

Mean flows and frequency prediction

Sam Turton (Cambridge, Part III —> MIT)

Yacine Bengana (PMMH-CNRS-ESPCI)

Nicolas Périnet (Univ. of Santiago)

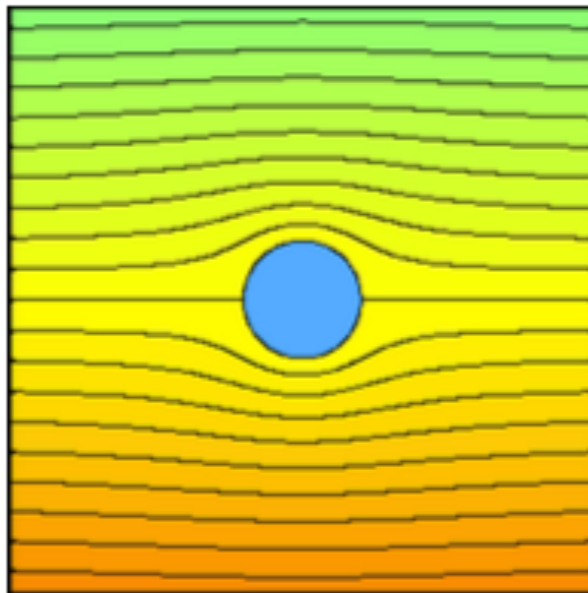
Laurette Tuckerman (PMMH-CNRS-ESPCI)

Dwight Barkley (University of Warwick)

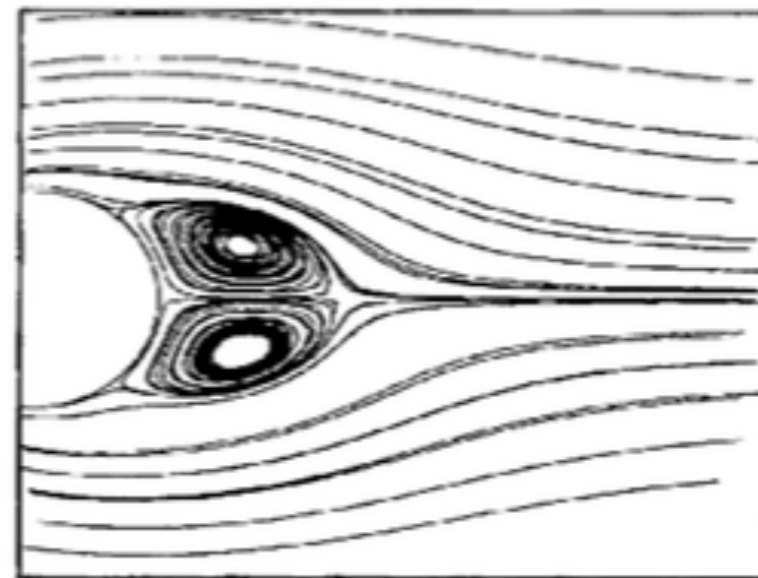


Cylinder wake

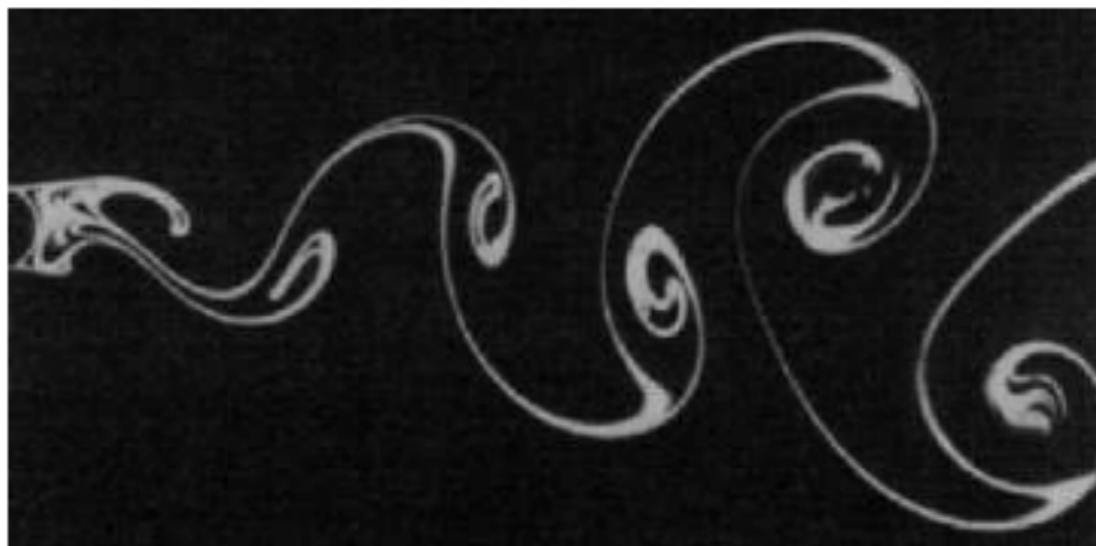
Ideal flow



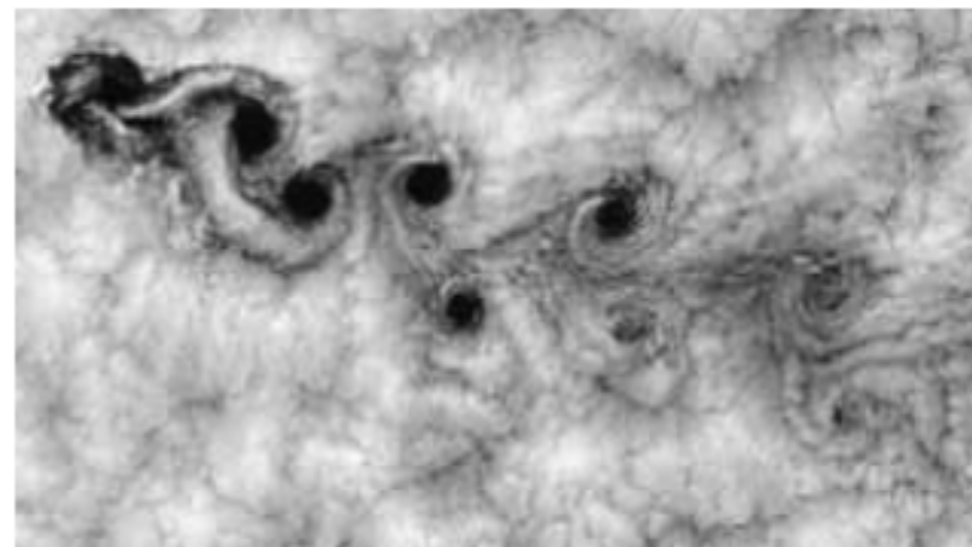
with downstream recirculation zone



Von Kármán vortex street ($Re \geq 46$)

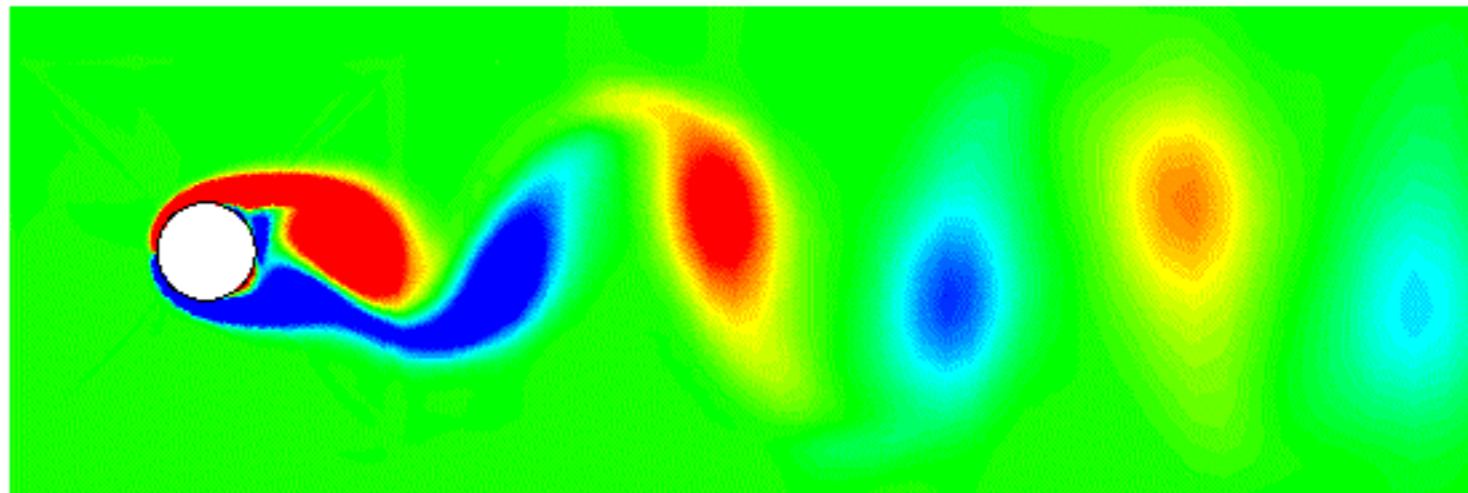
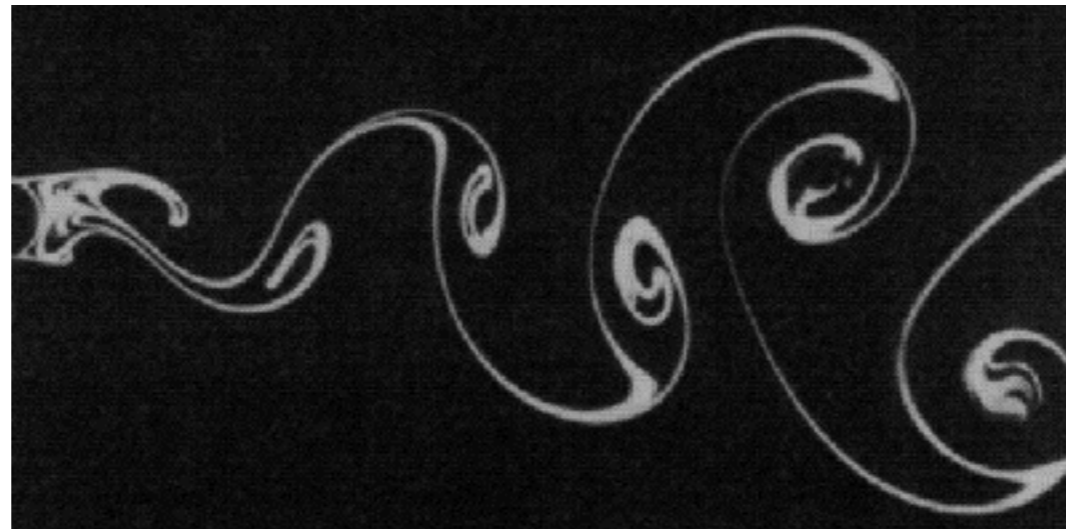


Laboratory experiment
(Taneda, 1982)

