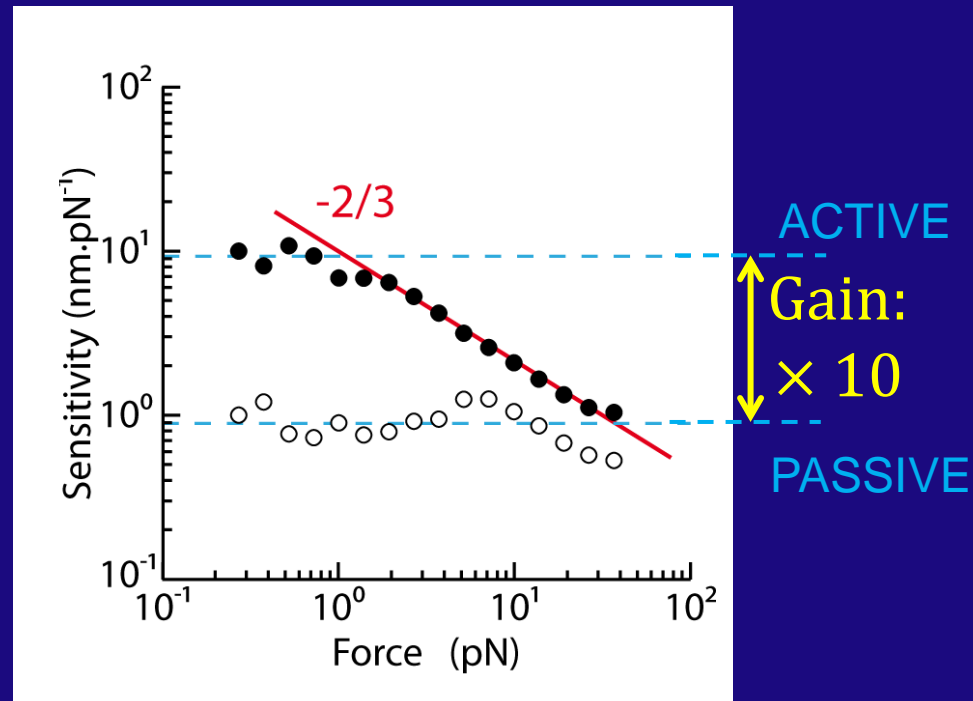


- Oscillatory (~ 8 Hz)
- Non oscillatory

f_c

Nonlinear amplification

STIMULUS: $F(t) = F_1 \sin(2\pi f_1 t)$

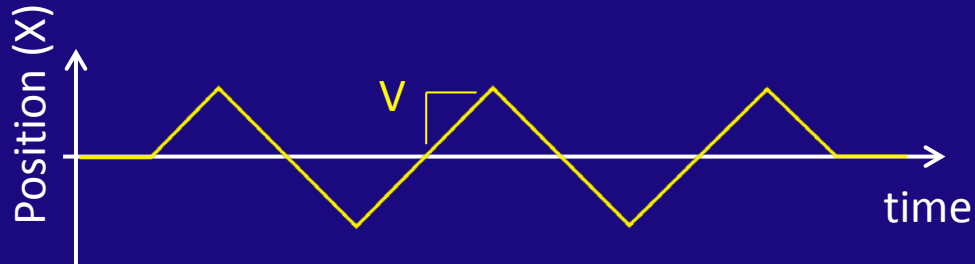


- at resonance ($f_1 = 9$ Hz)
- off resonance ($f_1 = 180$ Hz)

What limits the sensitivity to weak stimuli?

Friction

How to probe friction?



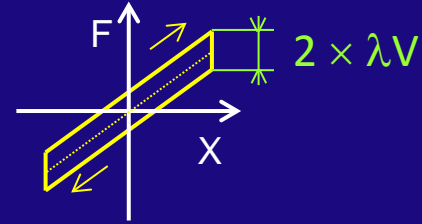
Elastic



External force

$$F = k X$$

Elastic + friction

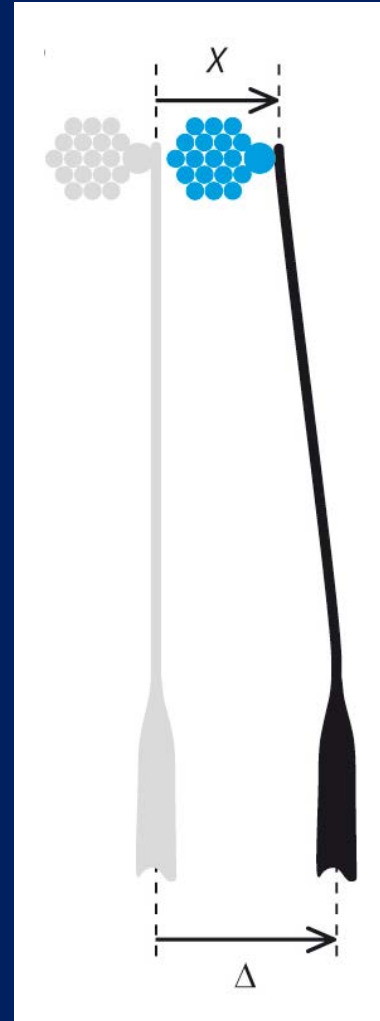
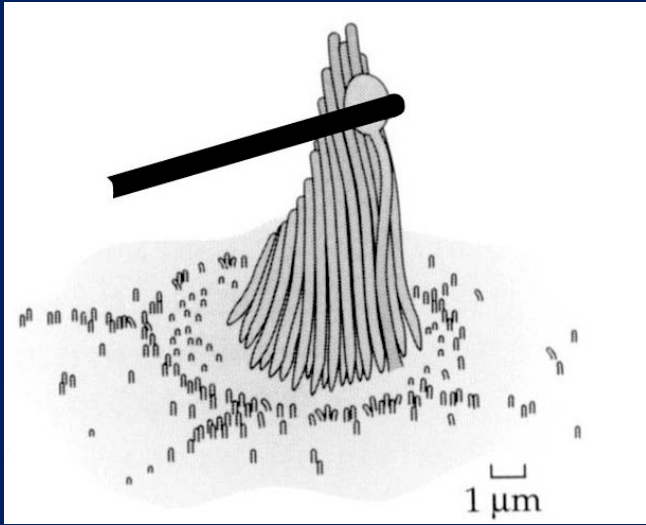


$$F^+ = k X + \lambda V$$

$$F^- = k X - \lambda V$$

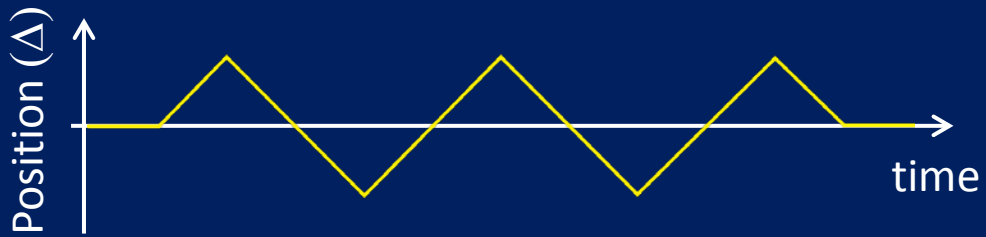
Friction force:

$$\Phi(X) = \frac{F^+(X) - F^-(X)}{2} = \lambda V$$



$$X = \pm 80\ \text{nm}$$

$$\dot{X} = 0.2 - 90\ \mu\text{m/s}$$

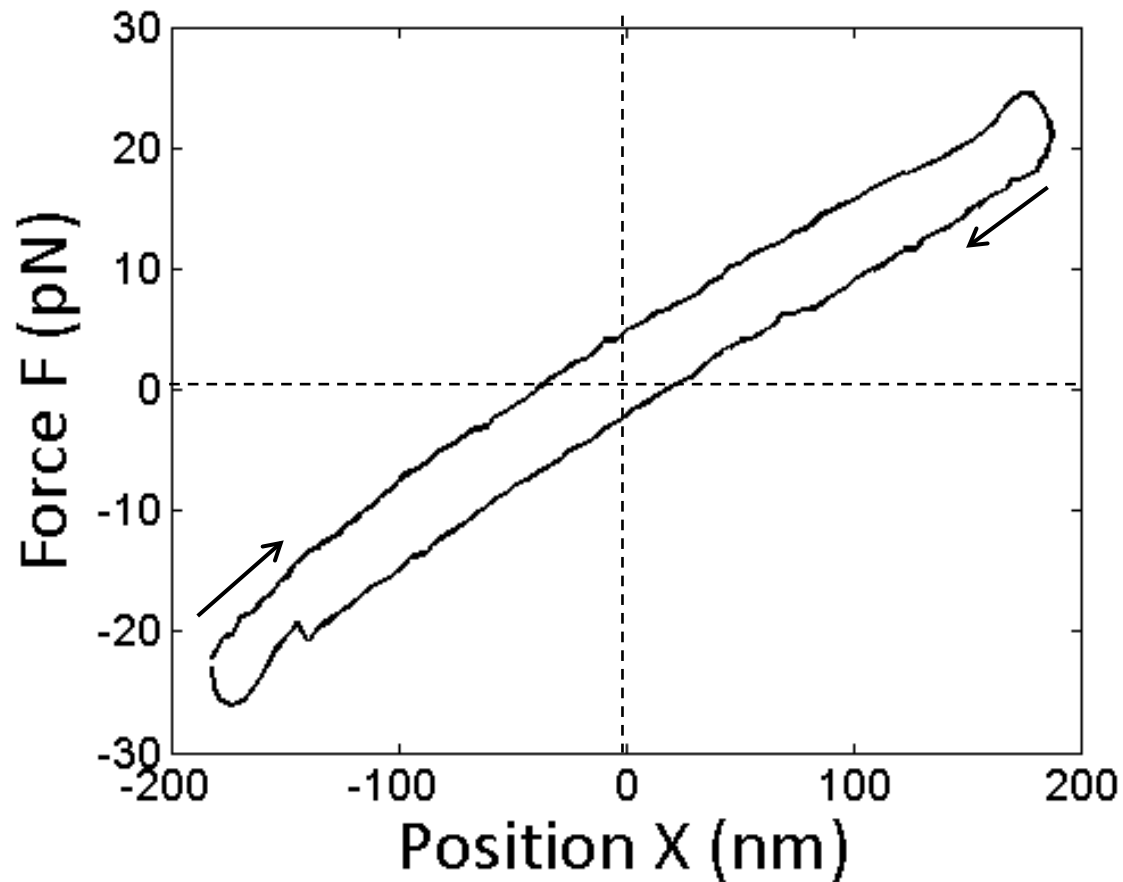
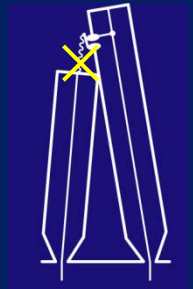


$$\Delta = \pm 300\ \text{nm}$$

$$\dot{\Delta} = 1 - 300\ \mu\text{m/s}$$

Hysteretic cycle

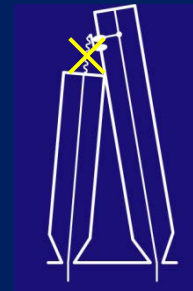
→ tip-links broken (with BAPTA)



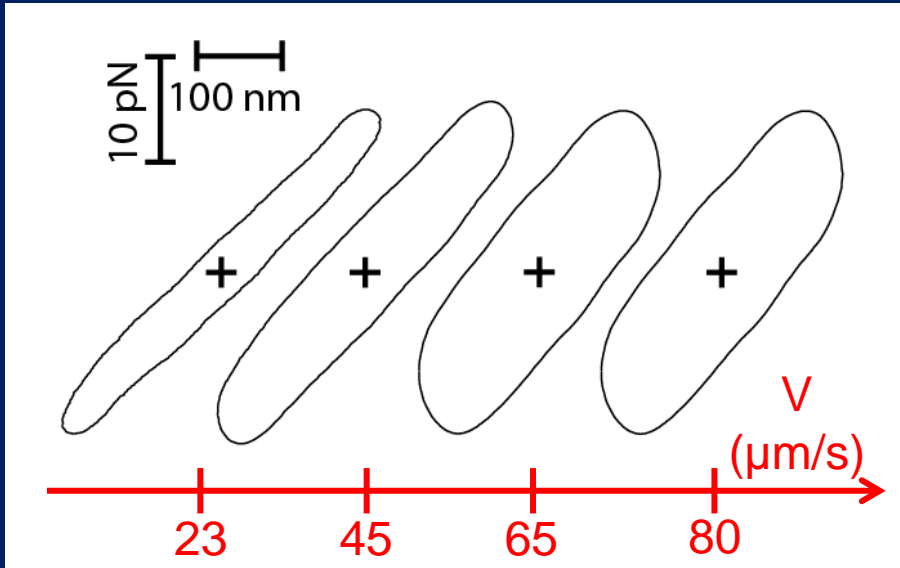
($V = 23 \mu\text{m/s}$)

