

# *From Atomistic Simulations to Macroscopic Interfacial Response*

Physical Principles of Multiscale Modeling,  
Analysis and Simulation in Soft Condensed Matter,  
Kavli Institute for Theoretical Physics, UCSB,  
May 3, 2012

M. O. Robbins with:

Fluids: X. Nie, J. Liu, S. Chen, W. E, C. Denniston

Solids: B. Luan, S. Hyun, N. Bernstein,

J. F. Molinari, T. Sharp, Lars Pastewka

Supported by the National Science Foundation

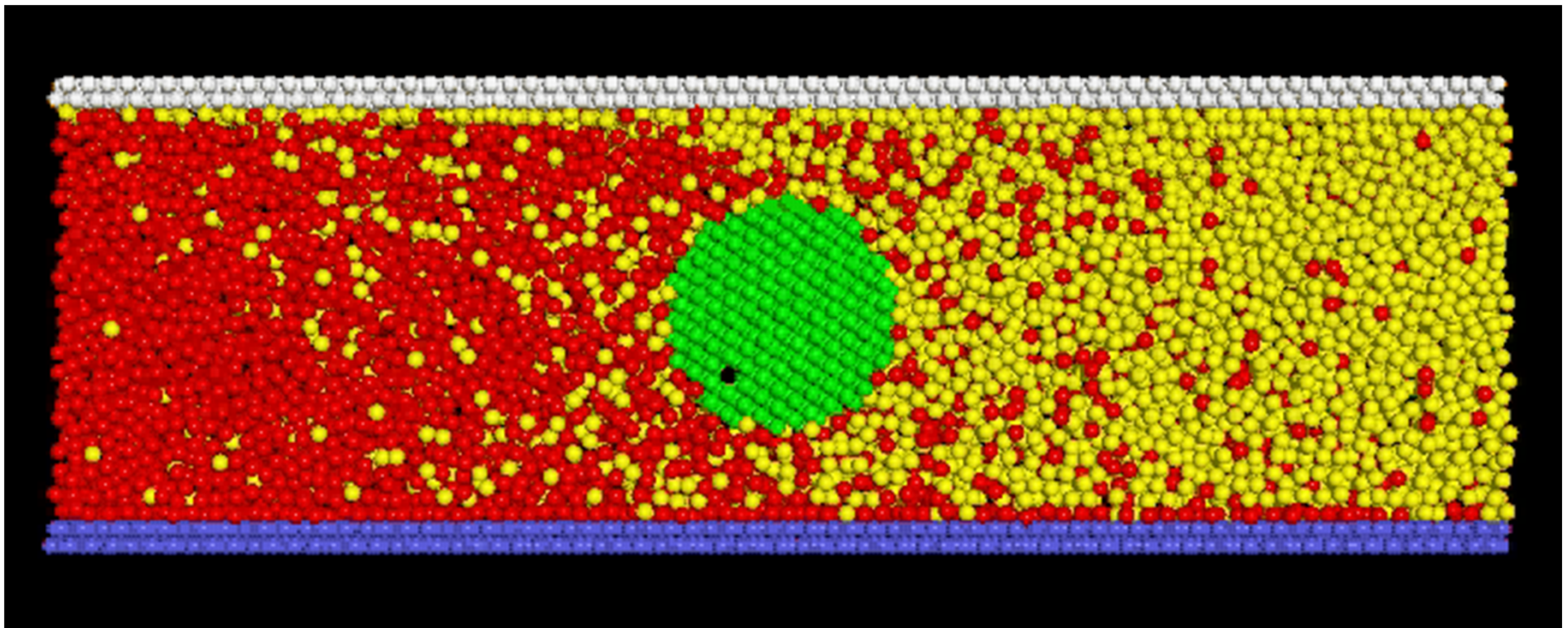


# *Unexpected Fine Scale Behavior*

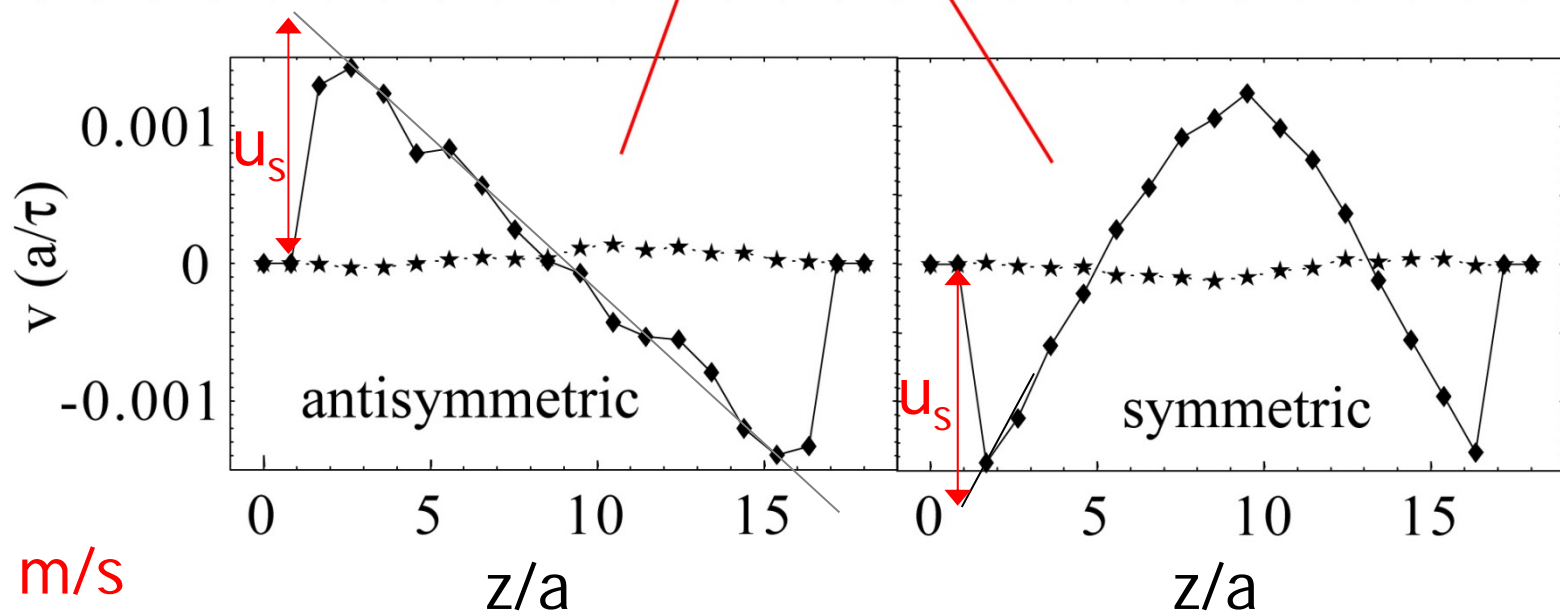
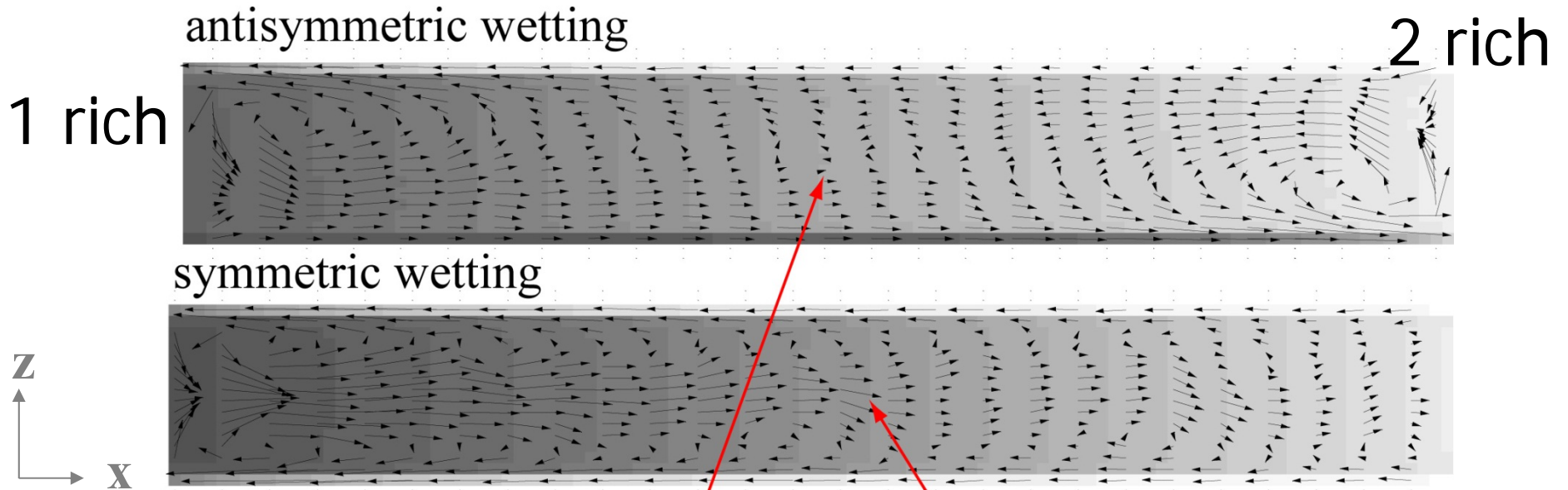
Many models coarse-grain to same equations

→ Micro model constructed to give a coarse-grained eqn (LB, SPH)  
can not be expected to give correct atomic and mesoscopic behavior

Nanomotor (C. Denniston & MOR, J. Chem Phys. 125, 214102, 2006)



# *Wetting + Conc. Gradient $\rightarrow$ Couette or Poiseuille-like flow between static walls*



$u_s \sim \text{m/s}$

# General Slip Boundary Condition

Atomistic flows fit by generalized sharp interface boundary conditions down to scales  $\sim$  a few nm

- Stress balance  $\rightarrow \Delta \sigma_{xz} \equiv \sigma_{xz}^b(w) - \sigma_{xz}^{wall} = \partial_x \gamma$
- Slip boundary condition

$$u_s = \frac{L_s}{\eta_b} \sigma_{xz}^b + \frac{L_m}{\eta_b} \partial_x \gamma + \left[ \frac{f_1}{c_1} - \frac{f_2}{c_2} \right] D \partial_x c_1$$

Navier Surface stress Diffusive

Can get net mass flux with no drag, negative slip lengths, ...

Velocities  $\sim$  m/s , stresses  $\sim$  MPa

# Phase-Field Model of Fluid-Fluid Interface

- If  $\xi \gg a \rightarrow$  coarse-grained F functional of  $\rho, \phi$
- Square-gradient theories

$$F = \int \left\{ \psi(\rho, \phi, T) + \frac{1}{2} K_\rho (\nabla \rho)^2 + \frac{1}{2} K_\phi (\nabla \phi)^2 + \frac{1}{2} K_{\rho\phi} (\nabla \rho \cdot \nabla \phi) \right\}$$

Usually ignore  $K_{\rho\phi}$  (odd in  $\phi$ ), assume  $K_{\rho\rho} > 0$

Often fix  $\rho$ , expand  $\psi$  as quartic polynomial in  $\phi$

**$\rightarrow$  None of these assumptions is good**

- Obtain  $\psi$  and K's from MD measurements of coexistence line, and pressure and linear response near coexistence
- Fit gives surface tension and width that agrees with MD results although not fit to them

Denniston & Robbins, Physical Review E69, 021505 (2004)

# Linear Response

- Apply perturbation:  $\delta\mu_\rho = -\mu_{\rho\theta} \sin qx$ ,  $\delta\mu_\phi = -\mu_{\phi\theta} \sin qx$

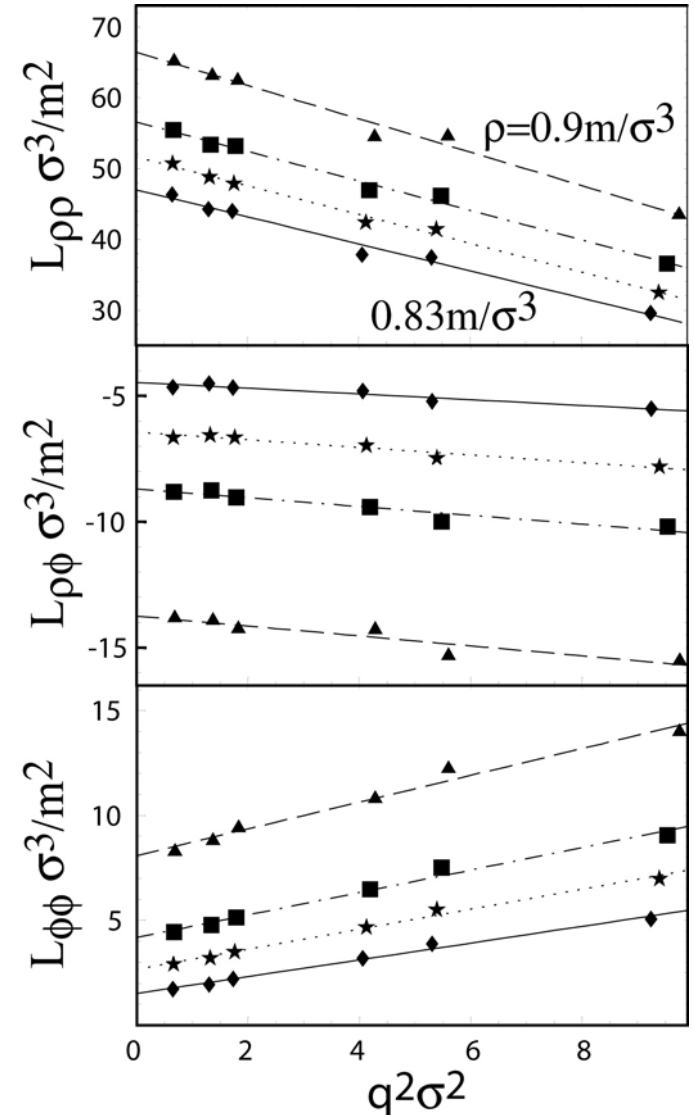
- Measure resulting  $\rho_q$ ,  $\phi_q$

$$\begin{pmatrix} L_{\rho\rho} & L_{\rho\phi} \\ L_{\rho\phi} & L_{\phi\phi} \end{pmatrix} \begin{pmatrix} \rho_q \\ \phi_q \end{pmatrix} = \begin{pmatrix} \mu_{\rho q} \\ \mu_{\phi q} \end{pmatrix}$$

$$L_{\rho\rho} = \partial^2 \psi / \partial \rho^2 + K_{\rho\rho} q^2, \dots$$

- Find L's linear in  $q^2$  to  $2\pi/q \approx 2\sigma$ , but  $K_{\rho\rho}, K_{\rho\phi} < 0$

- Usual to add  $q^4$  terms if  $K_{\rho\rho} < 0$  but expect  $K_{\rho\rho} \rightarrow 0$  as  $q \rightarrow \infty$  since cost of forcing atoms onto arbitrarily fine lattice  $\rightarrow 0$





# *Electro-Wetting on Dielectric (EWOD)*

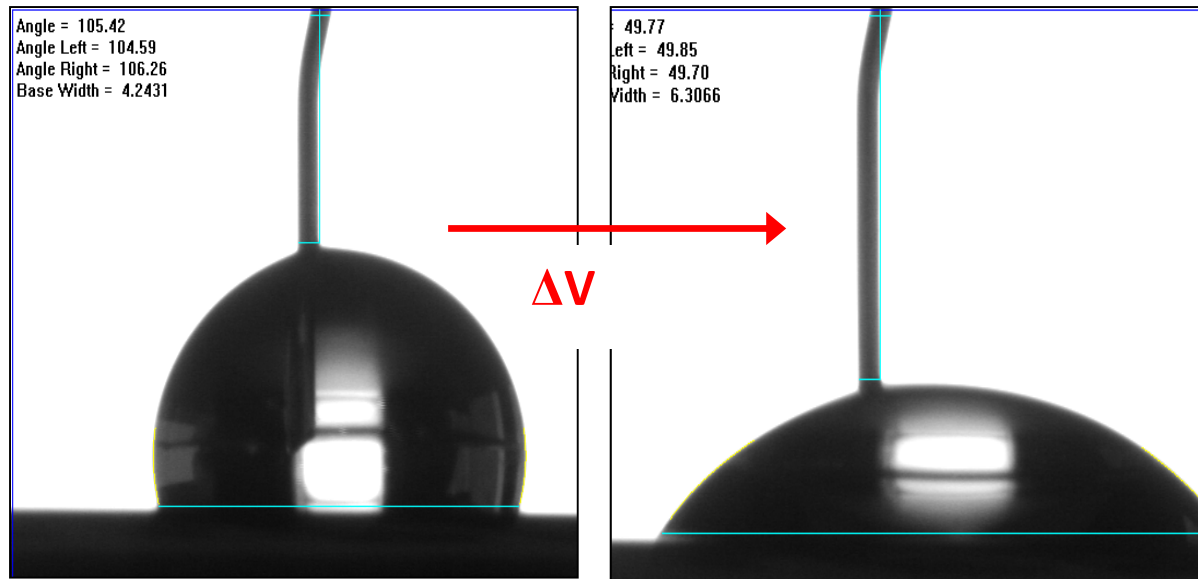
Electrowetting → Change in contact angle with voltage

Allows: Fluid drops to be guided on surface

Drop shape to be changed – active lenses

Questions: Can mechanism be used at nanometer scale?

Why does contact angle saturate before perfect wetting?



# *Electro-Wetting on Dielectric (EWOD)*

Equilibrium:  $\theta_0 \rightarrow$  balance between interfacial tensions

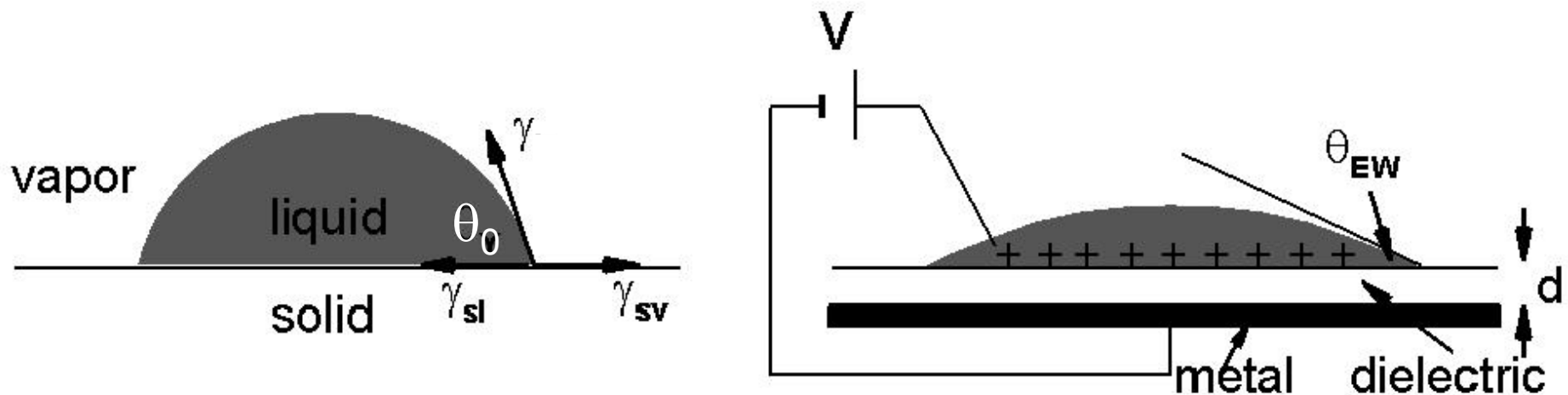
$$\text{Young's eqn: } \gamma \cos \theta_0 + \gamma_{sl} = \gamma_{sv}$$

Apply  $V$ : Must add effect of electrostatic energy

$$\text{Lippmann's eqn.: } \cos \theta - \cos \theta_0 = \epsilon_0 \epsilon_r V^2 / 2d\gamma = cV^2 / 2\gamma$$

$c$ =capacitance per unit area

Electrocapillary view  $\rightarrow$  surface tension reduced by electric energy per unit area:  $\gamma_{sl} \rightarrow \gamma_{sl} - cV^2/2$





# Experiments: Saturation at High Voltage

Proposed explanations:

Negative effective tension  $\rightarrow \gamma_{sl} - cV^2/2 < 0$

Quinn et al., J. Phys. Chem. B **109**, 6268 (2005).