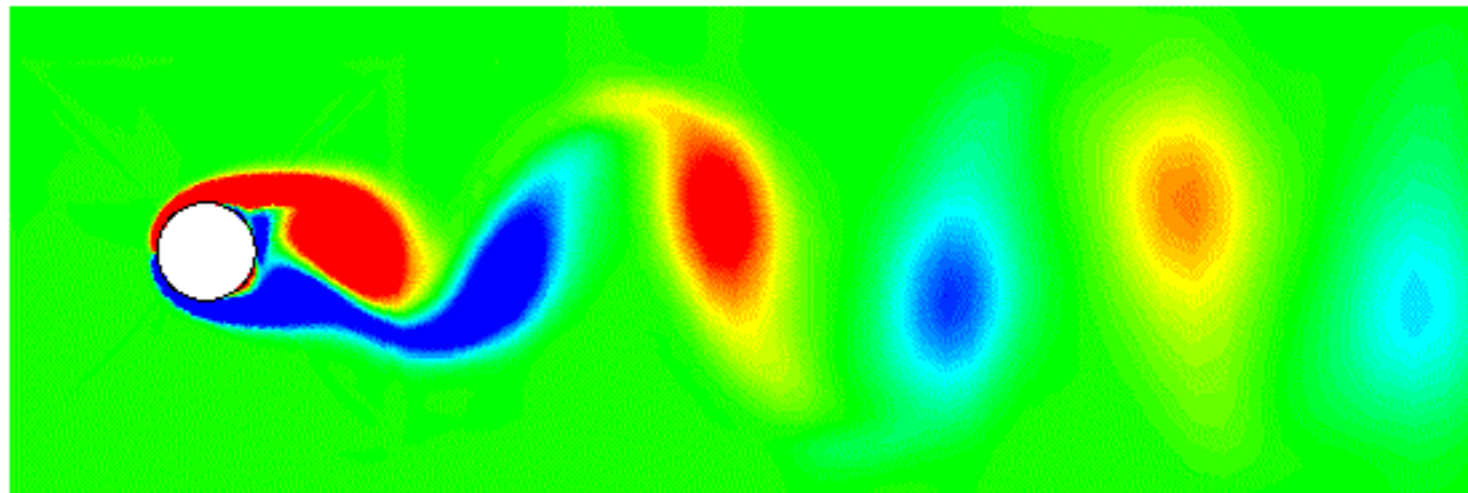
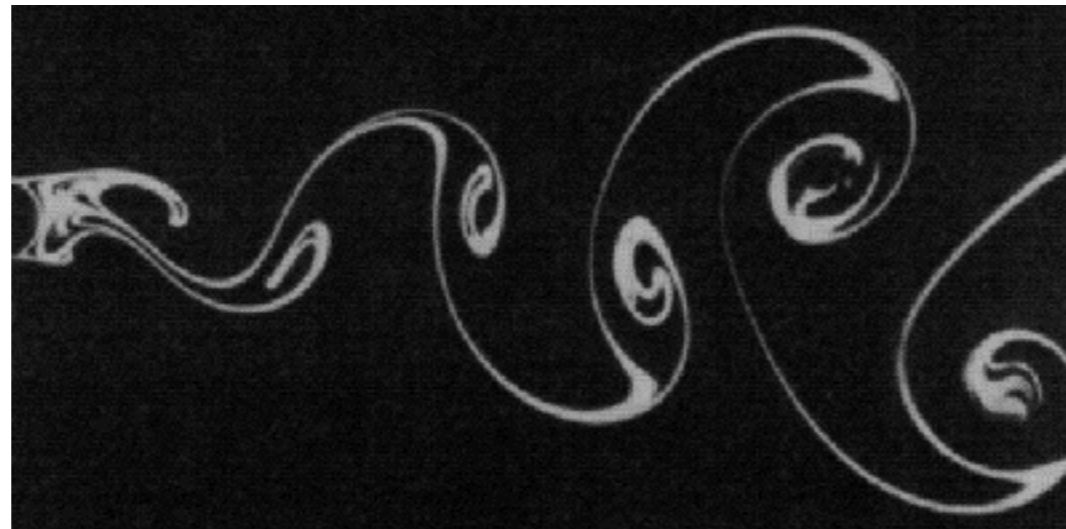


Off Chilean coast
past Juan Fernandez islands

Vortex-shedding frequency of cylinder wake

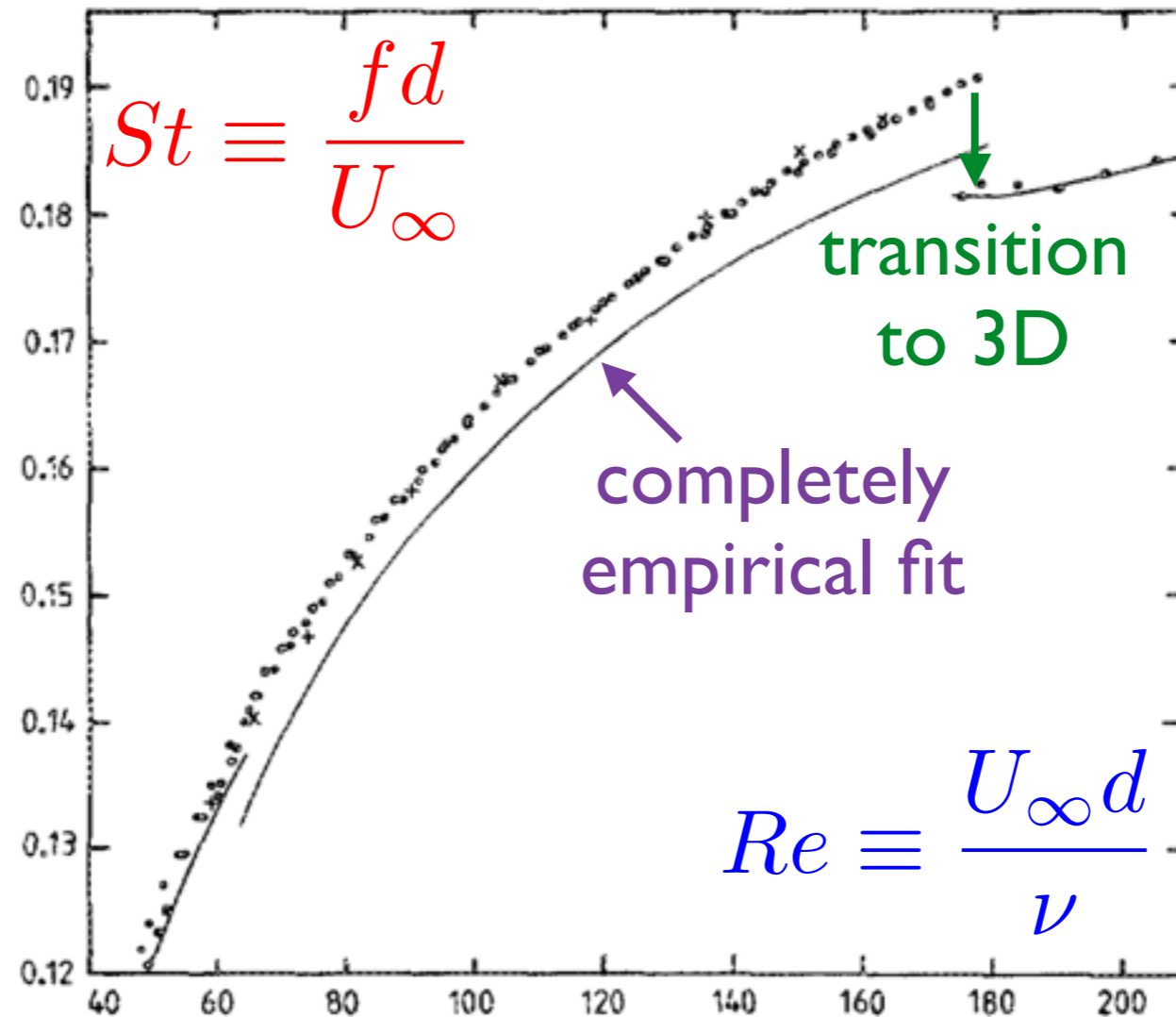


Vortex-shedding frequency of cylinder wake



Defining a universal and continuous Strouhal–Reynolds number relationship for the laminar vortex shedding of a circular cylinder

C. H. K. Williamson *Physics of Fluids* 31, 2742 (1988)

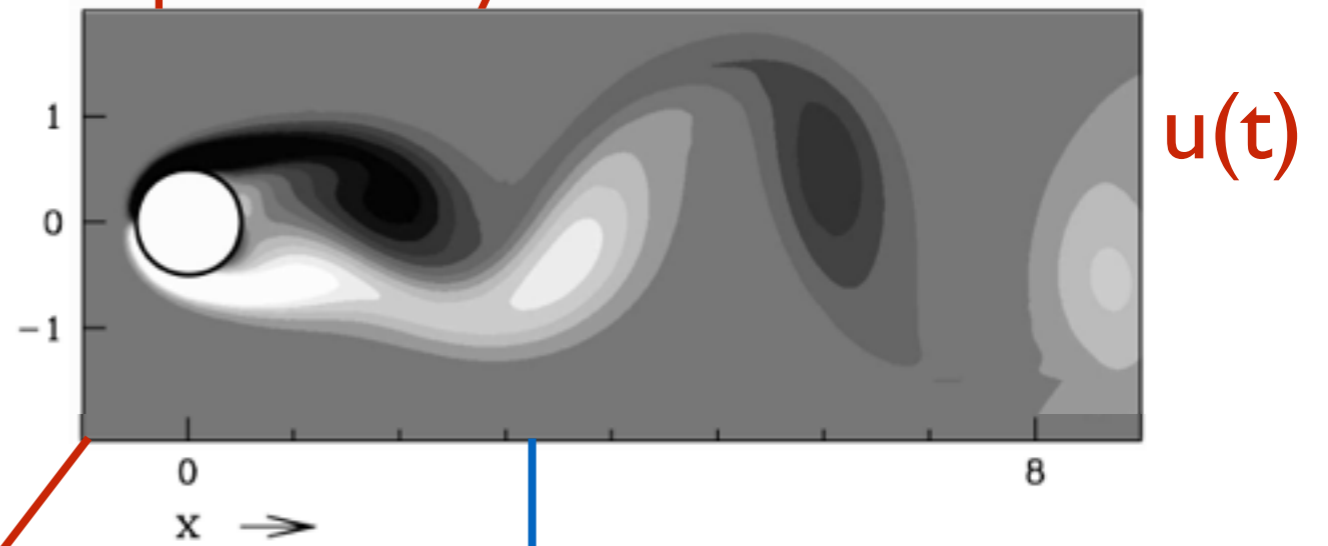


Seek prediction from equations/physics

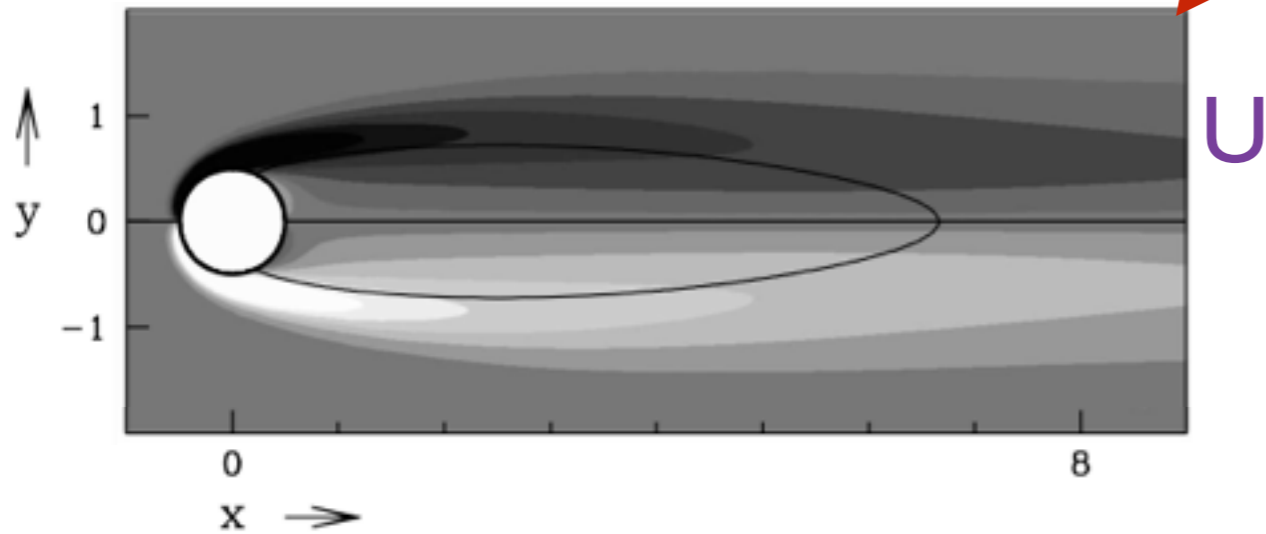
Linear analysis of the cylinder wake mean flow