Hysteretic cycle

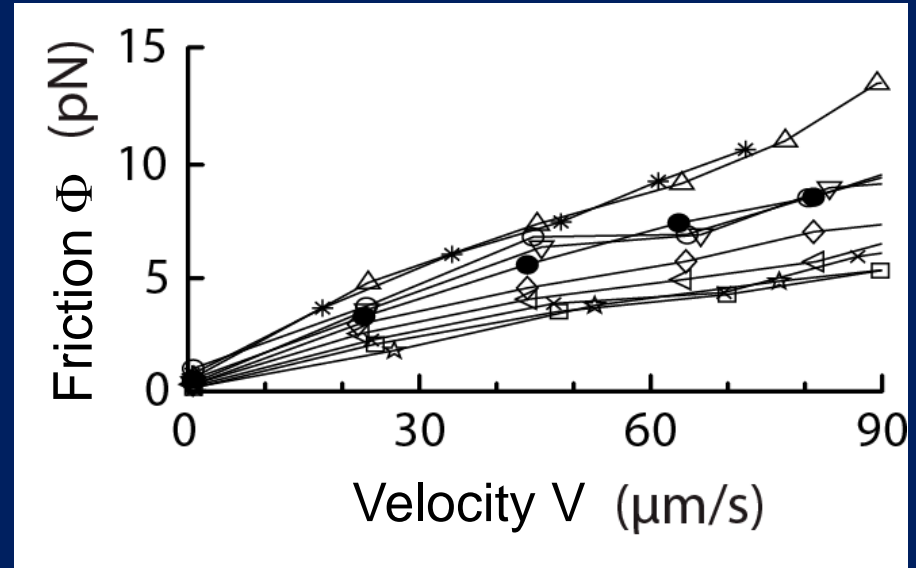
→ tip-links broken



Force-displacement cycles



Friction force vs. velocity

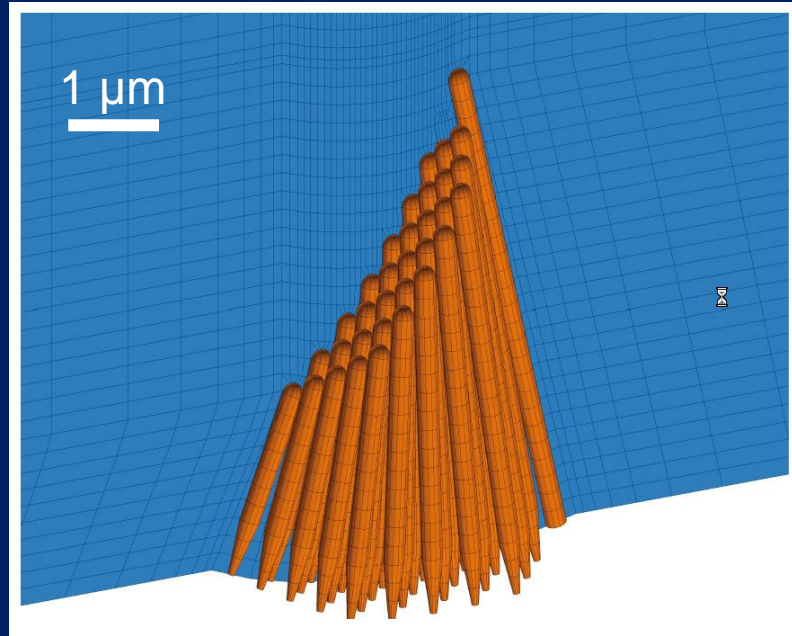


Friction
coefficient:

$$\lambda_H = 86 \pm 29 \text{ nN}\cdot\text{s/m} \quad (n=10)$$

Viscous drag

(calculation from finite-element analysis)



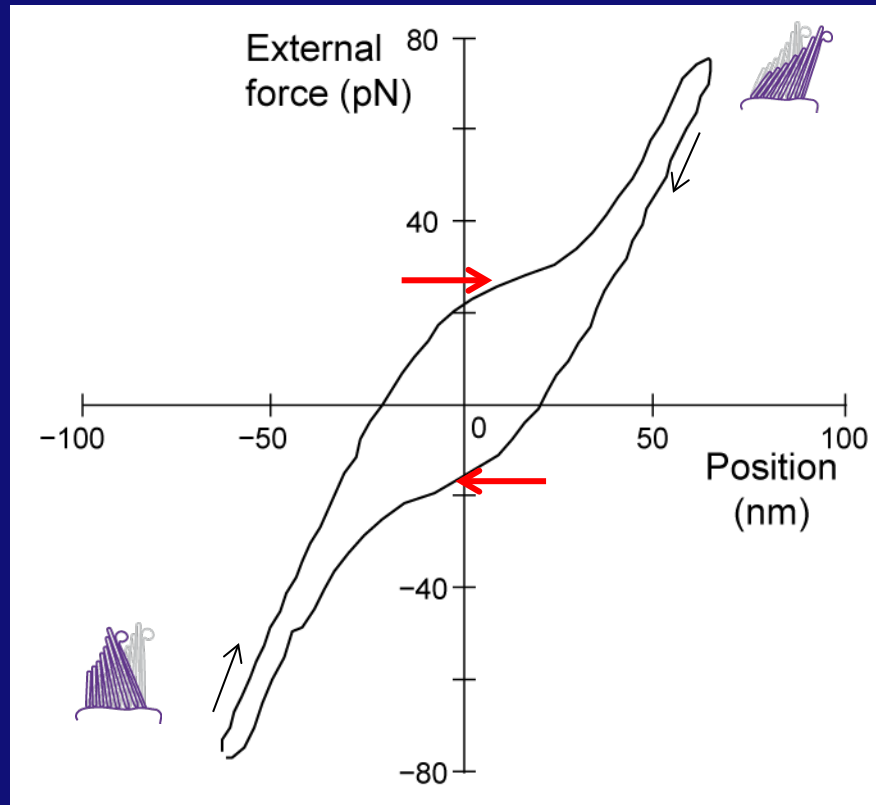
Friction coefficient:
 $\cong 100 \text{ nN}\cdot\text{s}/\text{m}$

Velocity of $10 \text{ }\mu\text{m}/\text{s}$ \Rightarrow Friction force of 1 pN

(Kozlov, Baumgart et al, Nature (2011))

Hysteretic cycle

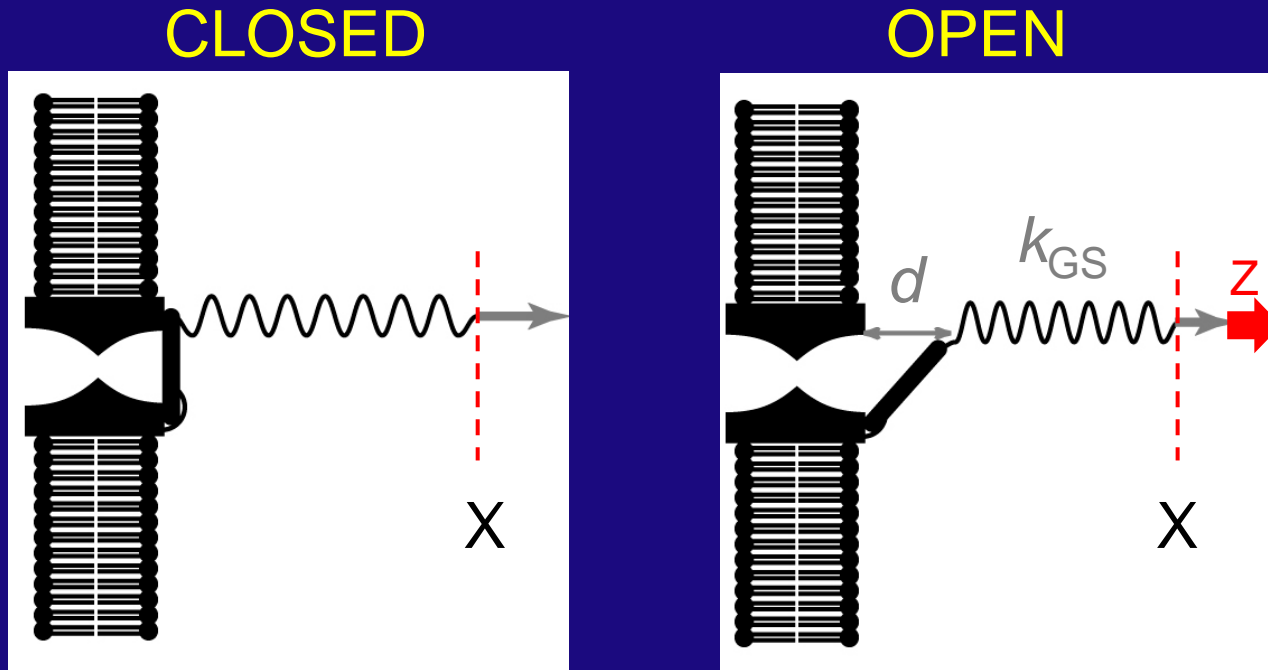
→ functional hair bundle



Bundle velocity:
25 $\mu\text{m/s}$

Gating compliance

(Howard and Hudspeth, 1988)