Field diverges as approach contact line

Dielectric breakdown  $\rightarrow$  Charging of dielectric

Papathanasiou et al., J. Appl. Phys. **103**, 034901, (2008)

Micro-droplet ejection

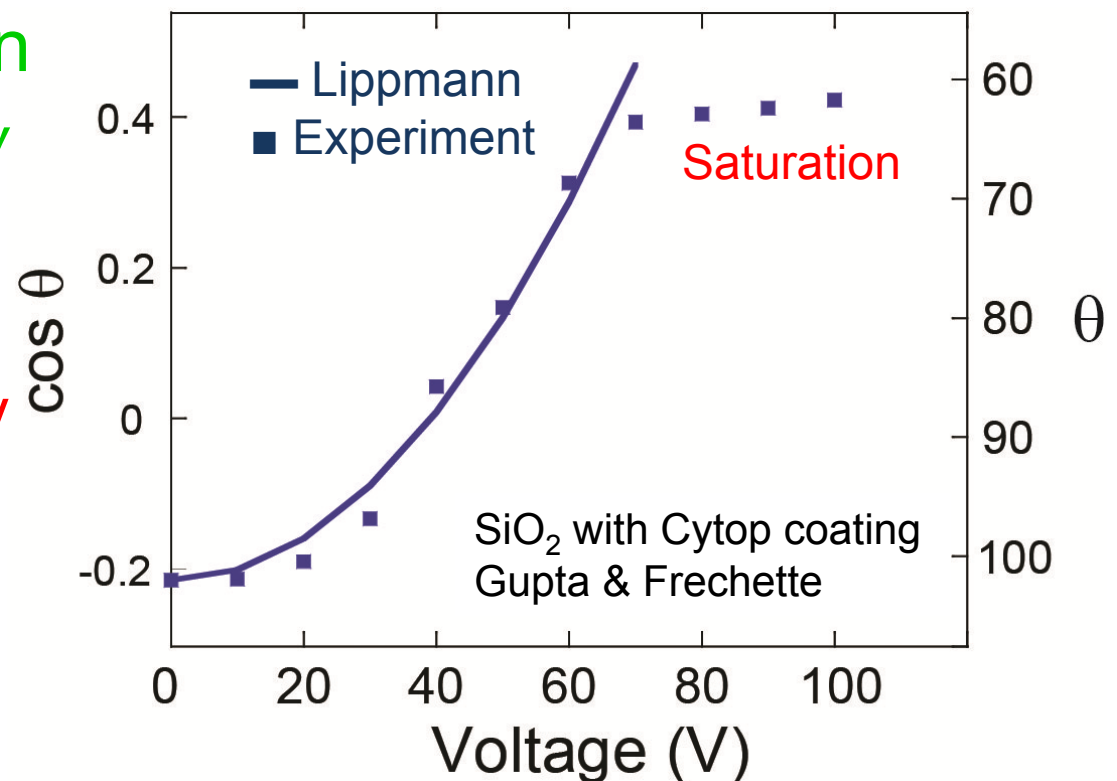
$\rightarrow$  Field overcomes  $\gamma$

Vallet et al. Eur. Phys. J. B **11**,  
583 (1999)

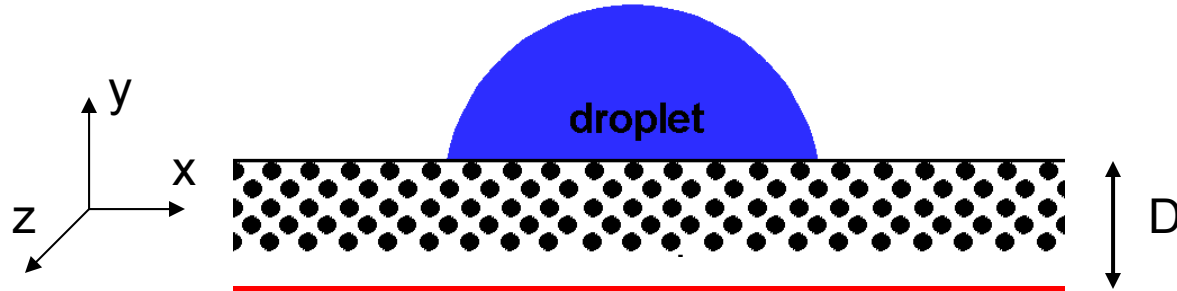
If continuum  $\rightarrow$  singularity

$\rightarrow$  atoms may matter

Moving contact lines,  
cavity flow, ...

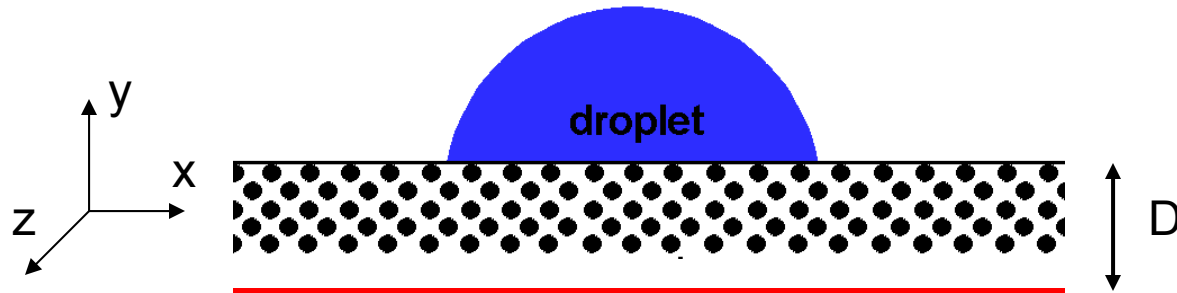


# Nanoscale Simulations of EWOD



- Fluid – short bead-spring chains 4 to 8 beads at  $T \sim 2T_g$   
 Covalent bonds on chain  $\rightarrow U_{\text{FENE}} = 0.5kR_0^2 \ln[1 - (r/R_0)^2]$   
 Interchain  $\rightarrow$  Lennard-Jones (LJ)  $U_{\text{LJ}} = 4u[(\sigma/r)^{12} - (\sigma/r)^6]$
- Rigid solid substrate, discrete atoms  $\rho_w = 0.61m\sigma^{-3}$
- Change solid-fluid binding energy  $u_{\text{sf}}$  to change  $\theta_0$
- Charge one monomer on some chains to increase  $V$
- Perfect conductor at depth  $D$  via image charges, uniform  $\epsilon$
- Periodic boundary conditions:  $L_x = 114.6\sigma$ ,  $L_z = 10.6\sigma$ ,  $L_y = 2L_x$   
 Correct to remove effect of periodic images along  $y$
- Measure  $\gamma$ ,  $\gamma_{\text{sv}} - \gamma_{\text{sl}}$ , capacitance  $c$  for uniform films – not fit

# Nanoscale Simulations of EWOD



Can express parameters in terms of key lengths  
normalized by molecular diameter  $\sigma$

Interface width  $\xi \sim 3\sigma$

→ Bjerrum length  $l_B = e^2 / \epsilon k_B T \rightarrow$  at  $l_B$  interaction =  $k_B T$

Gouy-Chapman screening length

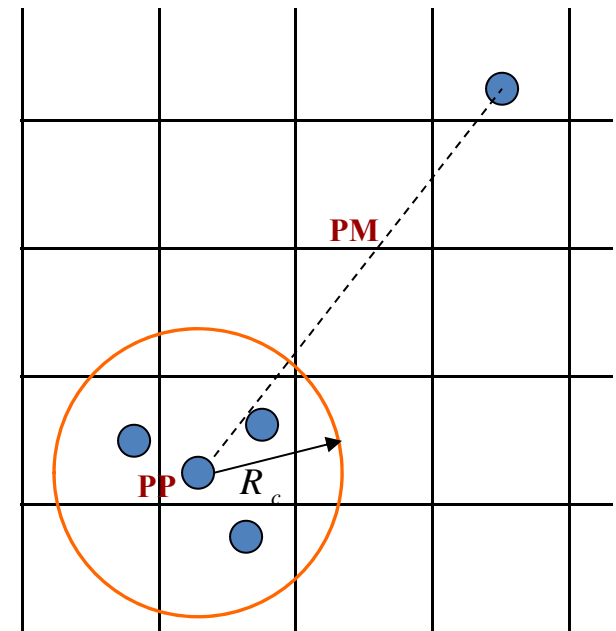
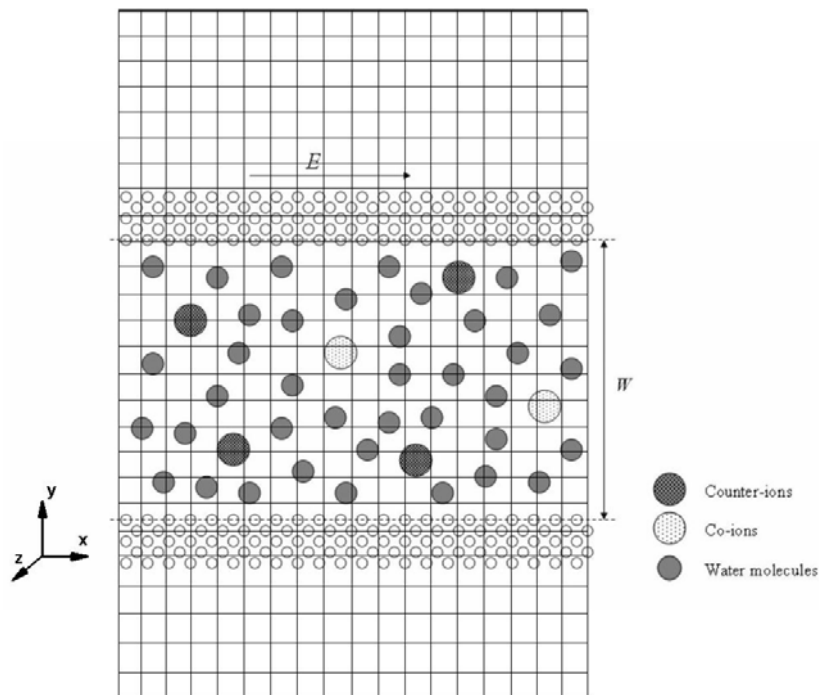
$\lambda_{GC} = e / 2\pi l_B cV$  where  $cV$  is surface charge density

Continuum theory assumes all lengths  $\sim 0$

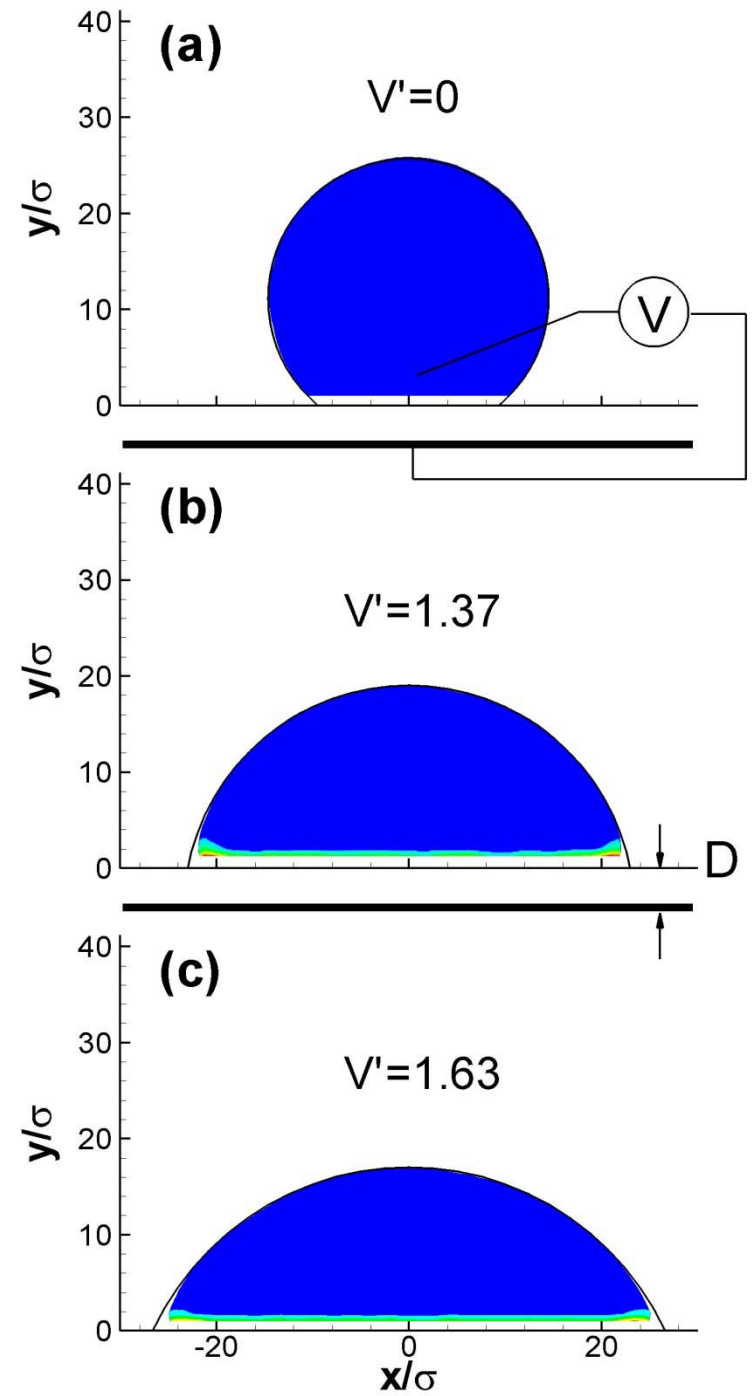
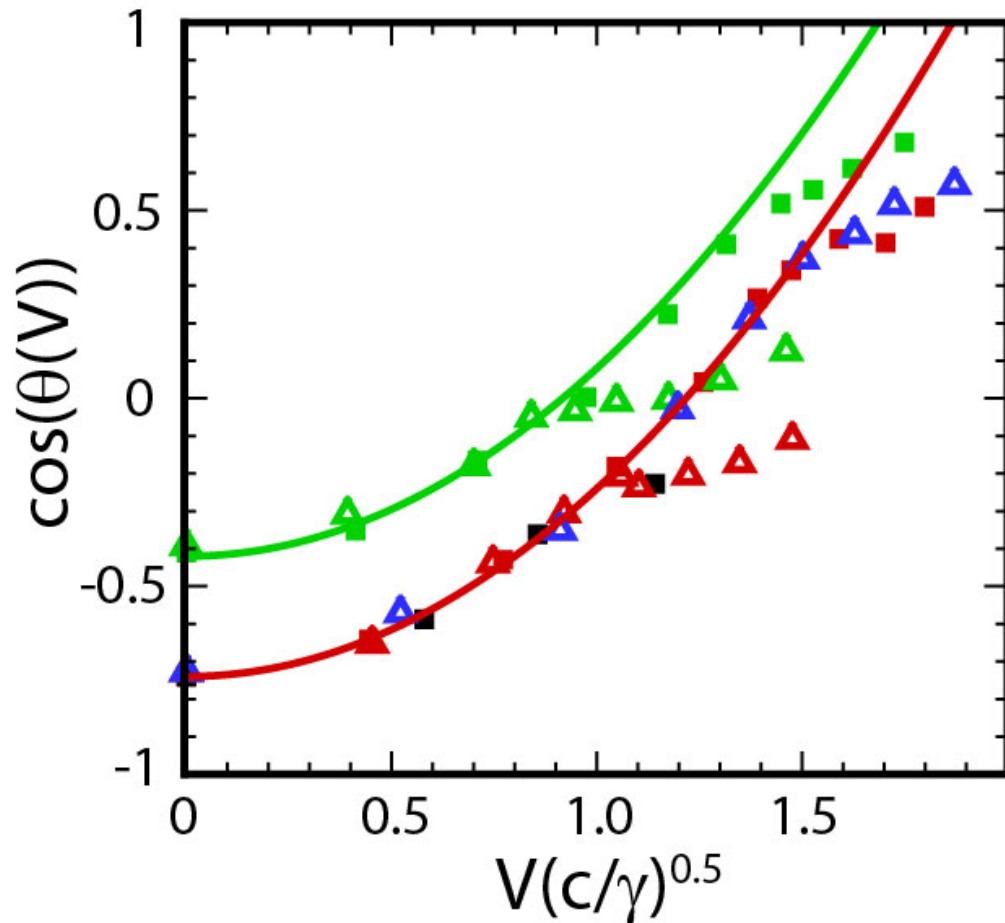
# Electroosmotic Flow & Electrowetting

- Direct summation of long range interactions is prohibitive for large systems.
- Use particle-particle particle-mesh with multigrid method for solving Poisson equation

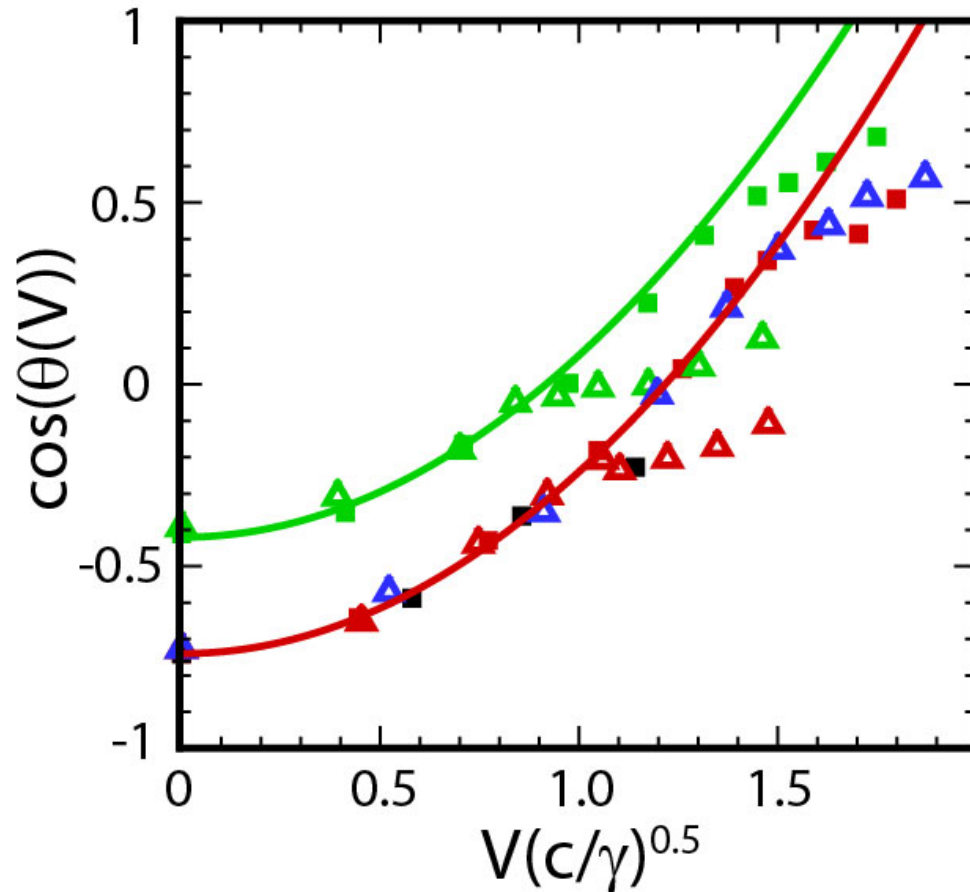
Liu, Wang, Chen and Robbins, J. Comput. Phys. **229**, 7834-7847 (2010)



# Behavior Like that in Macroscopic Experiments



# Comparison to Lippmann Equation



Lines – Lippmann  
with no fit params.

$\Delta$  chain length 4

■ chain length 8

Green: diff.  $u_{sf} \rightarrow \theta_0$

Black  $l_B = 96\sigma$

Red  $l_B = 12.32\sigma$

Blue  $l_B = 4\sigma$

As in experiment,  $\theta$  follows Lippmann at small  $V$  then saturates

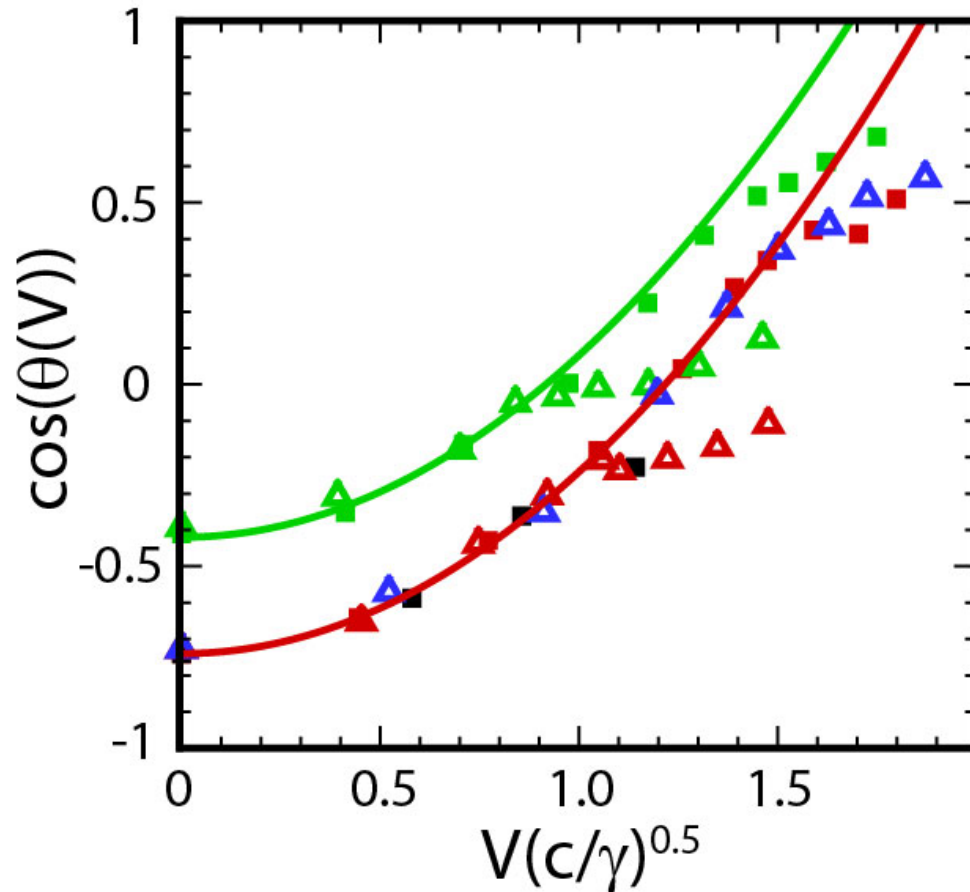
Saturation delayed for longer chains

since  $\gamma$  not changed by length  $\rightarrow$  molecular effect

Stronger screening, shorter  $l_B$ , delays saturation



# Comparison to Lippmann Equation



Lines – Lippmann  
with no fit params.