D. BARKLEY(*) *Europhys. Lett.*, **75** (5), pp. 750–756 (2006)

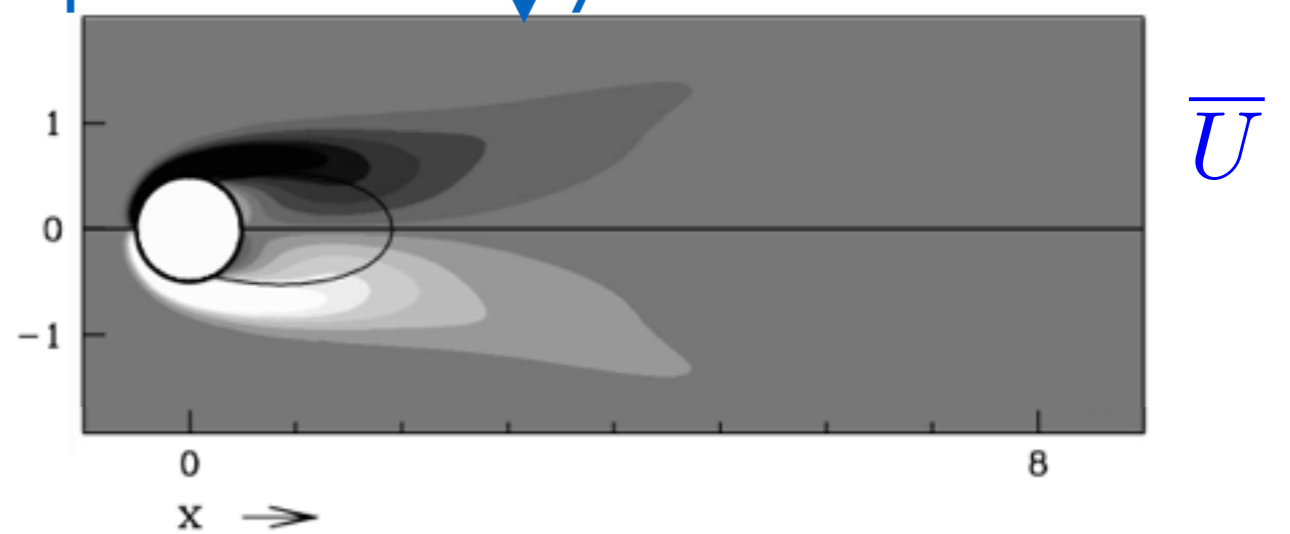
Snapshot of cylinder wake at $Re=100$



Unstable basic flow at $Re=100$



Temporal mean of cylinder wake at $Re=100$



Basic flow

$$0 = -(U \cdot \nabla)U - \nabla P + \frac{1}{Re} \nabla^2 U$$

Temporally periodic wake flow

$$\partial_t u = -(u \cdot \nabla)u - \nabla p + \frac{1}{Re} \nabla^2 u$$

Temporal mean

$$\bar{U} \equiv \frac{1}{T} \int_0^T u(t) dt$$

Linearise about steady base flow

$$\partial_t u = -(U \cdot \nabla)u - (u \cdot \nabla)U - \nabla p + \frac{1}{Re} \nabla^2 u$$

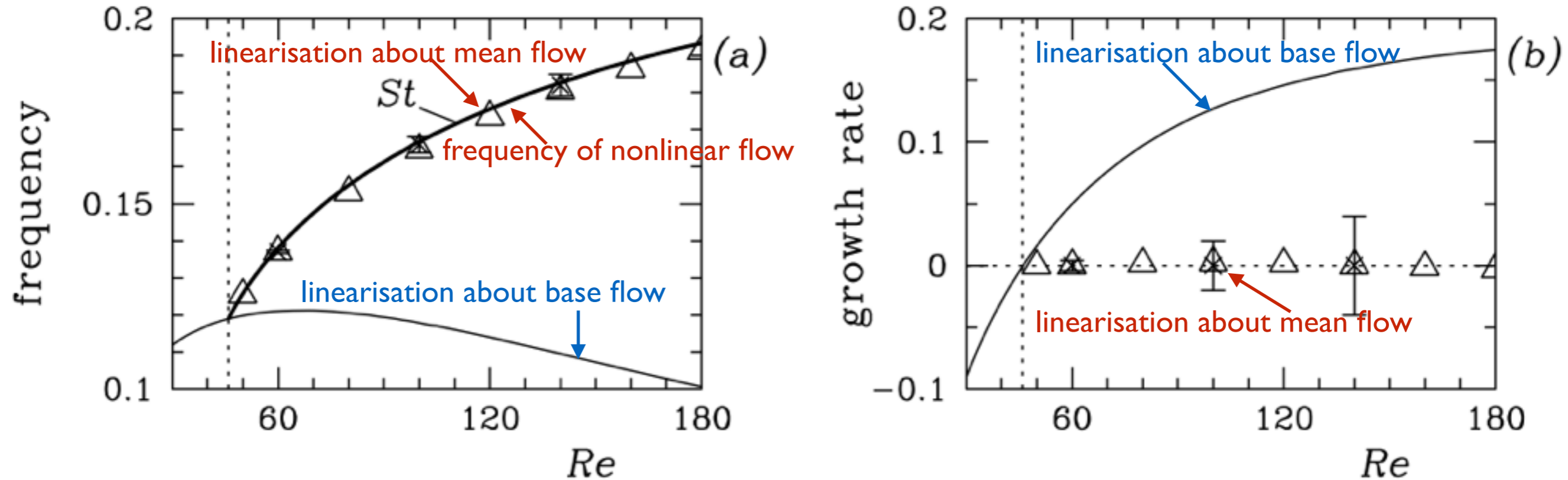
Linearise about temporal mean

$$\partial_t u = -(\bar{U} \cdot \nabla)u - (u \cdot \nabla)\bar{U} - \nabla p + \frac{1}{Re} \nabla^2 u$$

Strange and unjustified procedure, but quite successful !

Linear analysis of the cylinder wake mean flow

D. BARKLEY(*) *Europhys. Lett.*, **75** (5), pp. 750–756 (2006)



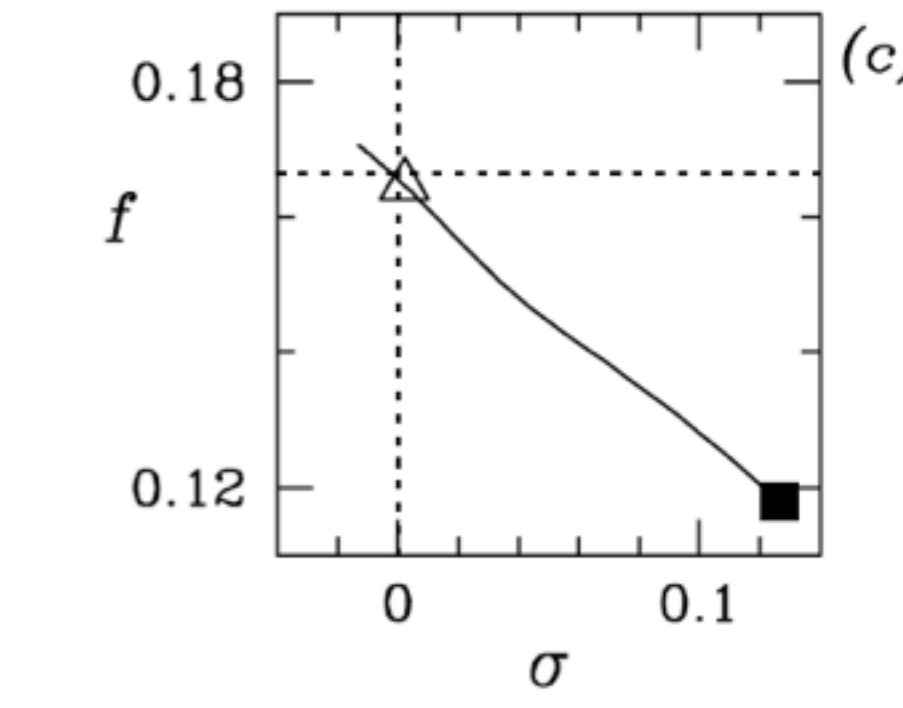
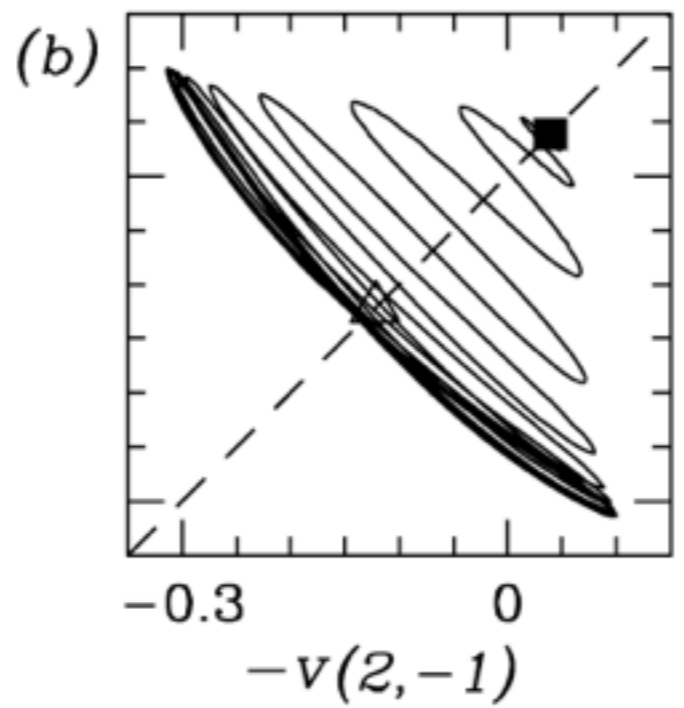
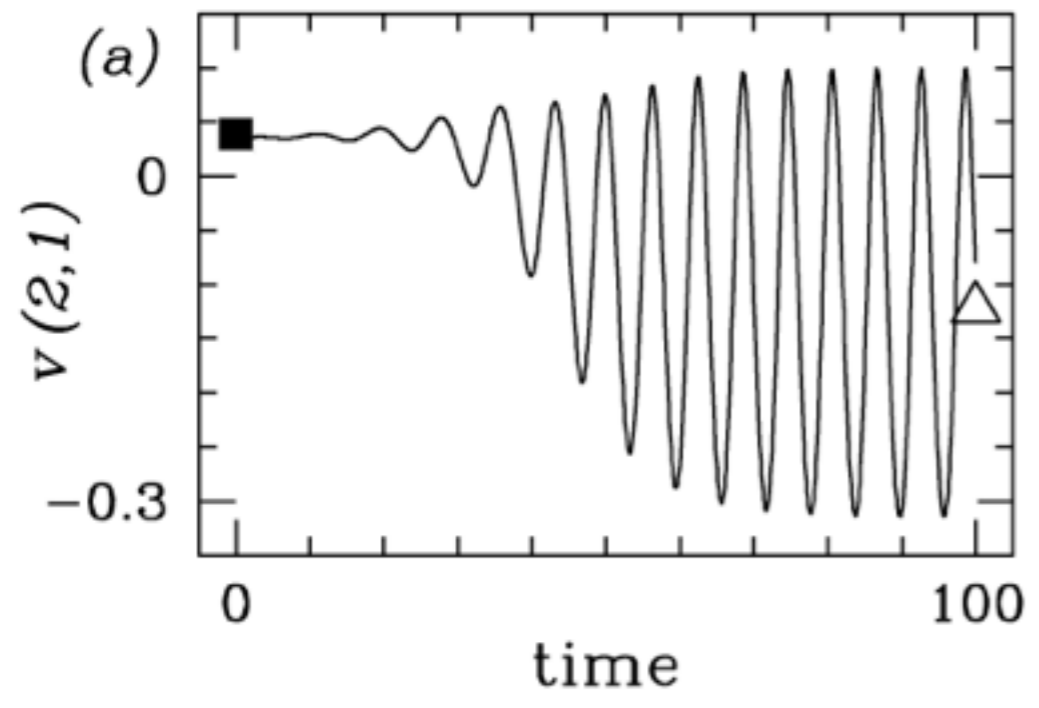
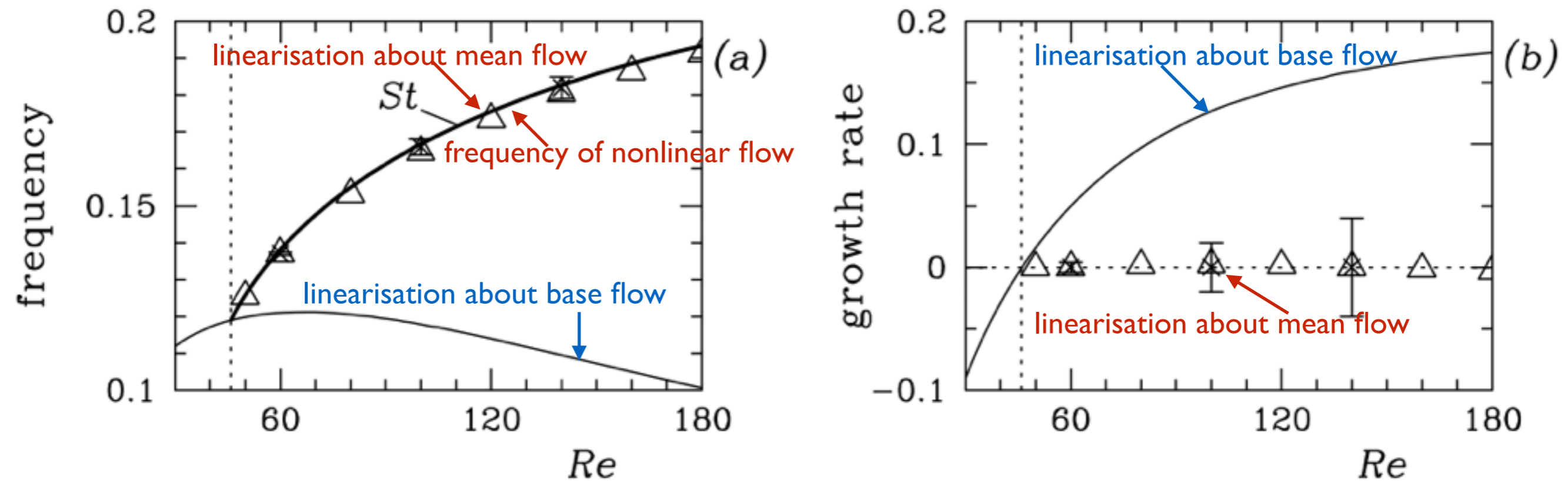
Mean flow eigenvalue has **RZIF** property:

