


**PLANAR NEGATIVE
REFRACTIVE INDEX
METAMATERIALS BASED ON
PERIODICALLY L-C LOADED
TRANSMISSION LINES**

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METAMATERIALS

META="BEYOND" IN GREEK
Materials with unusual properties, not encountered in nature

TYPE#1:
ARTIFICIAL DIELECTRICS SYNTHESIZED BY PERIODICALLY
LOADING A HOST TRANSMISSION-LINE MEDIUM WITH R,L,C
ELEMENTS (lumped or distributed):
PERIODICITY $\ll \lambda$

TYPE#2:
DIELECTRIC OR METALLIC PHOTONIC-BANDGAP-MATERIALS
(PBGs) FOR WHICH **PERIODICITY $\sim \lambda$**



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BACKGROUND: $\epsilon < 0$ AND $\mu < 0$ METAMATERIALS

Veselago, 1967

$\epsilon > 0, \mu > 0$

Regular Materials
(right-handed)

$\epsilon < 0, \mu < 0$ Backward Waves

Left-Handed Materials
 $n = -\sqrt{\epsilon\mu}$

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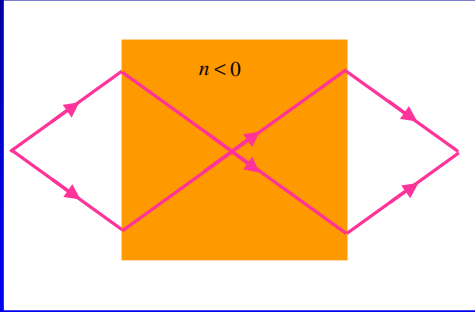
Negative Refraction

$$\frac{\sin \theta_i}{\sin \theta_t} = n$$

Negative Refractive Index Media

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Focusing from Planar $n < 0$ Slabs



- Flat but homogeneous lens
- Point-to-point focusing

• Unlike any other lens it offer sub-wavelength resolution!

Pendry 2000



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HOW CAN ONE MAKE $\epsilon < 0$ AND $\mu < 0$ METAMATERIALS?

3-D Arrangement of Split-Ring Resonators (SRR) and Straight Wires



R. A. Shelby, D.R. Smith, S. Schultz
Science, 2001 Demonstrated Negative Refraction at Microwave Frequencies

- Bulky: 3-D structure**
- Distributed cells: Large for usage at RF frequencies**
- Operates around resonances: Narrowband**
- Unit cells not connected: Difficult System Integration**

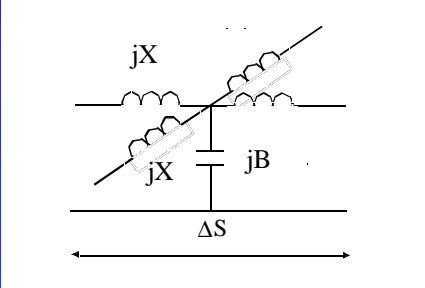


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RECONCEPTUALIZING $\epsilon < 0$ AND $\mu < 0$ METAMATERIALS


Start from the transmission line representation of normal dielectrics:



$$j\omega\mu = \frac{jX}{\Delta S} = \frac{j\omega L}{\Delta S} \Rightarrow \mu = \frac{L}{\Delta S}$$

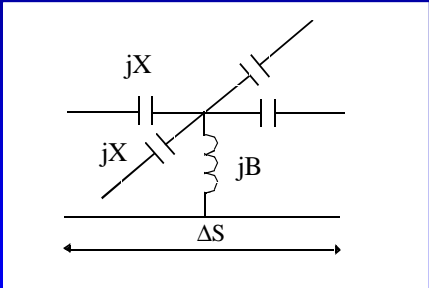
$$j\omega\epsilon = \frac{jB}{\Delta S} = \frac{j\omega C}{\Delta S} \Rightarrow \epsilon = \frac{C}{\Delta S}$$

How to synthesize $\epsilon < 0$, $\mu < 0$?



