

SHAKEN AND STIRRED: RANDOM ORGANIZATION, VISCOSITY AND DISSIPATION IN GRANULAR SUSPENSIONS

Romain Mari

Laboratoire Interdisciplinaire de Physique, CNRS-Université Grenoble-Alpes



Chris Ness

Dept. of Chemical Engineering
and Biotechnology, Cambridge



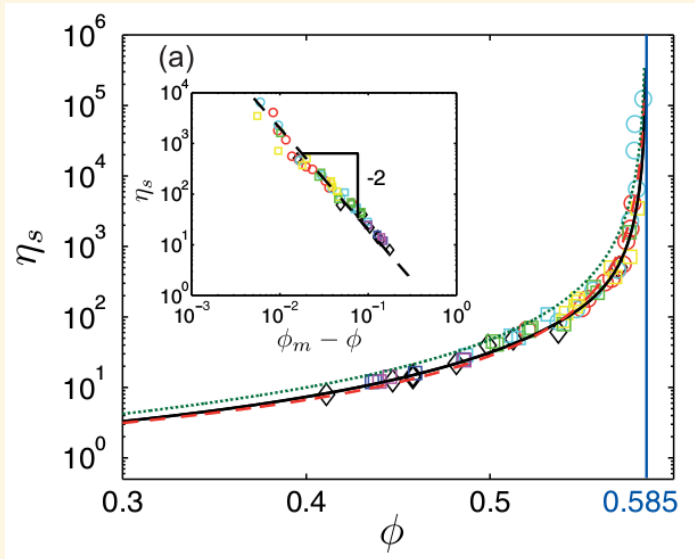
Mike Cates

DAMTP, Cambridge

VISCOSITY DIVERGENCE, JAMMING

MUCEM, Marseille

[Boyer, Guazzelli & Pouliquen, PRL 2011]



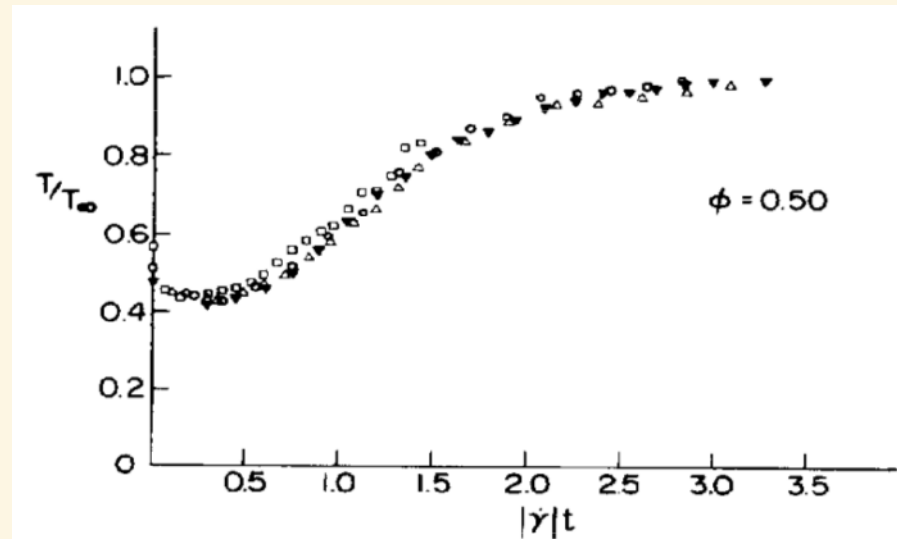
- Ultra-high performance concretes
- Lower water to cement ratio, very thick
- Use of "superplasticizers", i.e. composition tuning

MODEL GRANULAR SUSPENSIONS SHOW "SIMPLE" RHEOLOGY IN *STEADY STATE*.

EPTITOME OF UNSTEADY FLOW: SHEAR REVERSAL

[Gadala-Maria & Acrivos, JOR 1980]

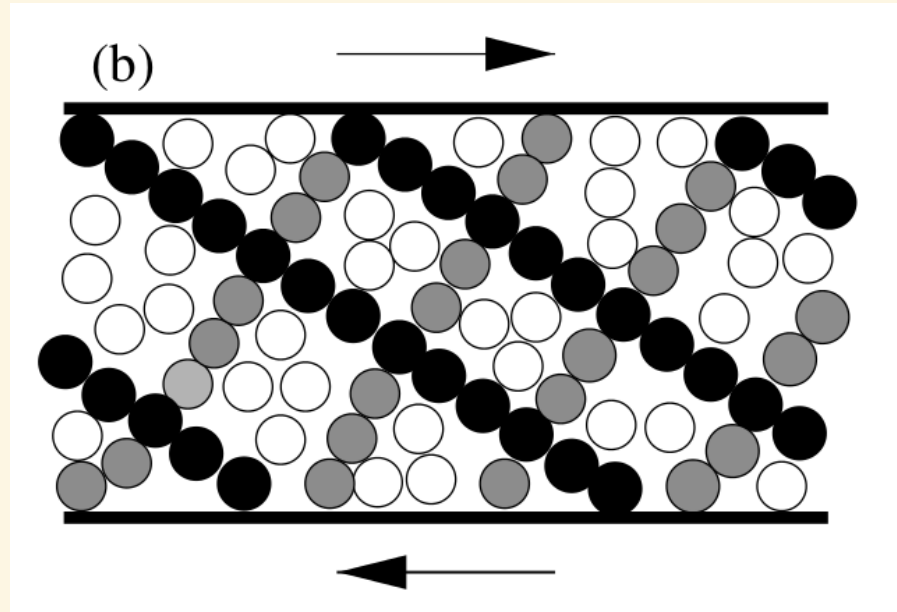
Shear up to steady-state in a given direction,
and suddenly apply opposite shear



"Memory" of past applied load

FRAGILITY OF DENSE SUSPENSIONS

[Cates, Wittmer, Bouchaud & Claudin, PRL 1998]



Mechanical response depends strongly on the compatibility of the instantly applied load with respect to the load history.

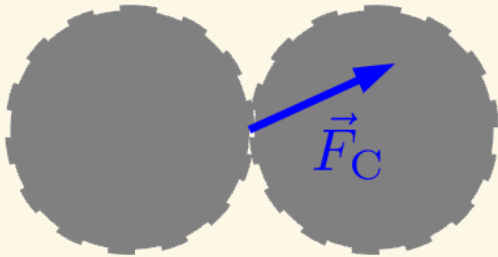
DEM + LUBRICATION SIMULATIONS

[Seto et al, PRL 2013]
[Mari et al, JOR 2014]
[Mari et al, PRE 2015]

Spherical hard particles in a Newtonian fluid in the Stokes regime,
short-range hydro (lubrication) + contacts

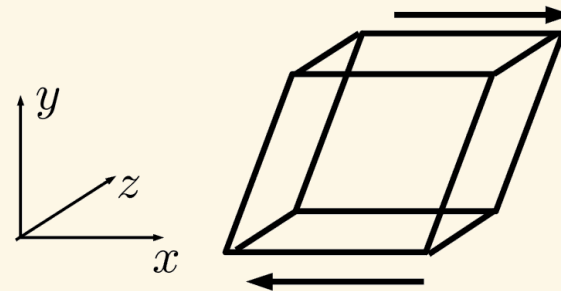
Eq. of motion (force balance)

$$0 = \mathbf{F}_H(\mathbf{U}) + \mathbf{F}_C$$



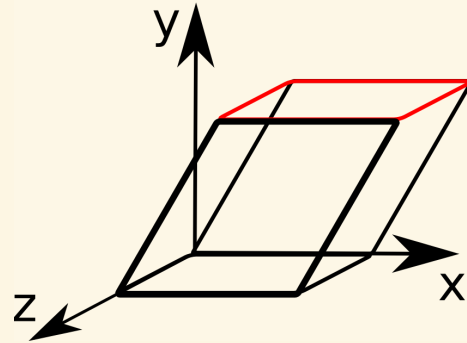
$$|\mathbf{F}_C^t| < \mu |\mathbf{F}_C^n|$$

Simple shear through Lees-Edwards b.c.