Real part is near **Zero**.

Imaginary part is near exact nonlinear **Frequency**.

Linear analysis of the cylinder wake mean flow

D. BARKLEY(*) *Europhys. Lett.*, **75** (5), pp. 750–756 (2006)



Malkus theory: Temporal mean of turbulent flow should be marginally stable

Outline of a theory of turbulent shear flow

W. V. R. Malkus

Journal of Fluid Mechanics / Volume 1 / Issue 05 / November 1956, pp 521 - 539

1956 Cambridge University Press

VOLUME 79, NUMBER 20

PHYSICAL REVIEW LETTERS

17 NOVEMBER 1997

Strongly Nonlinear Effect in Unstable Wakes

B. J. A. Zielinska,^{2,1} S. Goujon-Durand,^{1,3} J. Dušek,⁴ and J. E. Wesfreid¹

¹*Ecole Supérieure de Physique et Chimie Industrielles de Paris (ESPCI), PMMH-URA CNRS No. 857,*

J. Fluid Mech. (2002), vol. 458, pp. 407–417. © 2002 Cambridge University Press

DOI: 10.1017/S0022112002008054 Printed in the United Kingdom

On the frequency selection of finite-amplitude vortex shedding in the cylinder wake

By BENOÎT PIER

Department of Applied Mathematics and Theoretical Physics, University of Cambridge,
Silver Street, Cambridge CB3 9EW, UK

J. Fluid Mech. (2003), vol. 497, pp. 335–363. © 2003 Cambridge University Press

DOI: 10.1017/S0022112003006694 Printed in the United Kingdom

A hierarchy of low-dimensional models for the transient and post-transient cylinder wake

By BERND R. NOACK^{1†}, KONSTANTIN AFANASIEV²,
MAREK MORZYŃSKI³, GILEAD TADMOR⁴
AND FRANK THIELE¹

Global stability of base and mean flows: a general approach and its applications to cylinder and open cavity flows

DENIS SIPP AND ANTON LEBEDEV

ONERA, 8 rue des Vertugadins, 92190 Meudon, France

INTERNATIONAL JOURNAL FOR NUMERICAL METHODS IN FLUIDS

Int. J. Numer. Meth. Fluids 2008; **58**:111–118

Published online 20 December 2007 in Wiley InterScience (www.interscience.wiley.com). DOI: 10.1002/fld.1714

SHORT COMMUNICATION

Global linear stability analysis of time-averaged flows

Sanjay Mittal^{*,†}

PRL 113, 084501 (2014)

PHYSICAL REVIEW LETTERS

week ending
22 AUGUST 2014

Self-Consistent Mean Flow Description of the Nonlinear Saturation of the Vortex Shedding in the Cylinder Wake

Vladislav Mantič-Lugo,^{*} Cristóbal Arratia,[†] and François Gallaire

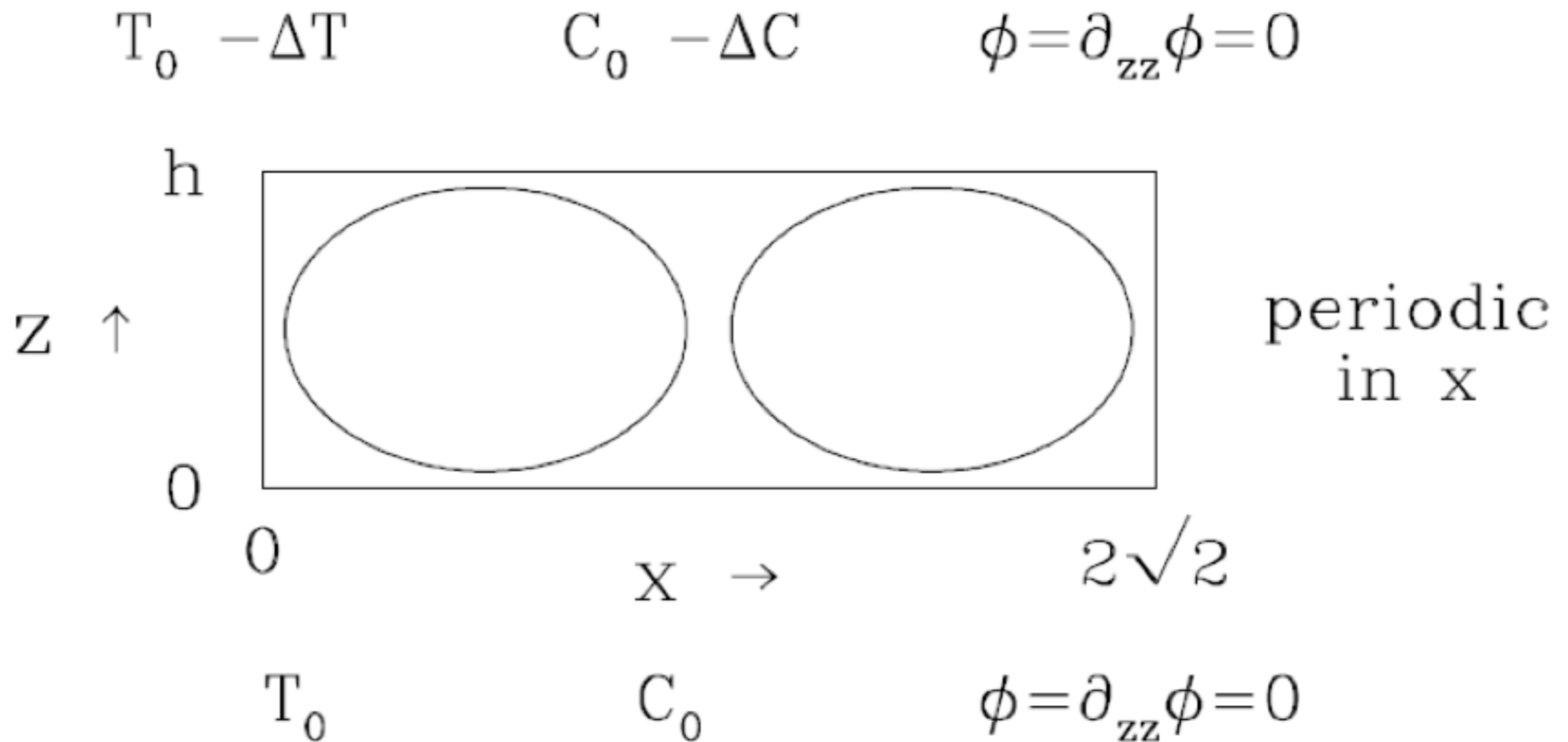
*Laboratory of Fluid Mechanics and Instabilities, École Polytechnique Fédérale de Lausanne, EPFL-STI-IGM-LFMI,
Lausanne CH-1015, Switzerland*

(Received 19 December 2013; published 20 August 2014)

When is RZIF satisfied ?

Why is RZIF satisfied?

Simple Model: 2D Thermosolutal Problem



Vertical thermal and solutal gradients imposed at $z = 0, 1$

Boundary conditions: free-slip at $z = 0, 1$; periodic in x with length $2\sqrt{2}$

Streamfunction $\mathbf{U} = \nabla \times \phi(x, z) \mathbf{e}_y$

Density: $\rho(T, C) = \rho_0 + \rho_T(T - T_0) + \rho_C(C - C_0)$

Diffusivities: κ_T (thermal), κ_C (solutal), ν (momentum)

Conductive solution:

$T = T_0 - z\Delta T/h,$ $C = C_0 - z\Delta C/h,$ $U = \nabla \times \phi e_y = 0$

Four nondimensional parameters:

Fix:	Lewis number $L \equiv \frac{\kappa_C}{\kappa_T} \ll 1$	Prandtl number $P \equiv \frac{\nu}{\kappa_T} \gg 1.$
Vary:	Rayleigh number $R \equiv \frac{g\rho_T\Delta Th^3}{\nu\kappa_T}$	Separation ratio $S \equiv \frac{\rho_C\Delta C}{\rho_T\Delta T}$

Subtract conductive solution and nondimensionalize.