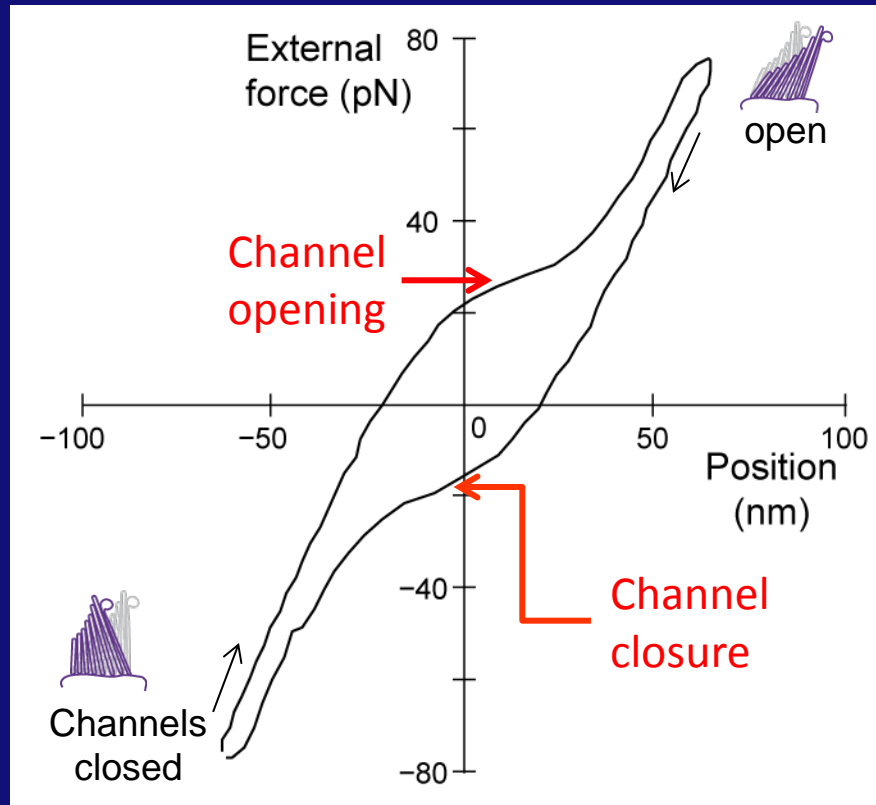
“gating force”: $Z = k_{GS} d$

$$\langle F_{EXT} \rangle(X) = k_{GS} X - P_o(X) Z + F_0$$

Open probability

Hysteretic cycle

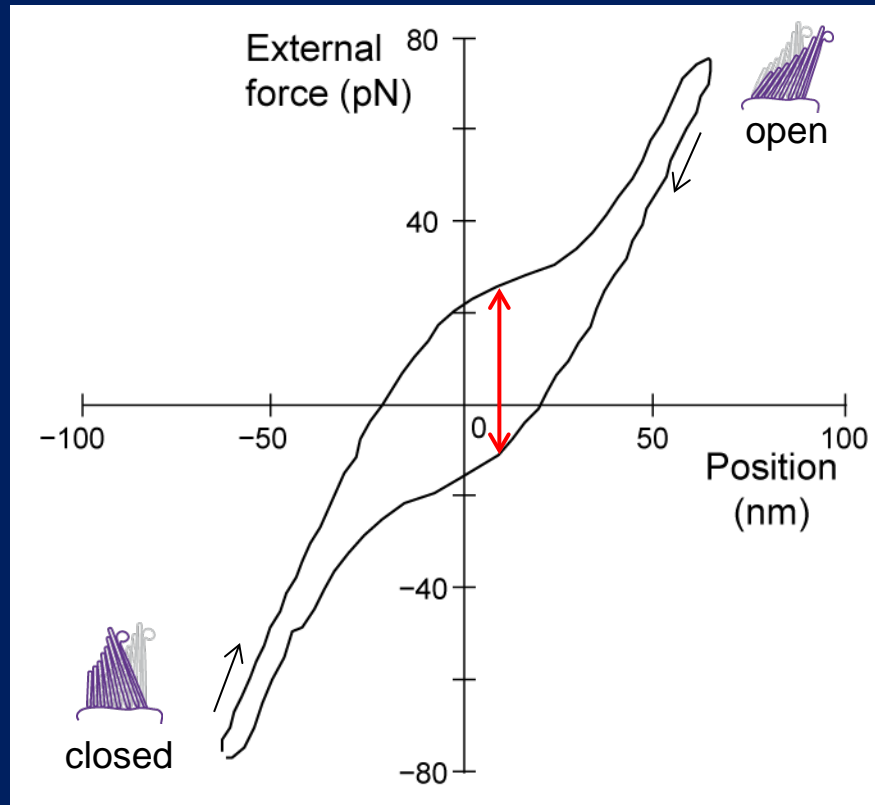
→ functional hair bundle



Bundle velocity:
25 $\mu\text{m/s}$

Hysteretic cycle

→ higher friction in the region of gating compliance

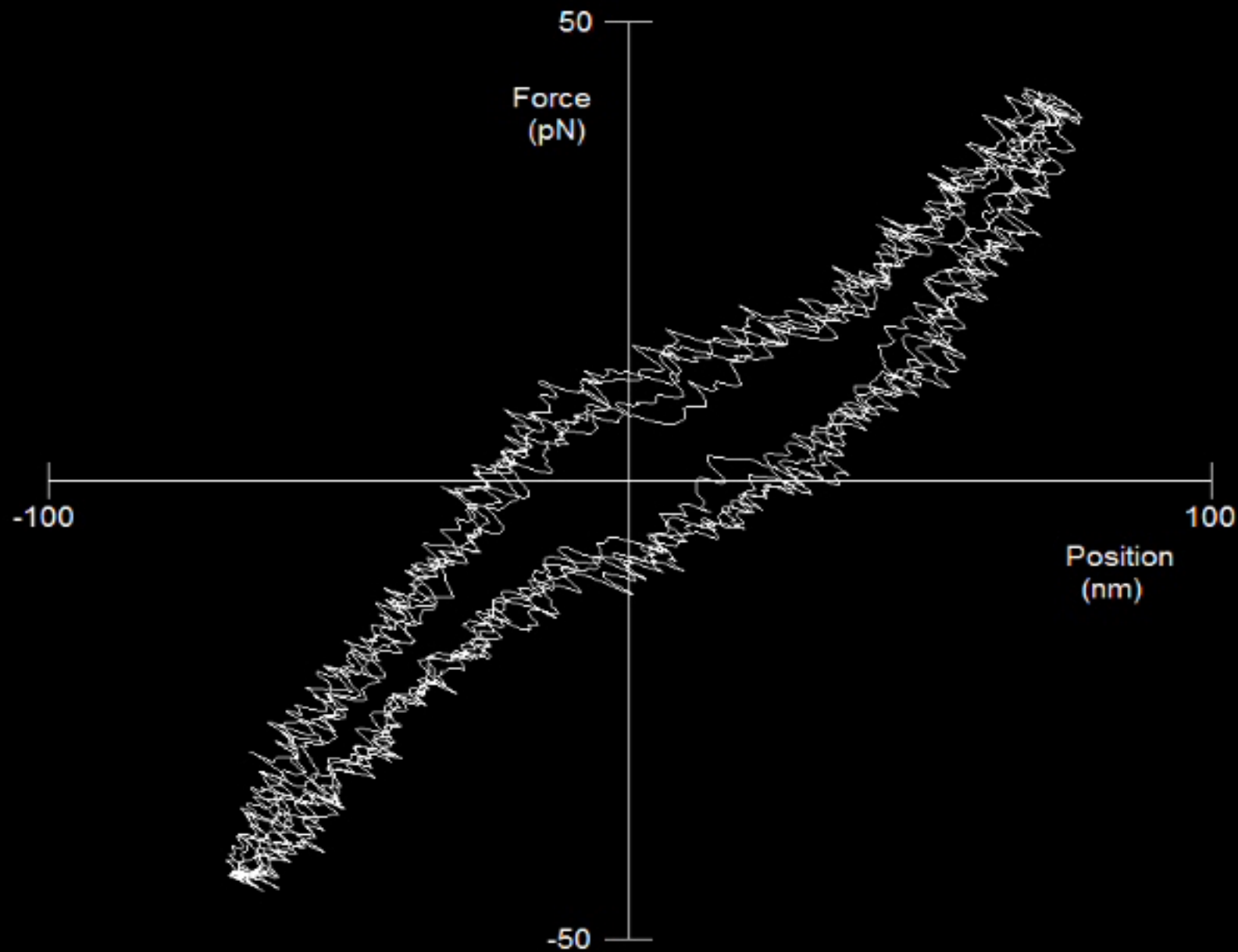


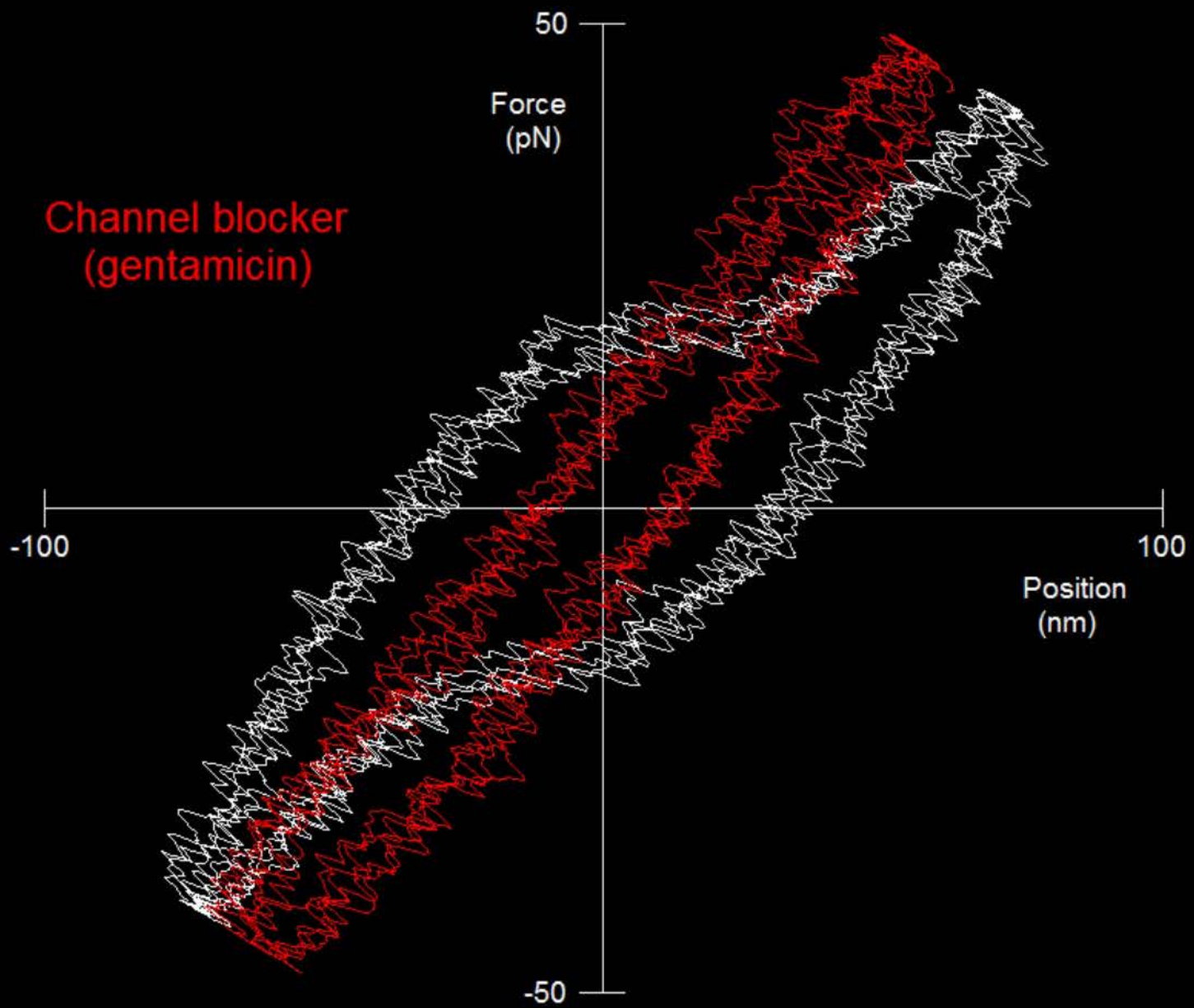
Bundle velocity:
25 $\mu\text{m/s}$

Friction force (20 pN) \gg Expected hydrodynamic friction (2.5 pN only!!)

Are the transduction channels contributing
to hair-bundle friction?

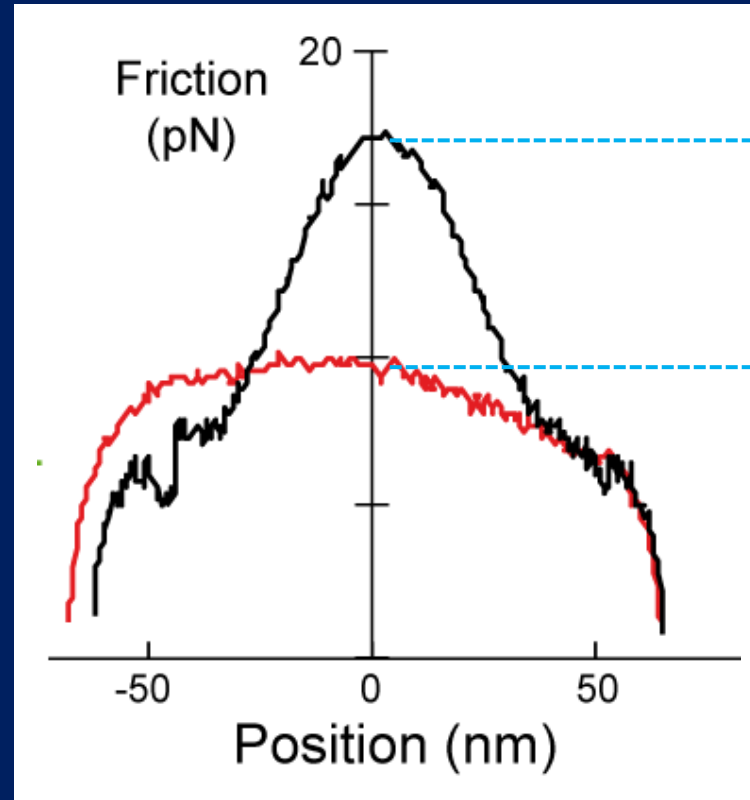
→ use a channel blocker (gentamicin)





Friction from channel gating

Bundle velocity:
25 $\mu\text{m/s}$

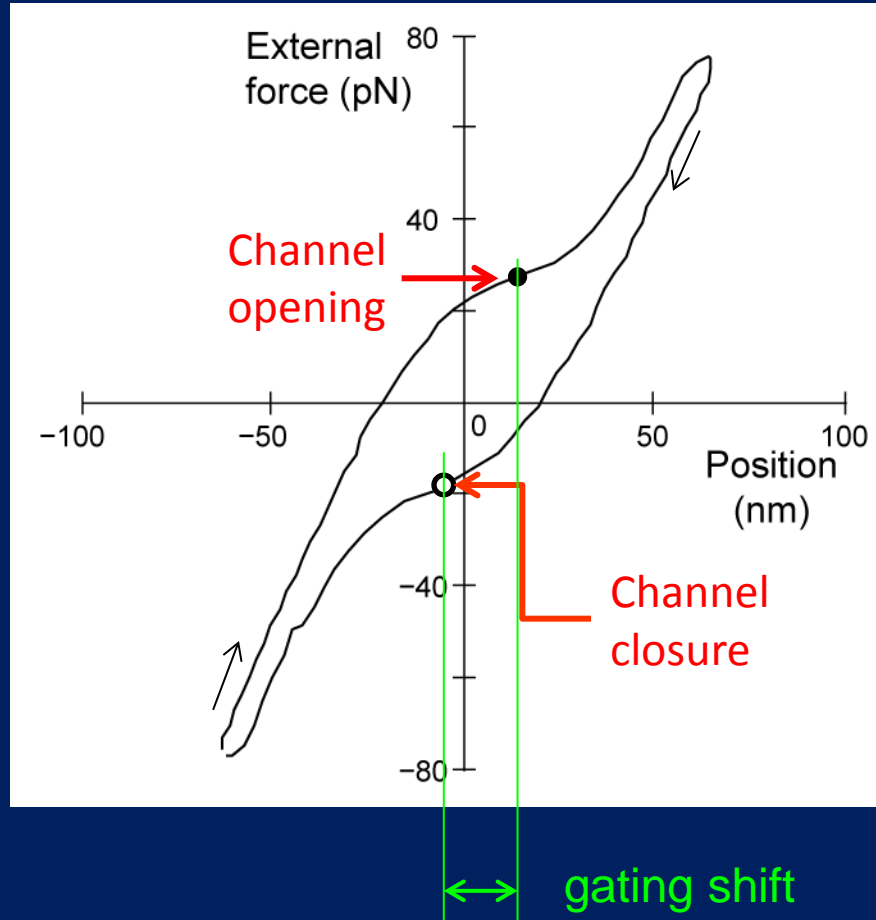
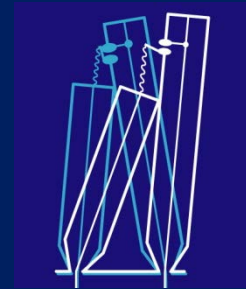


Channel friction

- : control conditions
- : channels blocked (Gentamicin)

Hysteretic cycle

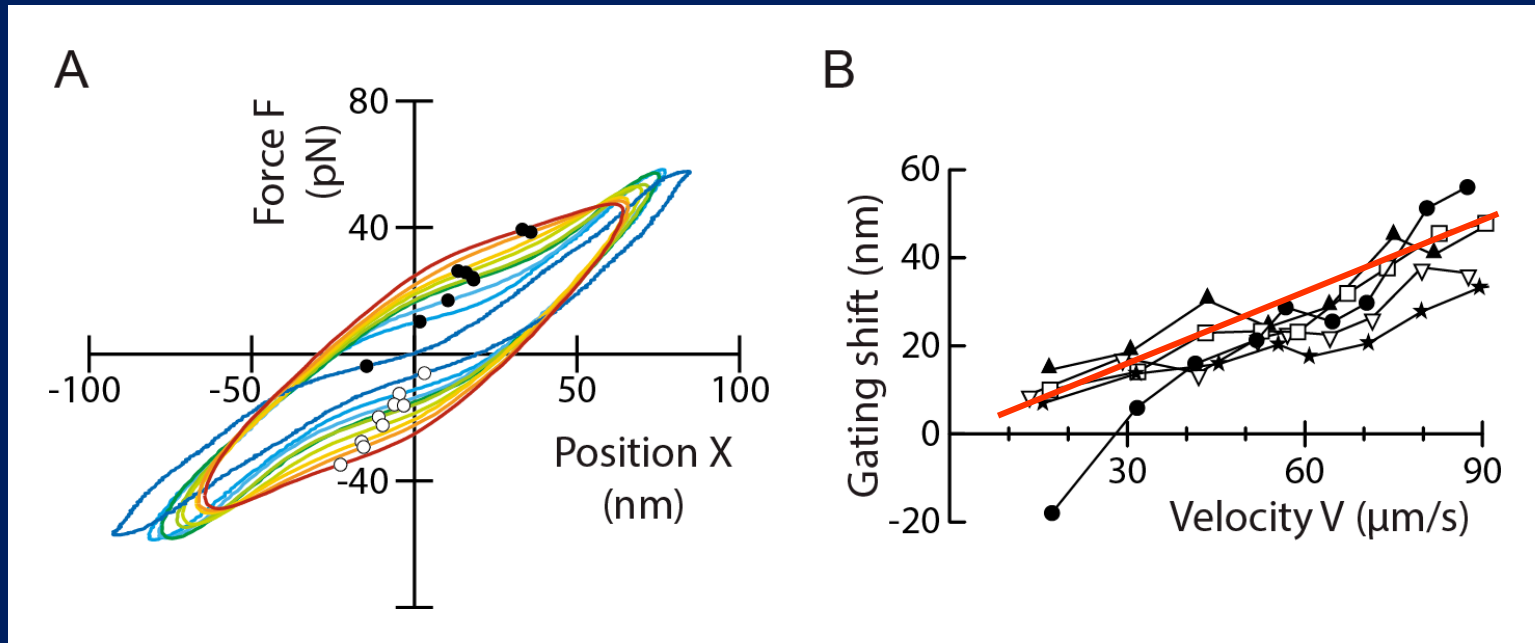
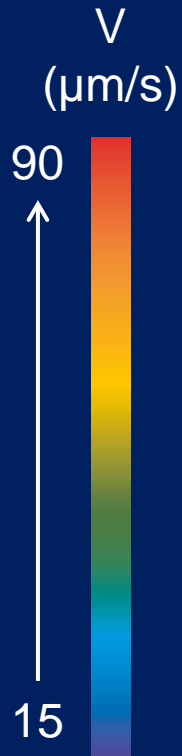
→ functional hair bundle



Bundle velocity:
25 $\mu\text{m/s}$

Gating shift

→ it takes time to open a channel!