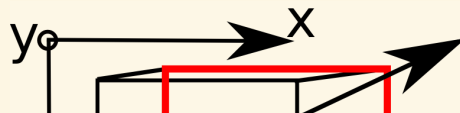
PROTOCOL

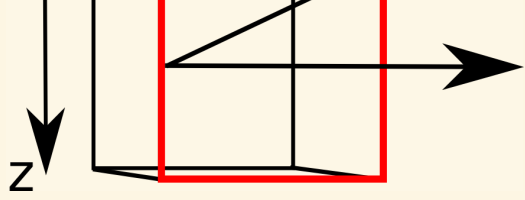
1. Shear at constant stress in the x direction (with gradient along y), up to steady-state



2. Shear in a new direction making an angle θ with x (keeping the gradient along y)

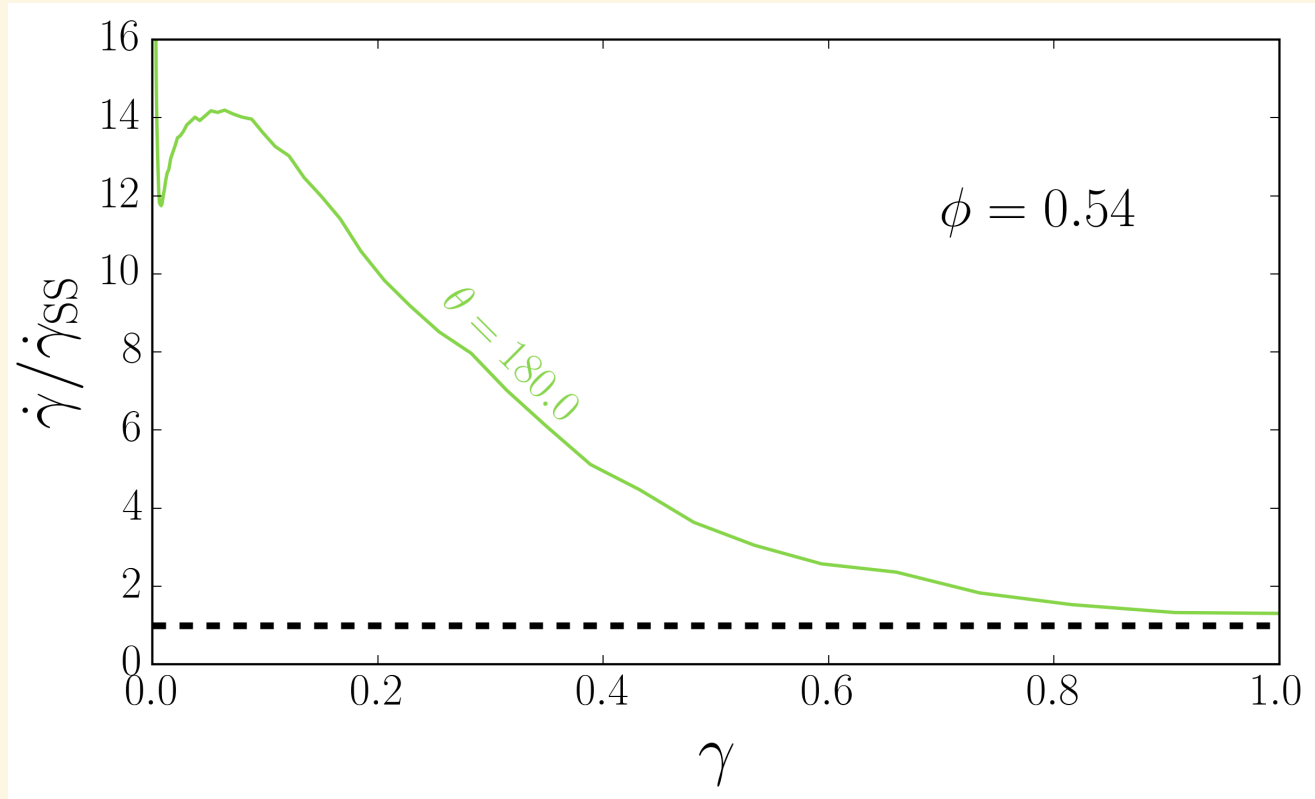
θ





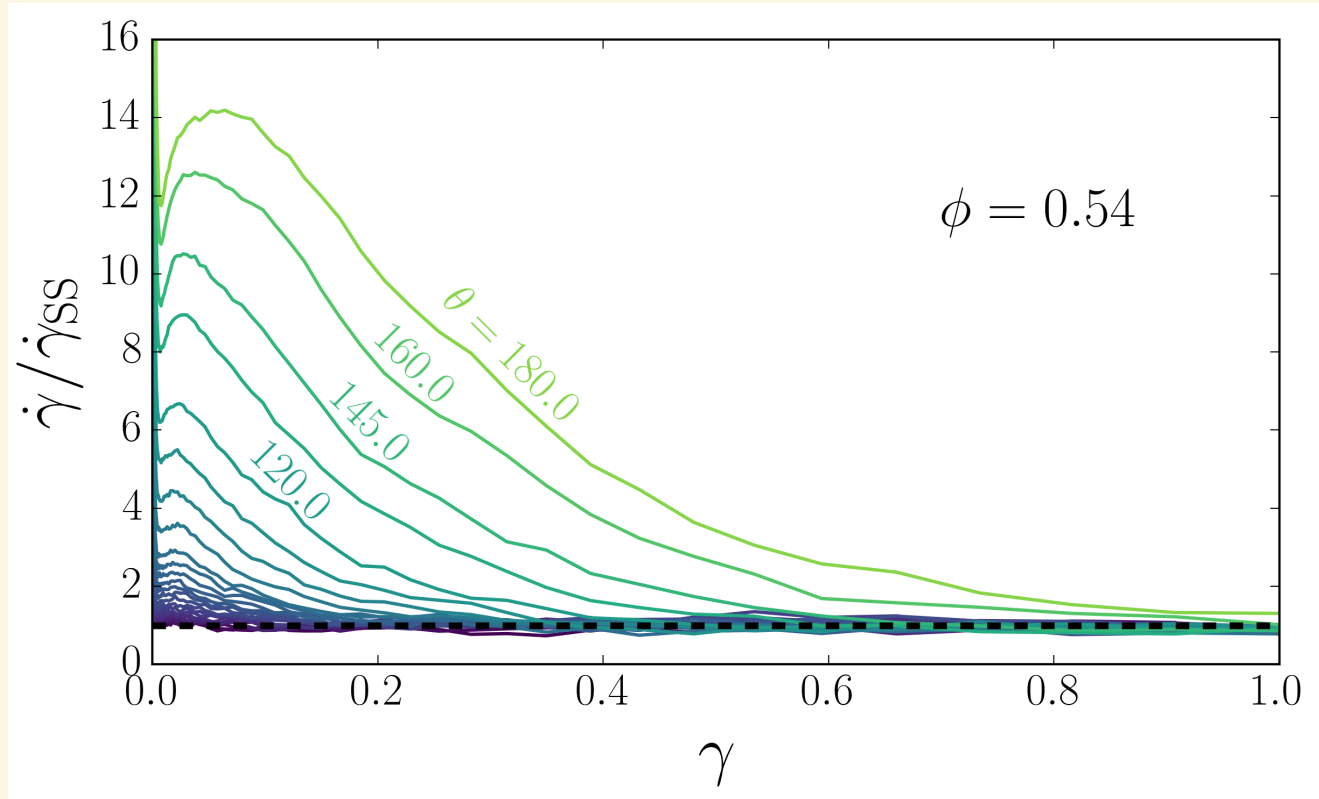
SHEAR RATE RESPONSE

$\theta = 180$ is shear reversal