$\Delta$  chain length 4

■ chain length 8

Green: diff.  $u_{sf} \rightarrow \theta_0$

Black  $I_B=96\sigma$

Red  $I_B=12.32\sigma$

Blue  $I_B=4\sigma$

Not negative effective tension  $\gamma_{sl} - cV^2/2 < 0$  (Quinn et al., 2005).

$\gamma_{sl} \sim$  independent of chain length, arbitrarily large

No dielectric breakdown (Papathanasiou et al., 2008)

Not related to  $\gamma$  as expected if microdroplet ejection (Vallet et al., '99)

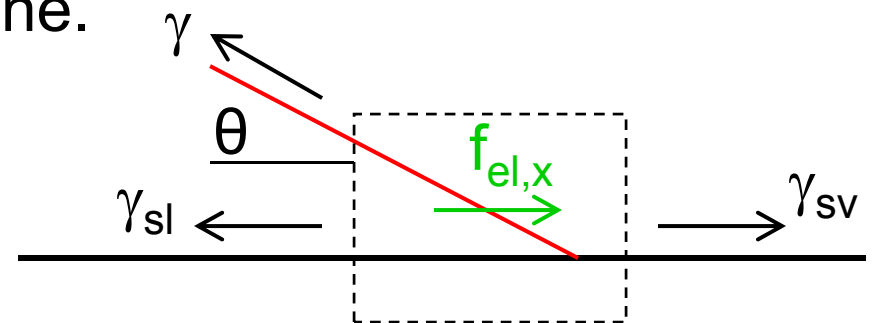
# Microscopic Force Balance Equation

Lippmann Equation derived from energy minimization with assumed geometry. May be violated.

Forces must balance everywhere in simulation

Consider region around contact line.

$f_{el,x}$  = Force per length from electric field on charge within region



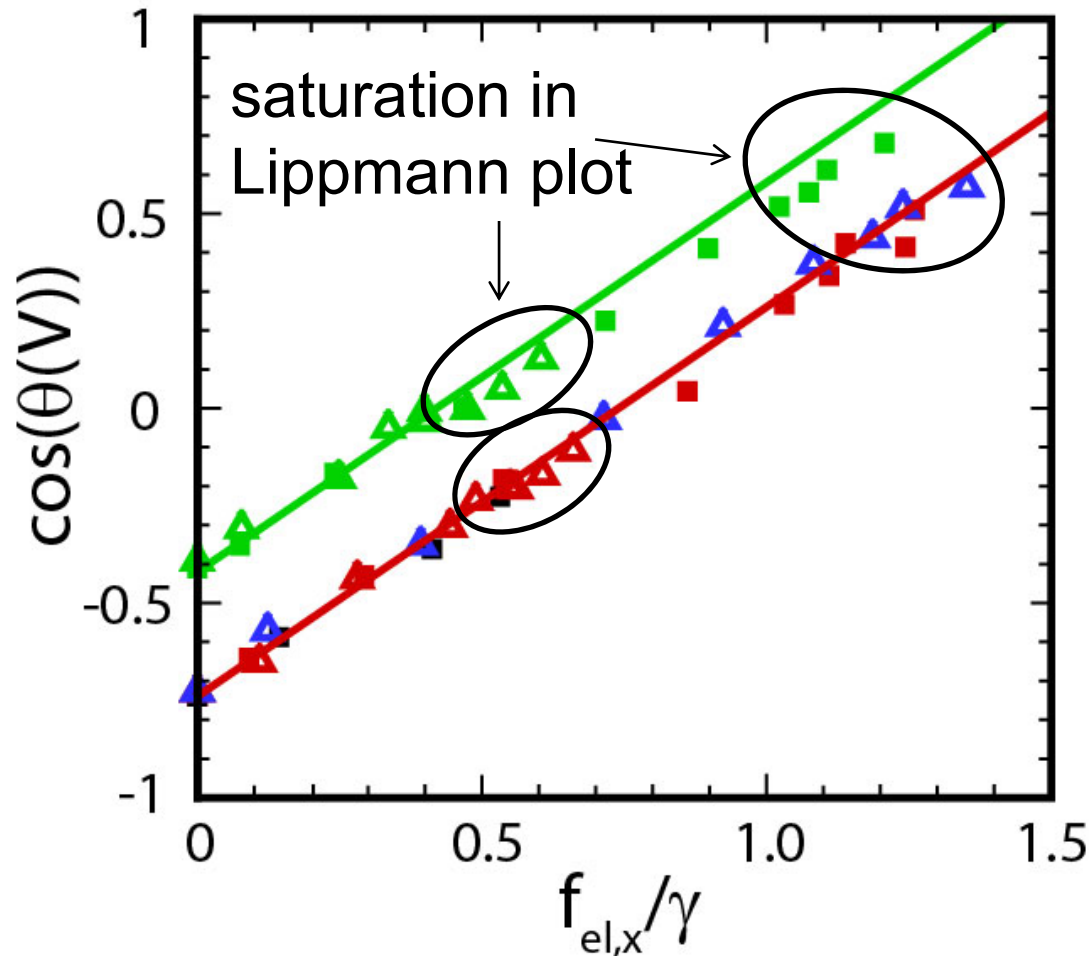
Net force must be zero  $\rightarrow f_{el,x} = \gamma [\cos \theta - \cos \theta_0]$

Reduces to Lippman if fringing fields don't change

Then only change with position of edge is increase in area with energy  $cV^2/2 \rightarrow f_{el,x}$

Choose region big enough to include most of electric field  $\sim 5\sigma$   
Bigger than interface width  $\sim 3\sigma \rightarrow$  capture entire surface tension

# Test of Force Balance Equation



$\Delta$  chain length 4

$\blacksquare$  chain length 8

Green: diff.  $\epsilon_{sf} \rightarrow \theta_0$

Black  $l_B=96\sigma$

Red  $l_B=12.32\sigma$

Blue  $l_B=4\sigma$

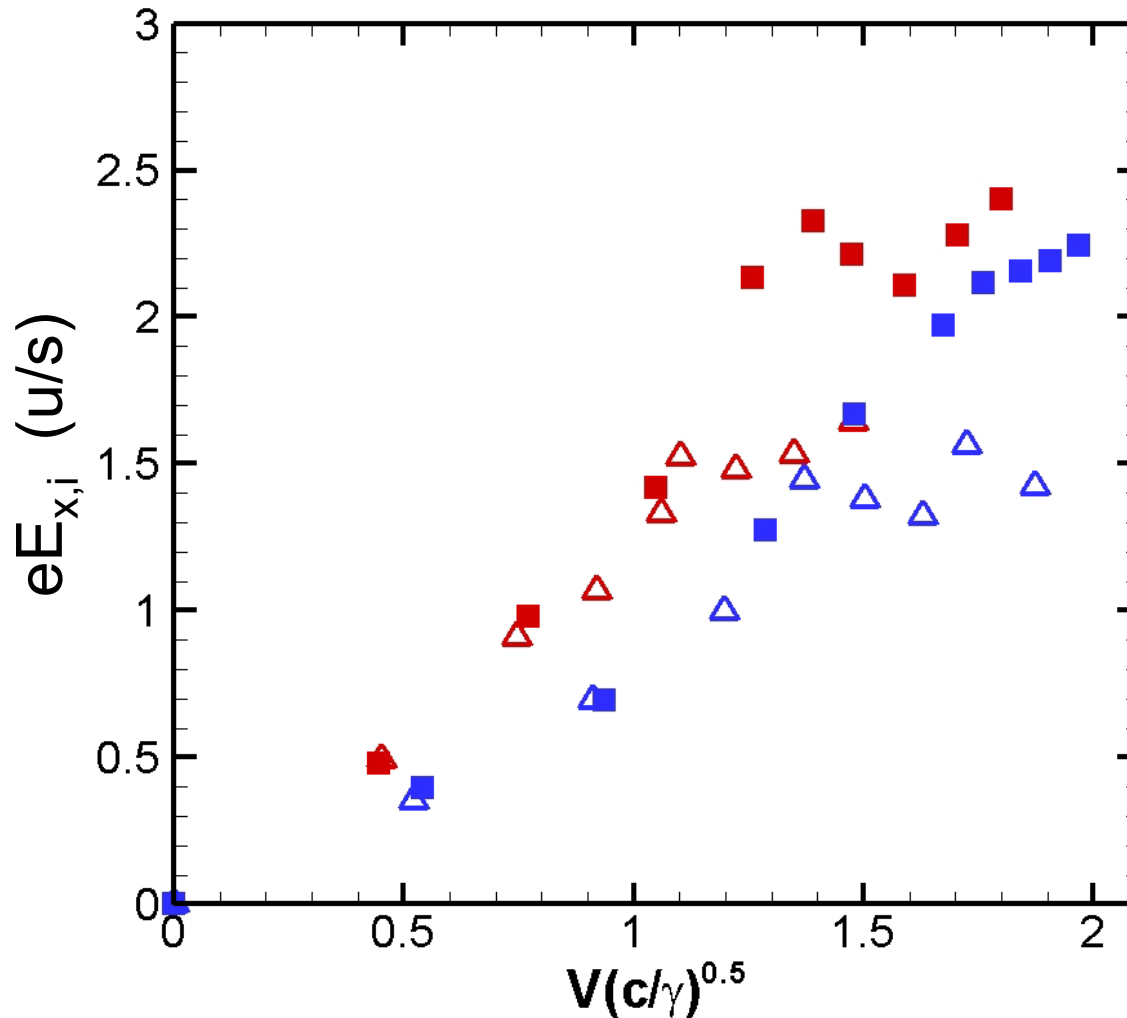
Lines assume bulk surface tensions.

Force balance holds at all voltages BUT  $f_{el,x}$  saturates.

Saturation depends on chain length.

At high field molecules leave drop, screen field at drop edge

# Maximum Force on Charges at Interface



$\Delta$  chain length 4

■ chain length 8

Red  $I_B=12.32\sigma$

Blue  $I_B=4\sigma$

Lateral interfacial field  $E_{x,i}$  rises at different rates for different  $I_B$ ,  $D$ , ...

Saturates at value that only depends on chain length  
Constant in saturation region of electrowetting

Exp.: Saturation delayed for larger ions (Heikenfeld)  
Saturation delayed for ac voltage (Ralston)

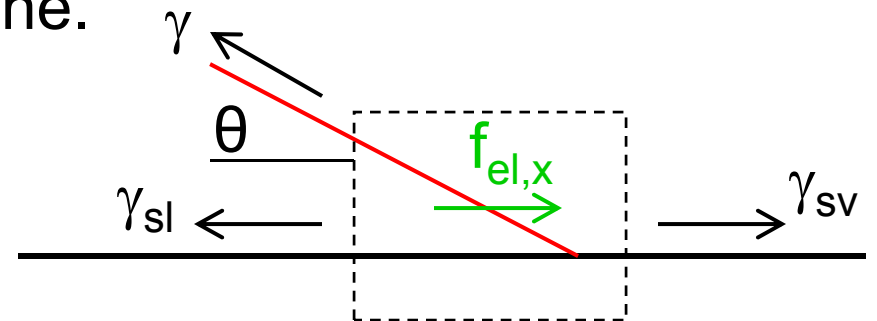
# Microscopic Force Balance Equation

Lippmann Equation derived from energy minimization with assumed geometry. May be violated.

Forces must balance everywhere in simulation

Consider region around contact line.

$f_{el,x}$  = Force per length from electric field on charge within region



Net force must be zero  $\rightarrow f_{el,x} = \gamma [\cos \theta - \cos \theta_0]$

Reduces to Lippman if fringing fields don't change

As region shrinks in size,  $f_{el,x} \rightarrow 0$  and  $\theta \rightarrow \theta_0$

although limited by finite width of interface

# *Electrowetting Conclusions*

- Similar electrowetting in  $\sim 10\text{nm}$  and macroscopic drops  
→ Can extend applications to nanoscales
- Lippmann equation fails as  $V$  increases,  $\theta(V)$  saturates
- Lateral force balance obeyed even after saturation  
Negligible changes in  $\gamma$ 's with  $V$
- Saturation → molecules pulled from drop at  $E_{x,l}$  that depends on molecular binding, size and not  $\gamma$   
Screen fringing fields  $f_{el,x}$  and limit increase in  $\cos\theta$
- May control saturation by varying ionic binding



# *Linking Atomistic and Continuum Regions*

Three overlap regions where solve both continuum and MD

Outermost → Continuum solution gives MD boundary condition

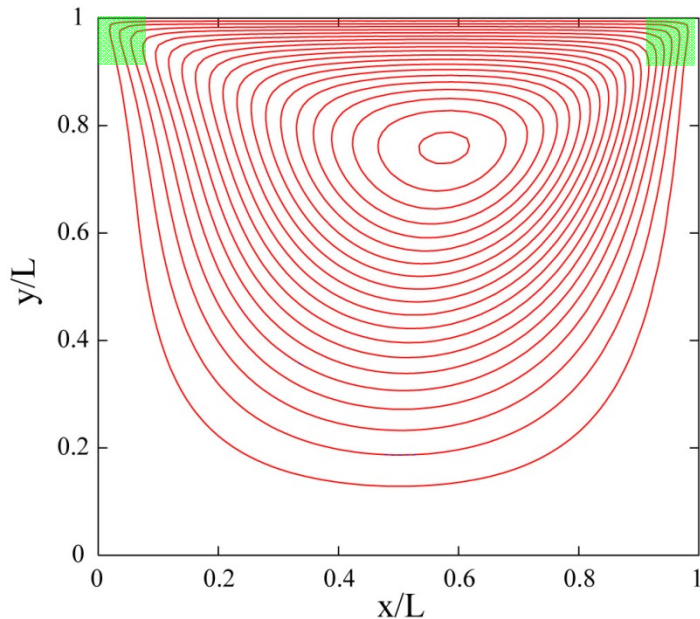
Innermost → MD gives continuum boundary condition

Middle → Two solutions equilibrate independently

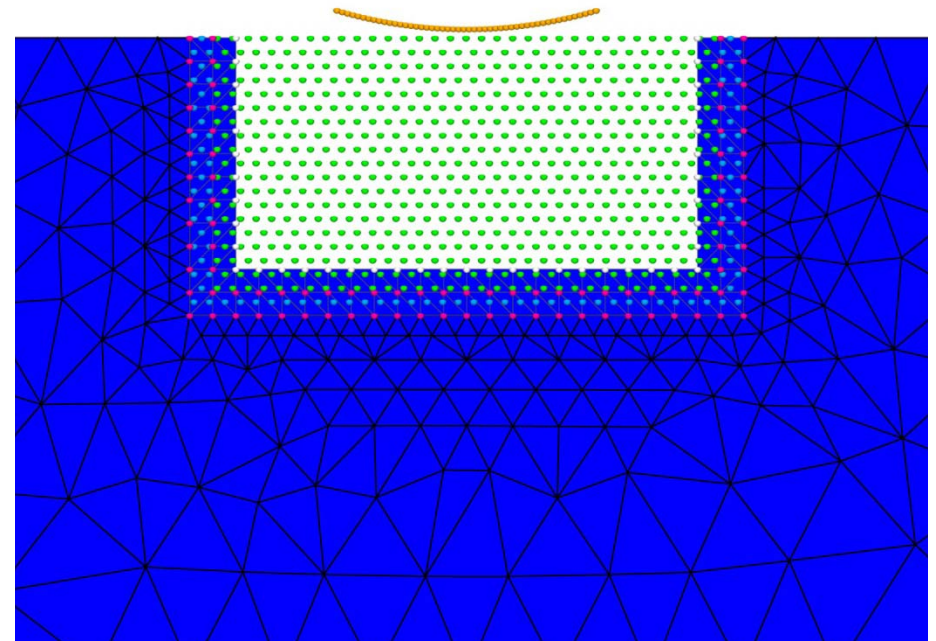
Fluids: Apply boundary conditions to velocities

Solids: Apply boundary conditions to displacements

Streamlines in  $L \sim 0.3\text{mm}$  channel with moving top wall. Atomistic solution in  $<1\%$  of area (green) removes continuum singularity



Model contact region atomistically, elastic deformations with finite-elements, constrain deformations in overlap region



# *Linking Atomistic and Continuum Regions*

Three overlap regions where solve both continuum and MD

Outermost → Continuum solution gives MD boundary condition

Innermost → MD gives continuum boundary condition

Middle → Two solutions equilibrate independently

Fluids: Apply boundary conditions to velocities

Solids: Apply boundary conditions to displacements

Fluids: S. T. O'Connell & P. A. Thompson, Phys. Rev. E52, R5792, (1995)

Why not use forces instead of displacements/velocities?

E. G. Flekkoy, G. Wagner & J. Feder, Europhys. Lett. 52, 271 (2000)

Fluids – Position of boundary is undetermined

→ drifts in response to fluctuations or systematic errors

General – Any error in constitutive relation creates problems in overlap region

Less sensitive when match displacements

any global factor in stress is irrelevant

# *Fluid Continuum – Incompressible Navier-Stokes*

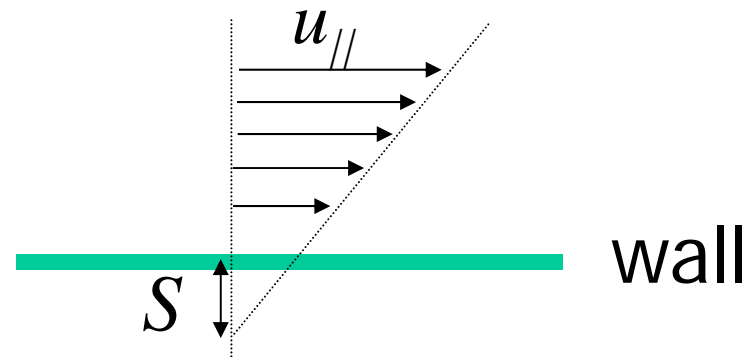
$$\partial_t \mathbf{u} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\frac{1}{\rho} [\nabla p + \mu \nabla^2 \mathbf{u}]$$

$$\nabla \cdot \mathbf{u} = 0$$

## *Navier slip boundary condition*

$$u_{\parallel}|_w = S \partial_{\perp} u_{\parallel}|_w \propto \text{stress}$$

↑  
Slip length



Knowledge of  $S$ ,  $\rho$  and  $\mu$  completely characterizes a simple fluid.

## *Atomistic Region → Molecular Dynamics*

Truncated and shifted Lennard-Jones potential

$$V^{\text{LJ}}(r) = 4\epsilon \left[ \left( \frac{\sigma}{r} \right)^{12} - \left( \frac{\sigma}{r} \right)^6 - \left( \frac{\sigma}{r_c} \right)^{12} + \left( \frac{\sigma}{r_c} \right)^6 \right]$$

$\sigma$ : Characteristic length, particle diameter.

$\epsilon$ : Characteristic energy.

$\tau \equiv (m\sigma^2/\epsilon)^{1/2}$ : Characteristic time of the potential.

$r_c$ : Cut-off distance, usually  $2.2\sigma$  for fluids

Integrate with velocity-Verlet, time step  $\Delta t_{\text{MD}} = 0.005\tau$

Determine parameters for fluid continuum model:

Temperature  $1.1\epsilon/k_B$ , density  $\rho = 0.81m\sigma^{-3}$ , viscosity  $\mu = 2.14\epsilon\tau\sigma^{-3}$ .