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Simply: Make the series reactance X and shunt susceptance B both negative!



$$i\omega\epsilon = \frac{jB}{\Delta S} = \frac{j(-1/\omega L)}{\Delta S} \Rightarrow \epsilon = -\frac{1}{\omega^2 L \Delta S}$$

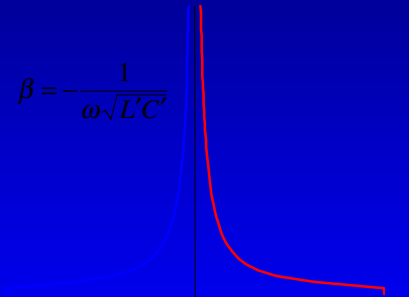
$$i\omega\mu = \frac{jX}{\Delta S} = \frac{j(-1/\omega C)}{\Delta S} \Rightarrow \mu = -\frac{1}{\omega^2 C \Delta S}$$

A.K. Iyer and G.V. Eleftheriades, "Negative Refractive Index Metamaterials Supporting 2-D Waves," IEEE MTT-S Intl. Microwave Symposium Digest, (Seattle, WA), vol. 2, pp. 1067-1070, June 2-7, 2002.



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CONTINUOUS LIMIT


$$\beta = -\frac{1}{\omega\sqrt{LC'}}$$


Backward Waves Supported

$$v_\phi = -\omega^2\sqrt{LC'}$$

$$v_g = \omega^2\sqrt{LC'}$$

This practically yields a very large bandwidth over which $n < 0$



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PERIODICALLY L-C LOADED TRANSMISSION LINES

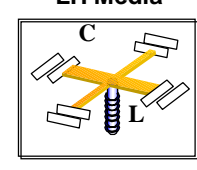
Backward Wave
 $v_p v_g < 0$

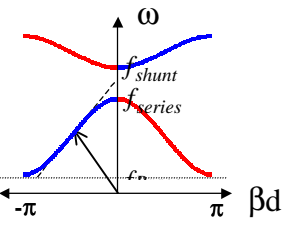
For short interconnecting lines $kd \ll 1$ and small phase-shifts per-unit-cell $\beta d \ll 1$

$$\epsilon_{eff} \cong \epsilon_0 - \frac{1}{\omega^2 LC'}$$

$$\mu_{eff} \cong \mu_0 - \frac{1}{\omega^2 LC'}$$

LH Media






Finite LHM
2-D Unit Cell
Period=d

$$f_{series} = \frac{1}{2\pi\sqrt{LC'}}$$

$$f_{shunt} = \frac{1}{2\pi\sqrt{LC'}}$$

$$f_{Bragg} = \frac{1}{2\pi\sqrt{LC'}}$$




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Negative Refraction

Such “Dual” L-C Networks Support Backward Waves
Explaining Negative Refraction (Key is phase matching)



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2-D Microstrip Implementation of $\epsilon < 0$ AND $\mu < 0$ Metamaterials

The blue wires represent inductors, and the gaps capacitors

2-D (coplanar) propagation

The gaps can be loaded with chip capacitors and the vias with chip inductors to lower the operating frequency



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ADVANTAGES/UNIQUE FEATURES

Low profile 2-D operation

Connected unit cells/Easy system integration

Broadband $n < 0$ bandwidth

By inserting lumped L-C elements, the operating frequency can be lowered for RF applications/Scalability

By using variable L-C elements and/or switches, controllable materials can be synthesized/Tunability