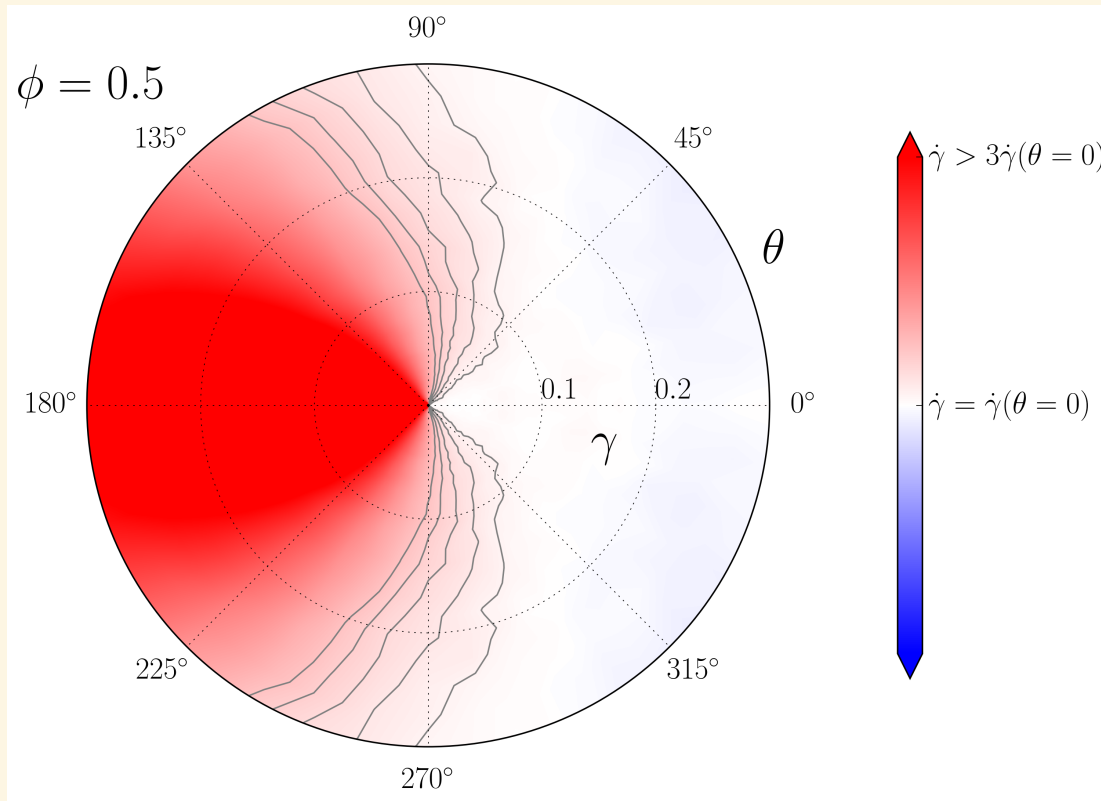


SHEAR RATE RESPONSE

$\theta = 180$ is shear reversal

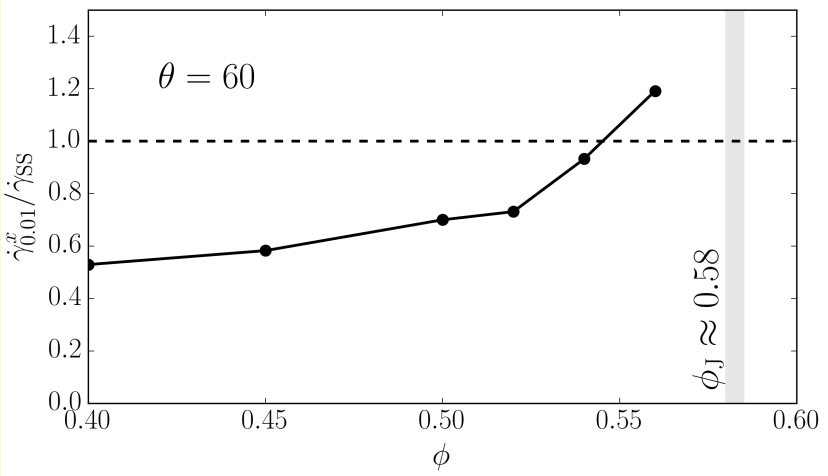
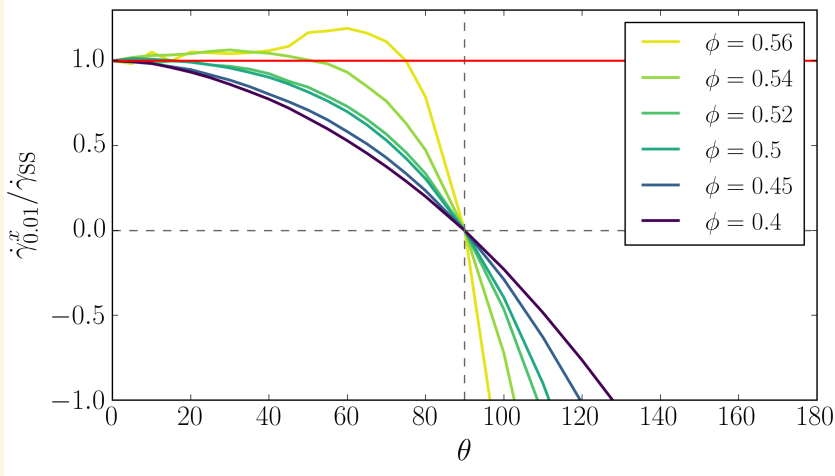


SHEAR RATE MAPS



SHEAR RATE GAIN

Maximum rate projected on the x direction

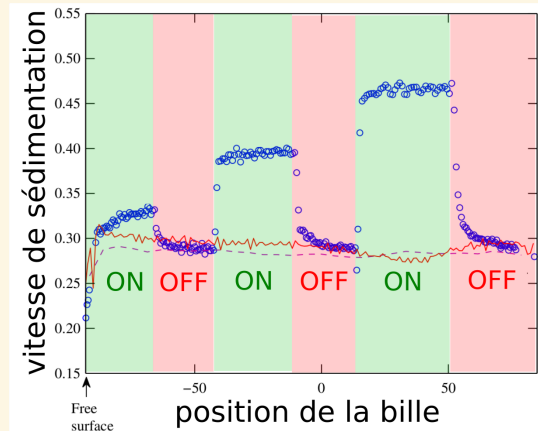
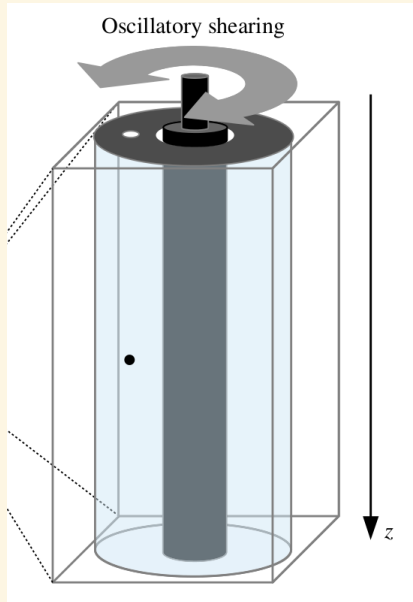


Can we use it and flow at lower viscosity
for more than a transient time?