Wall (111) surface of fcc crystal

Wall-fluid interaction  $\epsilon_{\text{wf}}$  controls flow boundary condition (BC)

$\epsilon_{\text{wf}} = 0.95\epsilon \rightarrow$  no-slip BC,  $S=0$

# Hybrid Algorithm Applied to Fluids

Continuum: Incompressible Navier-Stokes (Projection method)

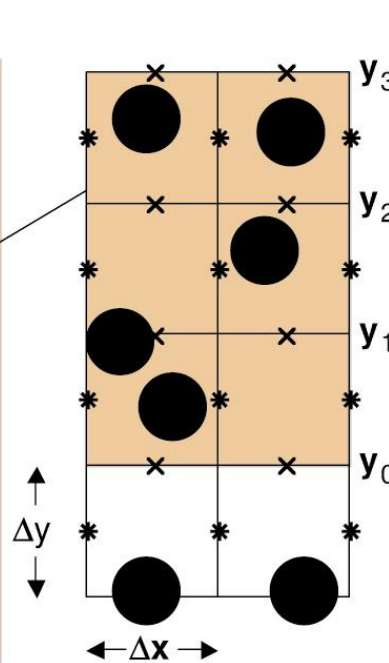
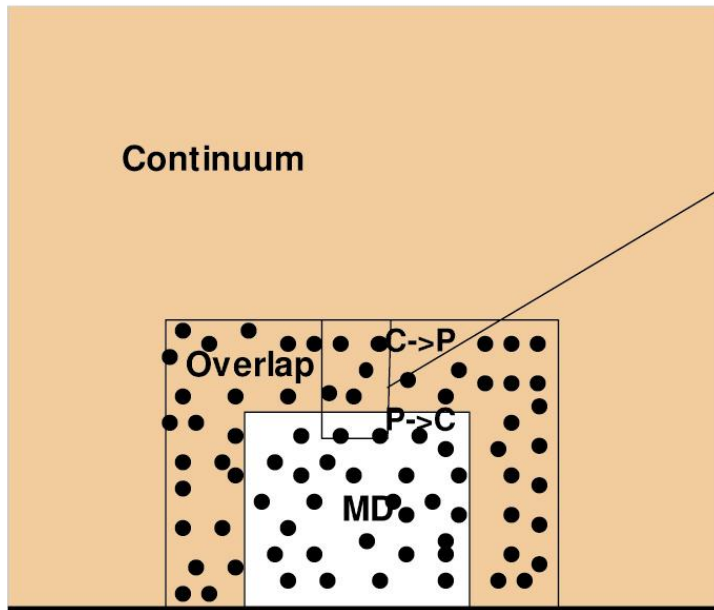
Atomistic: Molecular dynamics of Lennard-Jones atoms, no-slip

Potential:  $U(r) = 4\varepsilon((\sigma/r)^{12} - (\sigma/r)^6)$  ; Units  $\varepsilon, \sigma$

MD  $\rightarrow$  Continuum 
$$u_J = \frac{1}{N_J} \sum_{i=1}^{N_J} v_i$$

Continuum  $\rightarrow$  MD 
$$\frac{1}{N_J} \sum_{i=1}^{N_J} v_i = u_J(t) \quad m\ddot{x}_i = F_i - \frac{1}{N_J} \sum_{k=1}^{N_J} F_k + m \frac{Du_J}{Dt},$$

$$F_i = -\frac{\partial}{\partial \mathbf{x}} \sum_k V_{ik}^{LJ}.$$



C $\rightarrow$ P Potential confines particles at  $y_3$

P $\rightarrow$ C Insert/remove number of particles equal to net flux

# Equation of Motion for Constrained Particles

The equation of motion for the particle  $i$ :

$$\ddot{\mathbf{x}}_i = \frac{\mathbf{F}_i}{m} - \frac{1}{N_J m} \sum_{i=1}^{N_J} \mathbf{F}_i + \frac{D\mathbf{u}_J(t)}{Dt}, \quad \mathbf{F}_i = -\frac{\partial}{\partial \mathbf{x}_i} \sum_j V_{ij}^{\text{LJ}}$$

Finite Difference Scheme for the equation of motion:

$$\frac{\mathbf{x}(t + \Delta t_{MD}) - 2\mathbf{x}(t) + \mathbf{x}(t - \Delta t_{MD})}{\Delta t_{MD}^2} = \frac{\mathbf{F}_i}{m} - \frac{1}{N_J m} \sum_{i=1}^{N_J} \mathbf{F}_i - \frac{1}{\Delta t_{MD}} \left( \frac{1}{N_J} \sum_{i=1}^{N_J} \mathbf{v}_i(t) - \mathbf{u}_J(t) \right)$$

$\Delta t_{FD} = 40\Delta t_{MD} \rightarrow$  Staggered time grid

Average MD over  $\Delta t_{FD}$  to fix continuum boundary

Extrapolate continuum to integrate next MD interval



# Particle Confinement and Mass Flux

External force  $F$  for  $y_2 \leq y \leq y_3$

$$F_y = -\alpha p_0 \sigma \frac{(y - y_2)}{1 - (y - y_2)/(y_3 - y_2)}$$

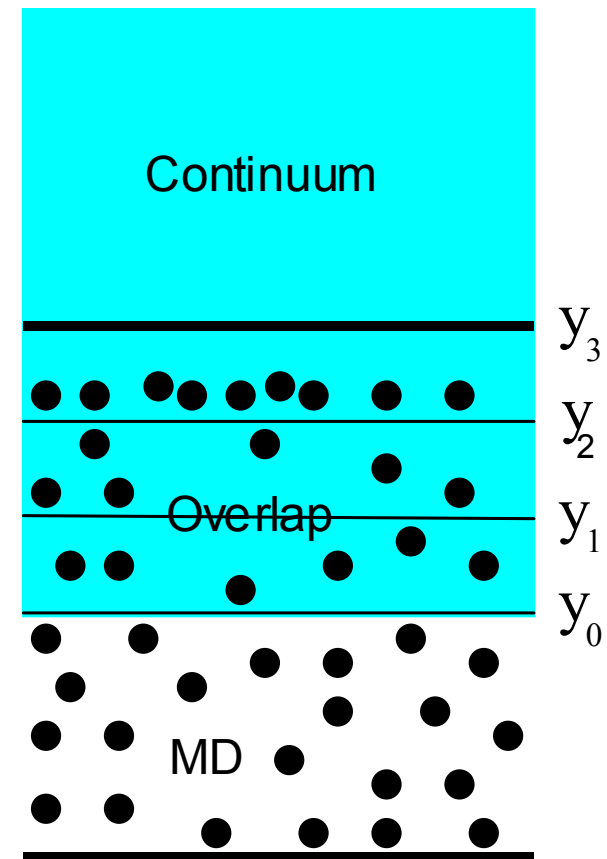
Maintain a mass flux by introducing particles  $n(x, t)$  near  $y = y_2$

$$mn(x, t) = -A \rho u_y(x, y_2, t) \Delta t_{MD}$$

Langevin thermostat for  $y_2 < y < y_3$  :

$$m\ddot{y}_i = \sum_{j \neq i} \frac{\partial V^{LJ}(r_{ij})}{\partial x_i} - m\Gamma \dot{y}_i + \zeta_i$$

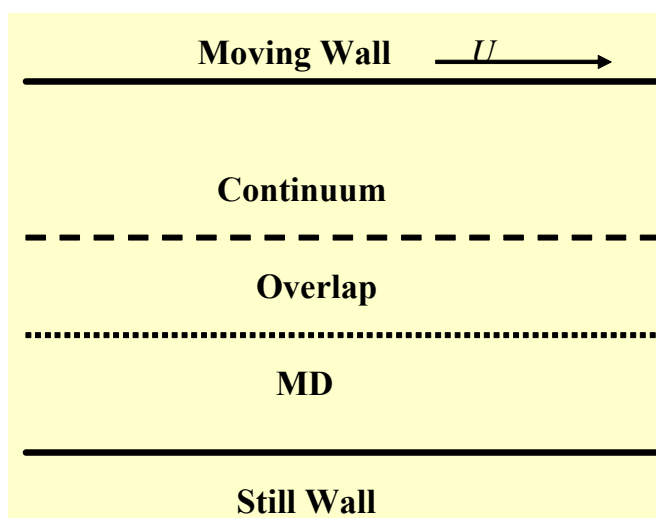
$$\langle \zeta_i(t) \zeta_j(t') \rangle = \delta_{ij} \delta(t - t') 2k_B T \Gamma$$



Werder et al. J. Comp. Phys. 205, 373 (2005)  
claim artifacts, but use different implementation

# Dynamic Couette Flow

## Schematic of simulation

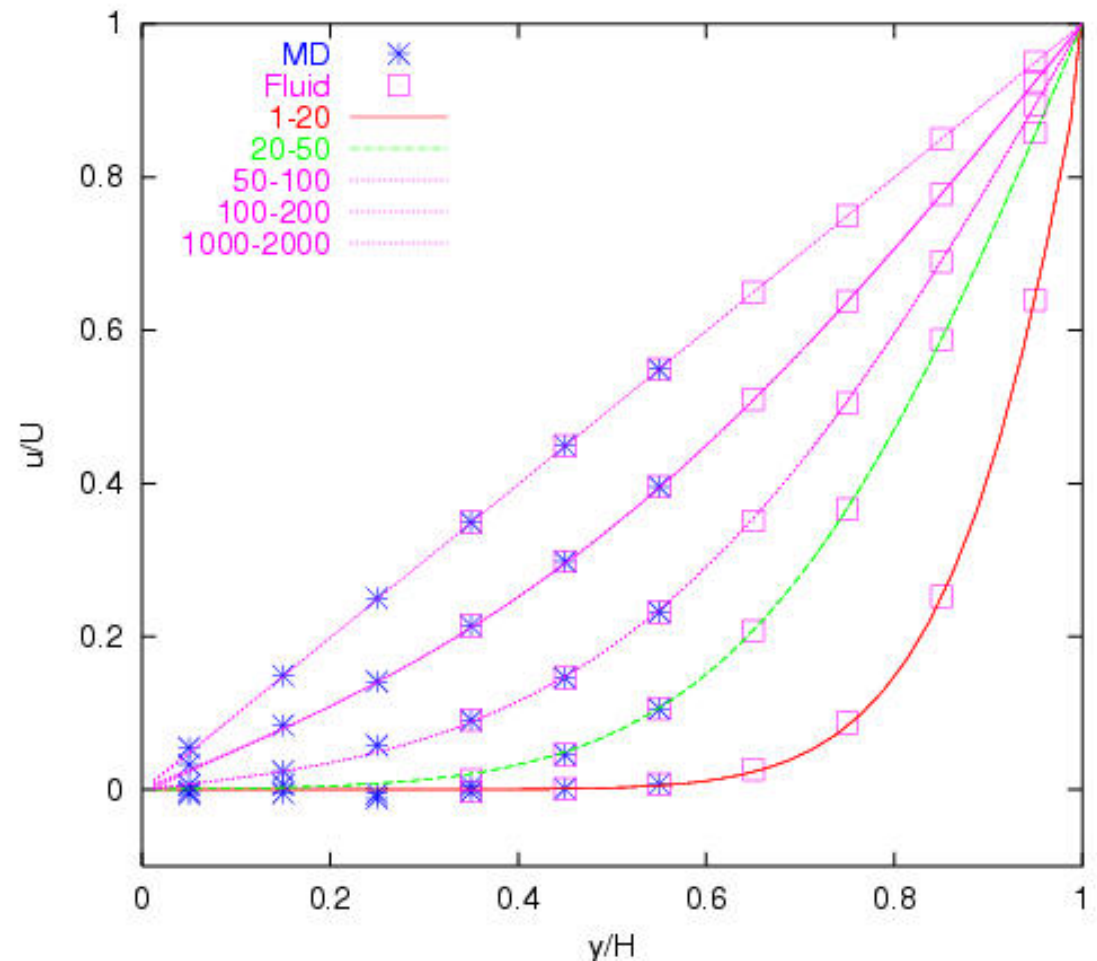


$$\Delta t_{FE} = 40 \Delta t_{MD}$$

Use 10 realizations of MD, 1 continuum

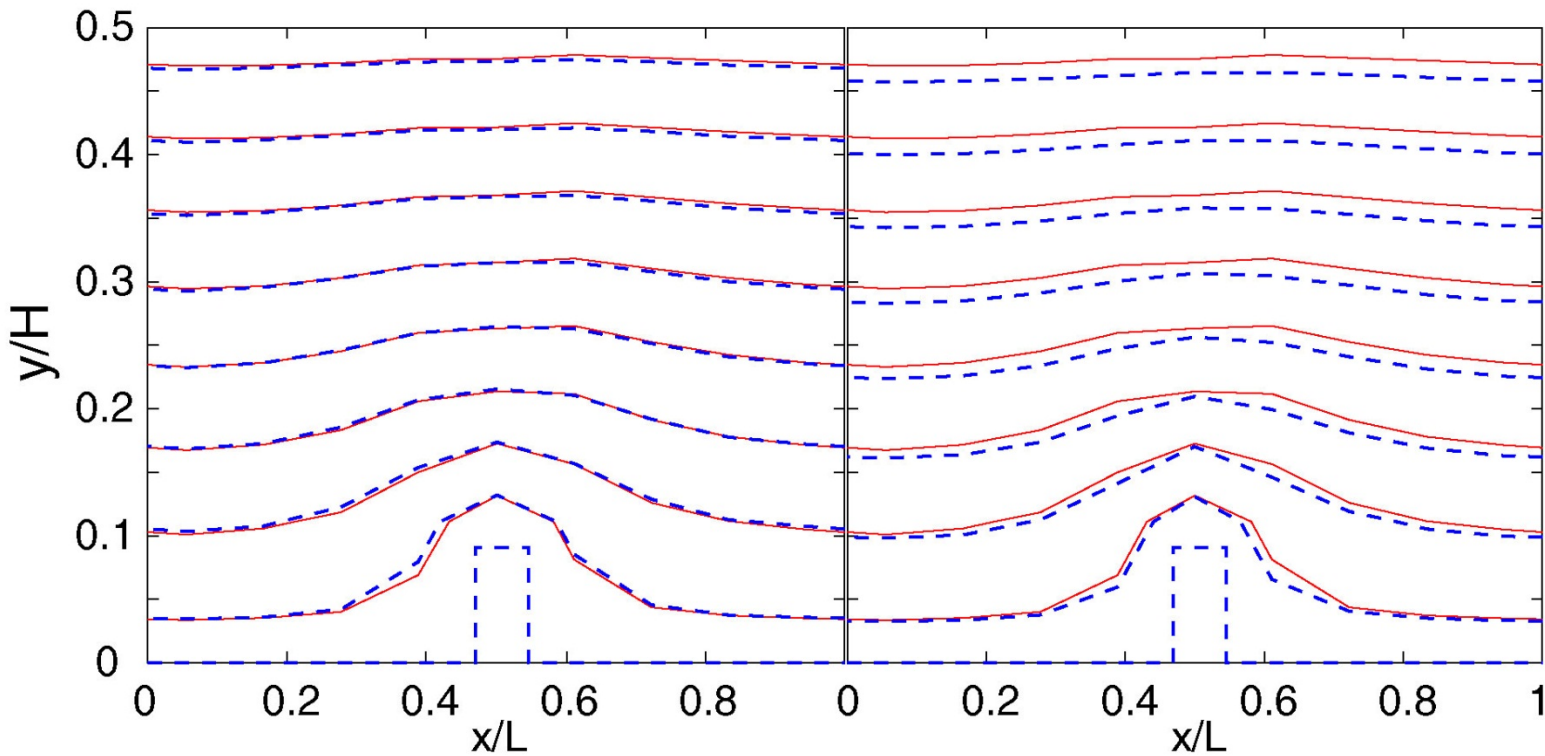
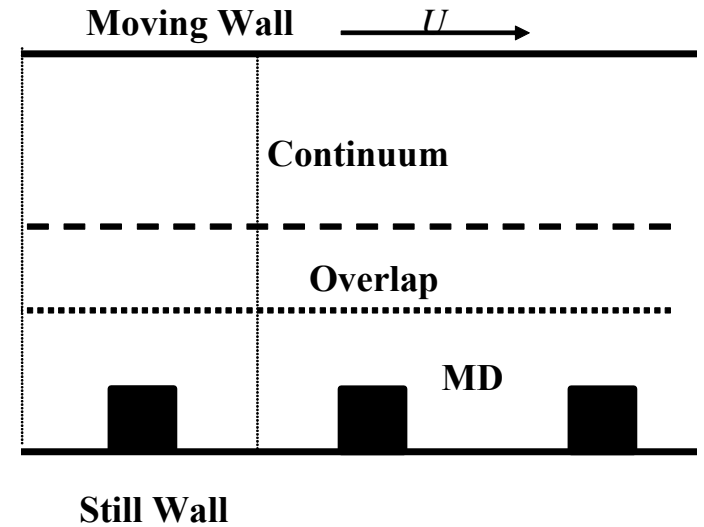
X. B. Nie, S. Y. Chen, W. N. E  
and M. O. Robbins, J. Fluid  
Mech. 2004.

Hybrid solution (symbols) tracks full continuum (lines) as a function of time after motion starts



# Flow past a rough wall

Streamlines from hybrid  $\approx$  MD  
includes flow between regions  
Continuum fails because doesn't  
match complex boundary  
condition around bump

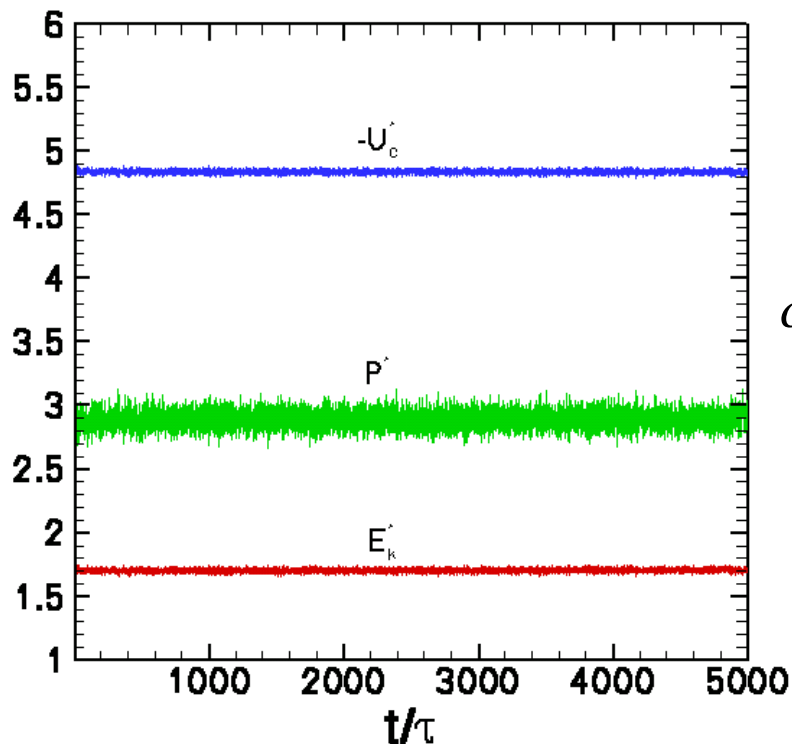


Hybrid vs. MD

Hybrid vs. Continuum

## Including Heat Flux

$$\left\{ \begin{array}{l}
 \nabla \cdot \mathbf{u} = 0 \\
 \rho(\partial_t \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u}) = -\nabla p + \mu \nabla^2 \mathbf{u} \\
 \rho c_V \left( \frac{\partial T}{\partial t} + \vec{u} \cdot \nabla T \right) = \lambda \nabla^2 T + \mu \left[ 2 \left( \frac{\partial u_x}{\partial x} \right)^2 + 2 \left( \frac{\partial u_y}{\partial y} \right)^2 + \left( \frac{\partial u_x}{\partial y} + \frac{\partial u_y}{\partial x} \right)^2 \right]
 \end{array} \right.$$



Heat capacity  $c_V$ , for incompressible fluid

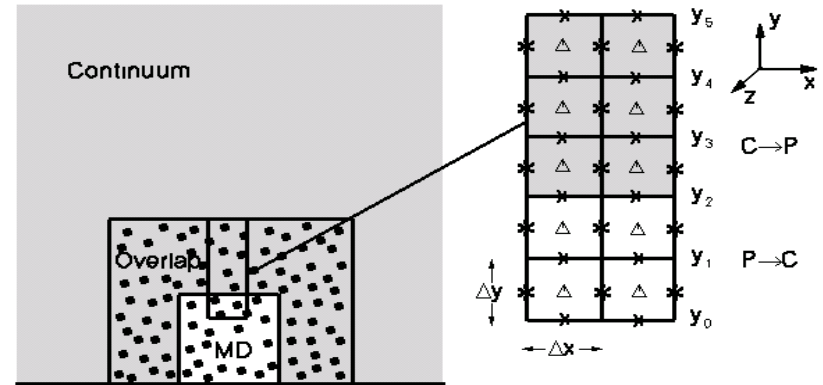
$$c_V = \frac{3k_B}{2m} \left[ 1 - \frac{2}{3N(k_B T)^2} \langle (\delta E_k)^2 \rangle \right]^{-1} = 2.43 \frac{k_B}{m}$$