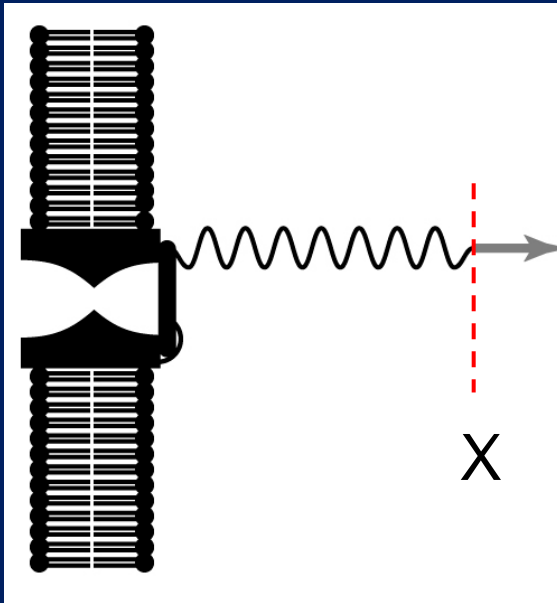


Characteristic activation time: $\tau_{exp} = 230 \pm 40 \mu\text{s}$ ($n = 5$)

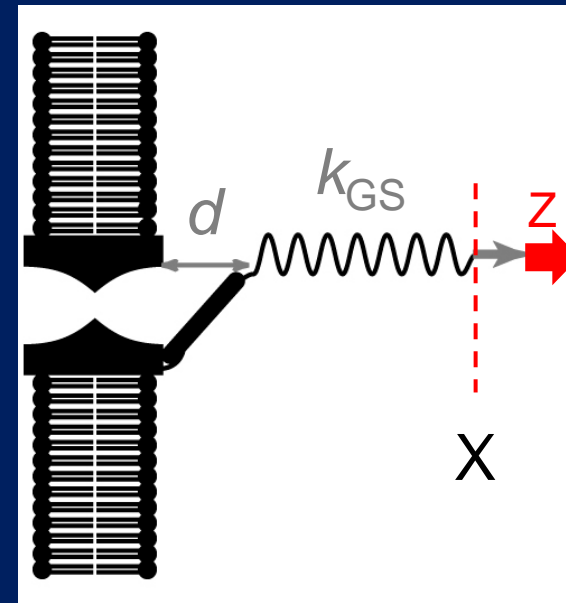
Gating-spring model

(Corey and Hudspeth, 1983)

CLOSED



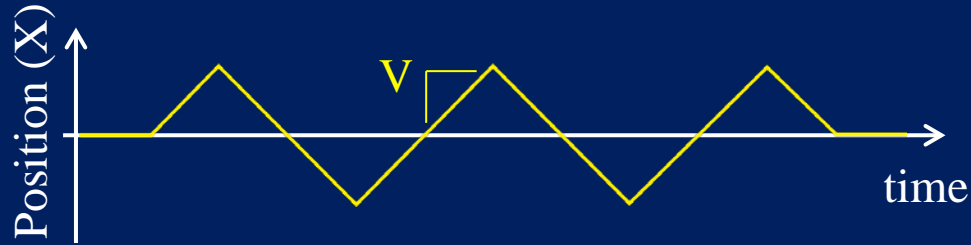
OPEN



“gating force”: $Z = k_{GS} d$

activation time : τ

Physical description



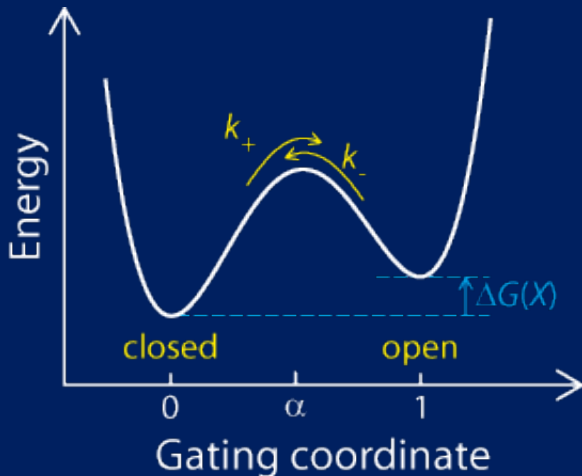
Force
-displacement:

$$F_{EXT}(X) = K_{HB}X - NP_o(X)Z + F_0$$

gating
compliance

Channel kinetics:

$$\tau \frac{dP_o}{dt} = P_\infty - P_o$$



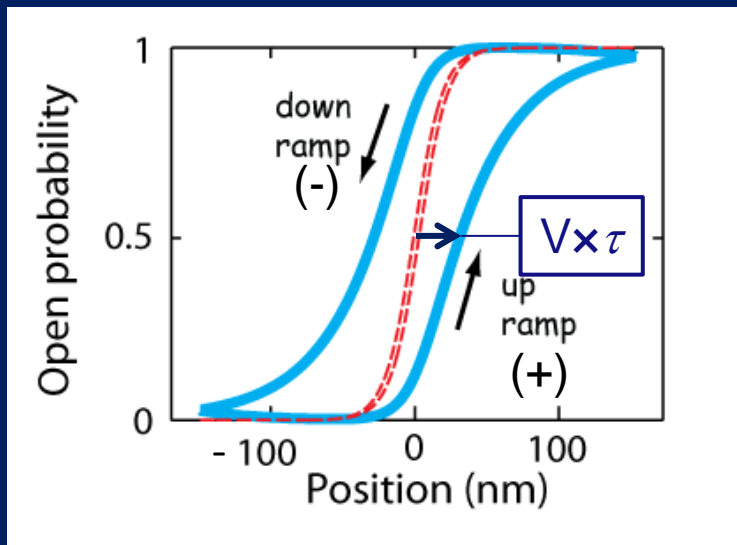
$$\tau = 1/(k_+ + k_-)$$

with

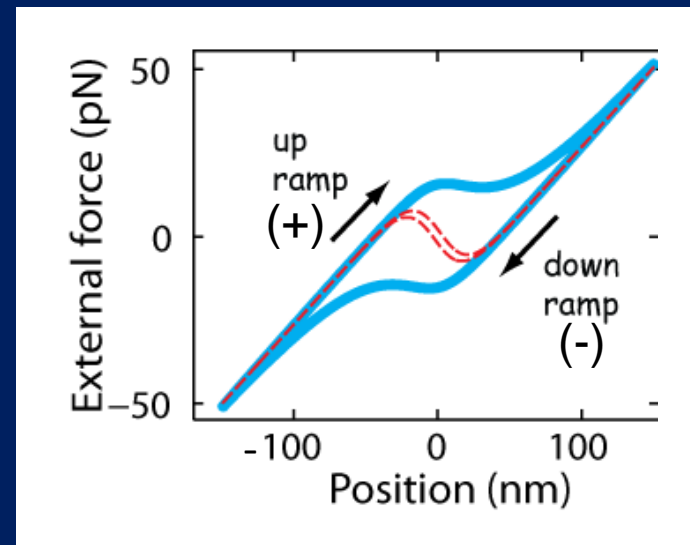
$$P_\infty = \frac{1}{1 + \exp\left(-\frac{Z \times X}{k_B T}\right)}$$

Dissipation from slow channel kinetics → simulations

Delayed channel gating



Dissipation



$$F^{\pm}(X) = K_{HB}X - NZ P_o^{\pm}(X) + F_0$$

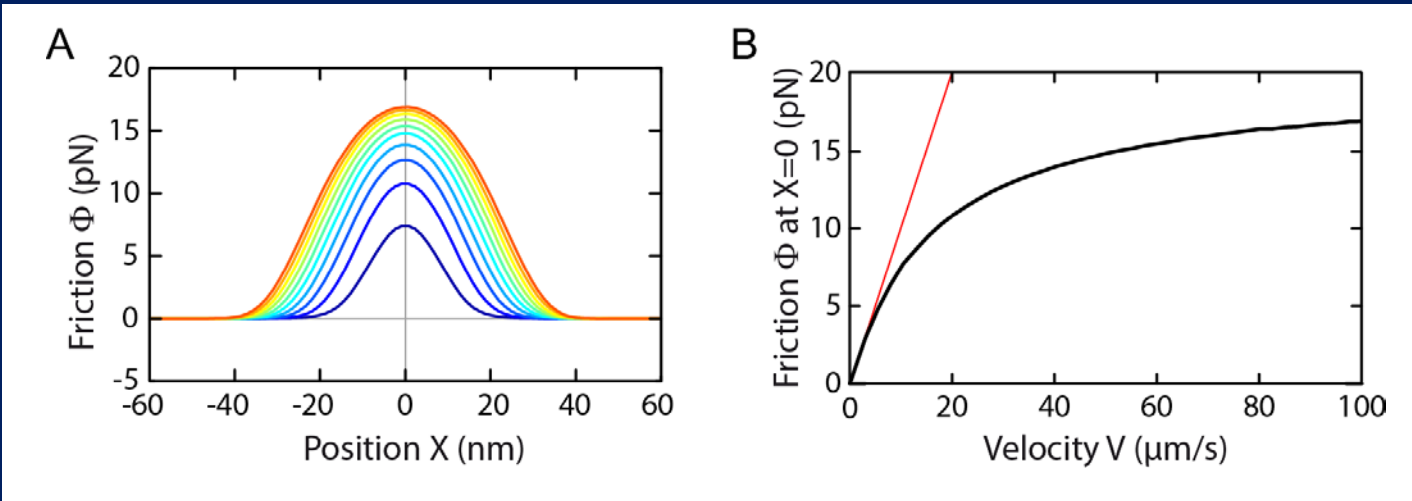
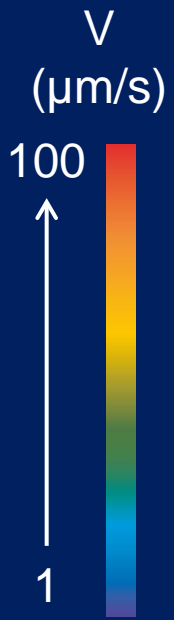
--- : low velocity
— : high velocity

Channel friction

→ simulations

$\tau = 0.5 \text{ ms}$
 $Z = 0.8 \text{ pN}$
 $N = 50$

$$\Phi(X) = [F^+(X) - F^-(X)]/2 = \frac{NZ}{2} [P^-(X) - P^+(X)]$$



$$\Phi(X = 0) \leq \Phi_{MAX} = NZ/2 = 20 \text{ pN}$$

Friction force:

$$\Phi(X = 0) \cong \left(\frac{NZ^2}{4k_B T} \tau \right) \times V \quad \text{at low velocities}$$

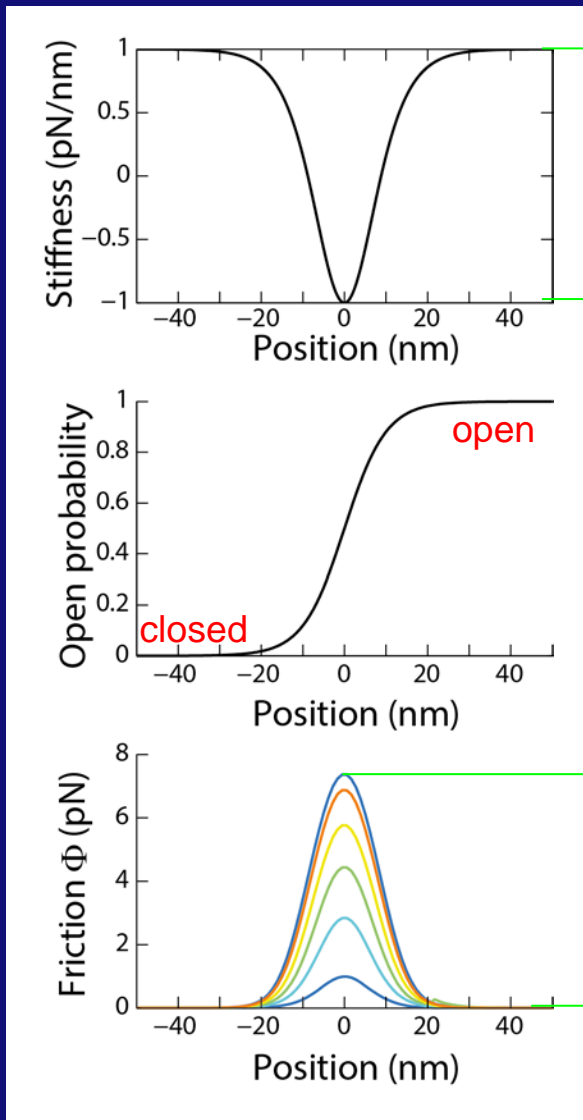
1 $\mu\text{N}\cdot\text{s/m}$
 (= $10 \times \lambda_{\text{Hydro}}$)

Channel friction

- Gating of the transduction channels provides a major contribution to hair-bundle friction (up to $\times 10$ hydro)
- Channel friction result from large gating forces and finite activation kinetics

(Bormuth, Barral, Joanny, Jülicher and Martin, PNAS (2014))

Dual role of gating forces (Z)



$$\Delta K = \frac{NZ^2}{4k_B T}$$

$$\Phi = \lambda_C V$$

Gating compliance

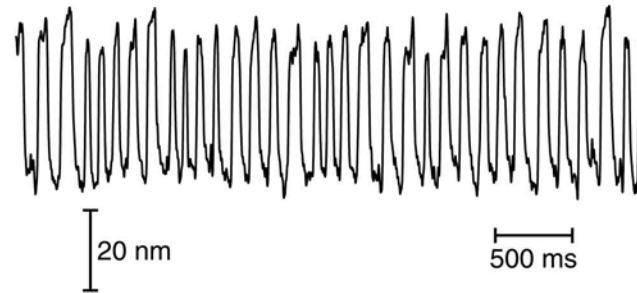
At low velocity:
 $\lambda_C = \Delta K \times \tau$

Gating friction

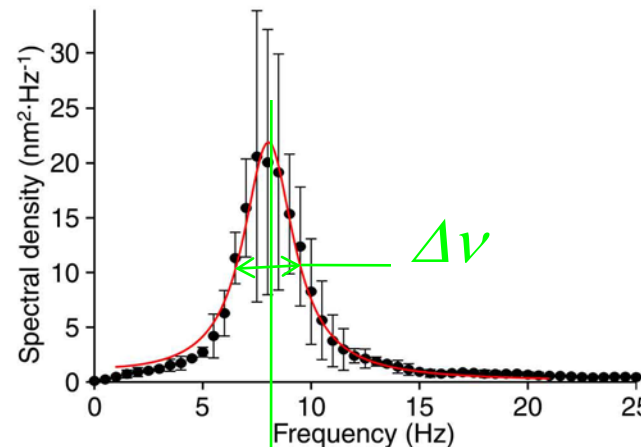
Noise

Characteristic frequency

Hair-bundle
position



Spectral
density



Noisy!