Governing Equations:

$$\partial_t \tilde{T} = \partial_x \tilde{\phi} + e_y \cdot (\nabla \tilde{\phi} \times \nabla \tilde{T}) + \nabla^2 \tilde{T}$$

$$\partial_t \tilde{C} = \partial_x \tilde{\phi} + e_y \cdot (\nabla \tilde{\phi} \times \nabla \tilde{C}) + L \nabla^2 \tilde{C}$$

$$\partial_t \nabla^2 \tilde{\phi} = PR \partial_x (\tilde{T} + S \tilde{C}) + e_y \cdot (\nabla \tilde{\phi} \times \nabla \nabla^2 \tilde{\phi}) + P \nabla^4 \tilde{\phi}$$

Linear Analysis:

$$\begin{Bmatrix} \tilde{T} \\ \tilde{C} \\ \tilde{\phi} \end{Bmatrix} (x, z, t) = \begin{Bmatrix} T \cos(kx) \\ C \cos(kx) \\ \phi \sin(kx) \end{Bmatrix} \sin(\pi z) e^{(k^2 + \pi^2)\sigma t}$$

Nonlinear interaction of these eigenmodes of the basic state

$$\nabla \phi \times \nabla \nabla^2 \phi = \nabla \phi \times \nabla (-k^2 - \pi^2) \phi = 0$$

$$\nabla \phi \times \nabla T = \phi T \frac{k\pi}{2} \sin(2\pi z)$$

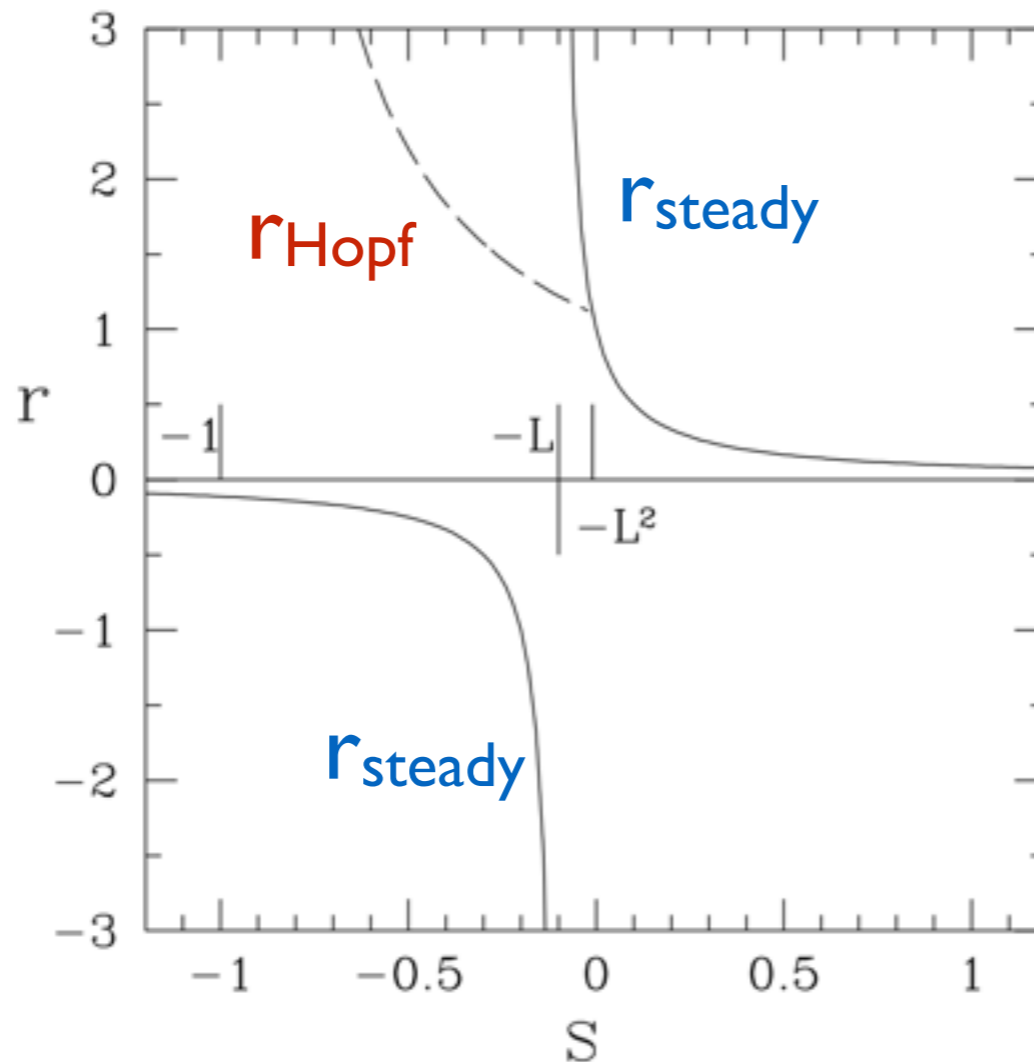
$$\nabla \phi \times \nabla C = \phi C \frac{k\pi}{2} \sin(2\pi z)$$

At lowest order, mean “flow” has $u = 0, T \neq 0, C \neq 0$

Hopf bifurcation to standing or traveling waves if separation ratio $S = Ra_C / Ra_T < 0$

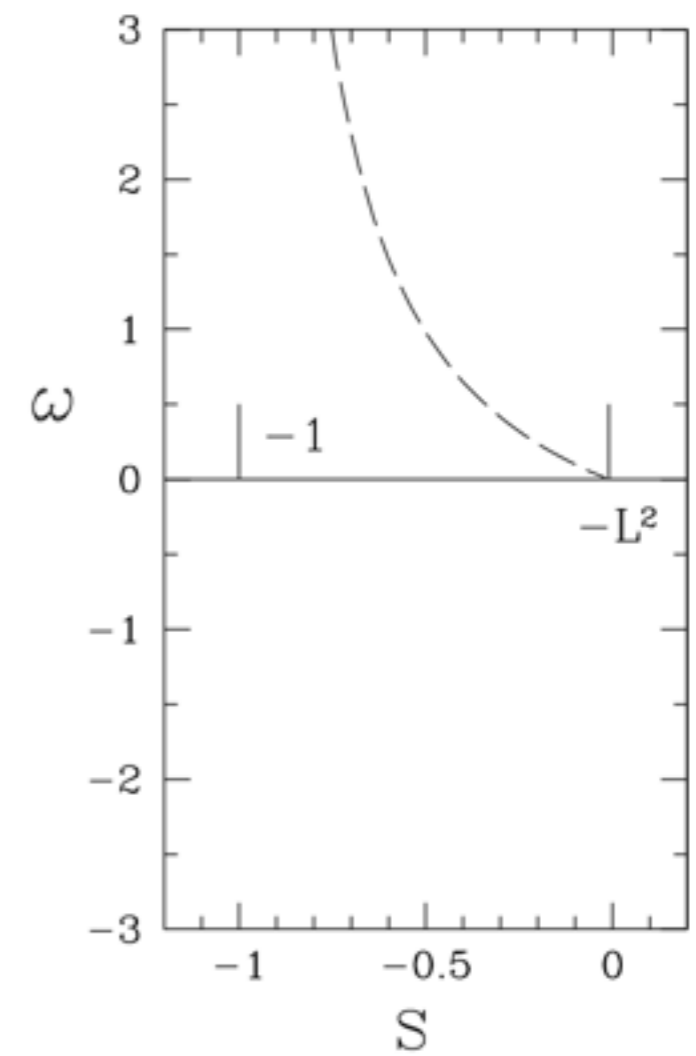
Temperature and concentration gradients are in opposite directions

convection threshold
(reduced Rayleigh number)