# Coupling Scheme: Momentum and Energy

MD → Continuum :

$$\frac{1}{N_J} \sum_i \mathbf{v}_i = \mathbf{u}_{J,MD}(t)$$

→ 
$$\frac{1}{N_J - 1} \sum_i \frac{1}{2} m (\mathbf{v}_i - \mathbf{u}_{J,MD})^2 = T_{J,MD}(t)$$



Continuum → MD (Constraint Dynamics and velocity rescaling):

$$\left\{ \begin{array}{l} \frac{1}{N_J} \sum_i \mathbf{v}_i = \mathbf{u}_{J,C}(t) \quad \ddot{\mathbf{x}}_i = \frac{D\mathbf{u}_{J,C}(t)}{Dt} + \zeta_i \quad \sum_i \zeta_i = 0 \\ \zeta_i = \frac{\mathbf{F}_i}{m} - \frac{1}{N_J m} \sum_{i=1}^{N_J} \mathbf{F}_i \quad \mathbf{F}_i = -\frac{\partial}{\partial \mathbf{x}_i} \sum_{j \neq i} V^{LJ}(r_{ij}) \quad \text{X. Nie et al. } JFM \text{ } 500, 55-64 \text{ (2004)} \\ \ddot{\mathbf{x}}_i = \frac{\mathbf{F}_i}{m} - \frac{1}{N_J m} \sum_{i=1}^{N_J} \mathbf{F}_i + \frac{D\mathbf{u}_{J,C}(t)}{Dt} \end{array} \right.$$

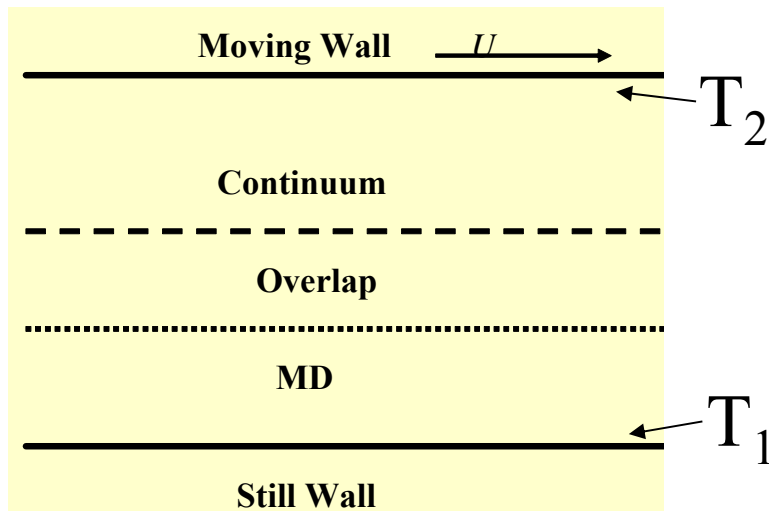
→ 
$$\mathbf{v}_i - \mathbf{u}_{J,MD} = \sqrt{\frac{T_{J,C}}{T_{J,MD}}} \times (\mathbf{v}_i - \mathbf{u}_{J,MD})$$

J. Liu, S. Chen, X. Nie, and M. O. Robbins, J Comp. Phys. (2007)

Mass flux across the interface :

$$n' = -A\rho u_y \Delta t_{FD} / m$$

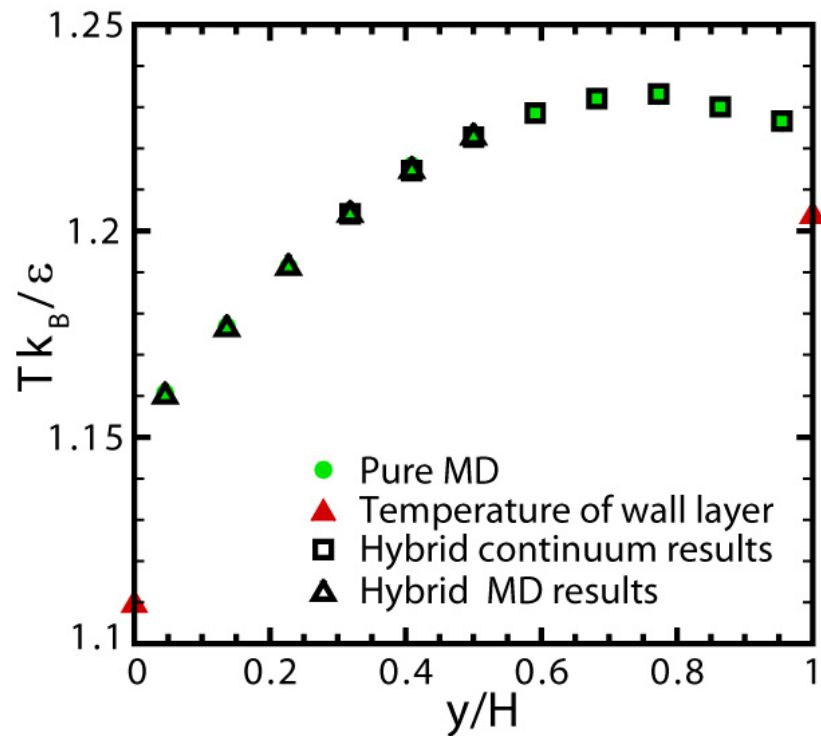
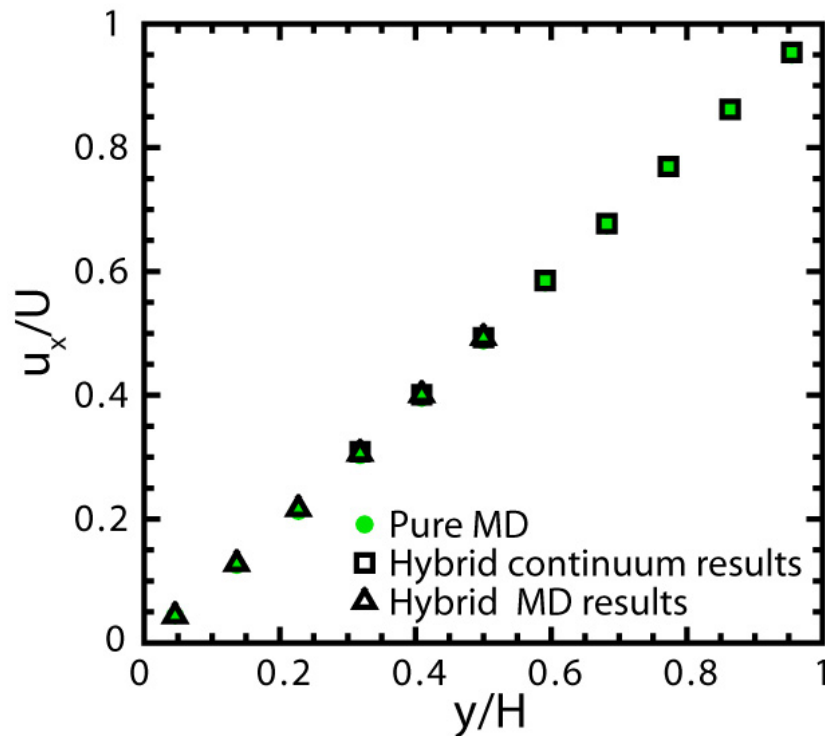
# Temperature in Steady State Couette Flow



At boundaries of overlap region:  
rms MD veloc.  $\leftrightarrow$  continuum T

Hybrid solution tracks pure MD

Reproduces behavior in fluid and  
Kapitza resistance at solid-fluid  
interface



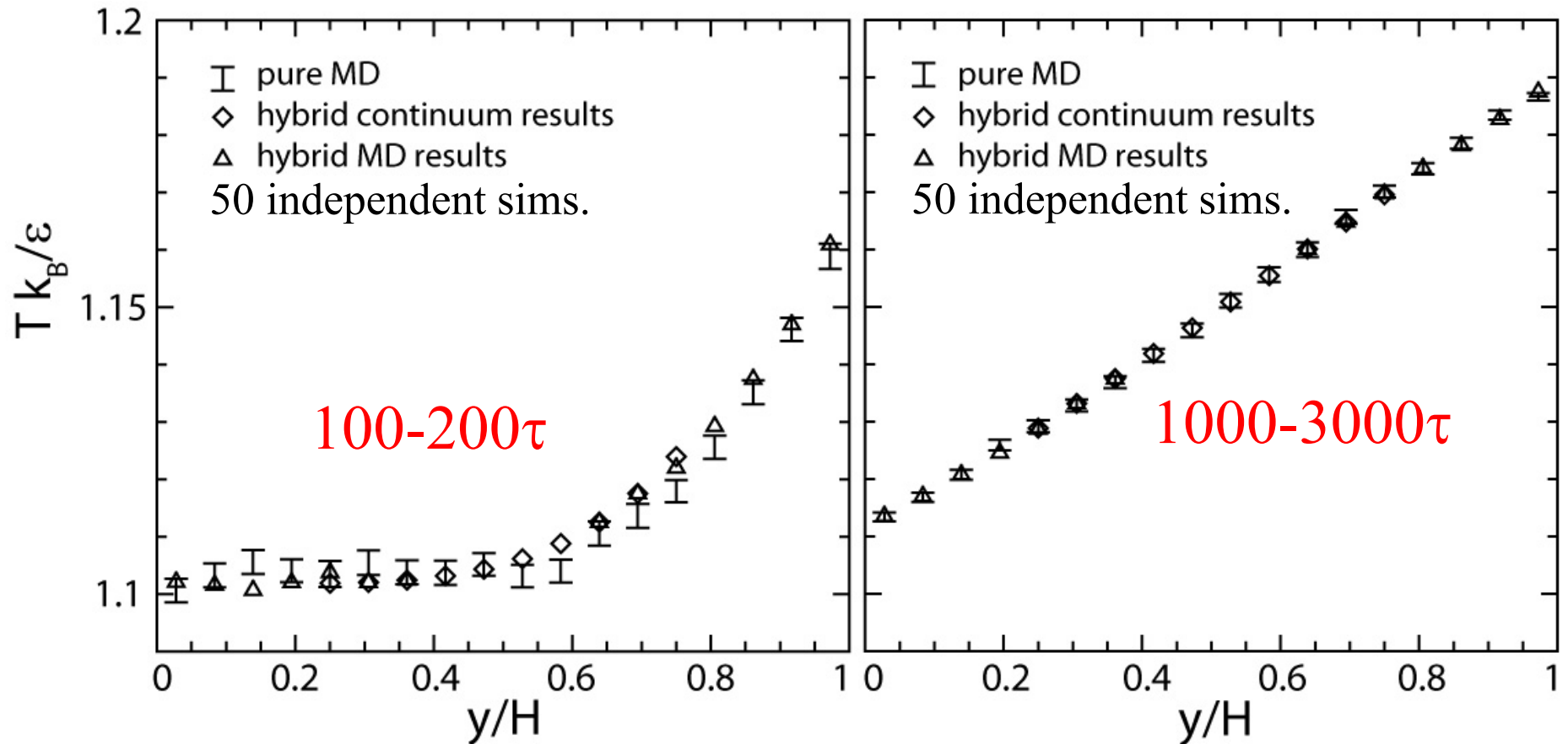


# *Unsteady Temperature Profiles*

Increase  $T$  of top wall to 1.2 at  $t=0$  follow evolution of  $T$

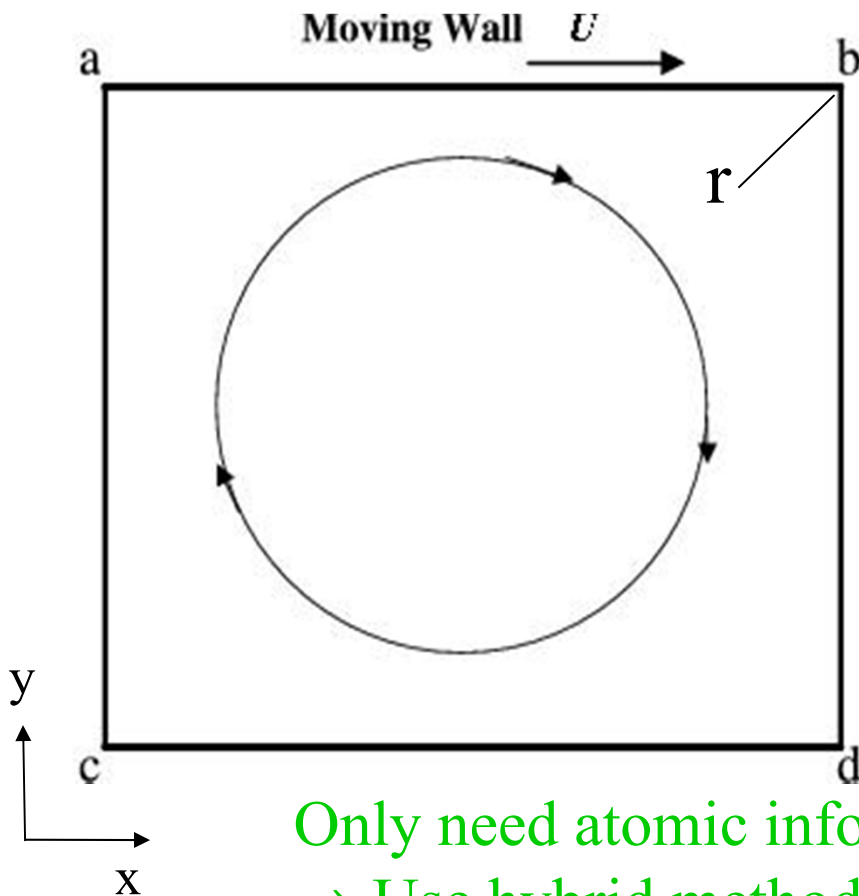
Hybrid agrees with pure MD

Hybrid has smaller statistical fluctuations since thermal noise only in MD region. Ave. before coupling to cont.



# *Singular Cavity Flow*

Continuum approach: Navier-Stokes + no-slip boundary condition (bc)  
Usually phenomenological no-slip bc has little effect at large scales



Corner flow  $\Rightarrow$  Molecular scale influences macroscopic forces

No-slip boundary condition is discontinuous at corners a, b  
 $\Rightarrow$  Stress diverges as  $1/r$   
 $\Rightarrow$  Log divergence in total force on wall

Only need atomic information near corners  
 $\Rightarrow$  Use hybrid method that treats bulk with continuum Navier-Stokes equations, corners with MD

# Coupling in Overlap Region

**MD  $\Rightarrow$  Navier Stokes**

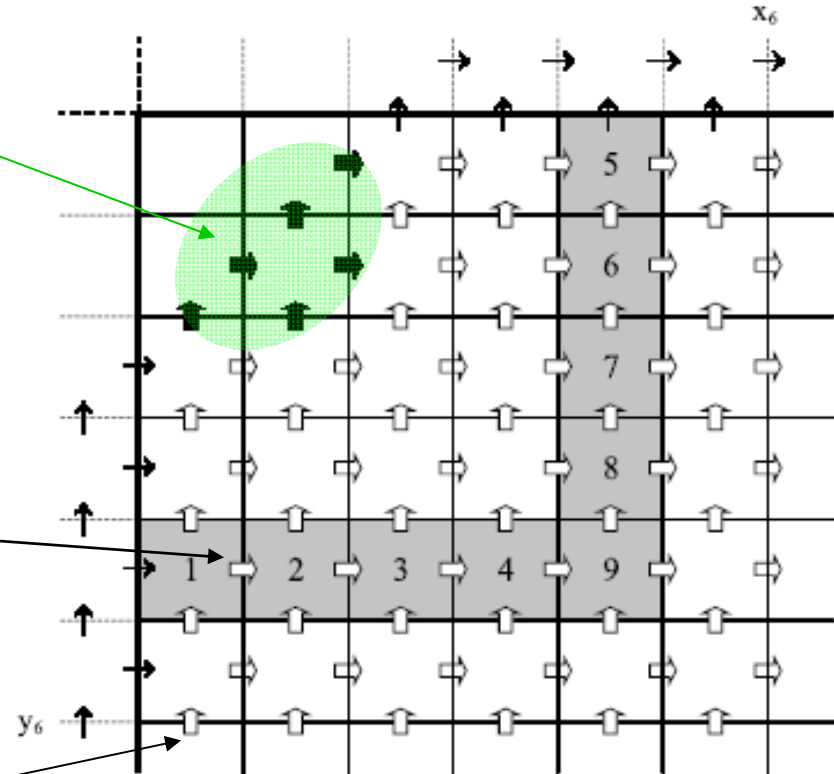
Mean atomic velocity gives  
boundary condition to NS eqs.

**Continuum  $\Rightarrow$  MD**

1) Average tangential MD velocity in  
shadowed bins forced to NS value:

$$\ddot{x}_i = \frac{F_i}{m} - \frac{1}{mN_J} \sum_{j=1}^{N_J} F_j + \frac{Du_J}{Dt}, F_j = -\frac{\partial}{\partial x_k} \sum_k V_{jk}^{LJ}$$

2) Normal MD velocity constrained by  
matching mass flux at boundary



Have tested:

Agrees with pure MD calculations.

Independent of continuum grid 1, 3 and  $6\sigma$  and specific set of  
constrained velocities (within MD noise)

X.B. Nie, S.Y. Chen and M. R. Robbins, Physics of Fluids **16**, 3579 2004.

# *Treating Large Range of Length Scales*

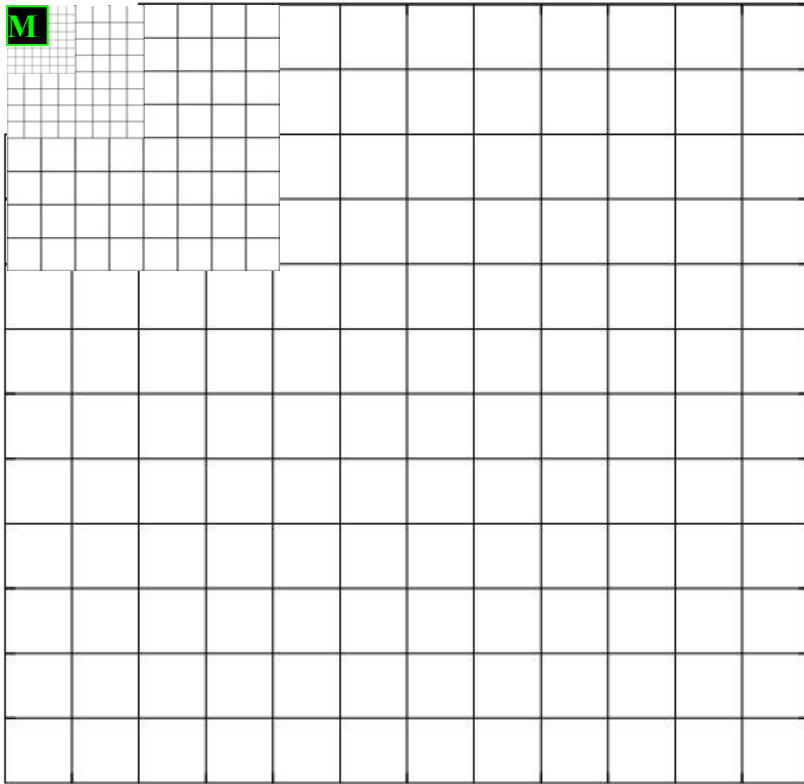
**Problem:** Size of atomistic region independent of system size  $L$   
BUT time to equilibrate NS flow field grows with  $L$ .  
Explicit dynamics approach limited to  $L \sim 0.1 \mu\text{m}$ .

**Solution:** Multigrid and time approach  
Integrate to steady state at each scale with optimum time step.  
Iterate between scales till self-consistent ( $\sim 10$  times).

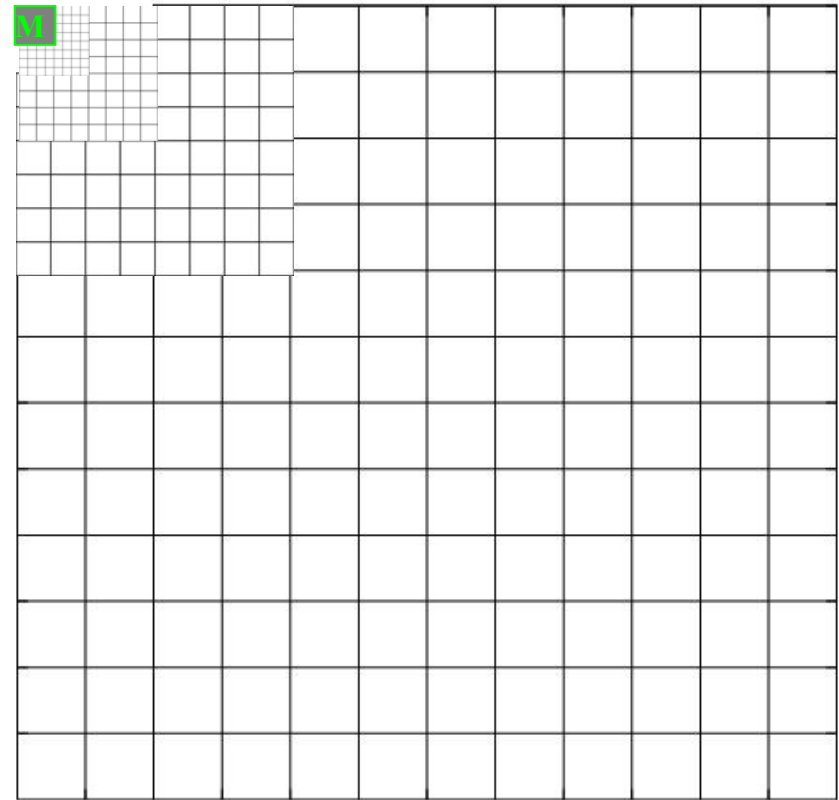
**Result:** Size limited only by onset of non-steady, turbulent flow  
Show results for 0.3mm cavities.  
> 10 orders of magnitude faster than fully atomistic  
 $\sim 20$  minutes per iteration  
Use average over 16 MD representations to accelerate

# *Schematic of Local Refinement*

Coarse -> Fine: Prolongation.