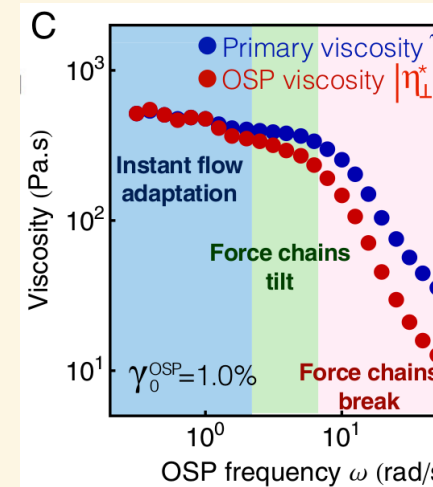
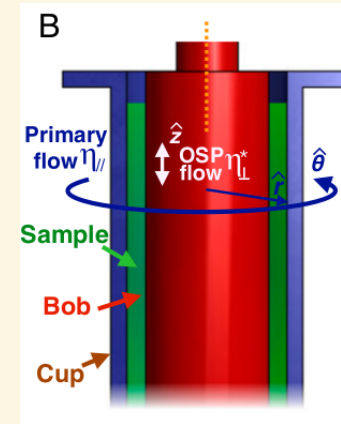
VISCOSITY REDUCTION: NEW IDEA, MECHANICAL DRIVING

Primary flows with oscillatory cross shear

Speeding sedimentation of a large intruder
[Blanc, Lemaire & Peters, JFM, 2014]



"Unthickening" of cornstarch
[Lin et al, PNAS, 2016]

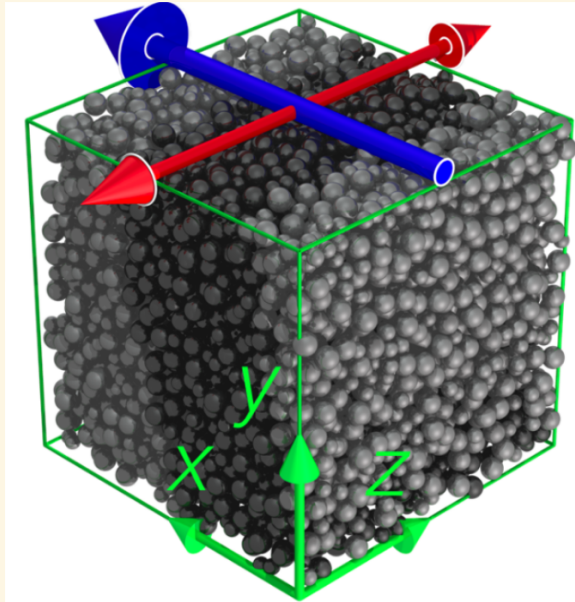


Viscosity drop generic?

Dependent on thickening? Works only for frictional systems?

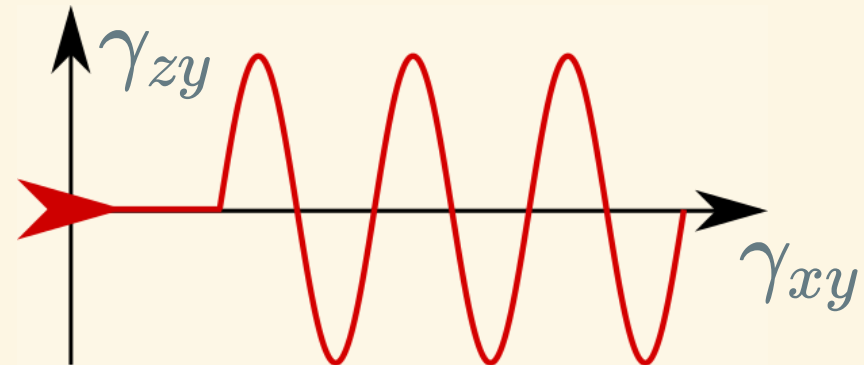
SIMULATIONS

Rate-independent suspension of particles with only lubrication and frictional contacts



$$\dot{\gamma}_{xy} = \dot{\gamma}$$

$$\dot{\gamma}_{zy} = \dot{\gamma}_{\perp} \cos(\omega t)$$

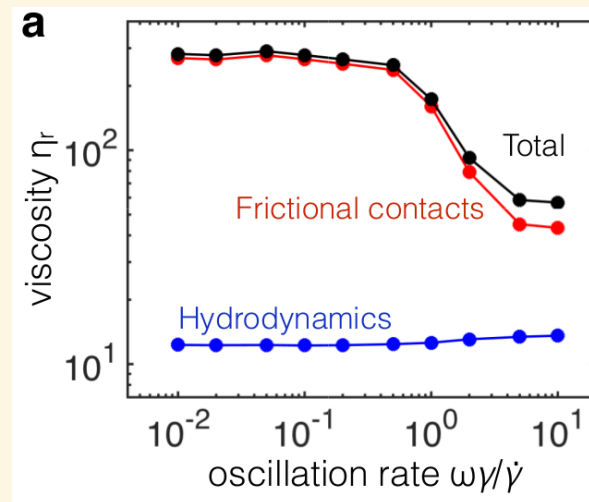
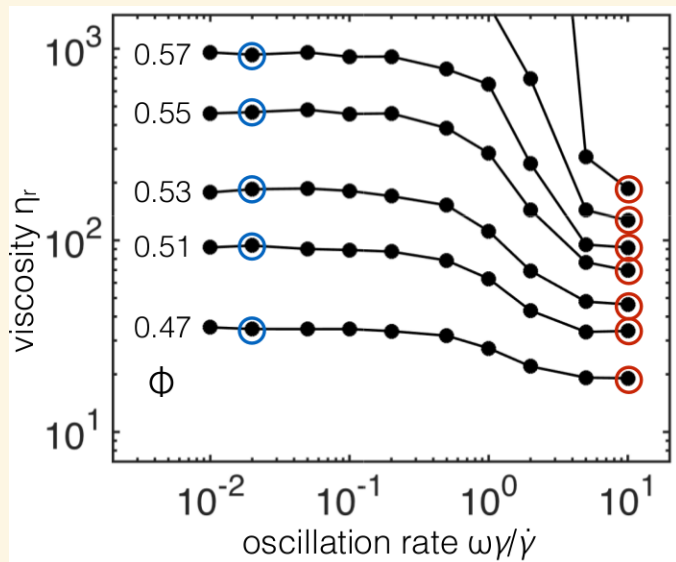


Viscosity:

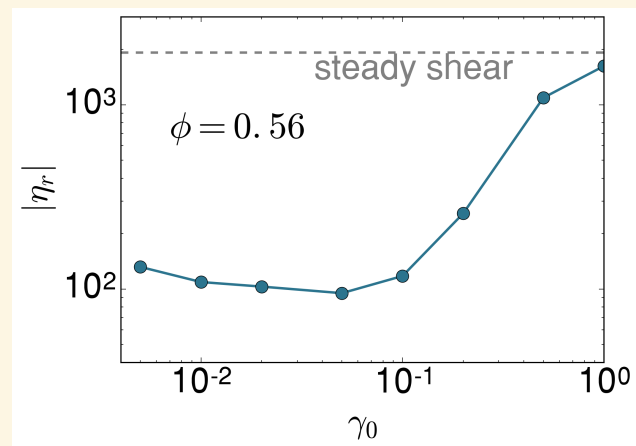
$$\eta = \sigma_{xy} / \dot{\gamma}_{xy}$$