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SIMULATION RESULTS

Negative Refraction

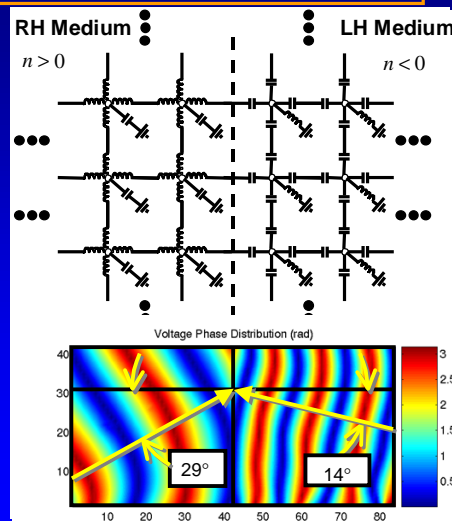
Microwave circuit simulation

Negative refraction observed at interface

Snell's Law verified for

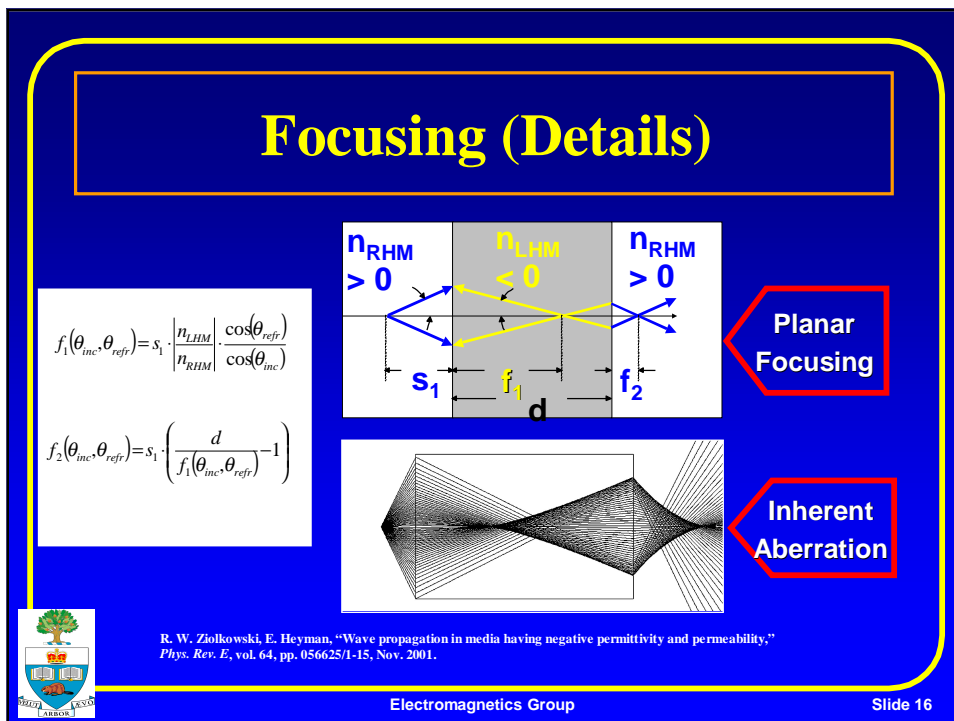
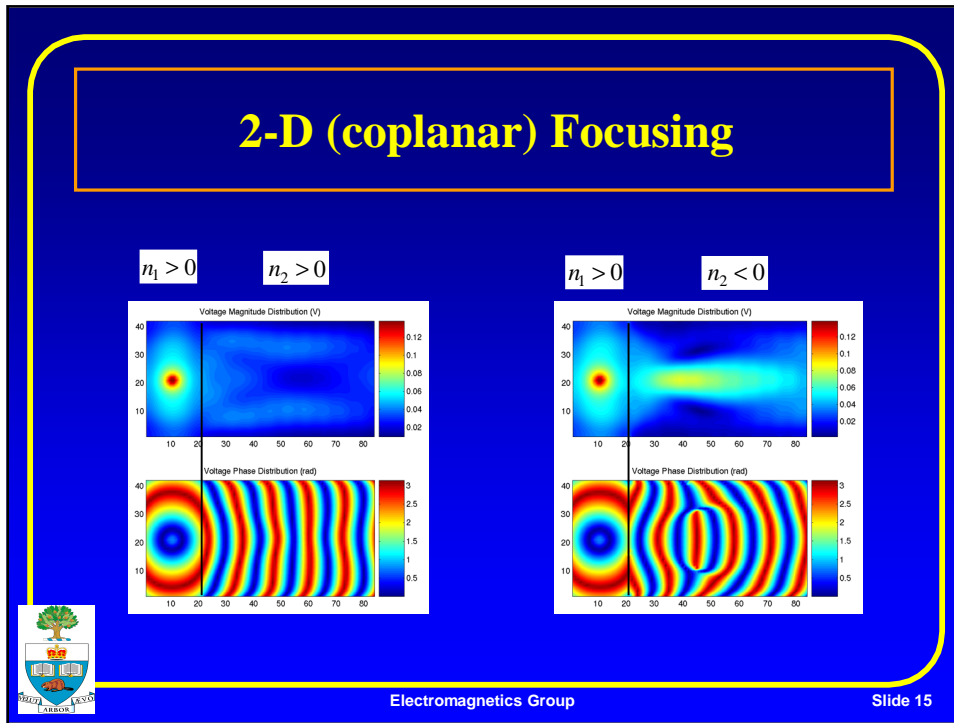
$$n < 0 \sin \theta_{\text{RHM}} / \sin \theta_{\text{LHM}}$$