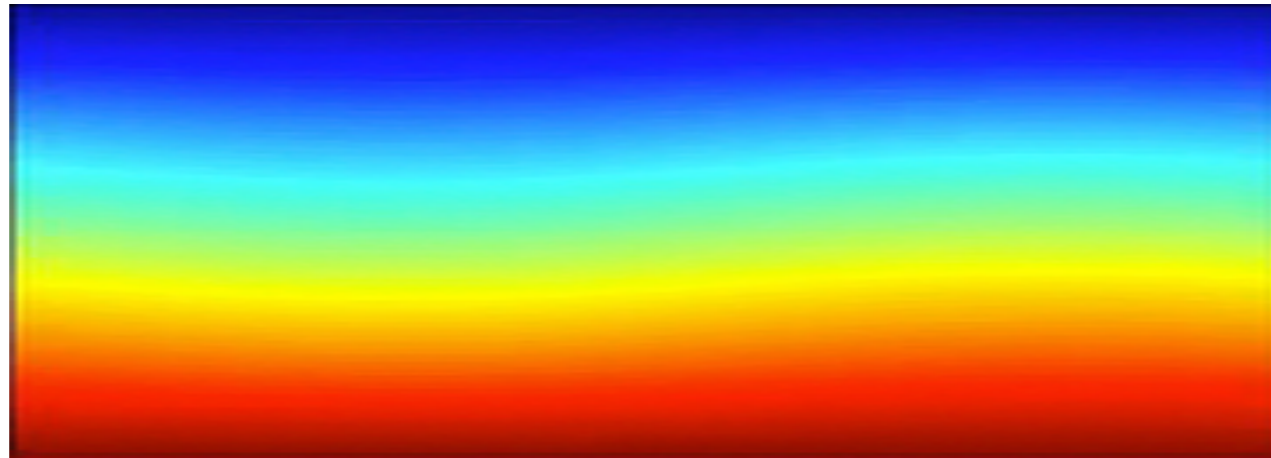
Separation ratio

Hopf frequency

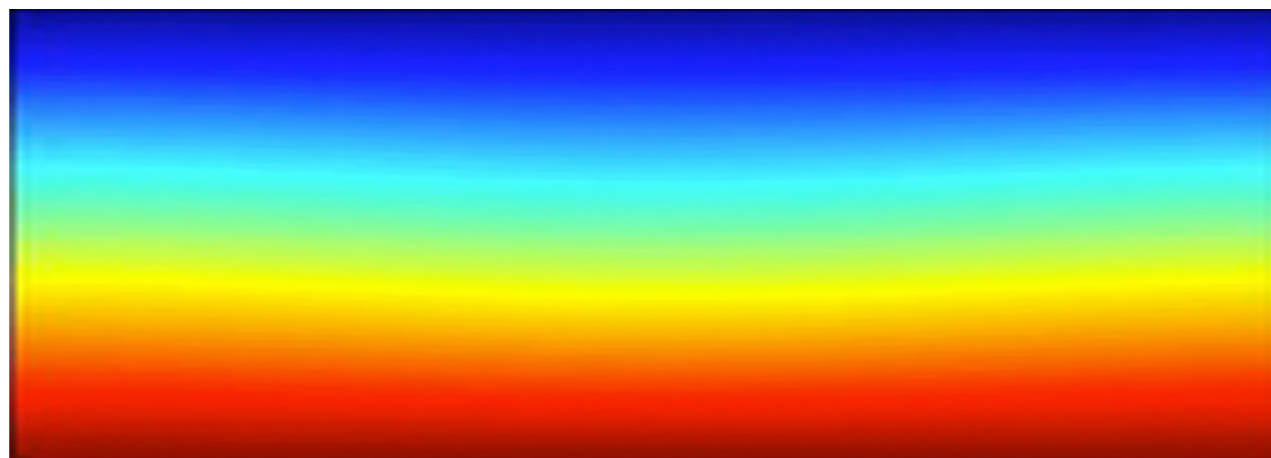


Separation ratio

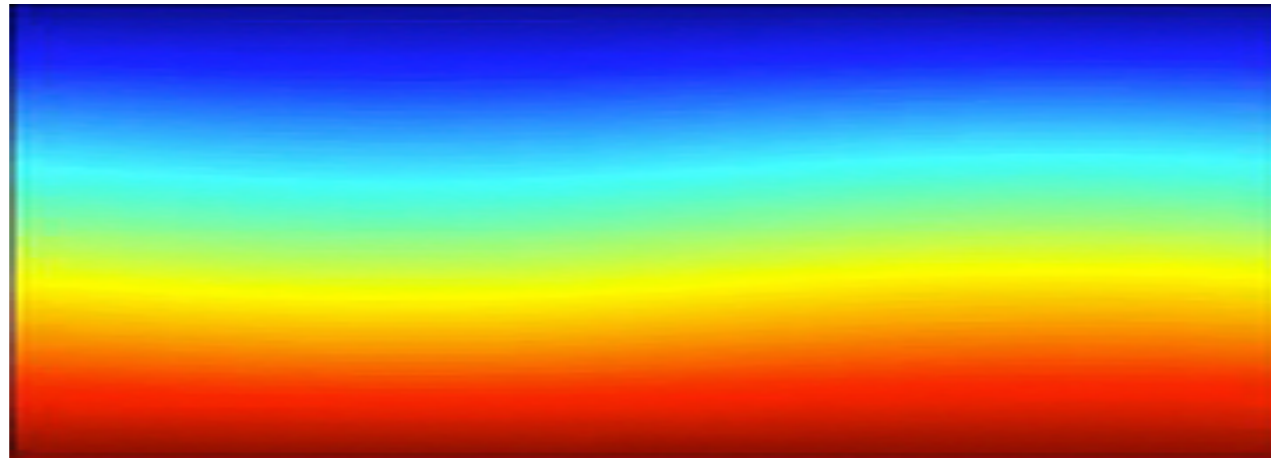
Traveling wave



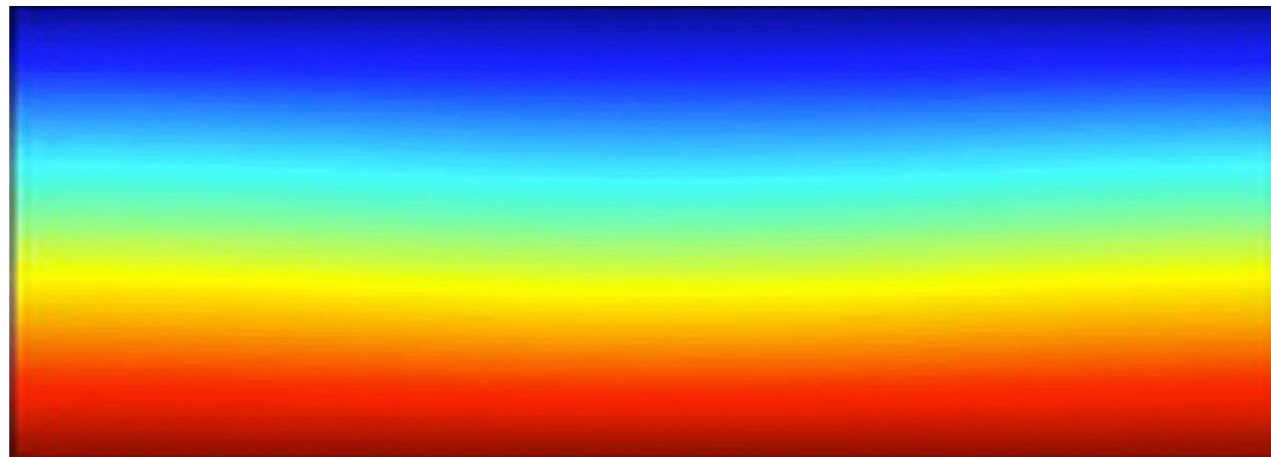
Standing wave



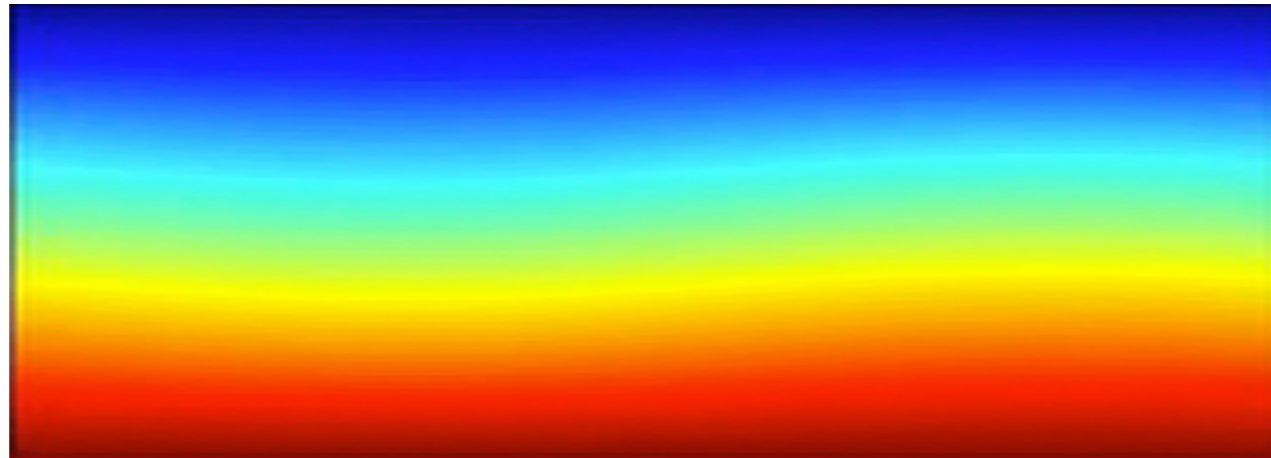
Traveling wave



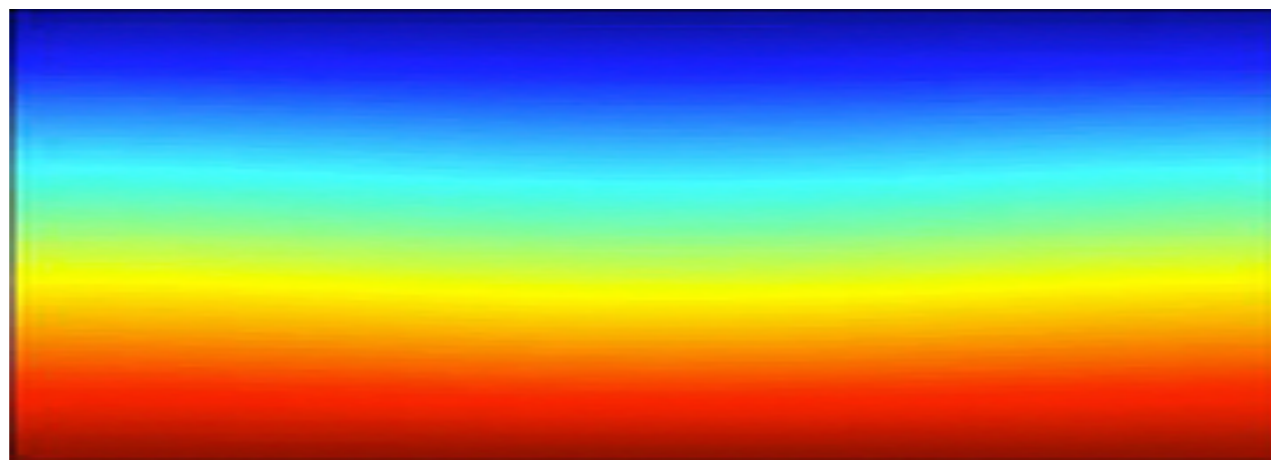
Standing wave



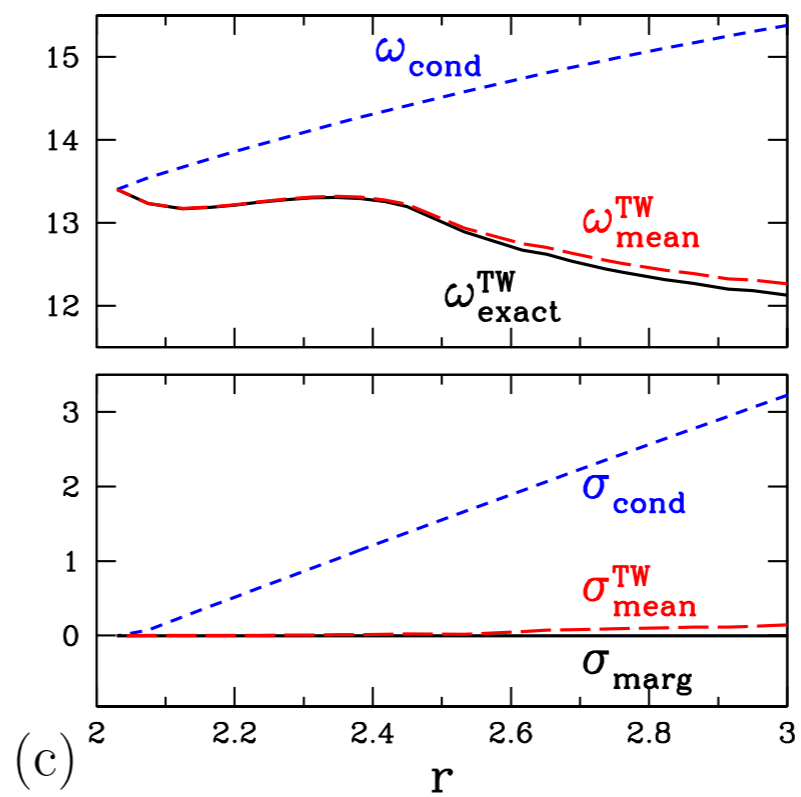
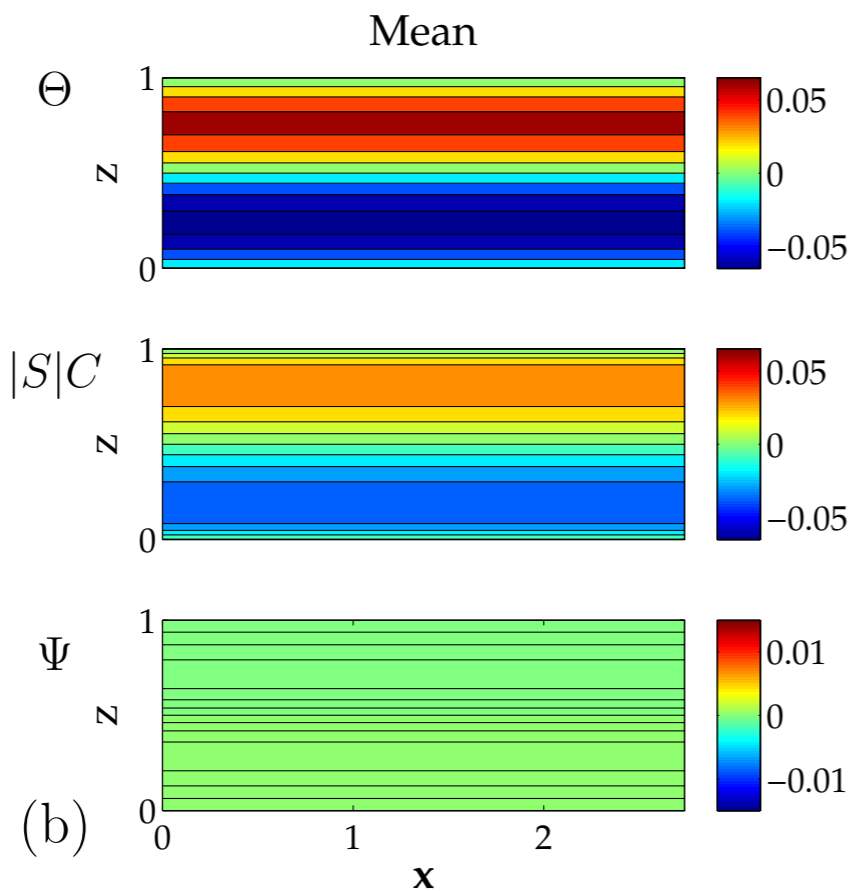
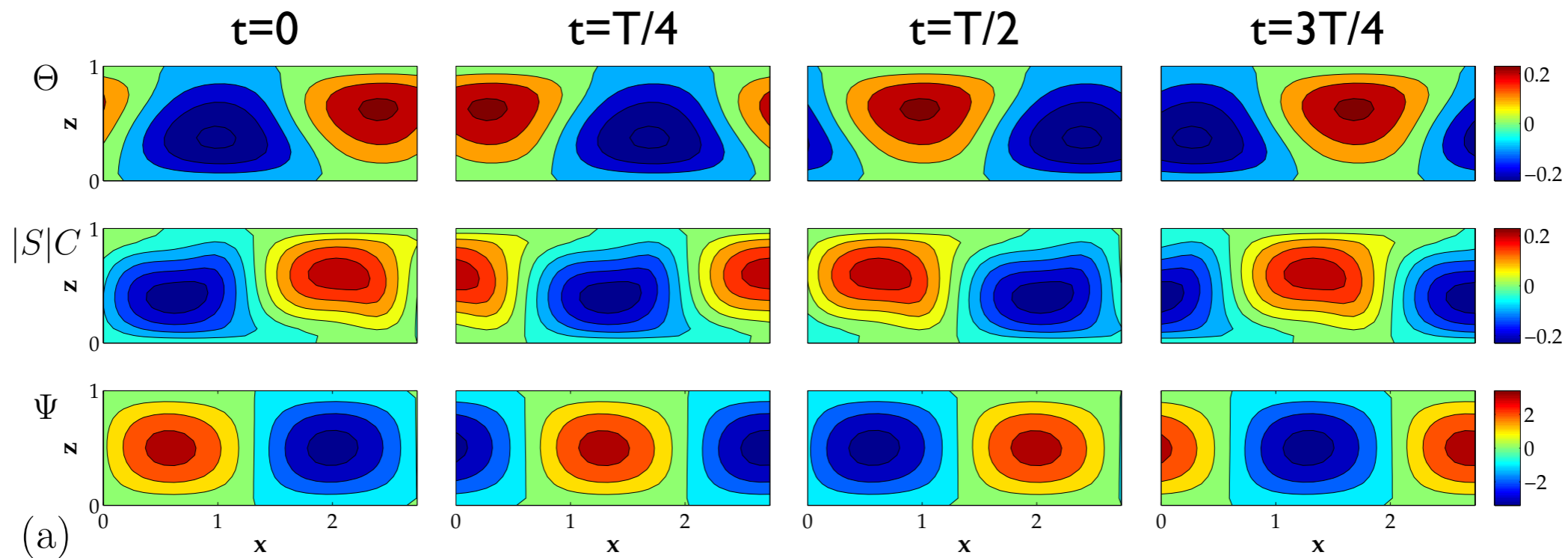
Traveling wave