VISCOSITY REDUCTION WITHOUT THICKENING

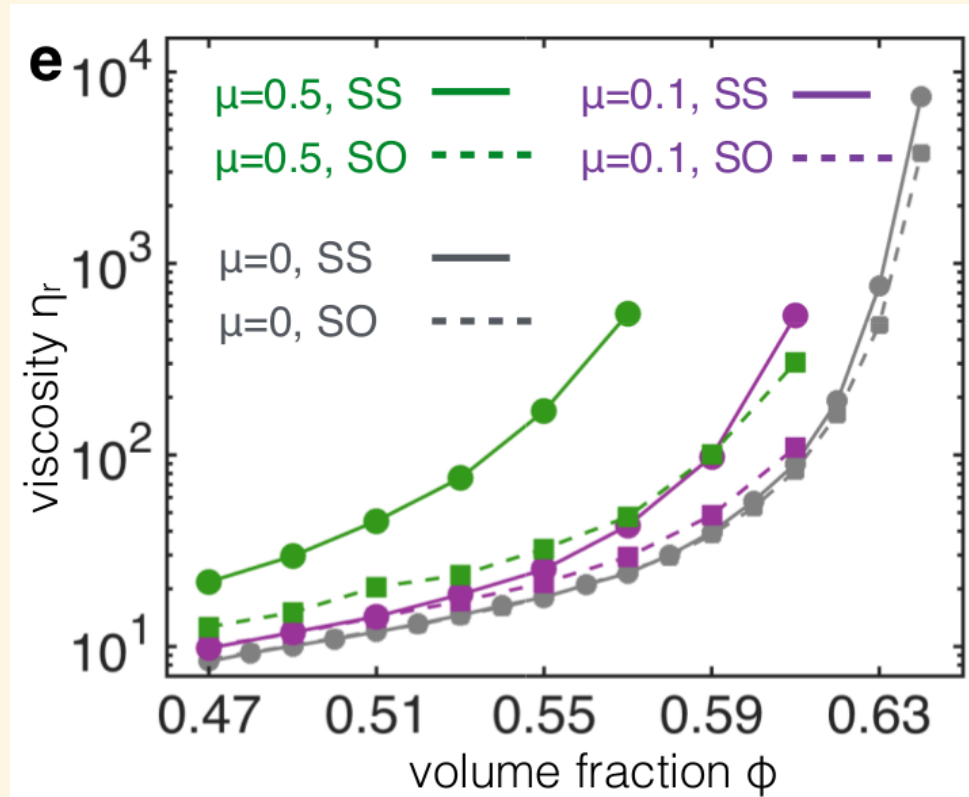
When $\gamma = 1\% - 5\%$,
strong viscosity drop.



Dependence on γ



VISCOSITY REDUCTION



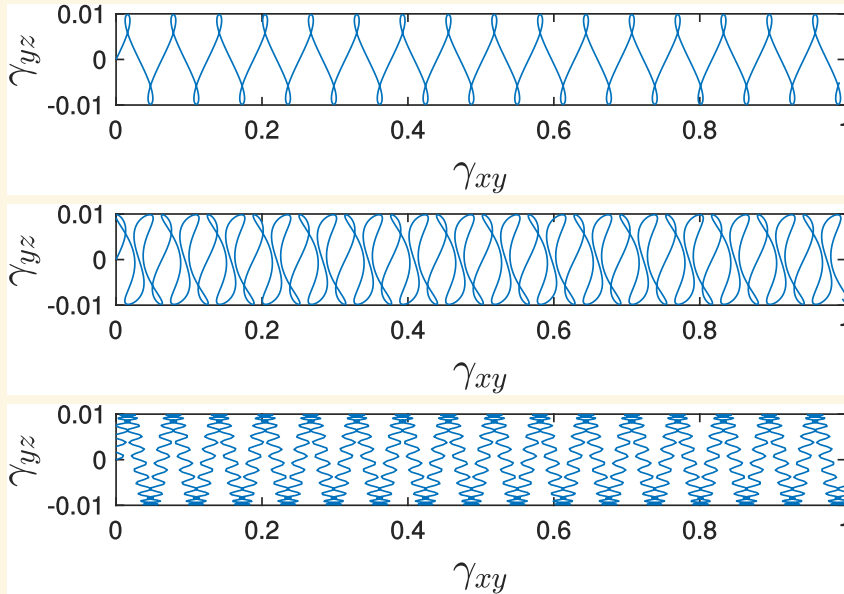
Arbitrary large gain close to jamming

Works for frictional suspensions!

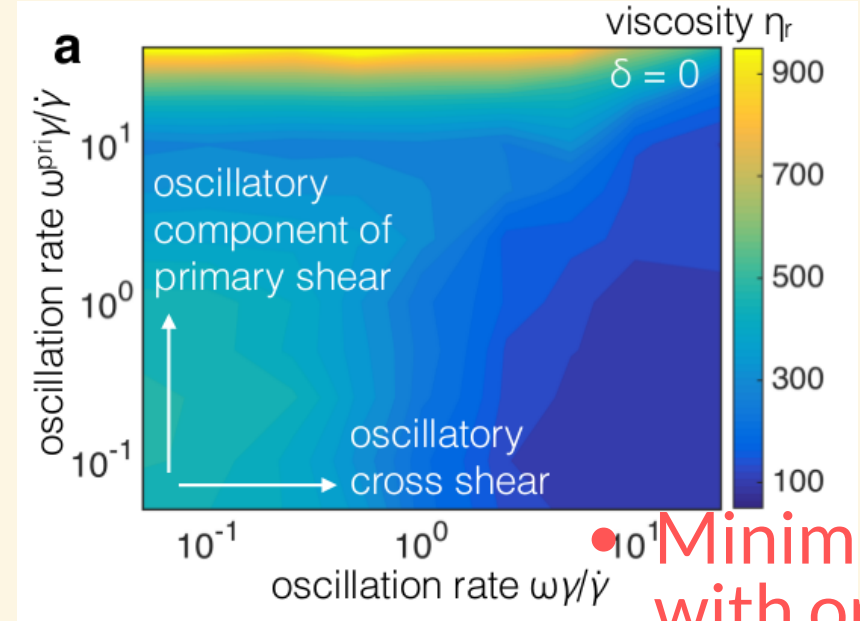
IS ANY OSCILLATION HELPING?