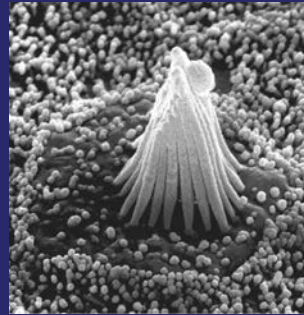
Low quality factor
($Q = \nu_C / \Delta\nu \cong 2$)

characteristic frequency: ν_C (range: 5-50 Hz)

(Martin and Hudspeth, PNAS (1999))

Noise sources

- Hydrodynamic:



Noise force η :

$$\langle \eta_H \rangle = 0$$

$$\langle \eta_H(t) \eta_H(0) \rangle = 2k_B T \lambda_H \delta(t)$$



friction

- Channel clatter:



$$\langle \eta_C \rangle = 0$$

$$\langle \eta_C(t) \eta_C(0) \rangle \cong 2k_B T \lambda_C \delta(t)$$



(Nadrowski, Martin and Jülicher, PNAS (2004))

Active dynamical system

Hair bundle: $\lambda \frac{dX}{dt} = -K_{GS}(X - X_a - DP_o) - K_{SP}X + F_{EXT}$

Motors: $\lambda_a \frac{dX_a}{dt} = K_{GS}(X - X_a - DP_o) - F_a$

Tip-link tension

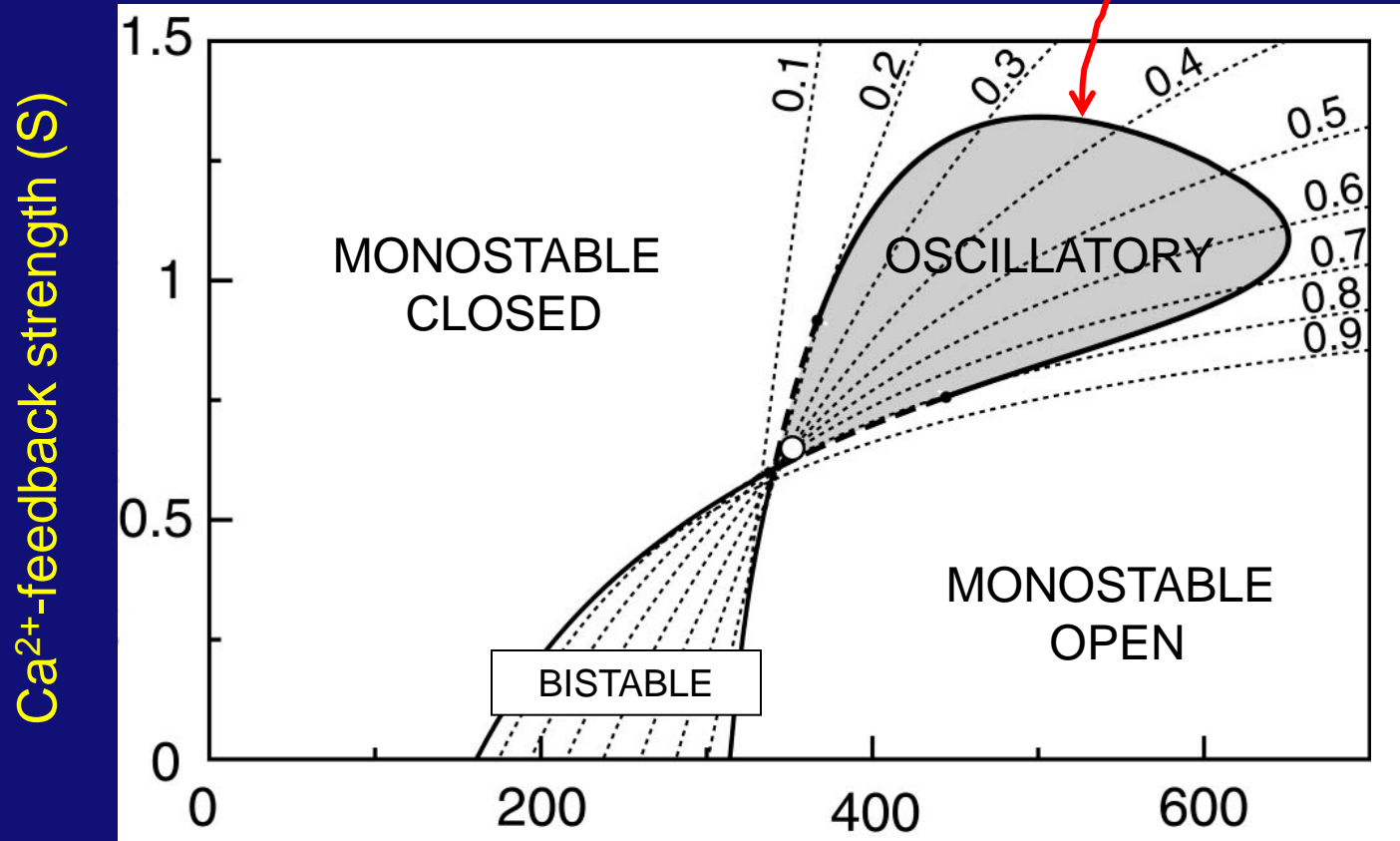
Motor force: $F_a = F_{MAX}(1 - SP_o)$

Open probability: $P_o = 1/[1 + A \exp(-Z(X - X_a)/(k_B T))]$

(Nadrowski, Martin and Jülicher, PNAS (2004))

Hair-bundle model: state diagram

Hopf bifurcation



Maximal motor force (F_{MAX} in pN)

(Nadrowski, Martin and Jülicher, PNAS (2004))

Active dynamical system WITH NOISE

Hair bundle: $\lambda \frac{dX}{dt} = -K_{GS}(X - X_a - DP_o) - K_{SP}X + F_{EXT} + \xi_X$

Motors: $\lambda_a \frac{dX_a}{dt} = K_{GS}(X - X_a - DP_o) - F_{MAX}(1 - SP_o) + \xi_a$

Tip-link
tension

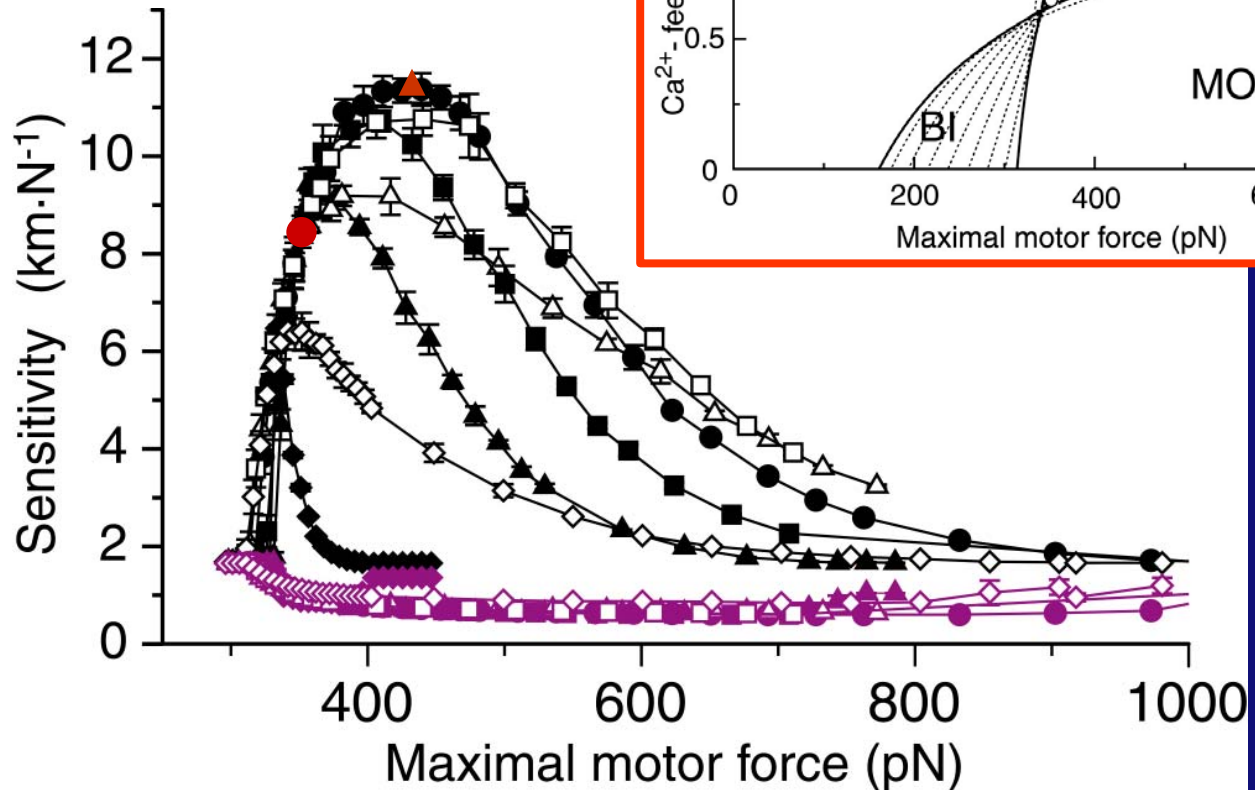
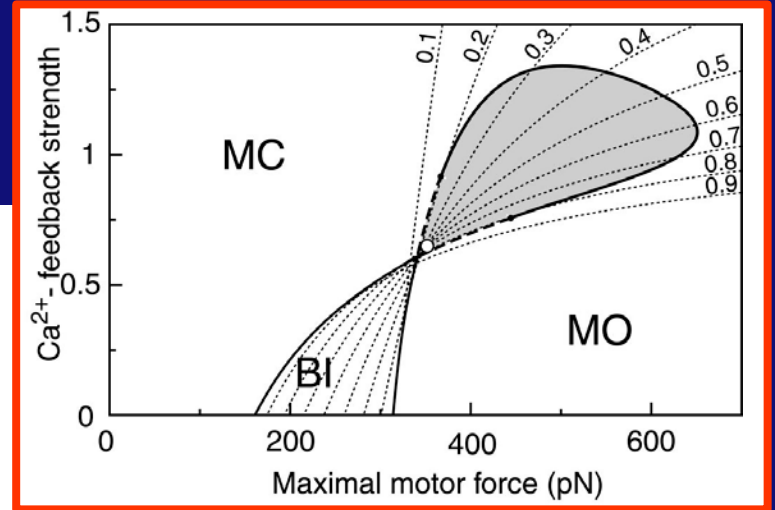
$$\langle \xi_X \rangle = 0; \langle \xi_X(t) \xi_X(0) \rangle = 2k_B T \lambda \delta(t)$$
$$\langle \xi_a \rangle = 0; \langle \xi_a(t) \xi_a(0) \rangle = 2k_B T_a \lambda_a \delta(t); T_a = 1.5 T$$

Open probability: $P_o = 1/[1 + A \exp(-Z(X - X_a)/(k_B T))]$

(Nadrowski, Martin and Jülicher, PNAS (2004))

Optimum of mechanosensitivity

→ limited by noise !



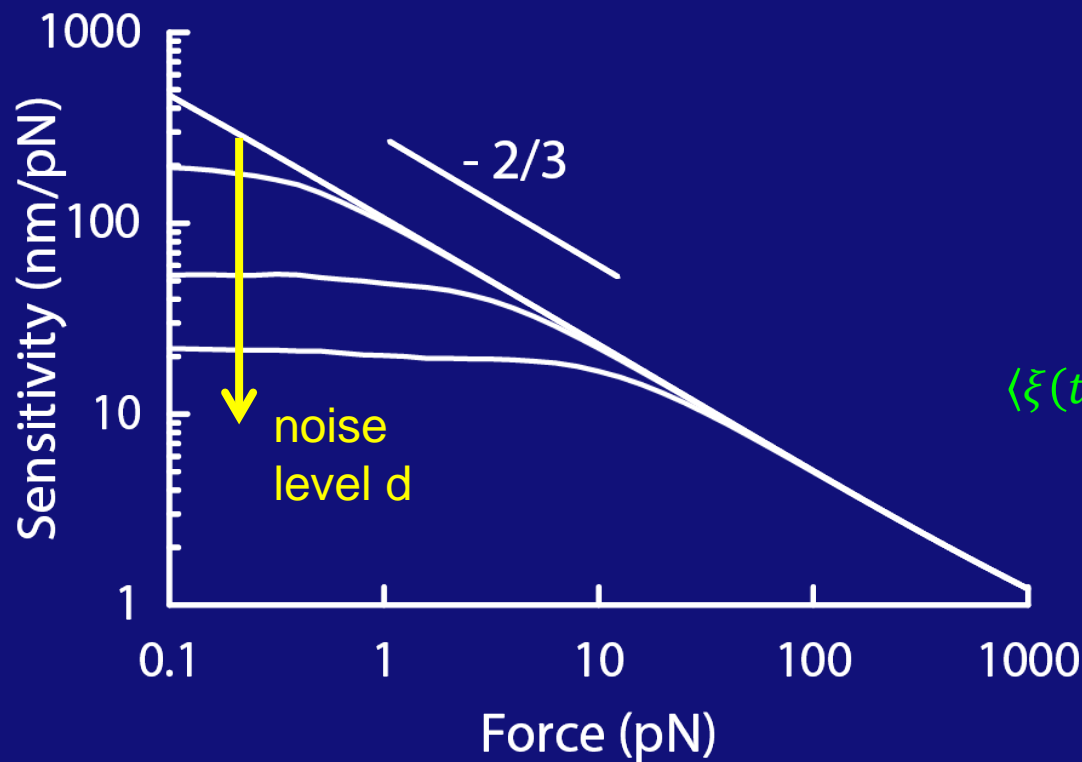
Open probability

- ◆ 0.1
- ▲ 0.3
- 0.4
- 0.5
- 0.6
- △ 0.7
- ◇ 0.9

Hopf bifurcation

→ « critical oscillator » with noise

$$\frac{dZ}{dt} \cong -(\Omega_c - \Omega - i \omega_0) Z - B|Z|^2 Z + \frac{F + \xi}{\Lambda}$$