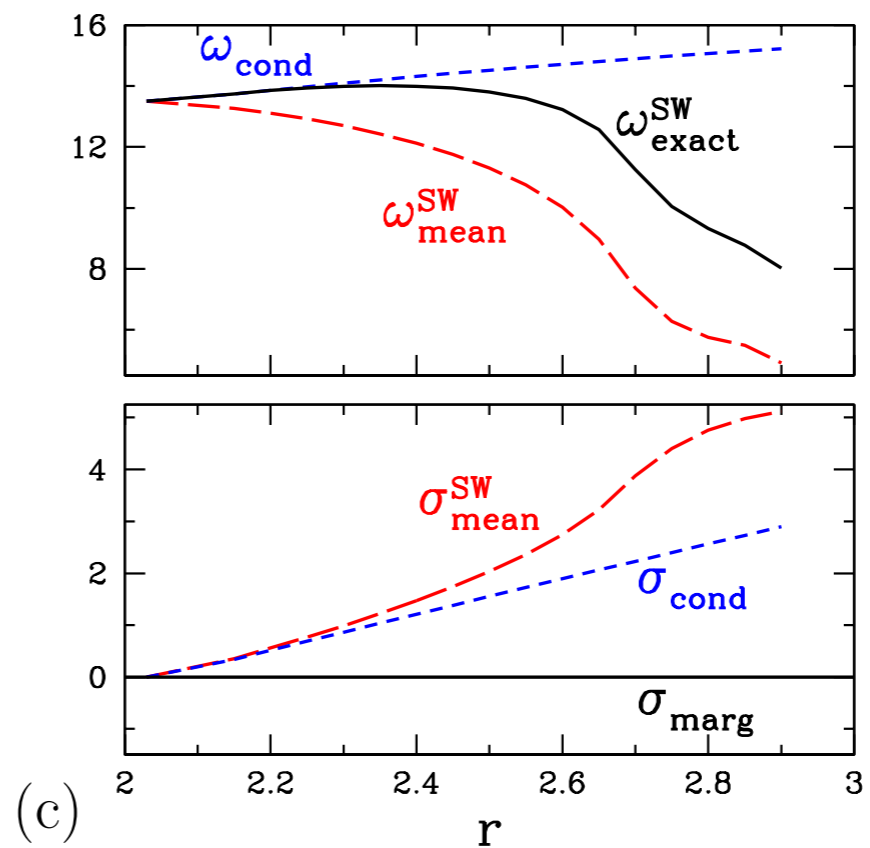
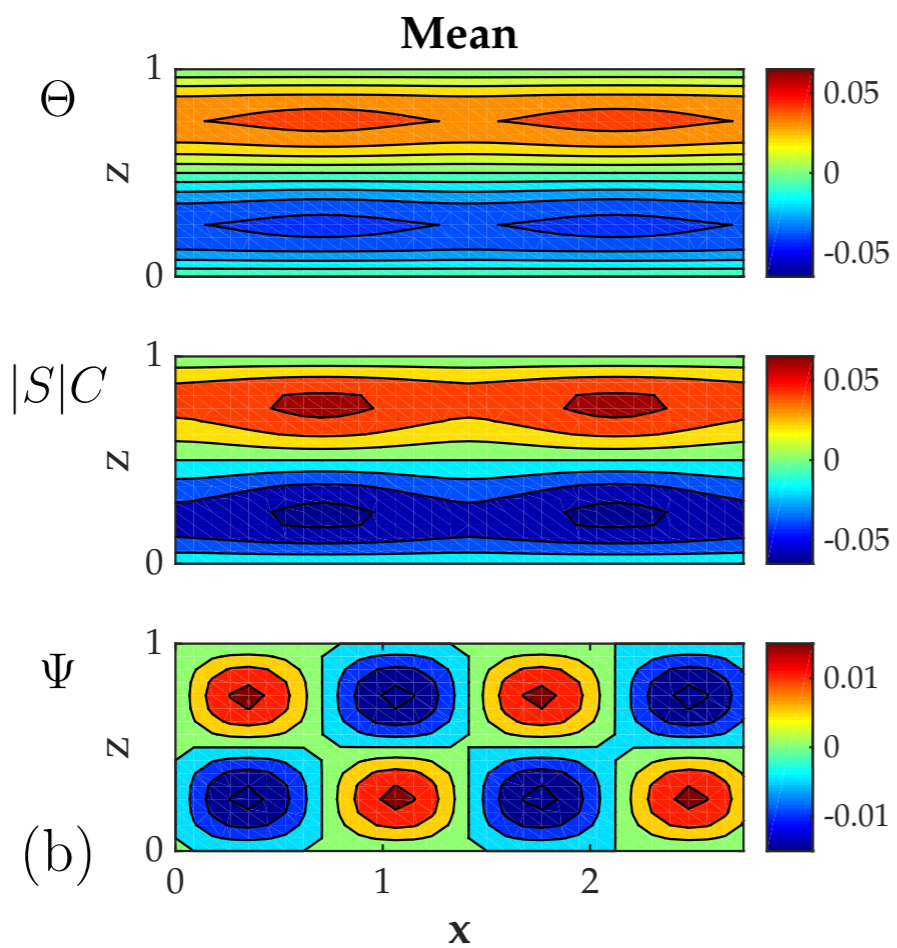
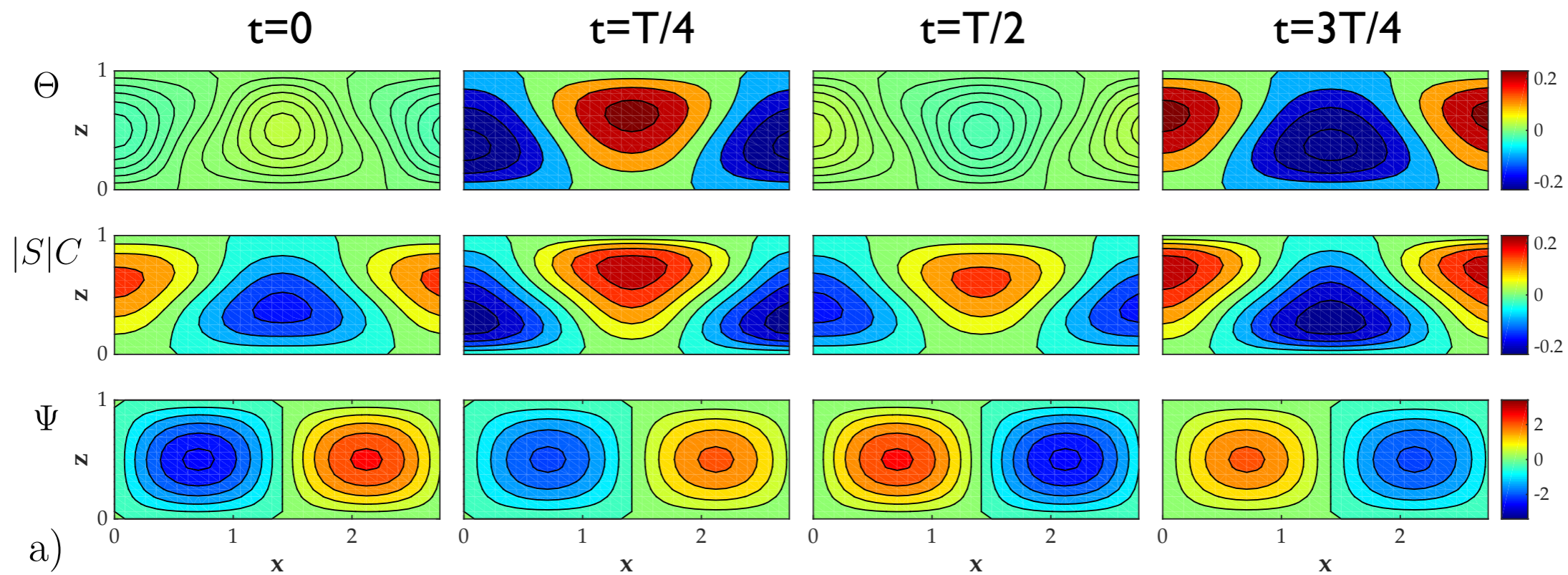
Standing wave