$$\dot{\gamma}_{xy} = \dot{\gamma} + \omega^{\text{pri}} \gamma \cos(\omega^{\text{pri}} t + \delta)$$

$$\dot{\gamma}_{zy} = \omega \gamma \cos(\omega t)$$



Viscosity map

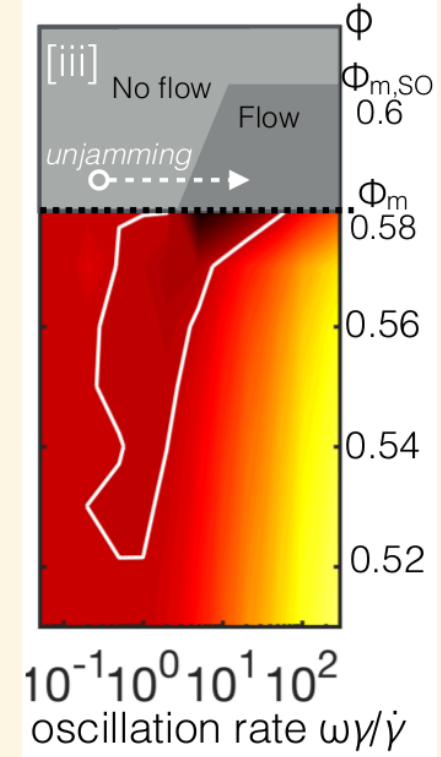
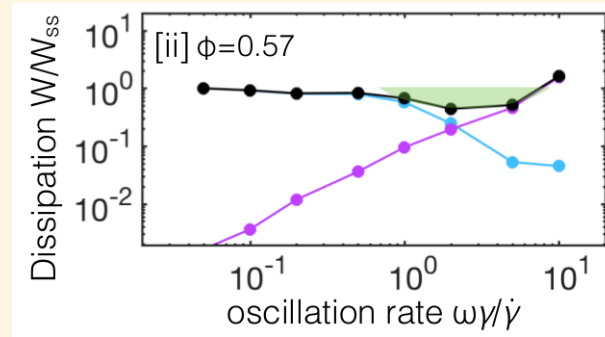
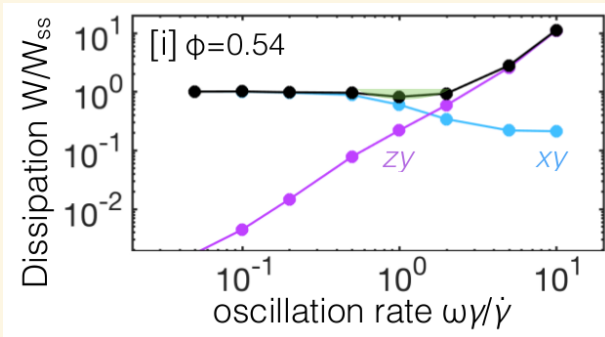


Minimum
with only
crosswise
oscillation

HOWEVER... DISSIPATION

Dissipation per unit strain $W = \frac{\int \Sigma : \dot{\Gamma} dt}{\int \dot{\gamma}_{xy} dt}$

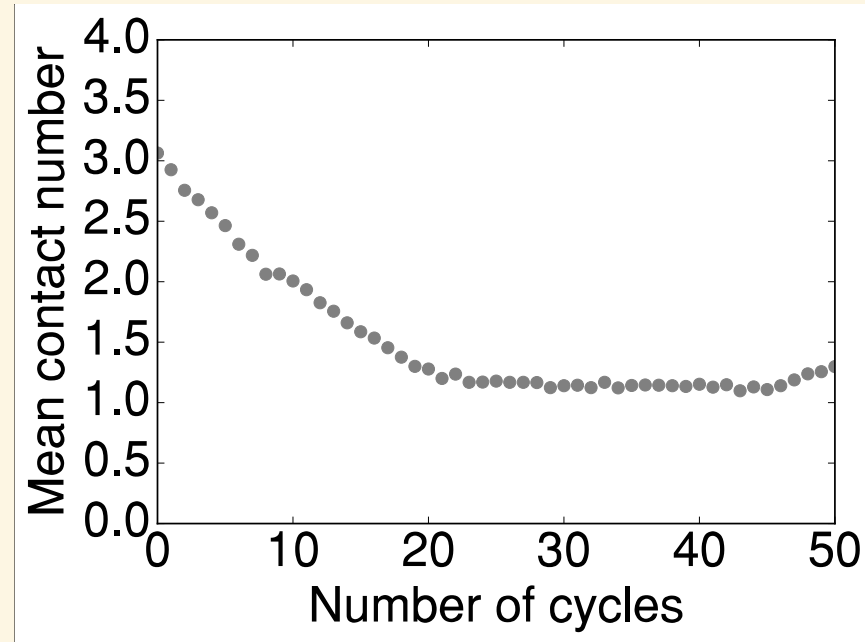
$\dot{\gamma}_{zy} \sim \omega, \Sigma_{zy} \sim \omega, \text{ so } W_{zy} \sim \omega^2.$



Can we do better?

ORIGIN OF THE VISCOSITY DROP

Contact drop, that is, *room making*

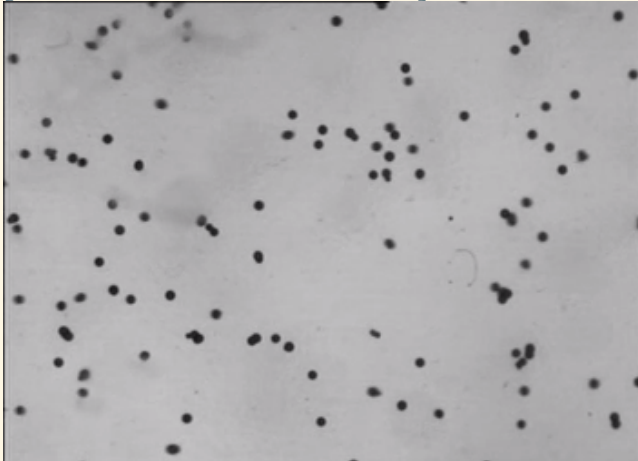


Room-making is slow

"ECHO" EXPERIMENT, RANDOM ORGANIZATION

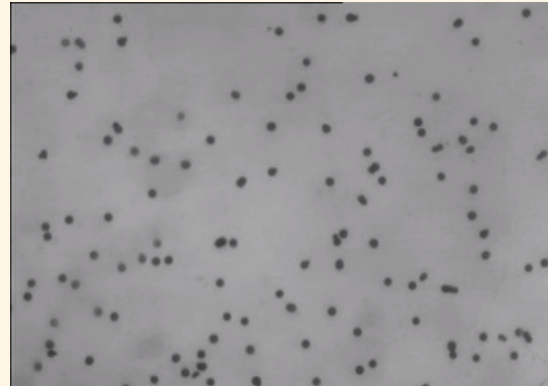
Self-organization, absorbing phase transition

[Pine et al. Nature 2005]