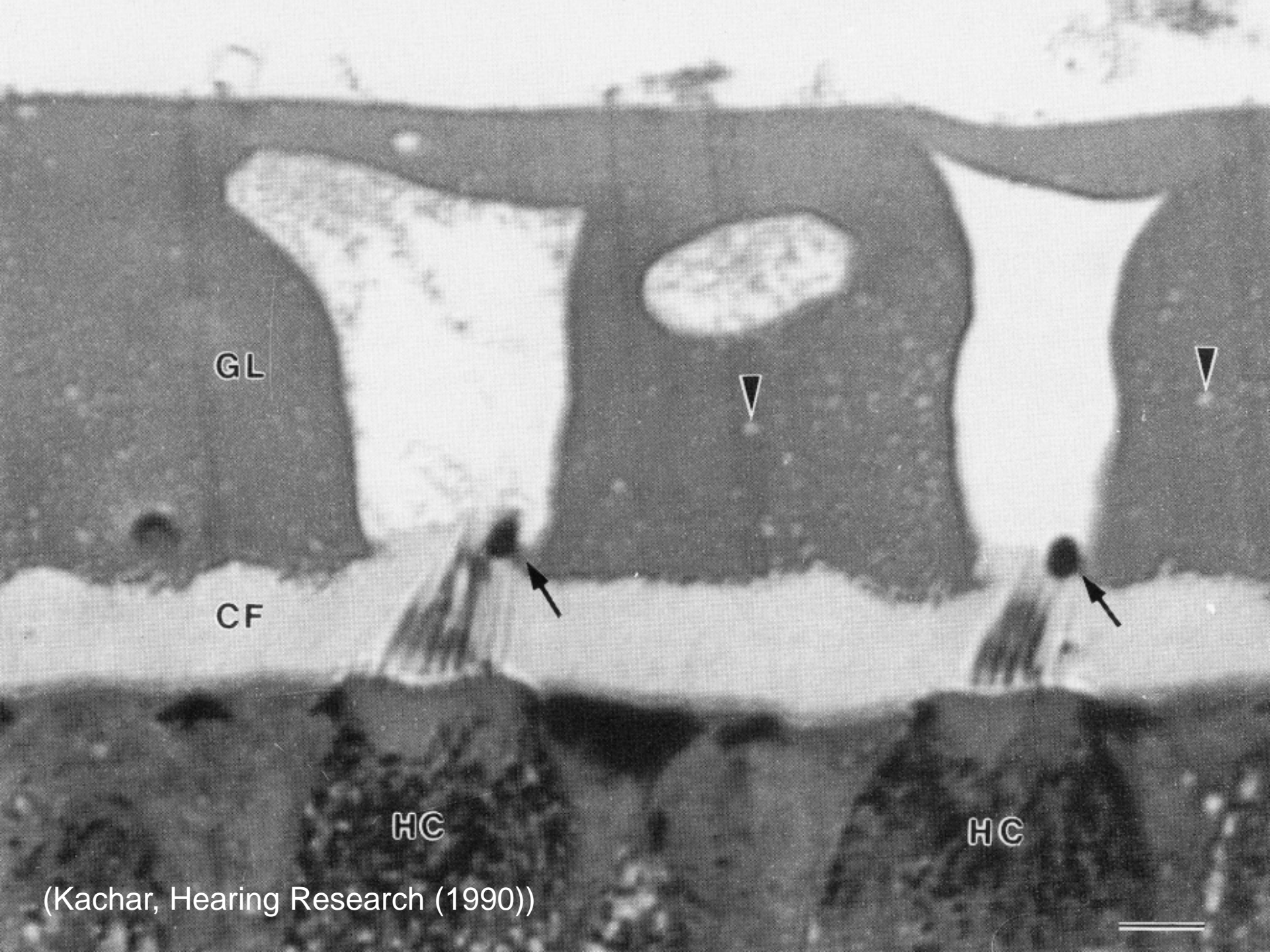
$$\Omega = \Omega_c$$

$$F(t) = F_0 \sin(\omega_0 t)$$

Noise force:

$$\langle \xi(t) \rangle = 0$$

$$\langle \xi(t) \xi(0) \rangle = 2d \delta(t)$$



GL

CF

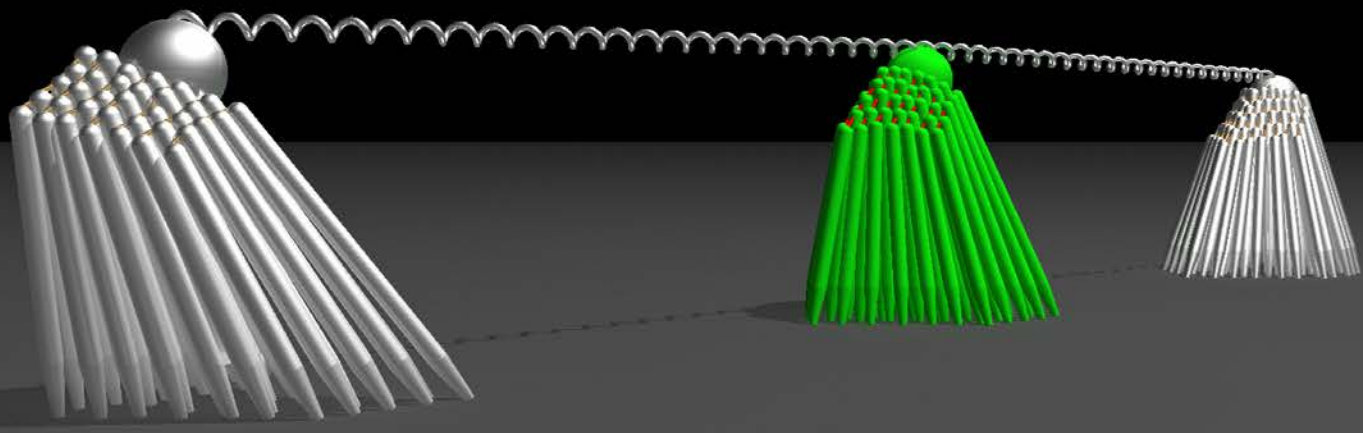
HC

HC

(Kachar, Hearing Research (1990))

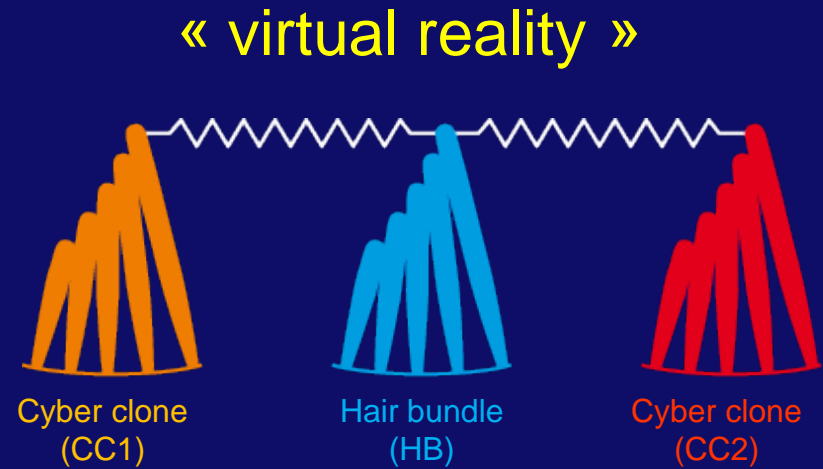
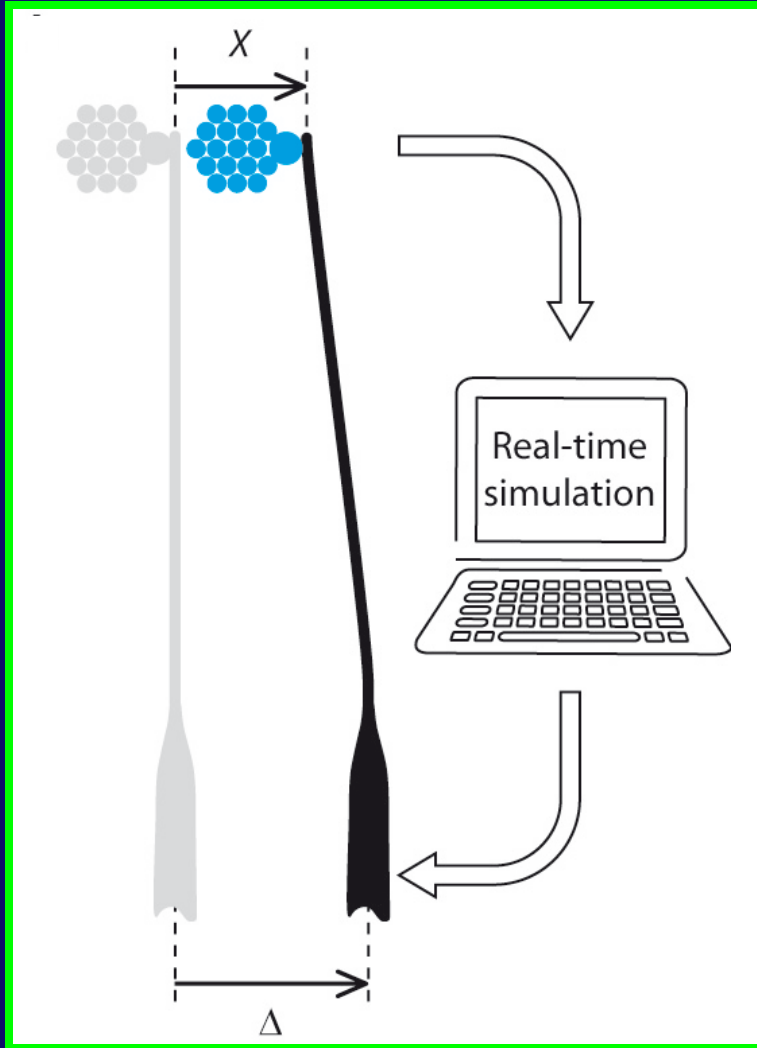


Coupling



(Kai Dierkes)

Coupling to « cyber clones »



Cyber clone?

Stochastic simulation that mimics quantitatively:

1. Spontaneous hair-bundle oscillations
(frequency, magnitude and quality factor)
2. Hair-bundle responsiveness
(sensitivity and gain)

Active dynamical system WITH NOISE

Hair bundle: $\lambda \frac{dX}{dt} = -K_{GS}(X - X_a - DP_o) - K_{SP}X + F_{EXT} + \xi_X$

Motors: $\lambda_a \frac{dX_a}{dt} = K_{GS}(X - X_a - DP_o) - F_{MAX}(1 - SP_o) + \xi_a$

Tip-link
tension

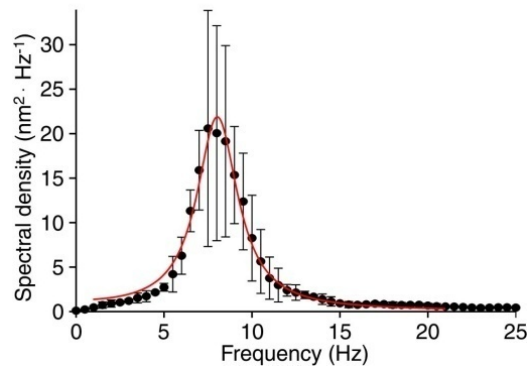
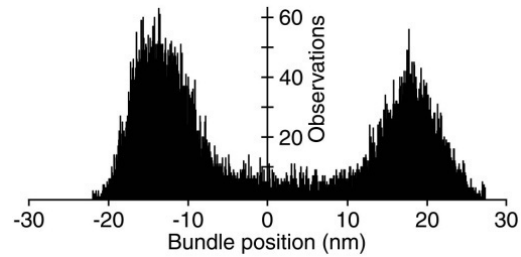
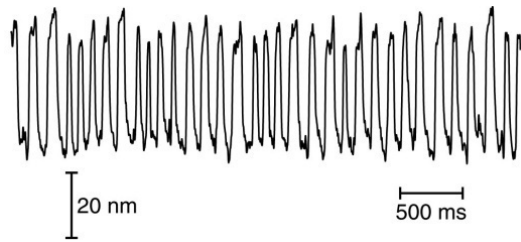
$$\langle \xi_X \rangle = 0; \langle \xi_X(t) \xi_X(0) \rangle = 2k_B T \lambda \delta(t)$$

$$\langle \xi_a \rangle = 0; \langle \xi_a(t) \xi_a(0) \rangle = 2k_B T_a \lambda_a \delta(t); T_a = 1.5 T$$

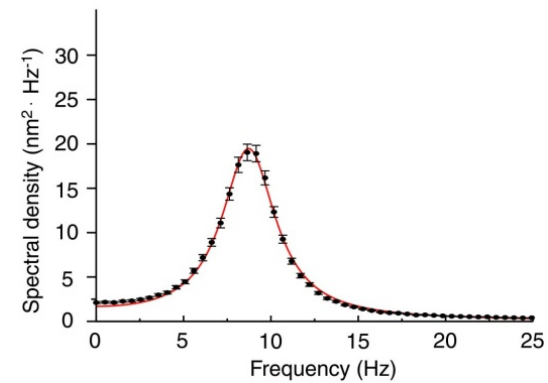
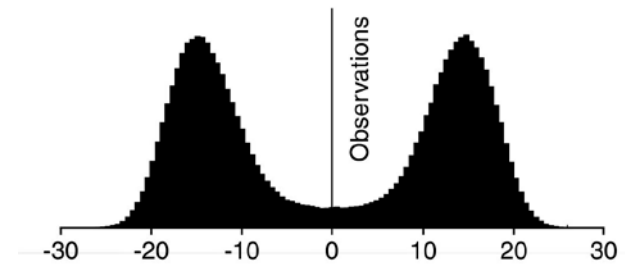
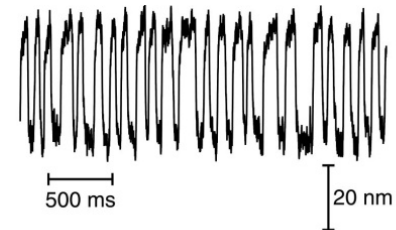
Open probability: $P_o = 1/[1 + A \exp(-Z(X - X_a)/(k_B T))]$