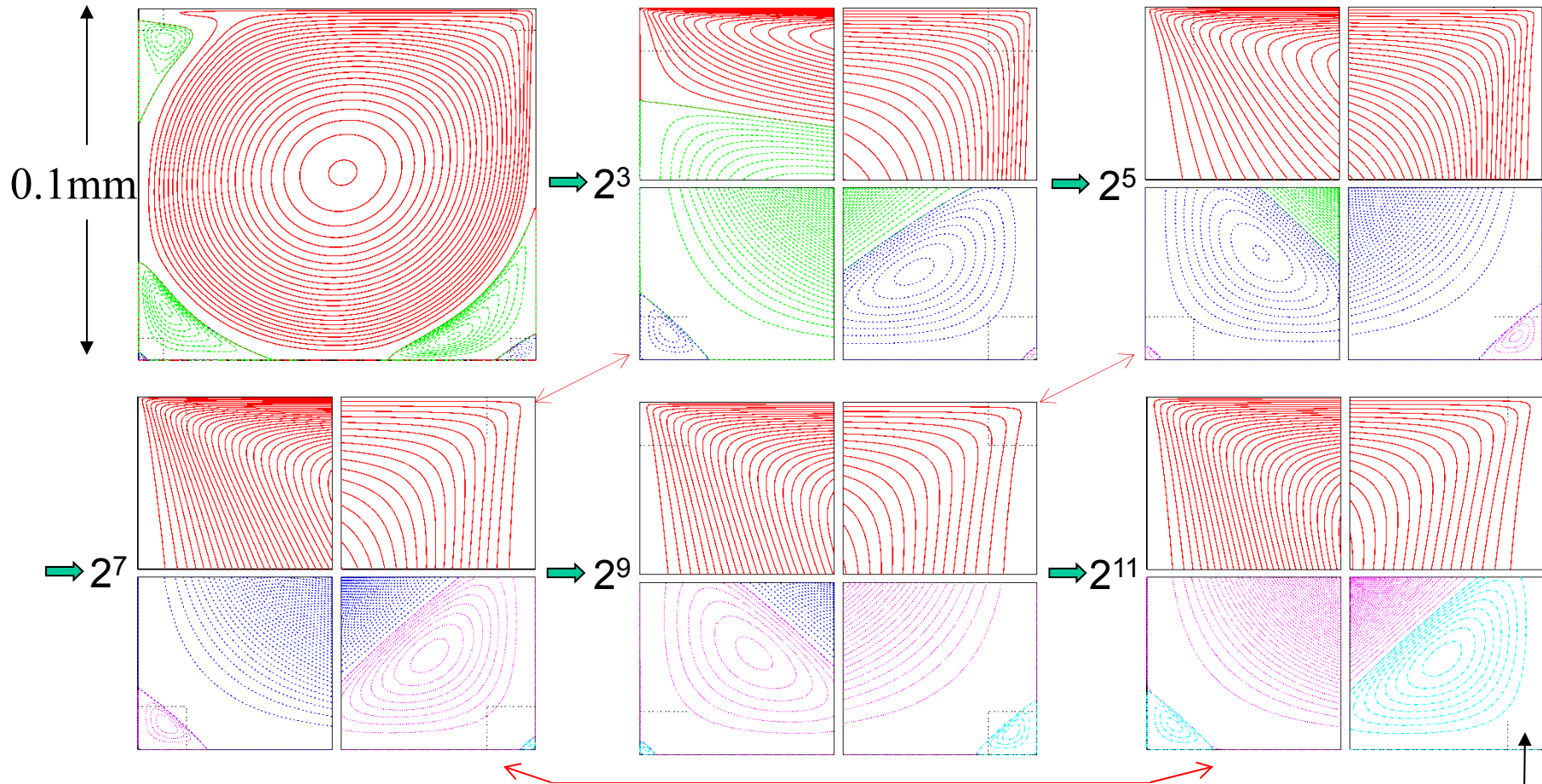


Fine -> Coarse: Restriction.



Flow at each scale reaches steady state at its own characteristic time (Phys. Rev. Lett. **96** 134501 (2006))

# Multiscale Solution for $Re=6400$ ( $U=0.068\sigma/\tau$ )



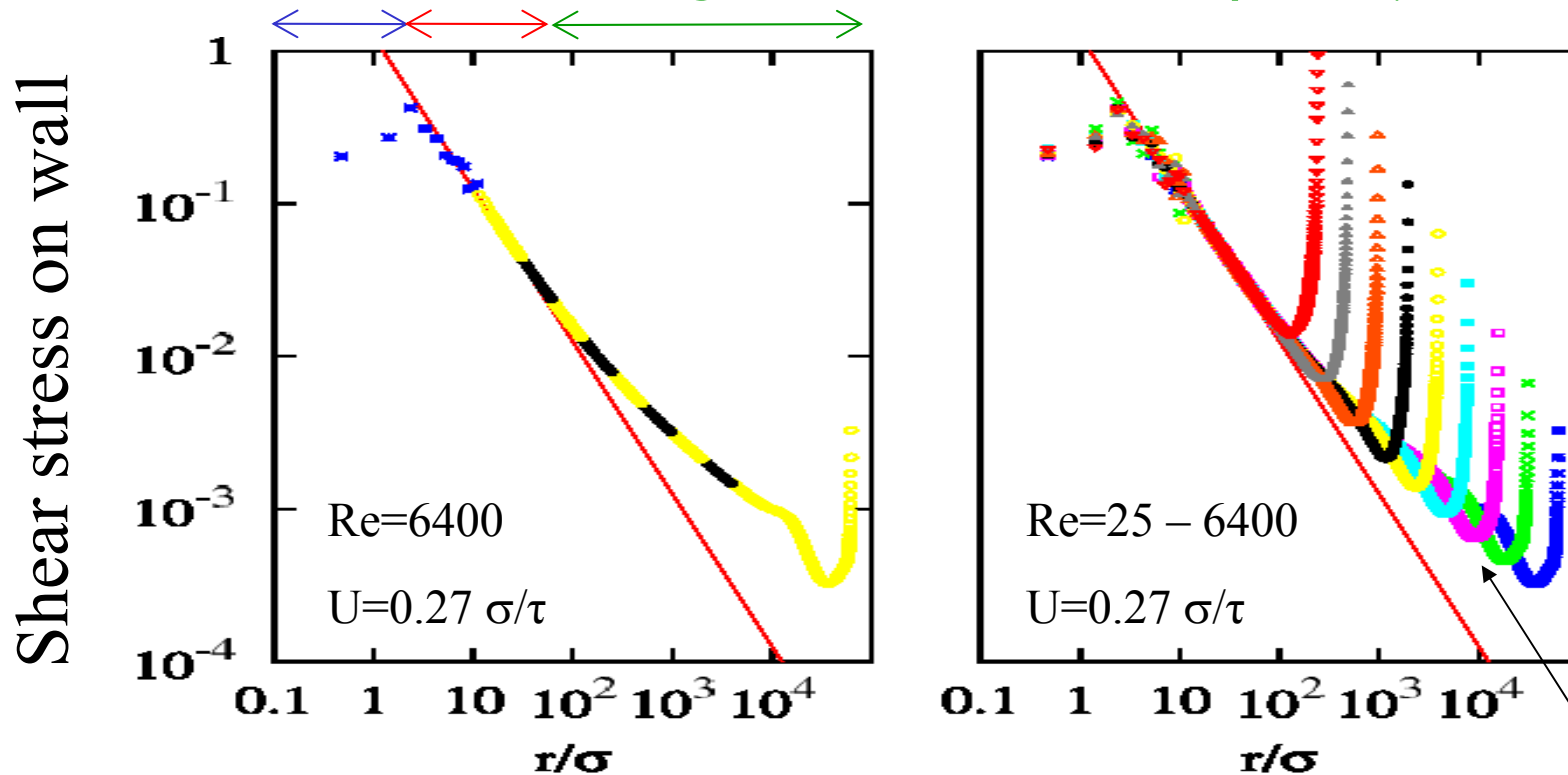
- Ten grid levels, largest  $256 \times 256$ , others  $64 \times 64$ , smallest mesh  $0.95\sigma$
- Dashed lines: the regions expanded in successive plots. Final plot  $\rightarrow$  MD region
- Stokes equations  $\rightarrow$  bottom corners self-similar under mag. by  $\sim 16$  (red arrows)  
This scaling is cut off by atomic structure.
- Computational time saving more than  $10^{10}$  over fully atomistic.

# Stress along the moving wall

Three regions contribute to force F:

Atomistic, Stokes, high Re

$Re = \rho UL / \mu$

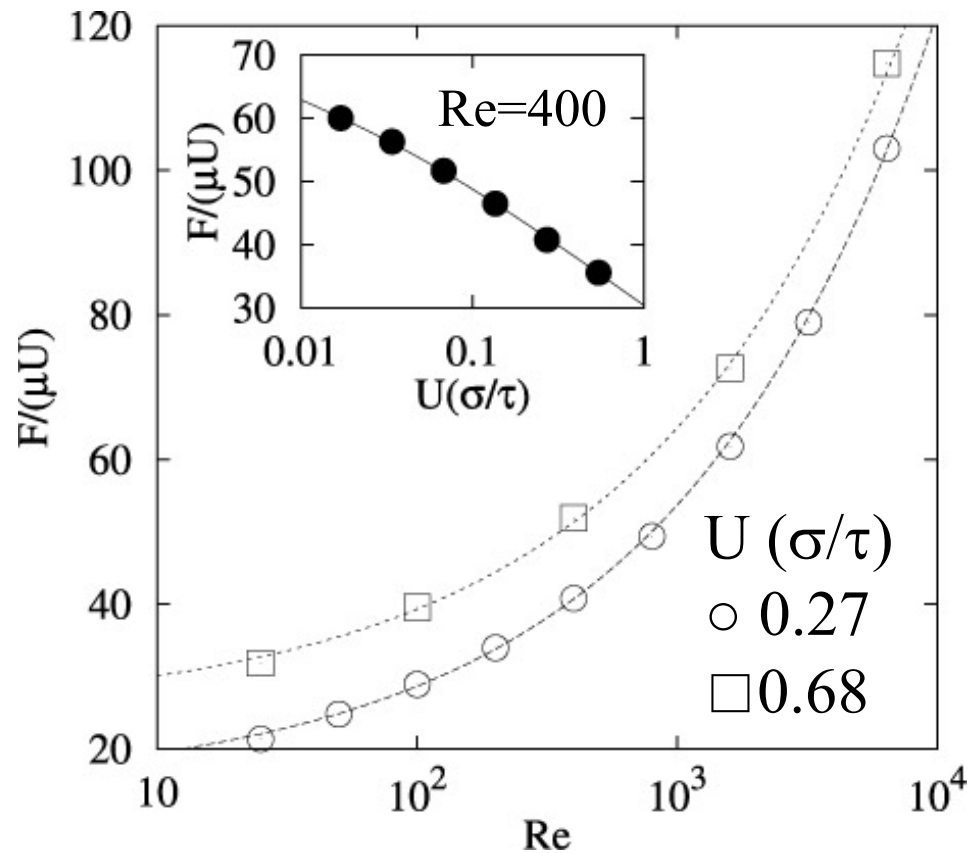


Breakdown of Stokes for  $r < S$  – atomistic or  $r > R_I \equiv \mu/\rho U$  – inertial  
 Little change for  $r < R_I$  as increase  $Re$  by increasing  $L$   
 Large  $r$  contribution gives change in  $F$  for fixed  $U$ , atomic props.

## *Total Force on the Moving Wall*

Re - only parameter in continuum theory

Find strong variation with U at fixed Re, atomic model



$$\frac{F}{\mu U} = \underset{\substack{\uparrow \\ r < S}}{f_S} + \underset{\substack{\uparrow \\ S < r < R_I}}{f_{Stokes}} + \underset{\substack{\uparrow \\ R_I < r}}{f_{Re}}$$

$$f_S = 4.3$$

$$f_{Stokes} = \frac{8\pi}{\pi^2 - 4} \ln(R_I / S)$$

$$f_{Re} = 3.85 + 1.98 Re^{0.434}$$

$f_S$  given by assumption that stress saturates at  $S$

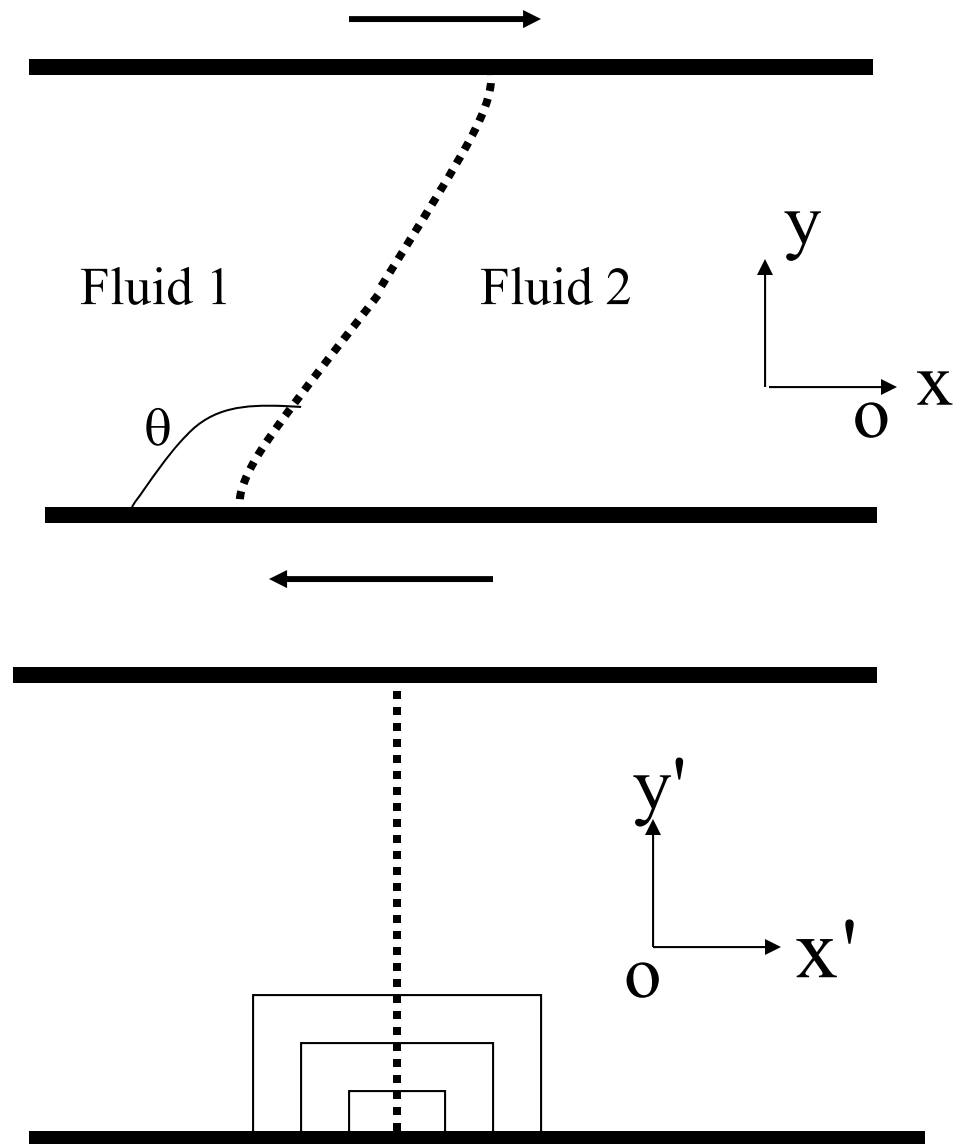
$$S = 0.3 + 7U t_{LJ}$$

$f_{Re}$  is phenomenological fit



# *Similar Singularity at Moving Contact-Line*

AND must solve for interface shape self-consistently



Transformation:

$$\text{Interface: } x_s = f(t, y_s)$$

Transformation :

$$x' = x - f(t, y)$$

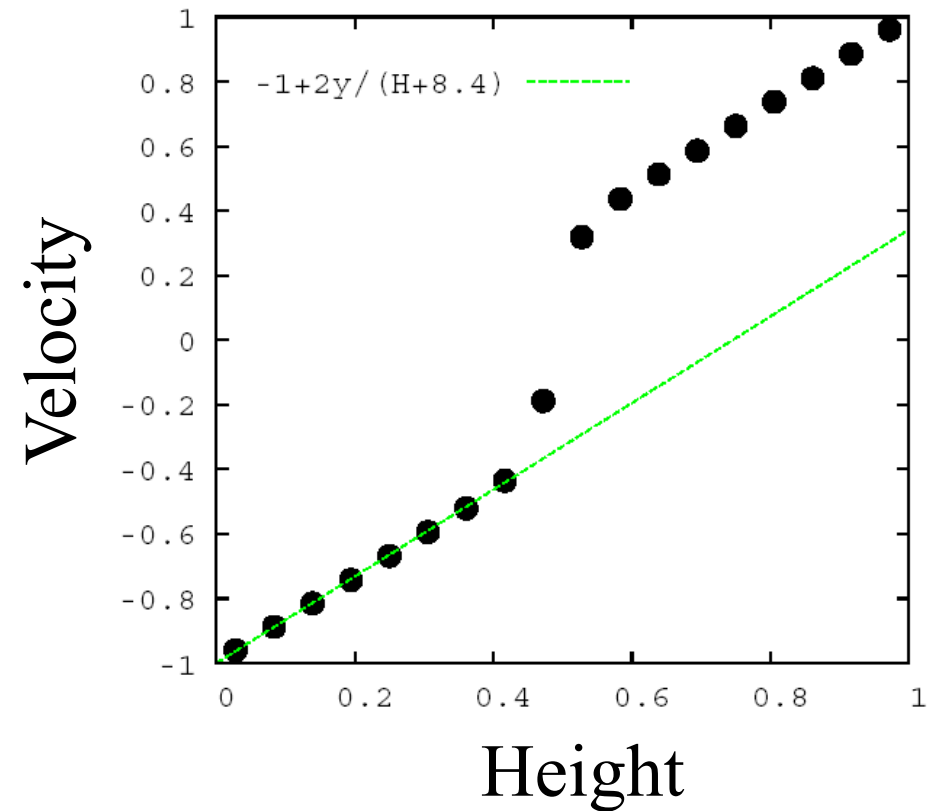
$$y' = y$$

# *Find Slip at Fluid-Fluid Interface*

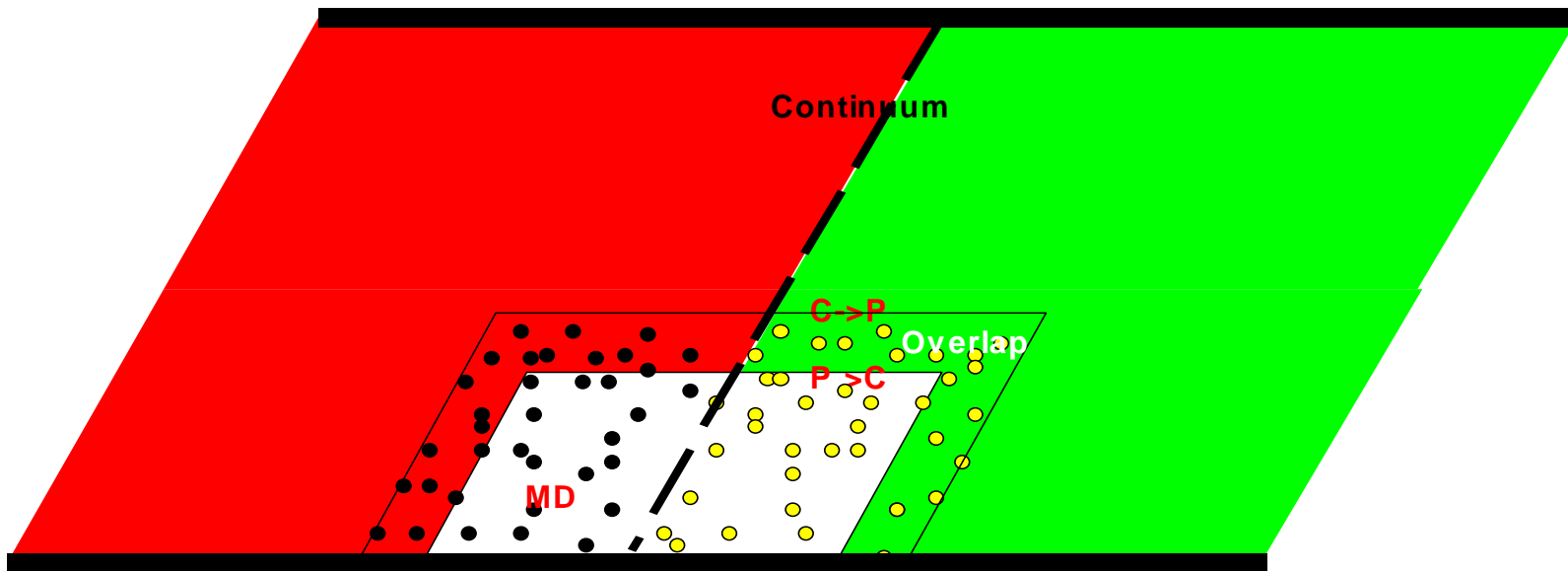
Choose wall-fluid coupling  
so no-slip far from contact  
line