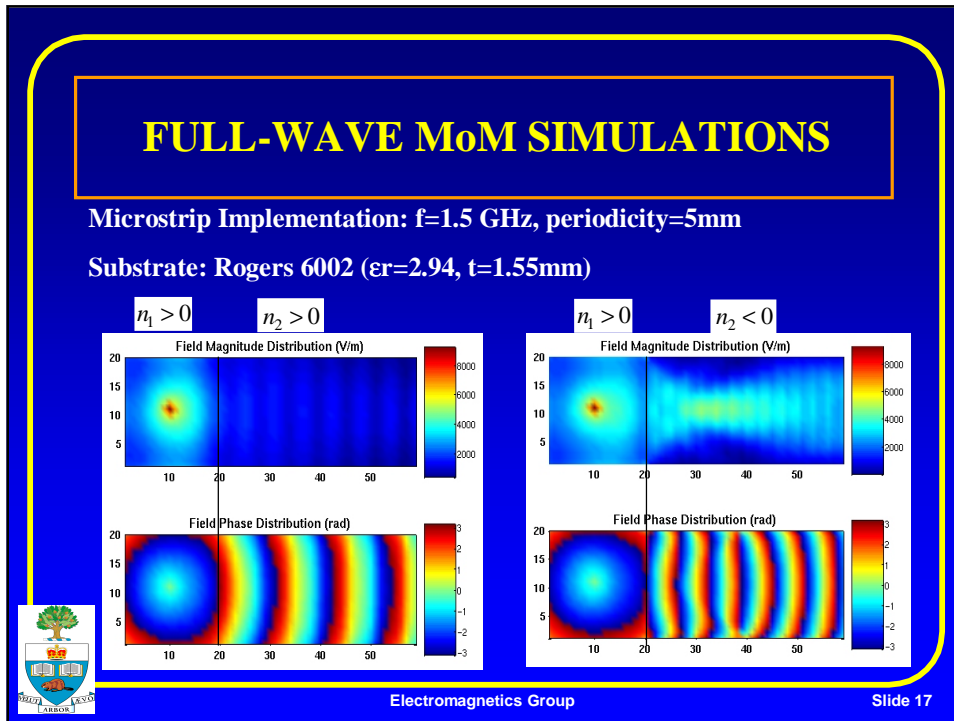
$$= n_{\text{LHM}} / n_{\text{RHM}} < 0$$



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A LEAKY BACKFIRE ANTENNA

source

\vec{S}

\vec{k}

\vec{k}_0

θ

$0 < n < 1$

$\cos(\theta) = \frac{c}{v_\phi}$

source

\vec{S}

\vec{k}

\vec{k}_0

θ

$-1 < n < 0$

Analogous to Reversed Cherenkov Radiation

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Implementation

F=15GHz

150 μm

100 μm

300 μm

600 μm

600 μm

1067 μm 2134 μm 1067 μm

$\lambda = 20\text{mm}$

Period $< \lambda/6$

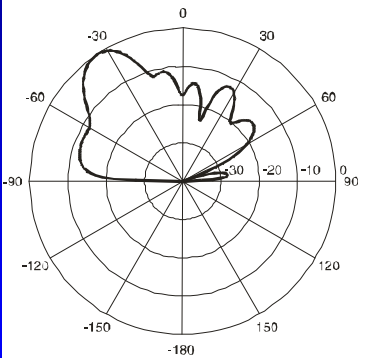
conductor
 slot

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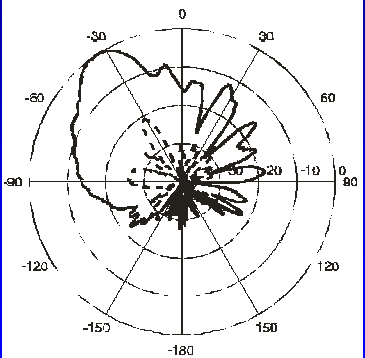
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Patterns