(Nadrowski, Martin and Jülicher, PNAS (2004))

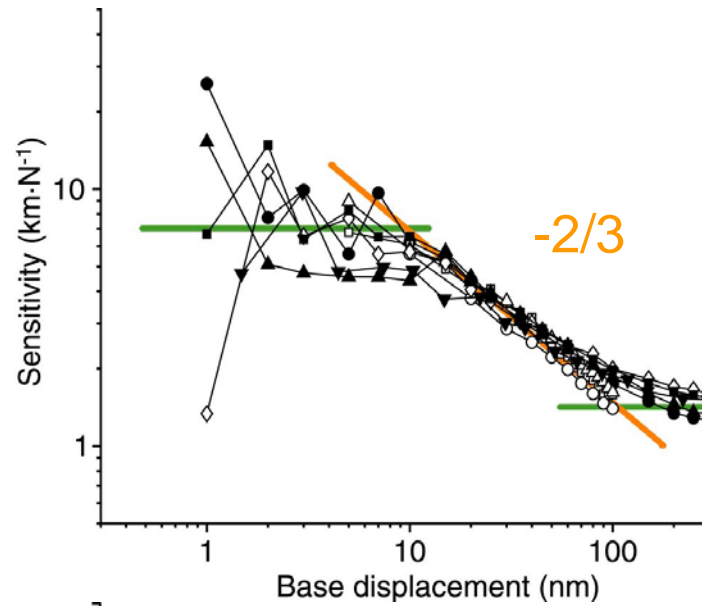
Experiment



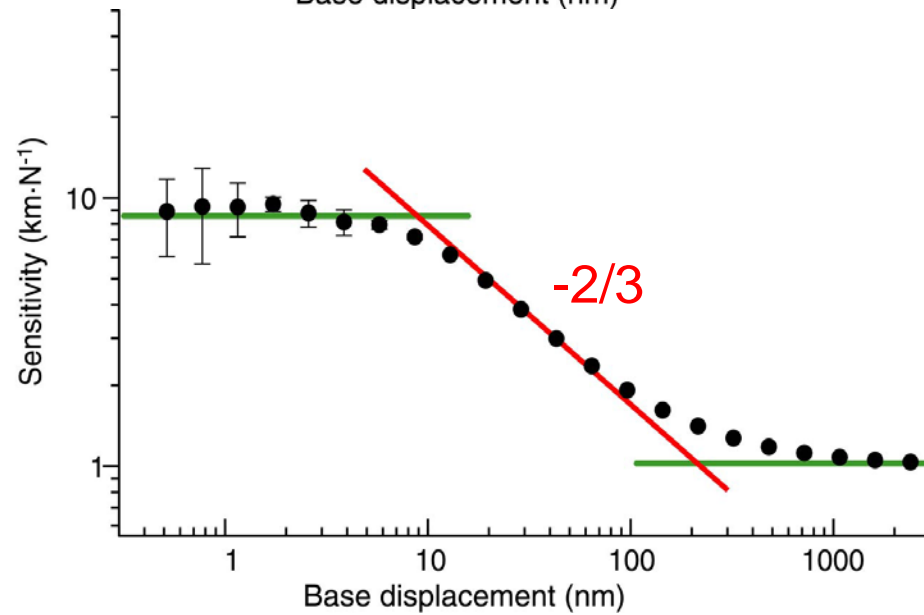
"Cyber clone"



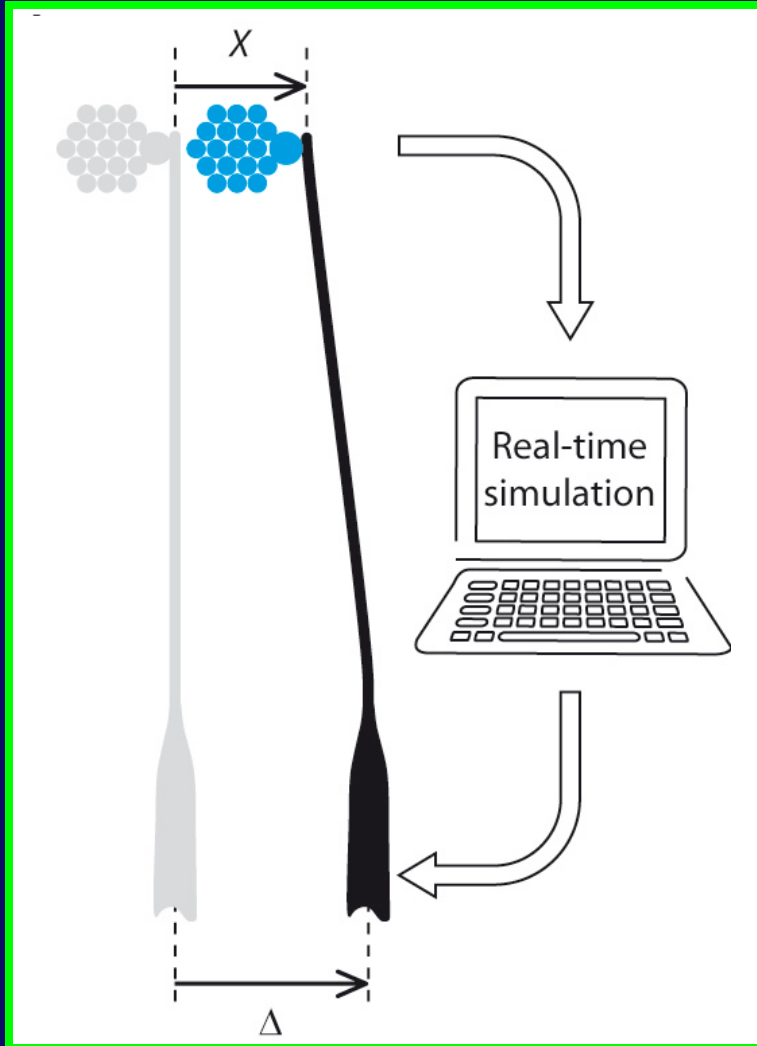
Experiment



Simulation

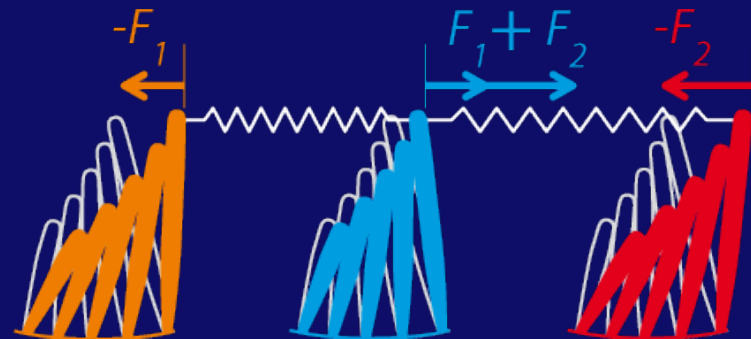


Dynamic force clamp

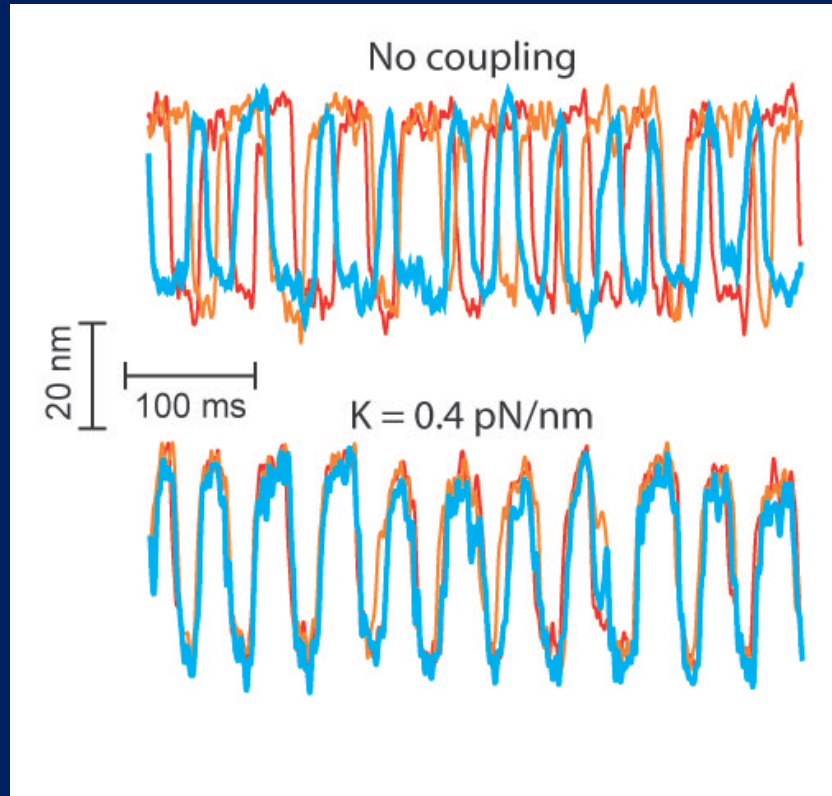


(Time: $t = n \, dt$;
sampling rate: 2.5 kHz)

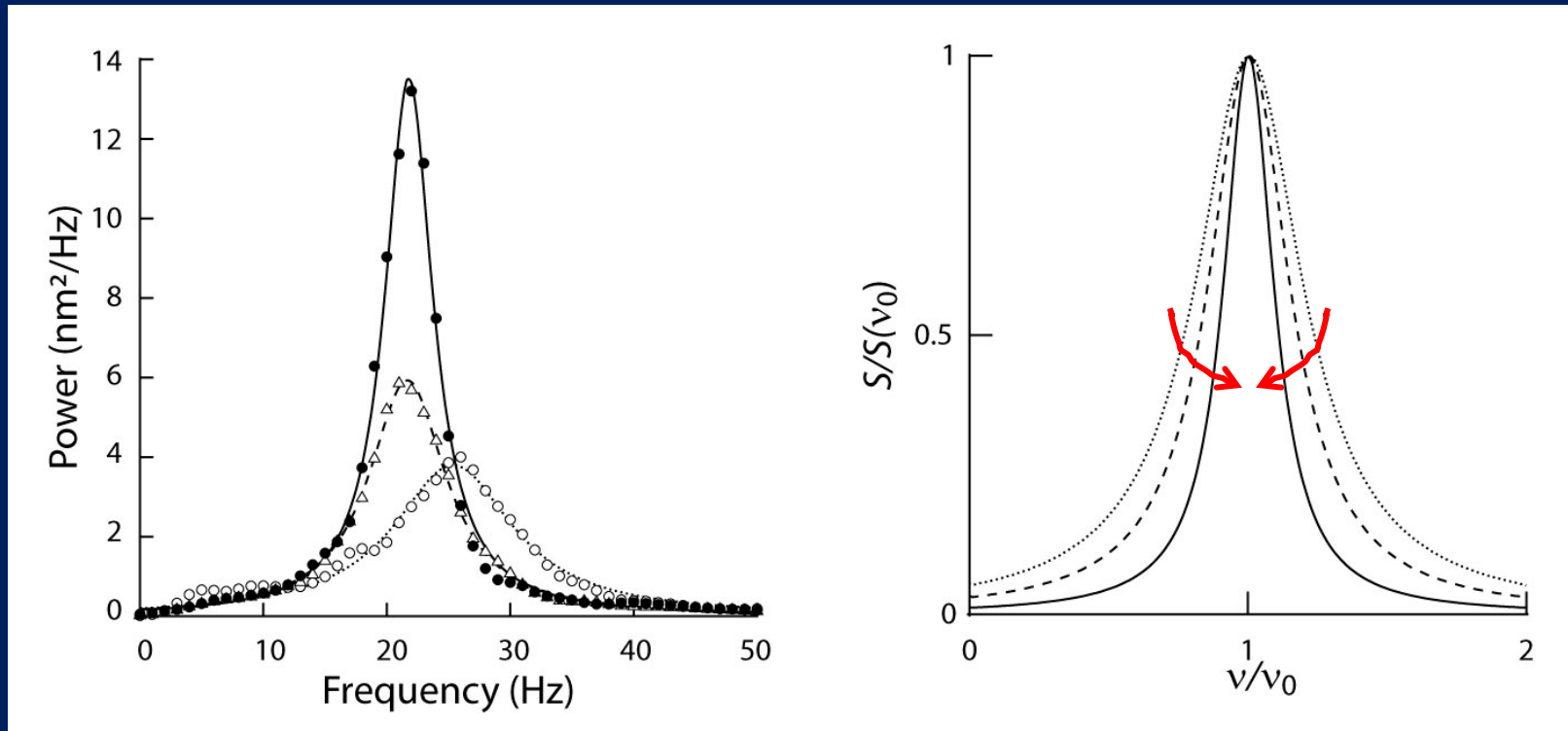
1. Measure $X(n)$
($X_1(n)$ and $X_2(n)$ known from step $n-1$)
2. (i) Calculate $F_1(n)$ and $F_2(n)$
(ii) Integrate stochastic differential equations with $-F_1(n)$ and $-F_2(n)$ to get $X_1(n+1)$ and $X_2(n+1)$
3. Move the fiber to $\Delta(n) = X(n) + F(n)/K_F$ with $F(n) = F_1(n) + F_2(n) + F_{EXT}$



Synchronization



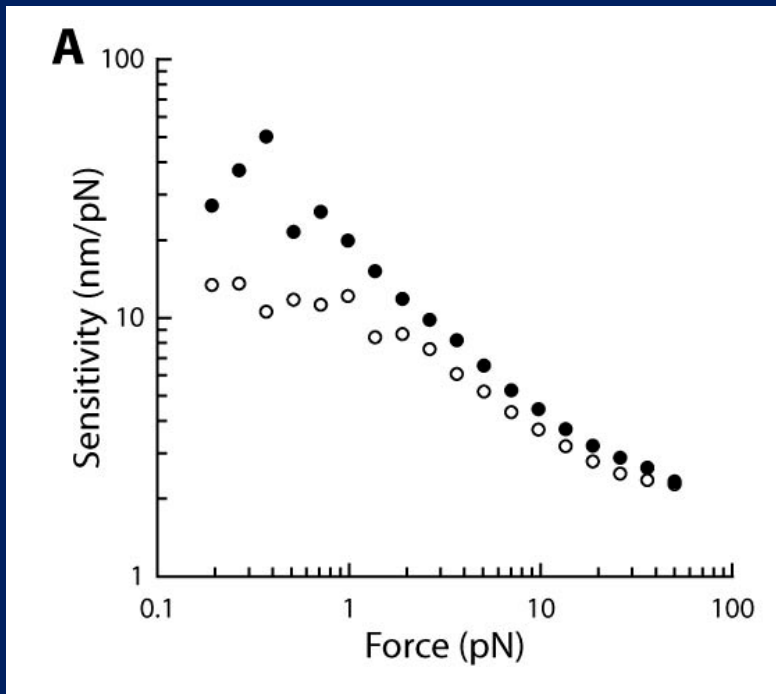
More regular oscillations!