BUT slip at fluid-fluid  
interface

Must build this into  
continuum model



# *Hybrid Scheme for Two Phase Flow: P->C*



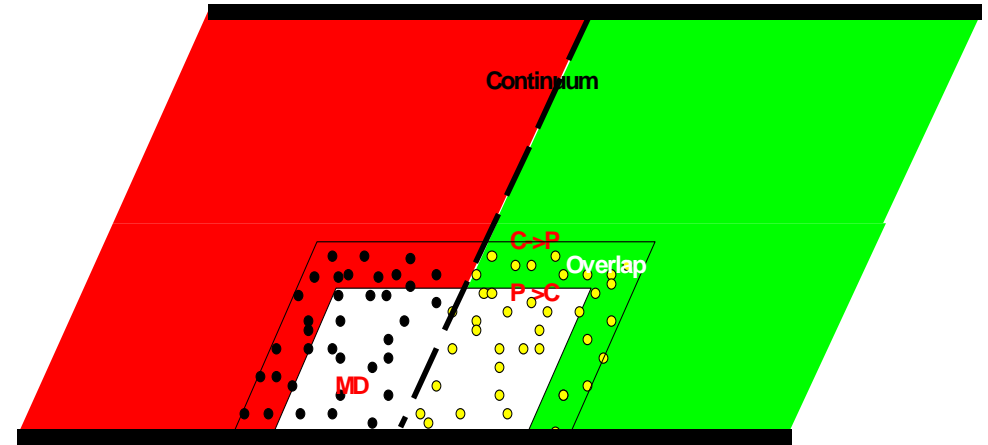
**P->C:**

1. Average particle velocity to give continuum  $u$
2. Determine the interface direction in the overlap from MD and constrain continuum interface

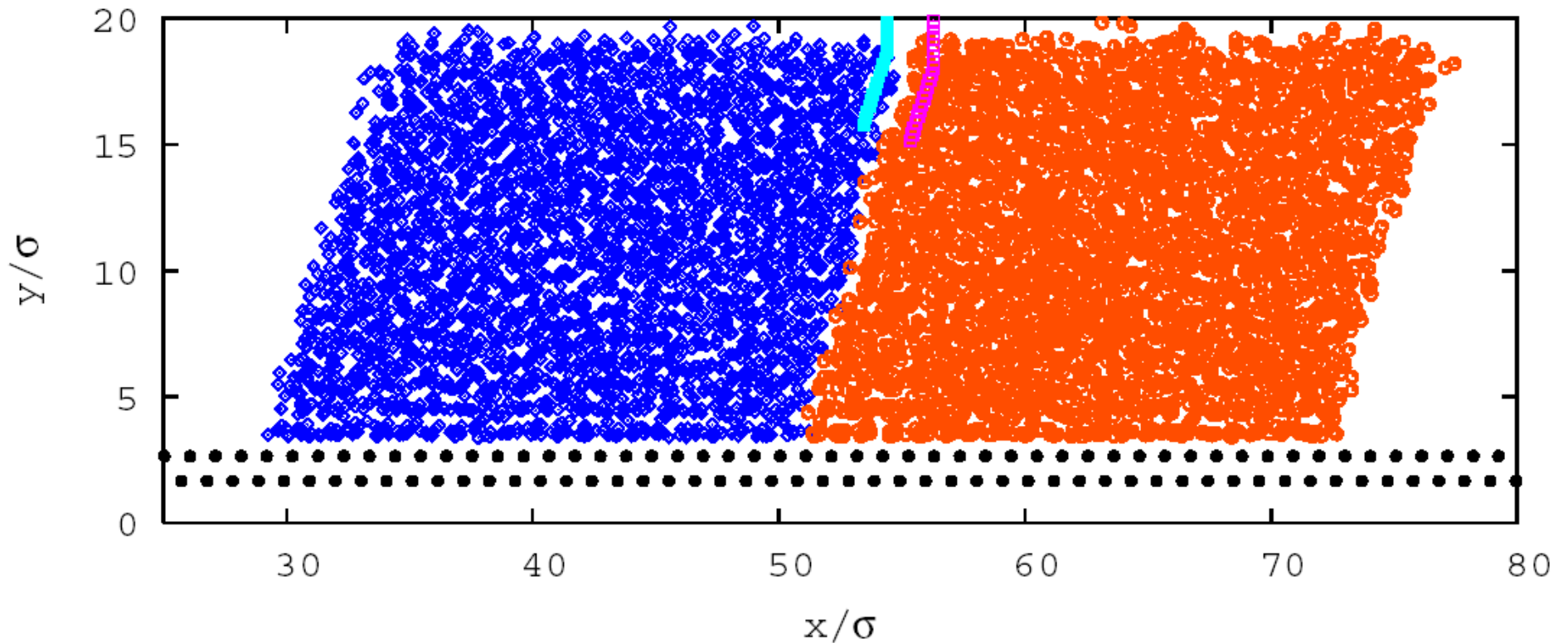
# Hybrid Scheme for Two Phase Flow: C->P

C->P:

- 1) Constrain velocities and mass flux as above
- 2) Force the interface to follow continuum interface equation by putting a membrane in the overlap region.
- 3) Solve flow for given boundary and iterate until self-consistent

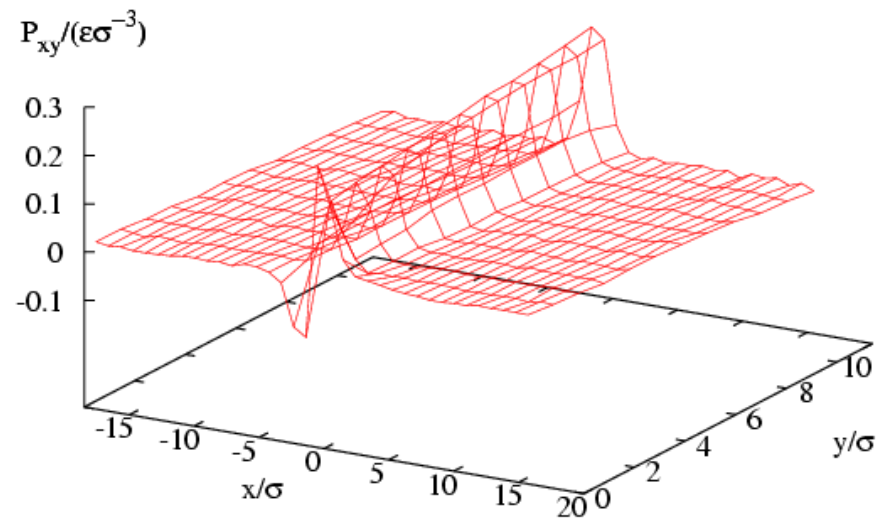
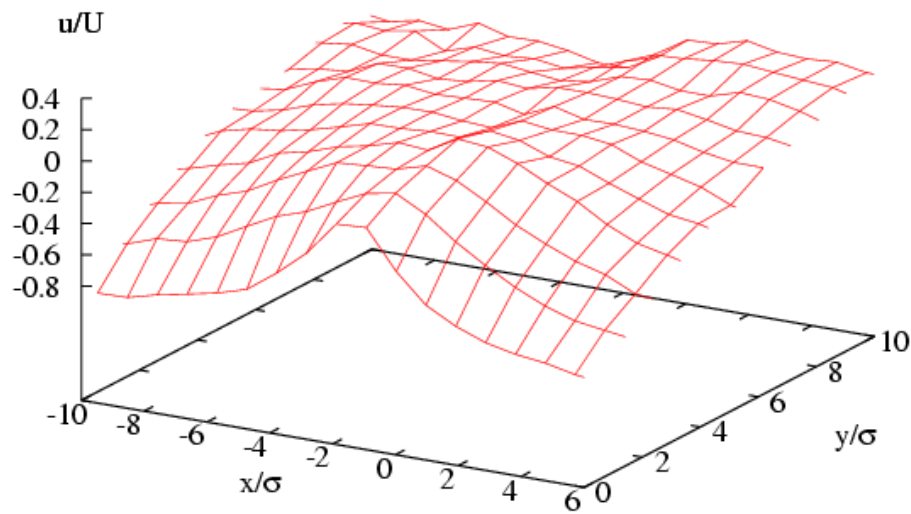
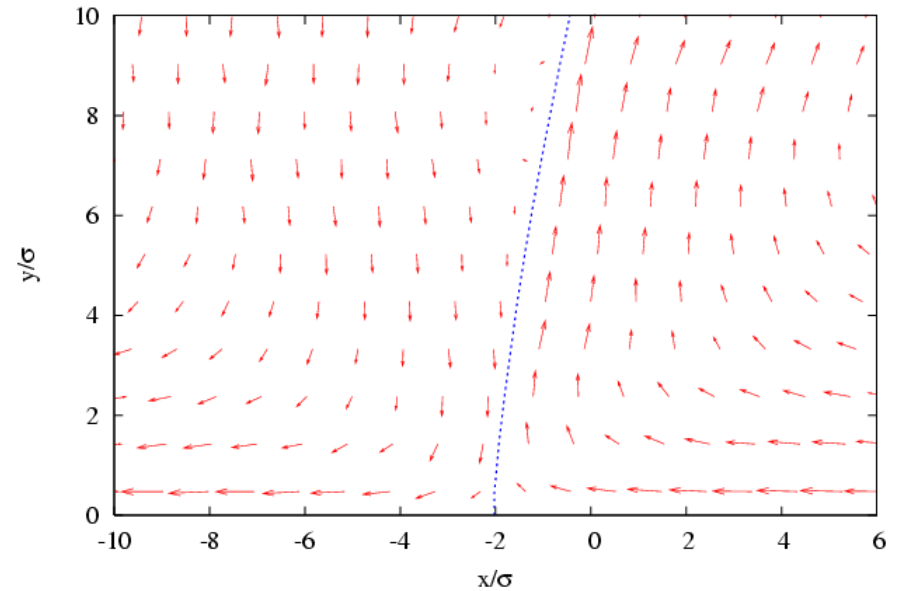
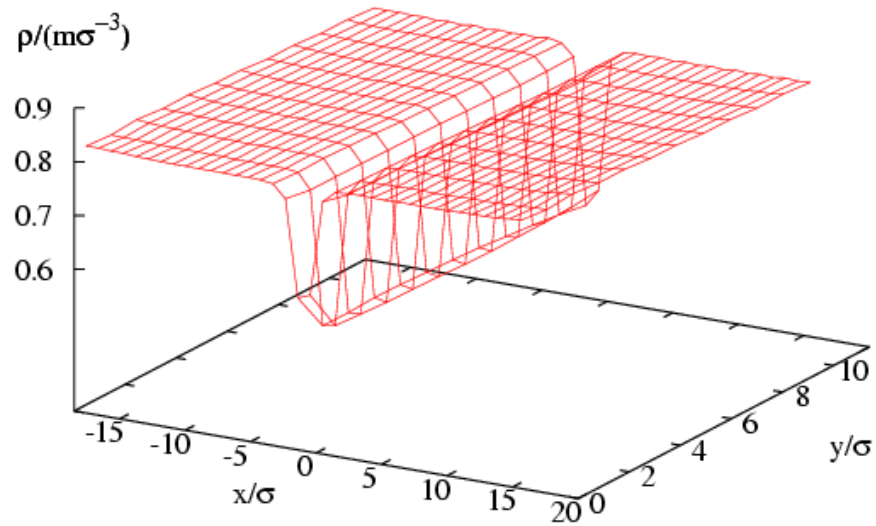


# Procedure to reach steady state in MD

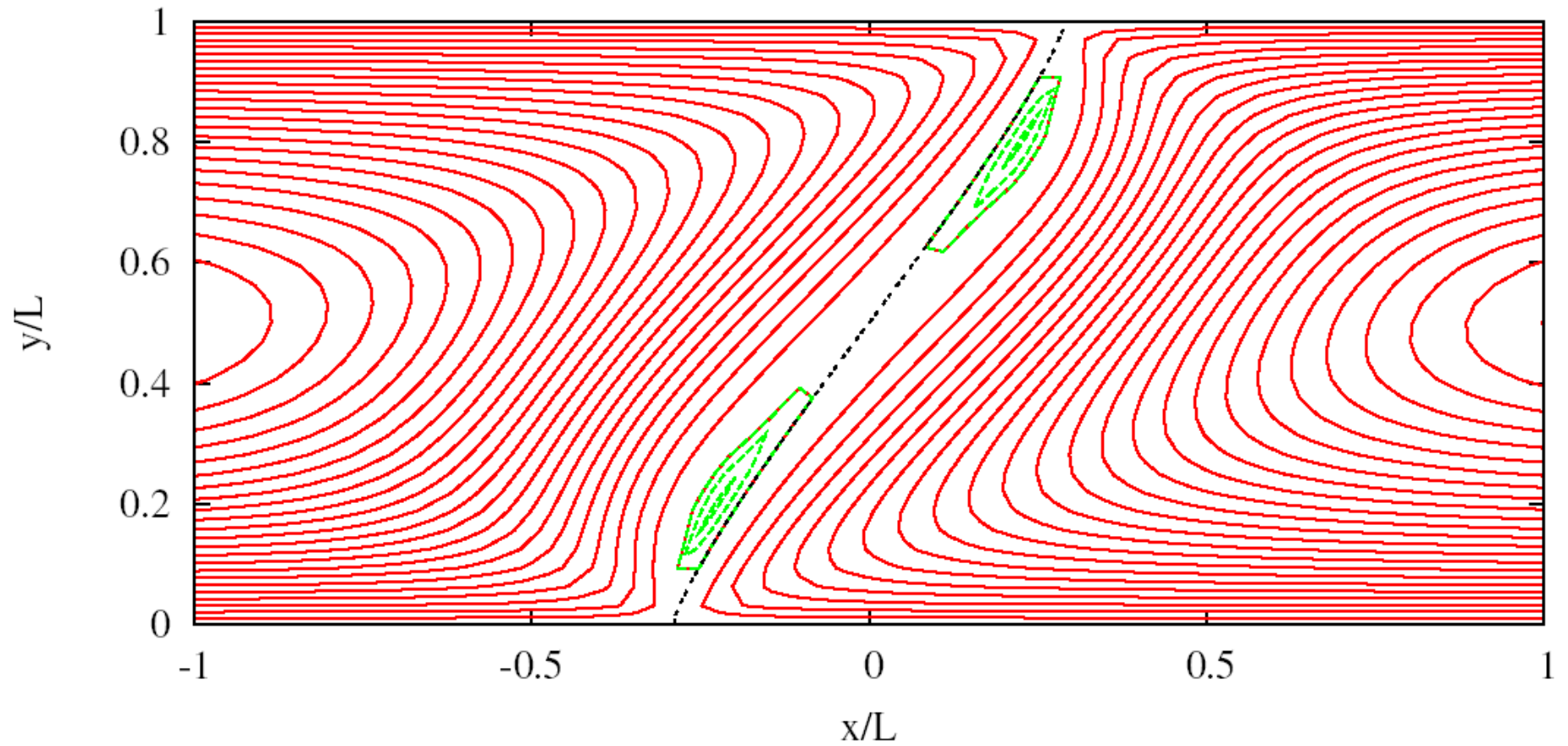


- Fix the boundary shape to let the system reach steady state.
- Correct the boundary shape according to the new interface and then repeat the last step until the boundary and the interface shapes are consistent.