MoM Simulation



F=15GHz Measured



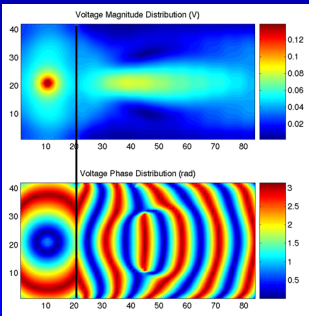
[1.] A. Grbic and G.V. Eleftheriades, "A backward-wave antenna based on negative refractive index L-C networks," Proc. of the *IEEE Intl. Symposium on Antennas and Propagation*, Vol. IV, pp. 340-343, June 16-21, 2002, San Antonio, TX.

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Focusing

$n_1 > 0$

$n_2 < 0$

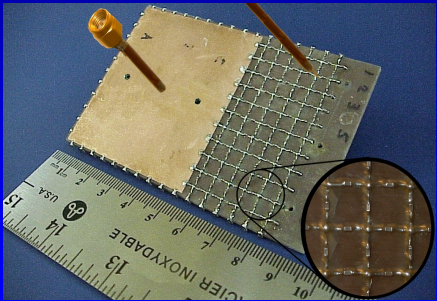


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RF-Lens Device

- NRI metamaterial prototype fabricated/Interfaced with a parallel-plate waveguide
- Vertical E-field probed over metamaterial surface
- Scattering parameter data (transmission) collected from 0-3GHz

11×6-cell NRI metamaterial in microstrip



Measured E-field

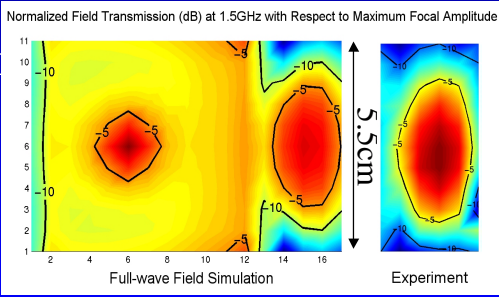



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Full-Wave Simulation/Experiment

- Full-wave (thin-wire MOM) simulation
- Designed for $-2.5 < n_{REL} < -1.5$ @ 1.5 GHz
- Focusing demonstrated
- TM_z mode predominant

MOM Simulation PP Waveguide	LHM	Experiment LHM
<p style="font-size: x-small;">Normalized Field Transmission (dB) at 1.5GHz with Respect to Maximum Focal Amplitude</p>  <p style="font-size: x-small;">Full-wave Field Simulation Experiment</p>		
<p style="font-size: x-small;">5.5cm</p>		<p style="font-size: x-small;">3cm</p>



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FURTHER EXPERIMENTAL RESULTS