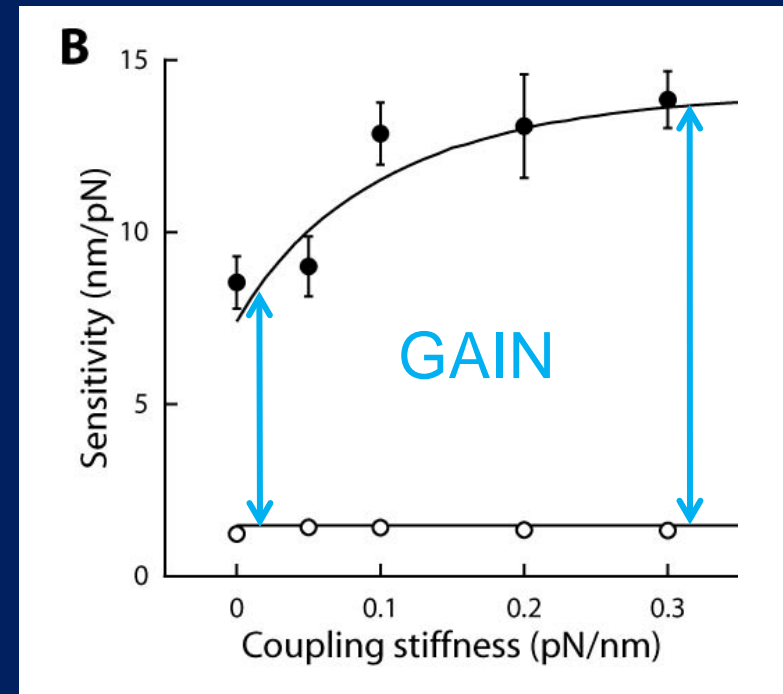
- : no coupling
- : $K = 0.2$ pN/nm
- : $K = 0.4$ pN/nm

Sensitivity to external stimuli

$$F_{\text{EXT}} = F_0 \sin(2\pi \nu_0 t)$$

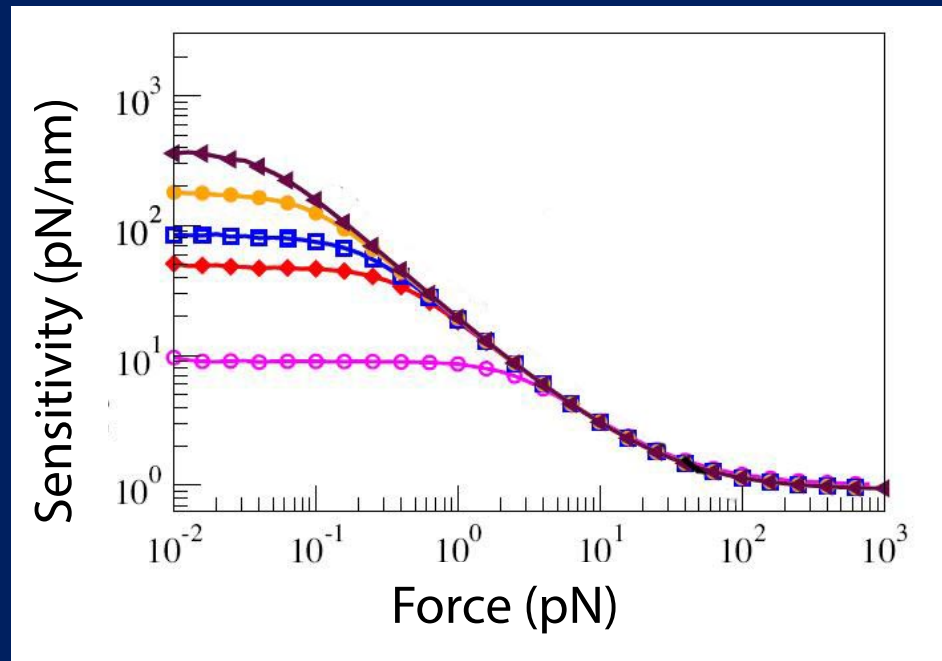


●: $K = 0.2$ pN/nm
○: no coupling

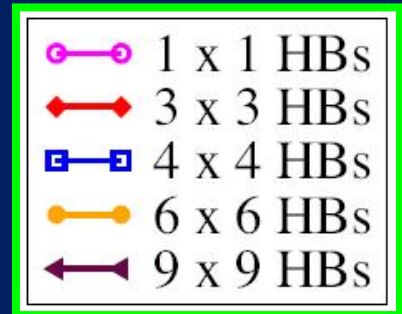
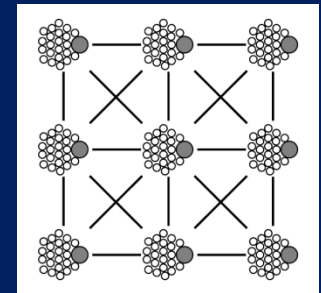


●: $F_{\text{EXT}} = 0.5$ pN
○: $F_{\text{EXT}} = 50$ pN

Groups of coupled hair bundles (simulations)



Oscillatory module:

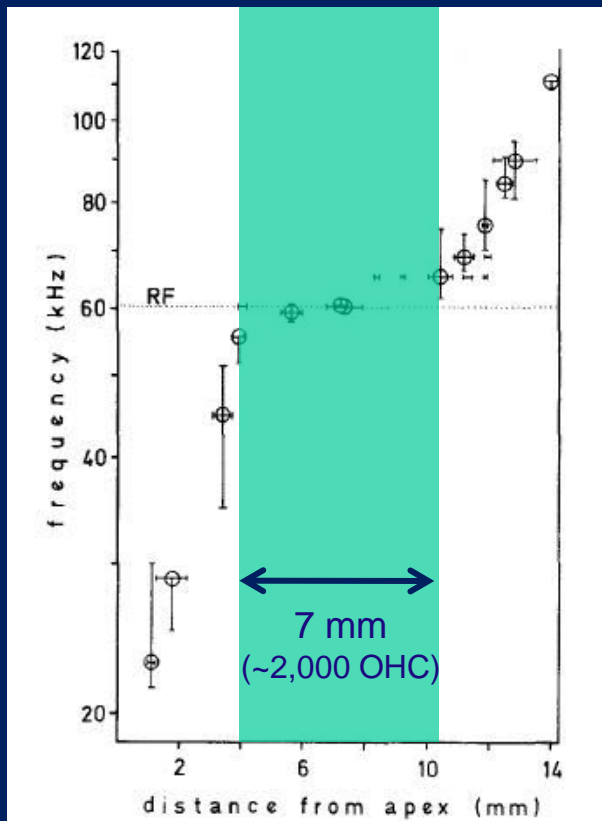


(Dierkes et al., PNAS (2008))

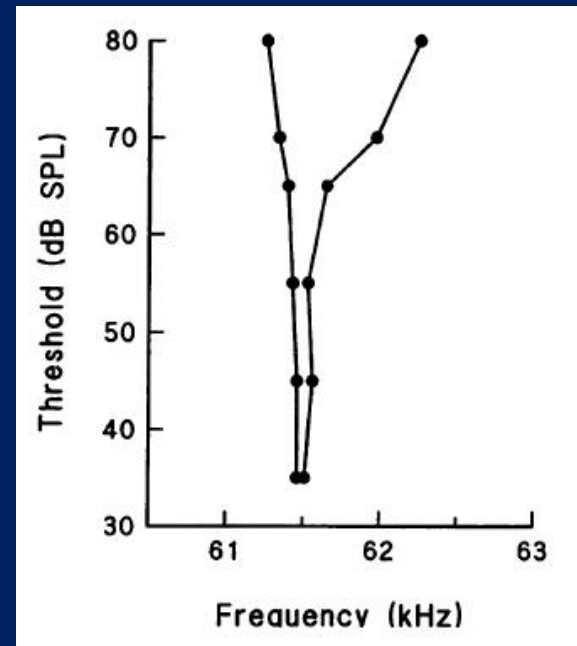
Tuning in the cochlea of the mustache bat (*Pteronotus*)



Tonotopic map



Iso-response tuning curve

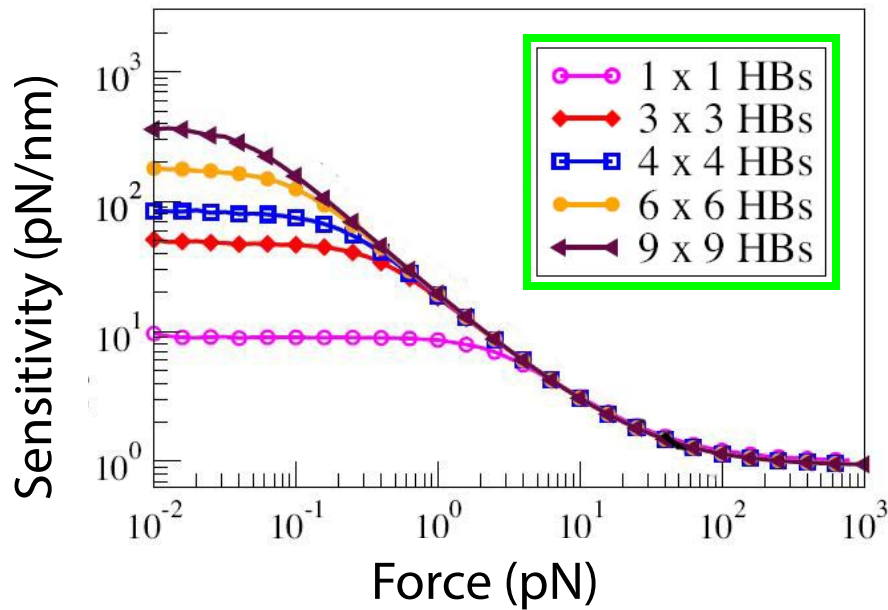


$Q > 1000!$

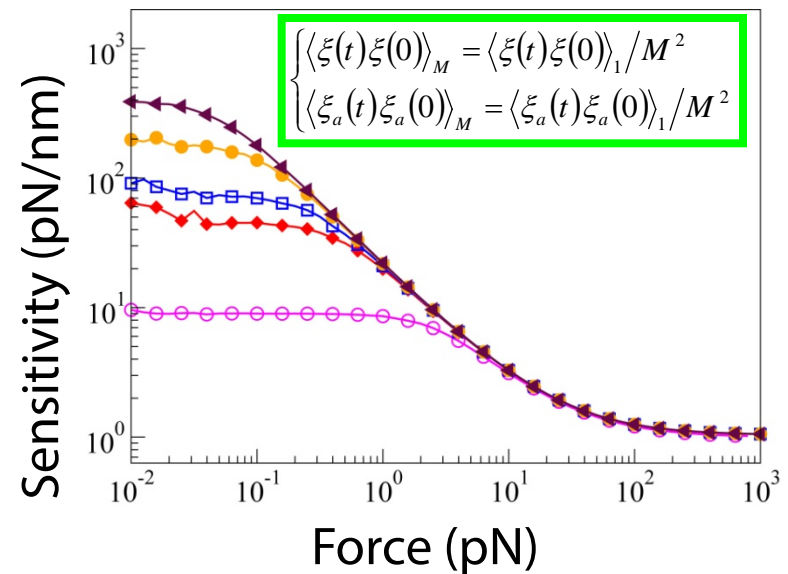
(Kössl and Russel, PNAS (1995))

Coupling \rightarrow noise reduction (simulations)

$M \times M$ cyber bundles



1 cyber bundle - reduced noise



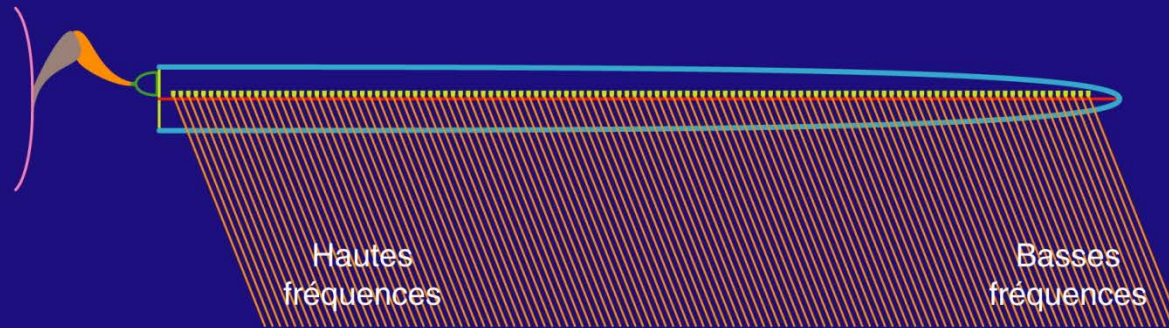
(Dierkes et al., PNAS (2008))

Self-sustained oscillators: nonlinear amplifiers for hearing

1. Amplified movements for small stimuli
2. Extended dynamic range of responsiveness
3. Increased frequency selectivity
4. « Essential » compressive nonlinearity: **prominent cubic distortions within the active bandwidth.**
5. Channel friction / noise limits amplification by a single cell
6. Coupling between cells reduces noise and enhances amplification

Outlook:

tonotopic organisation of critical oscillator modules



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