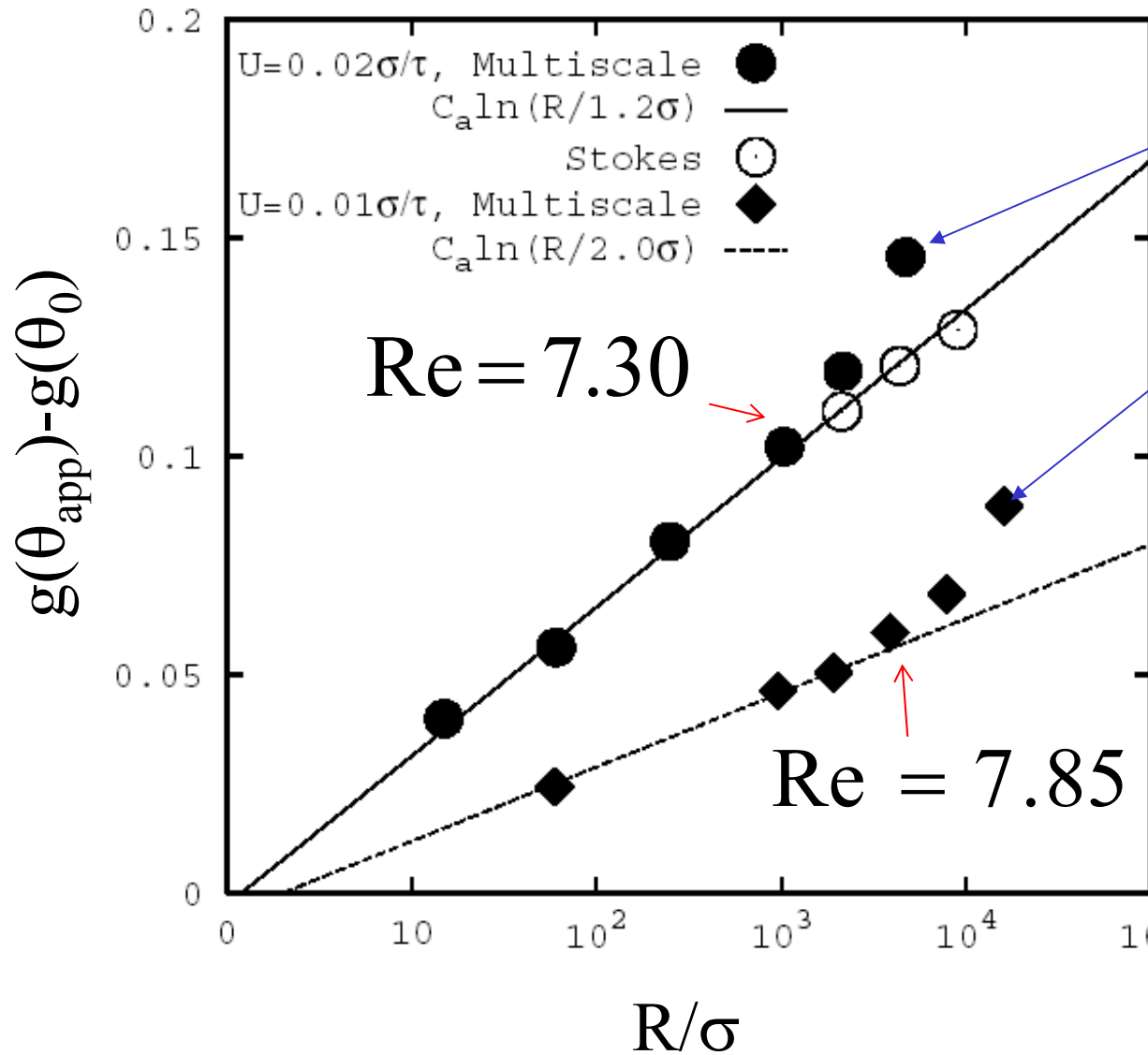
# *Typical Results Near A Contact-line*



# *Typical Results of the Whole Flow Field*



# Deviation from Cox Solution



**We = 0.448**

**We = 0.525**

**Weber #**  $We = \frac{\rho R U^2}{\sigma}$   
**Reynolds #**  $Re = \frac{\rho R U}{\mu}$

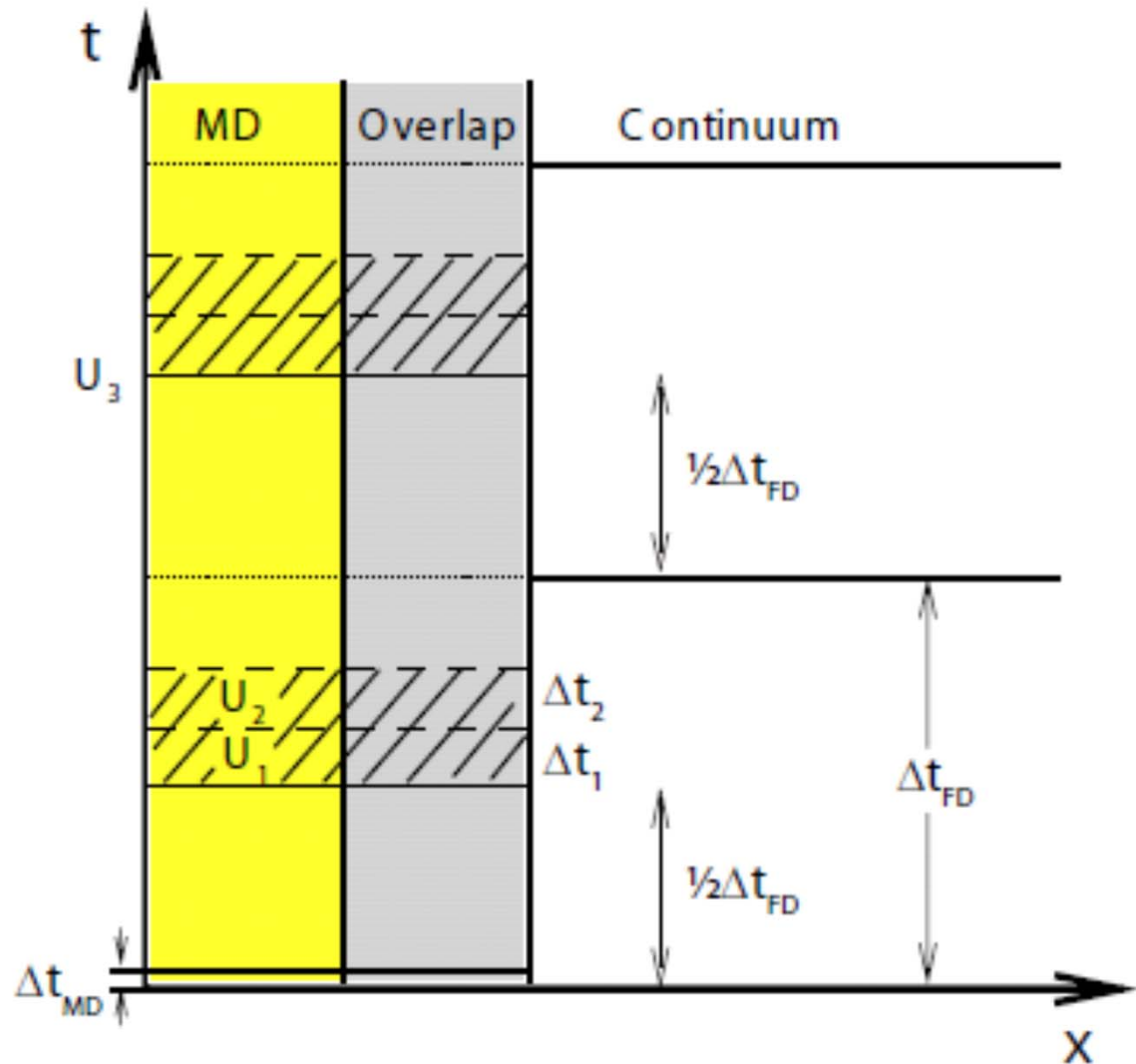


# *Time Extrapolation Scheme*

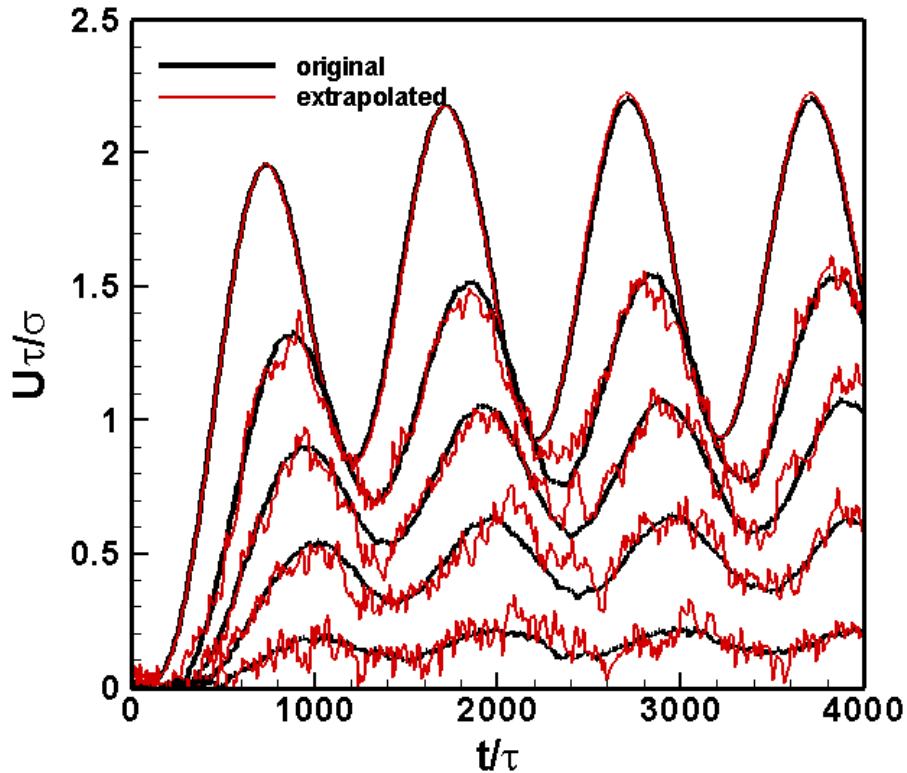
Need different approach for dynamic problems

MD for short  $\Delta t$   
then extrapolate to  
continuum time  
step

Problem:  
Extrapolate  
signal AND noise



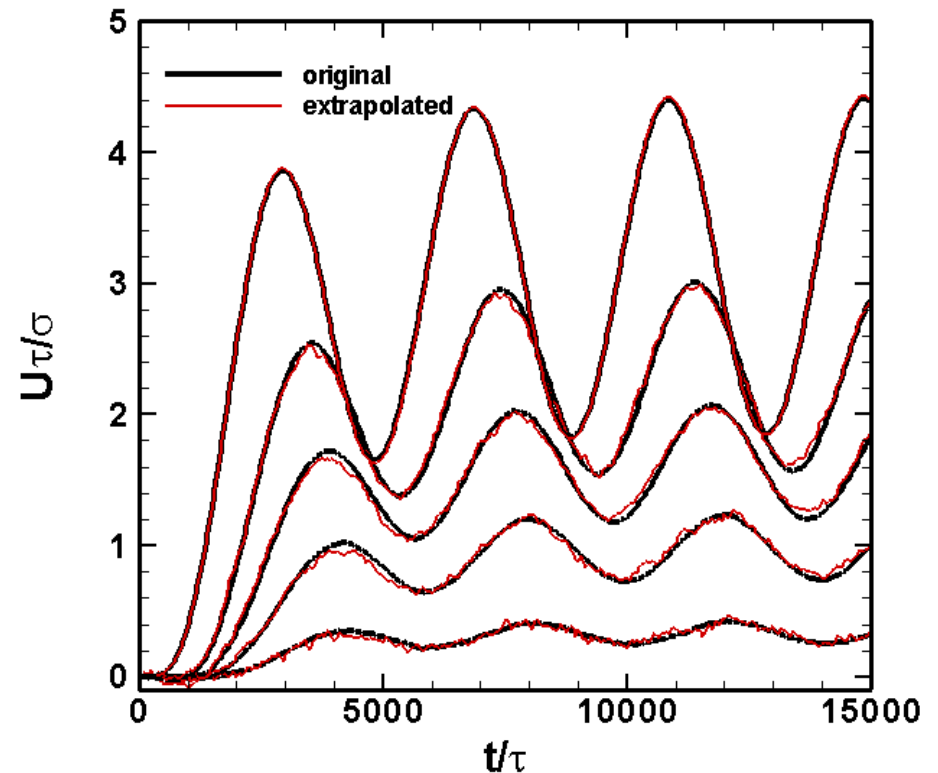
## *Couette flow driven by oscillating wall*



$$\Delta x = \Delta y = 15.6\sigma, \Delta t_{\text{FD}} = 10\tau,$$

$$\Delta t_1 = \Delta t_2 = 0.5\tau$$

Ten-fold extrapolation in time

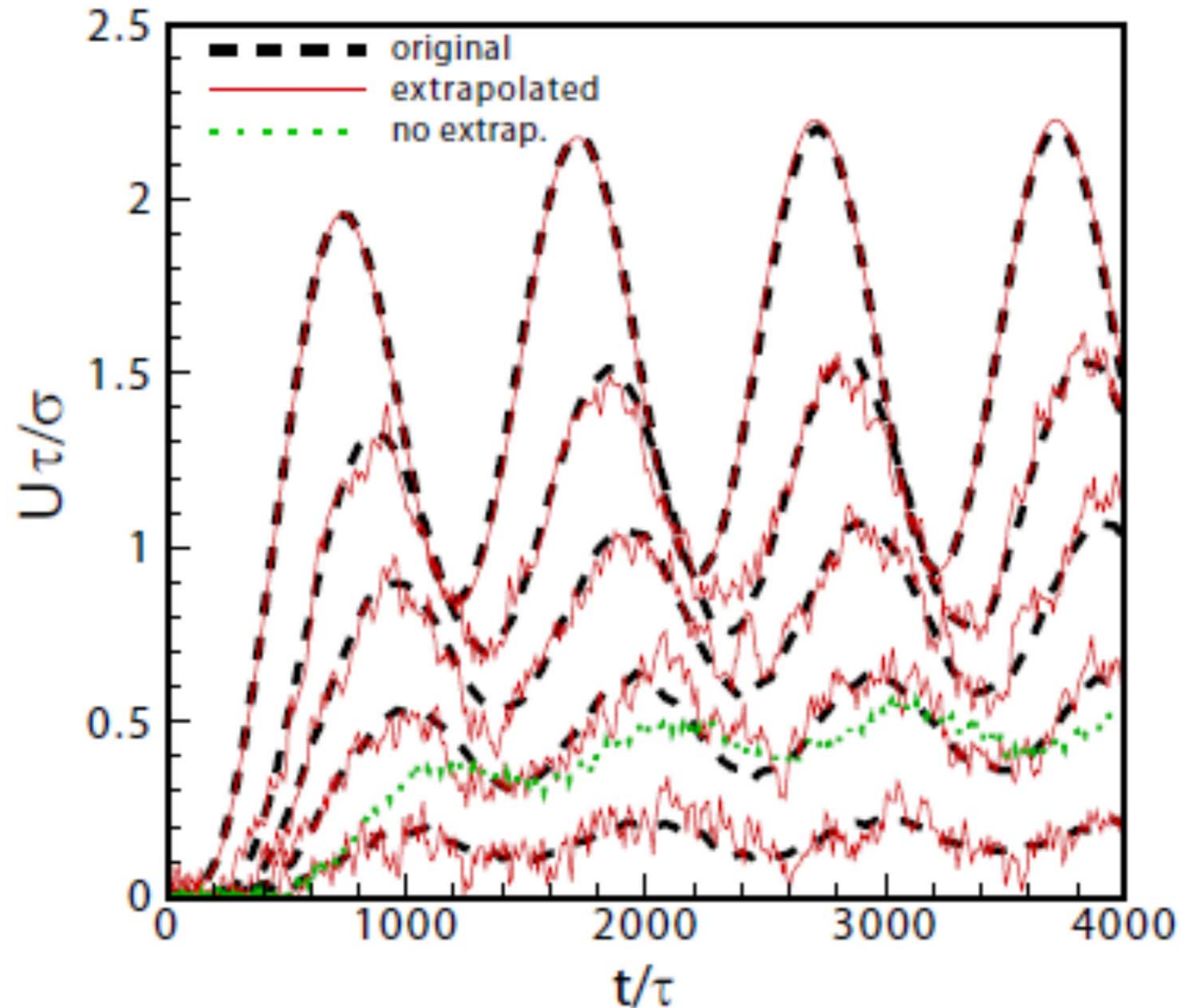


$$\Delta x = \Delta y = 31.3\sigma, \Delta t_{\text{FD}} = 50\tau,$$

$$\Delta t_1 = \Delta t_2 = 2.5\tau$$

Comm. In Comp. Phys. **4**, 1279 (2008)

# *See Delay If No Time Extrapolation*



Weinan E, W. Ren, and E. Vanden-Eijnden, and Yamamoto and collaborators have considered non-extrapolated case.  
OK if large time scale separation

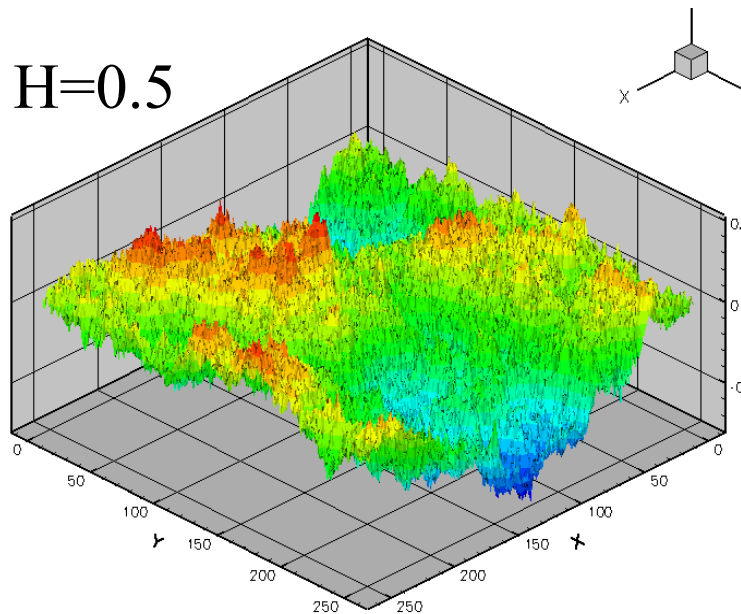
# *Multi-scale modeling of contacts between self-affine surfaces*

Contact geometry and stresses central to friction & adhesion

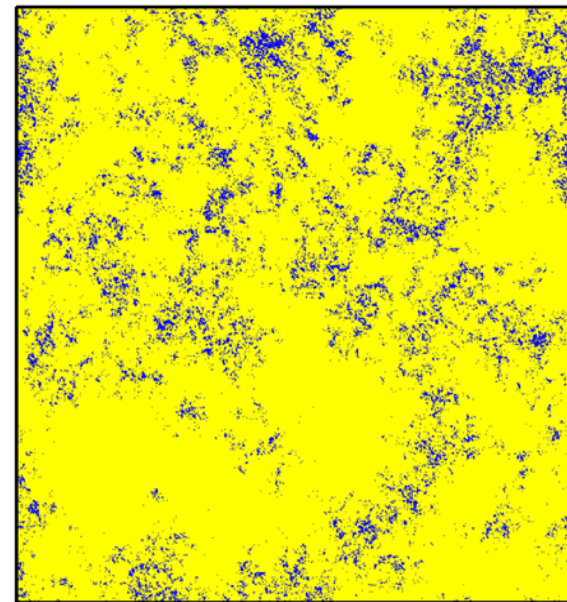
Real surfaces often rough on many scales  $\rightarrow$  self-affine -  $\delta h \sim l^H$

Surfaces steeper at smaller scales, fractal contact regions,  
most connected regions of contact at resolution of calculation

$\Rightarrow$  Not clear continuum mechanics applies



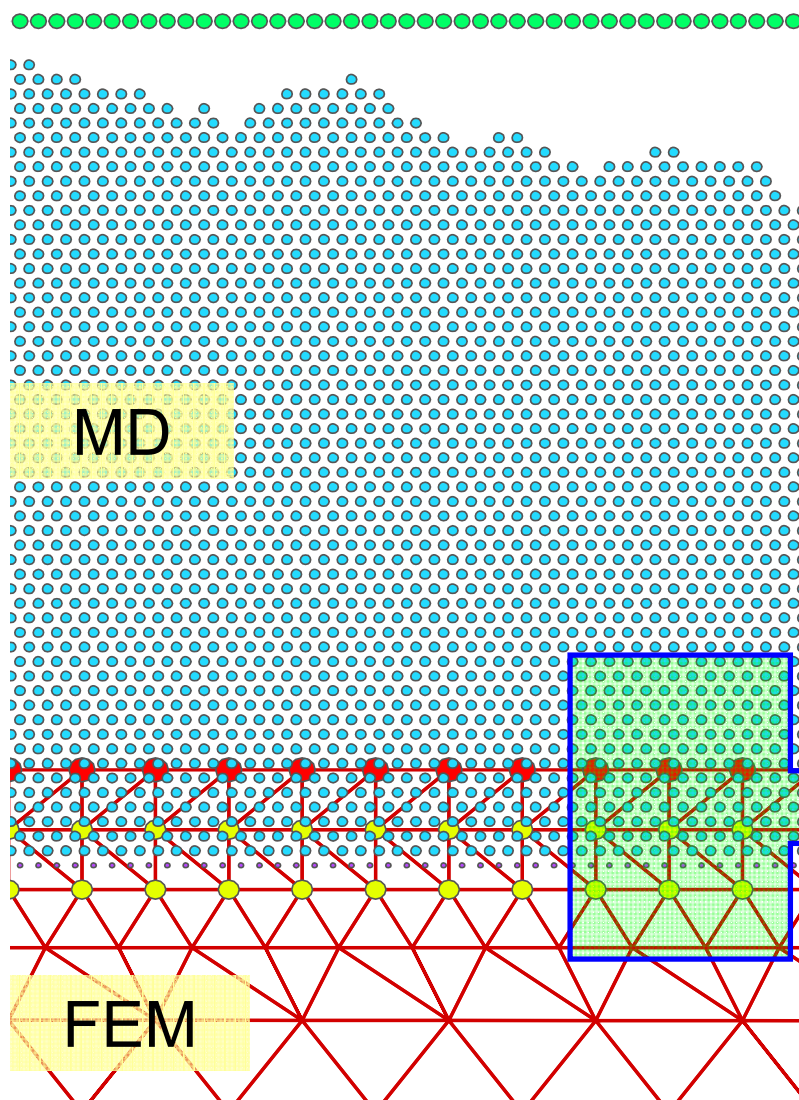
Self-affine surface



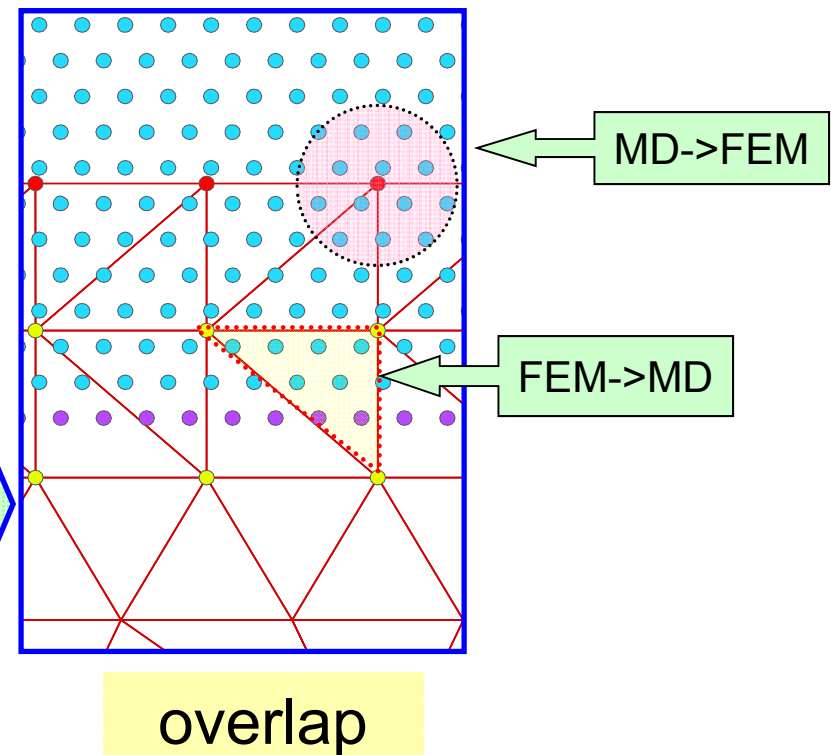
Contact (blue) of self-affine surface

# Hybrid model for 2d self-affine surfaces

Easily treat volumes with  $\sim 10^8$  atoms



At edge of overlap region  
MD and FEM  
displacements provide  
BC's for each other





# Discrete Greens Function Approach

Lennard-Jones (LJ) interactions

Discrete atoms near surface

Green's function for multilayer interactions for substrate

Energy minimization,  $T=0$

Systems up to  $10^{12}$  atoms

Simulate up to  $10^8$  at surface

Simulate bulk: Greens function atoms