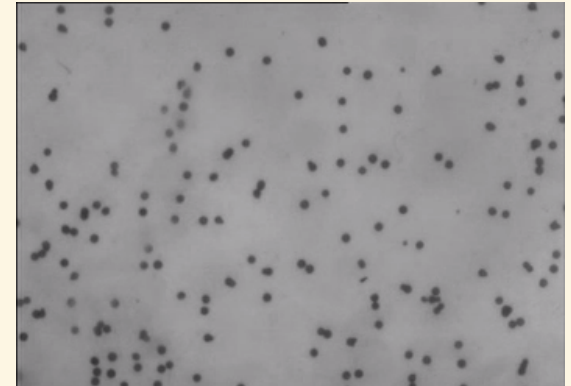
▶ 0:00 / 0:09 ●

$$\phi > \phi_c$$



▶ 0:00 / 0:11 ●

$$\phi < \phi_c$$



▶ 0:00 / 0:19 ●

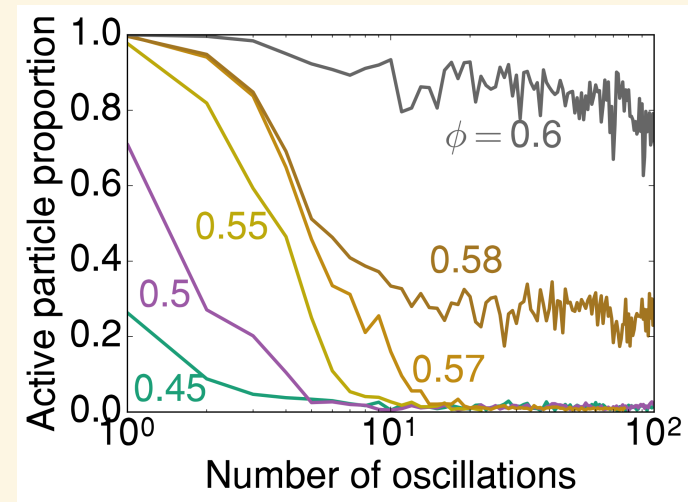
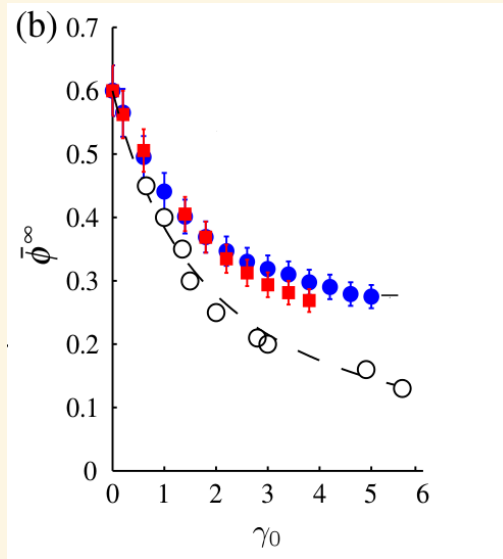
WHERE IS THE ABSORBING PHASE TRANSITION?

For large $\gamma \approx 1$, phase transition at $\phi_c \approx 0.3$

But in our case $\gamma \approx 1\% \ll 1$!

[Corté et al, PRL, 2009]

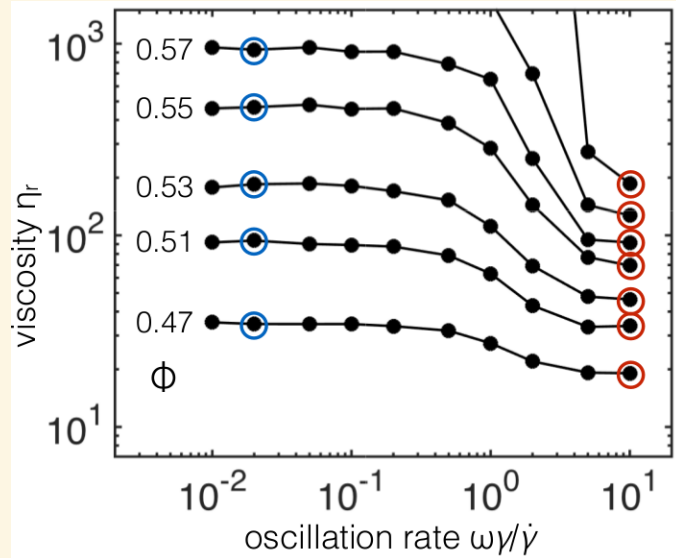
Our system, oscillatory shear only, $\gamma = 2\%$:



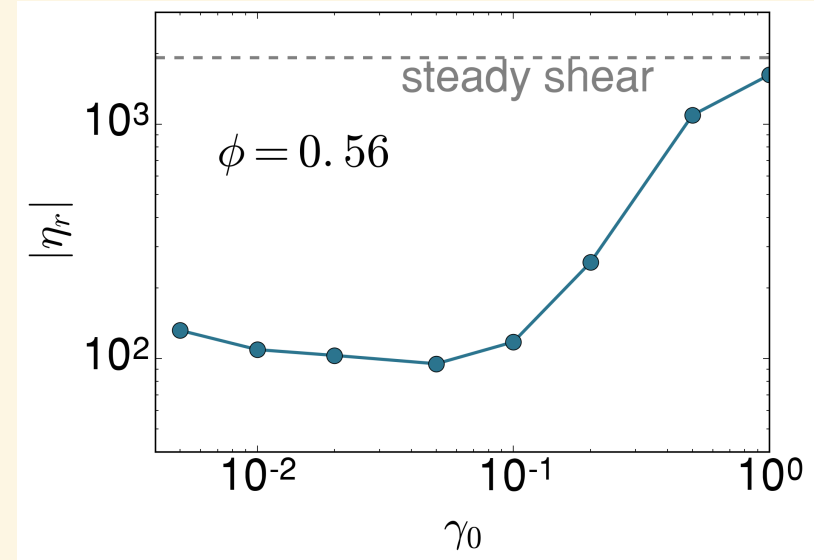
Transition very close to jamming

VISCOSITY REDUCTION AND RANDOM ORGANIZATION

Dependence on frequency



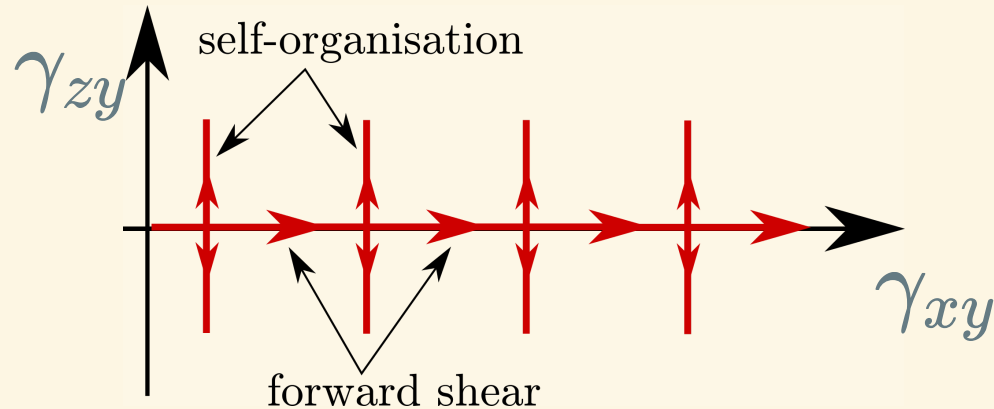
Dependence on amplitude



OCS is using random organization to improve flowability

AN ALTERNATIVE PROTOCOL

Decouple self-organization from primary shear

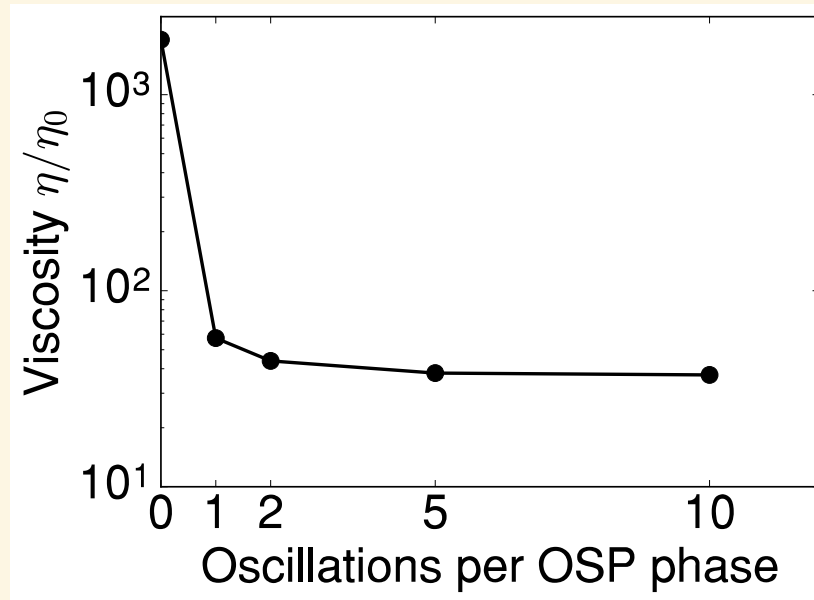


Parameters:

- Strain in the primary direction Γ
- Amplitude of the oscillations γ
- Number of oscillations per period n
- [Proportion of time in oscillations α]

ALTERNATING RANDOM ORGANIZATION AND SHEAR

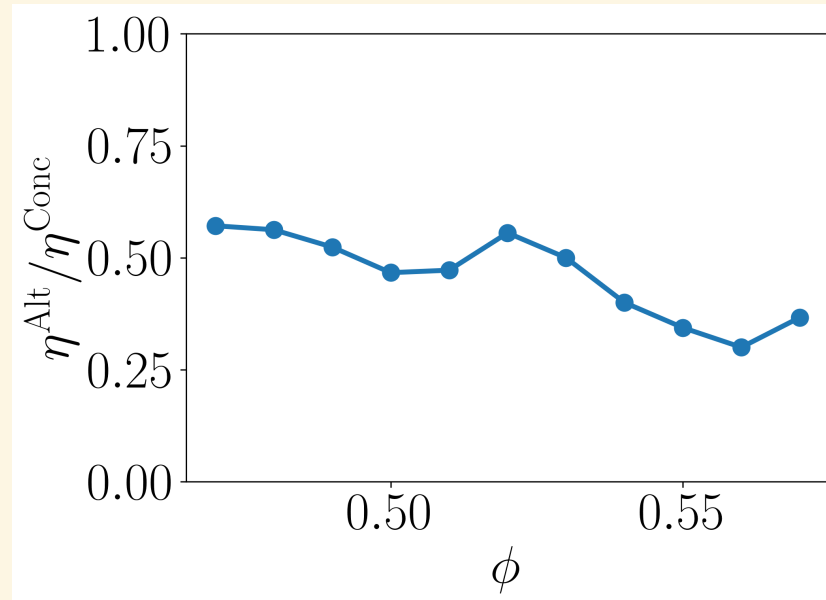
For $\gamma = 2\%$ and $\phi = 0.56$:



Few oscillations are enough

ALTERNATING VS CONCURRENT OCS

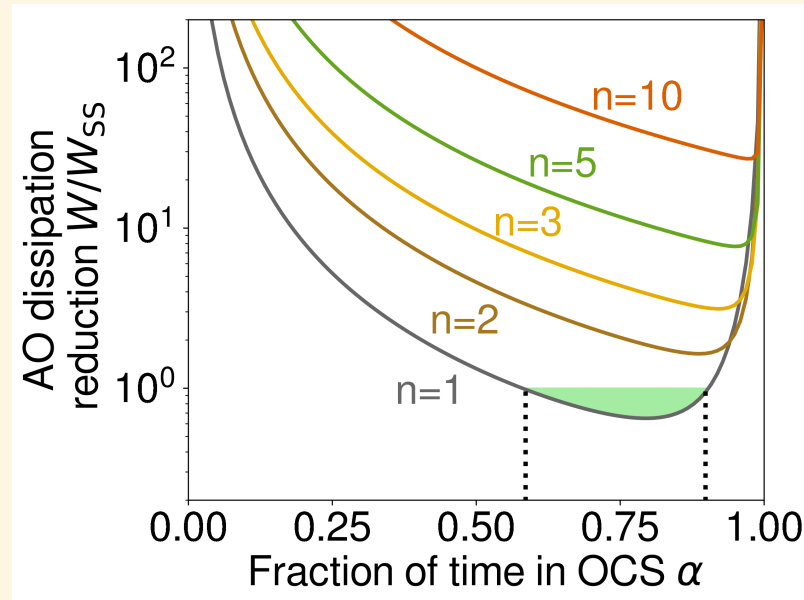
Viscosity obtained for alternating OCS with $n = 1$ and $\gamma = 1\%$ compared to high ω viscosity for concurrent OSP with same γ .



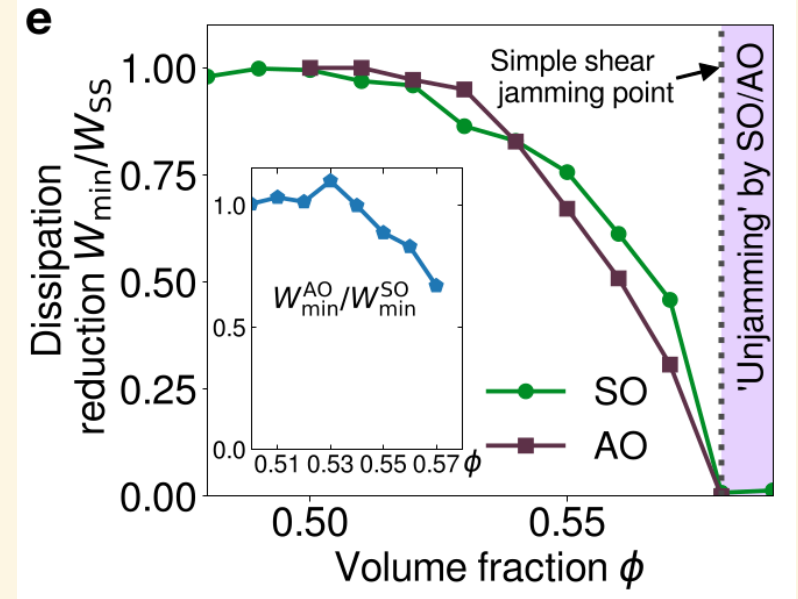
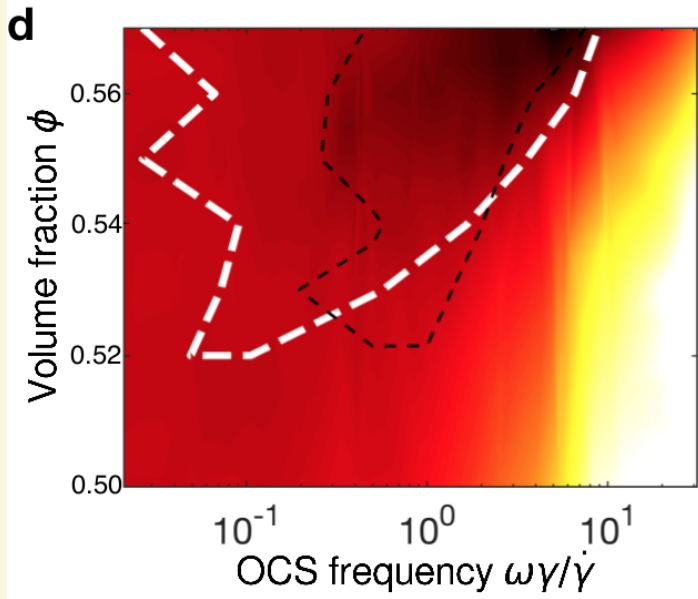
BACK TO DISSIPATION

Depends on the time proportion spent in self-organization α !

For $\gamma = 1\%$ and $\phi = 0.56$:



BACK TO DISSIPATION



CONCLUSION

- Powerful tool for viscosity/dissipation reduction *without* composition tuning
- Generic to granular suspensions
- Use of a nonequilibrium phase transition in a rheological context
- Adaptable for industrial devices?