Measured Phase

1.55GHz

1.65GHz

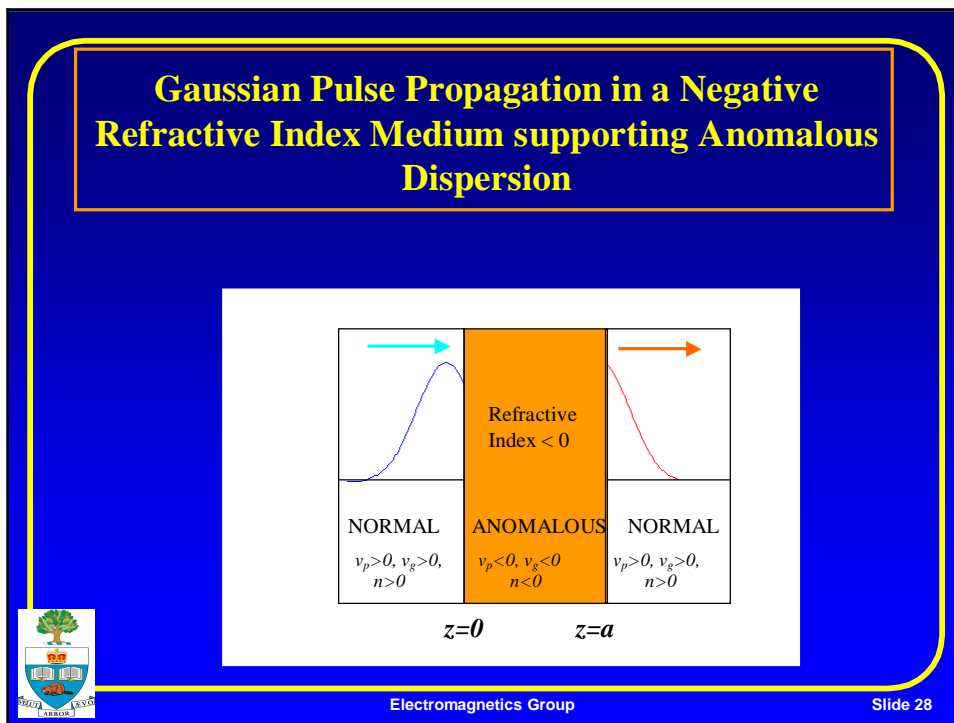
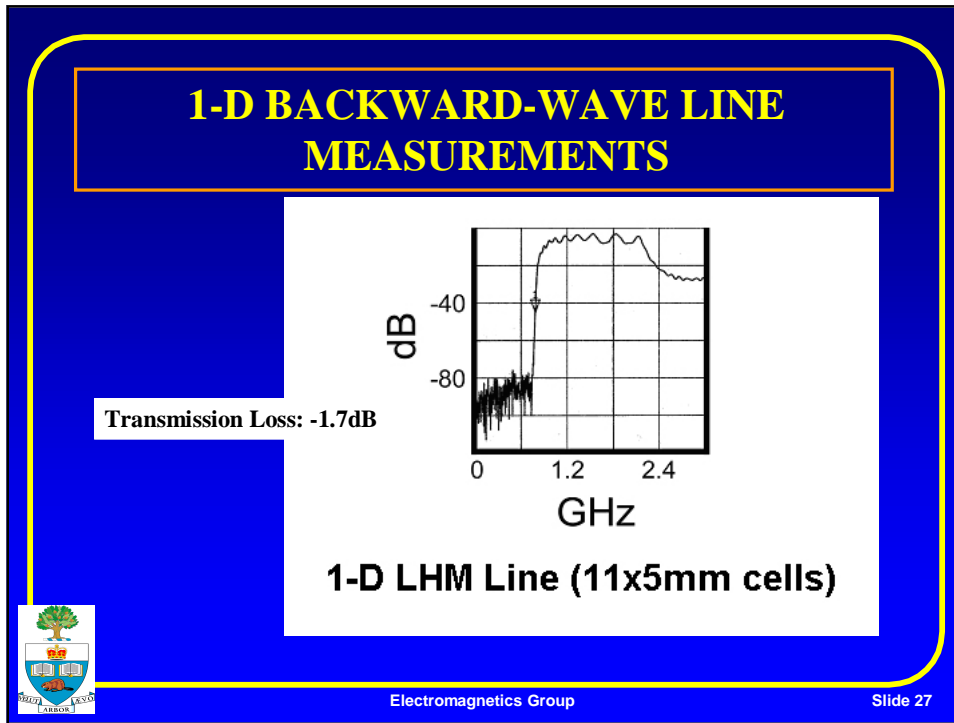
2.55GHz

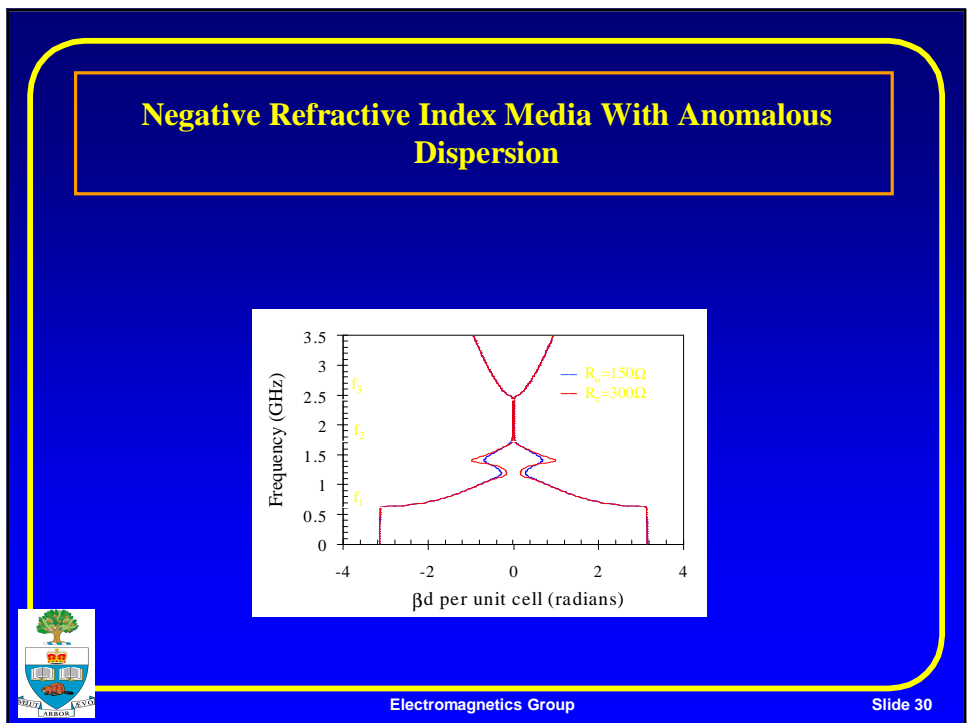
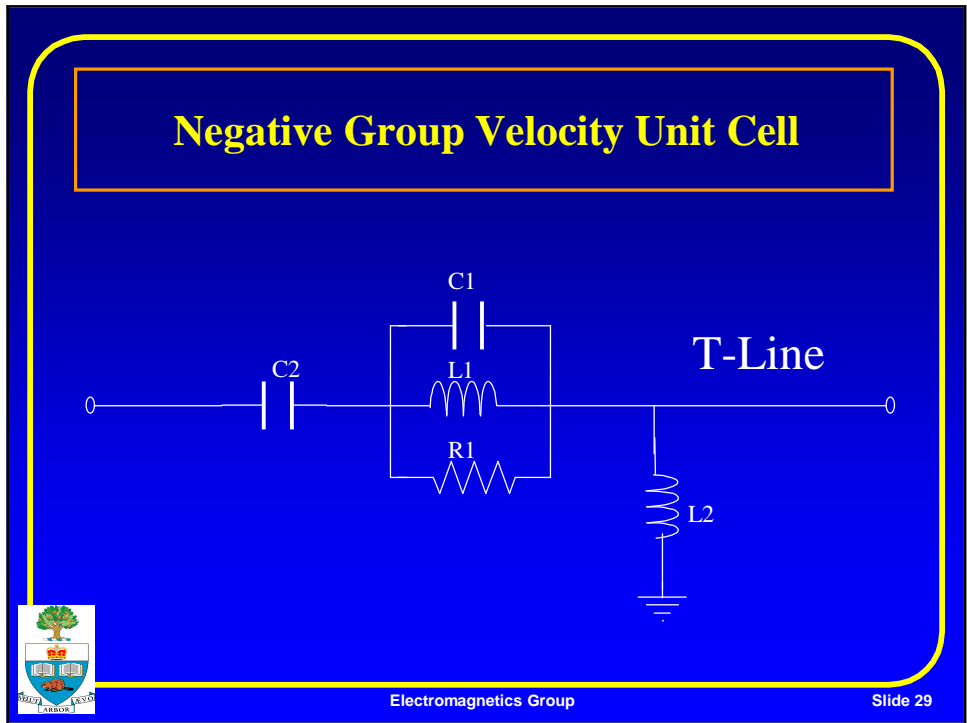
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- **$n < 0$ observed from 1-2 GHz (broadband)**
- **Confined focal region near 1.5 GHz ($-2.5 < n_{rel} < -1.5$)**
- **15dB distinction between peak and edges over an area of 4cmX3cm, $\lambda = 20$ cm**
- **Focal region recedes to interface as frequency increases (n reduces)**

Vertical E-Fields at 11x6-cell NRI metamaterial Surface

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CONCLUSIONS

By loading planar transmission-line networks periodically with L-C elements, a new generation of NRI metamaterials can be implemented

Low profile 2-D operation

No SRR resonators/Broadband $n < 0$ bandwidth

Connected unit cells/Easy system integration

By inserting lumped L-C elements, the operating frequency can be lowered for RF applications/Scalability



Note: Provisional patents filed, May 2002