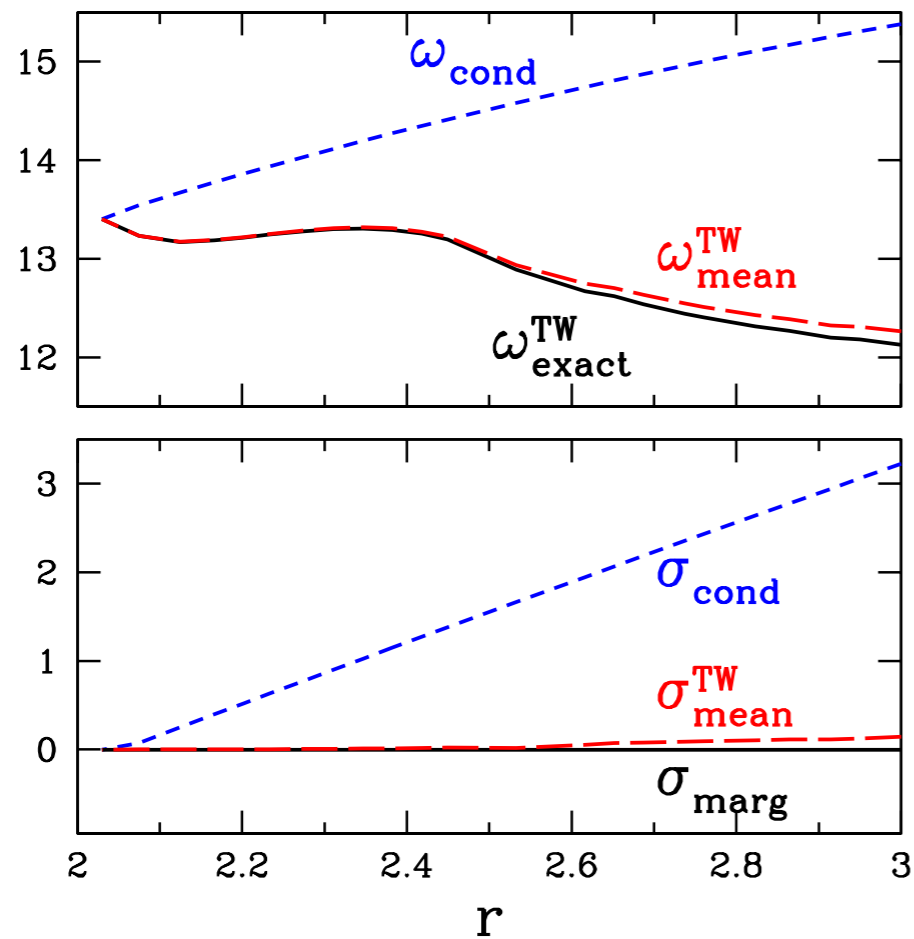
Traveling waves



Standing waves



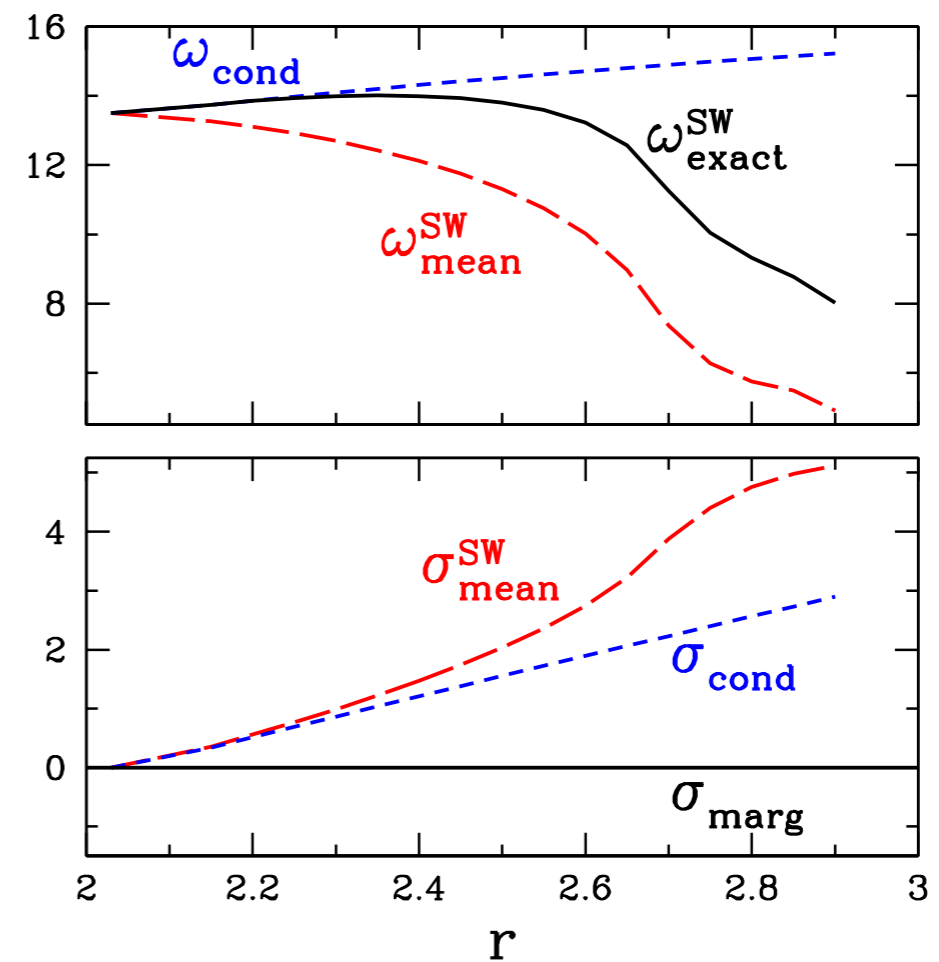
Traveling waves



mean = exact

RZIF

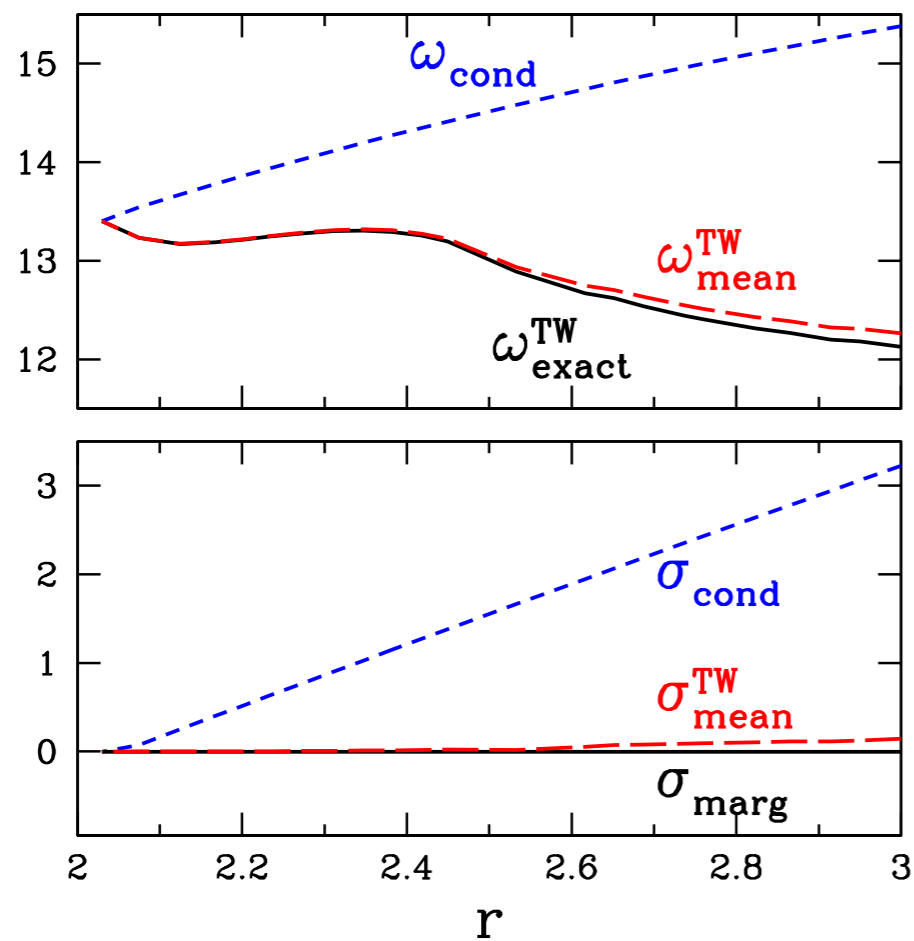
Standing waves



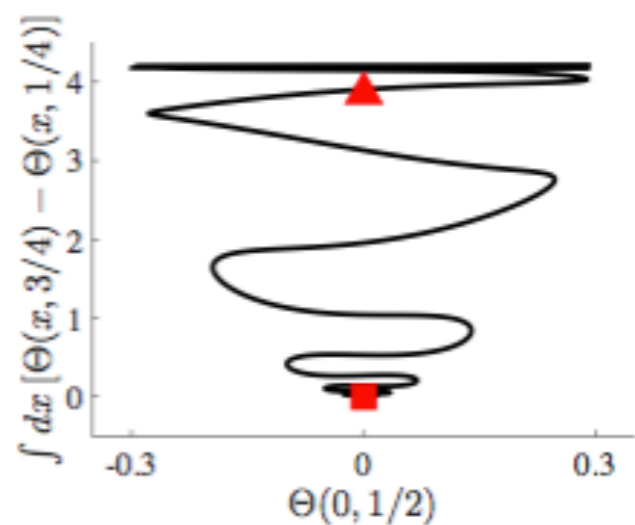
mean \neq exact

~~**RZIF**~~

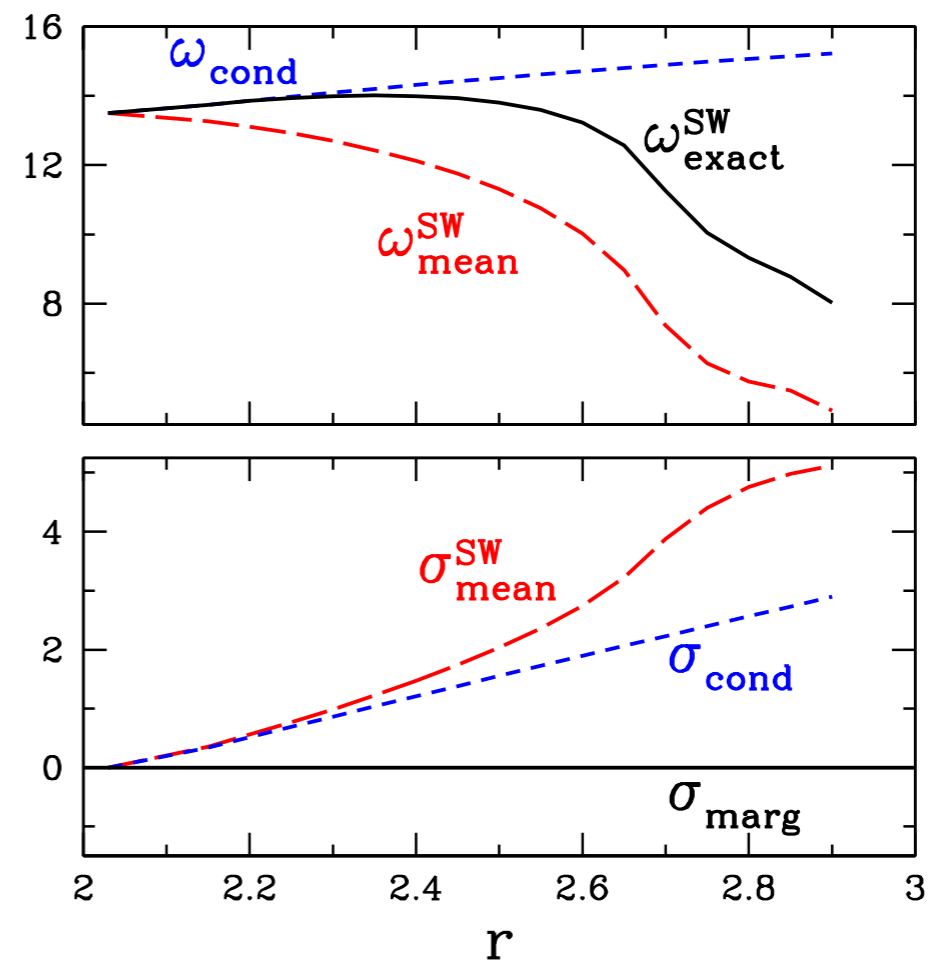
Traveling waves



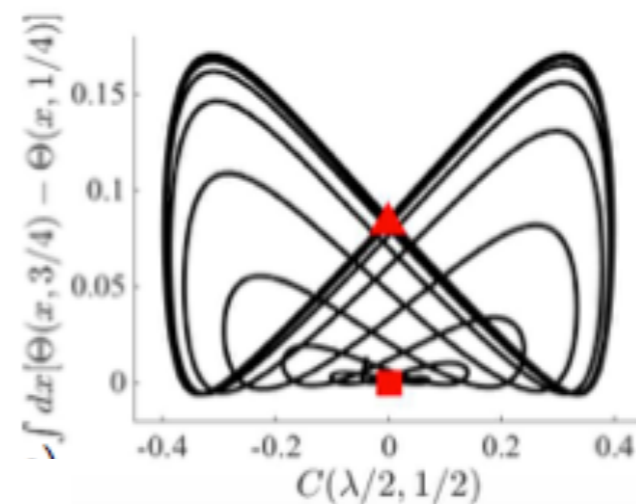
mean = exact



Standing waves



mean \neq exact



Evolution equation:

$$\partial_t \mathbf{U} = \mathcal{L}\mathbf{U} + \mathcal{N}(\mathbf{U}, \mathbf{U})$$

Temporal Fourier decomposition:

$$\mathbf{U} = \bar{\mathbf{U}} + \sum_{n \neq 0} \mathbf{u}_n e^{in\omega t}$$

Substitute into evolution equation

Component 0:

$$0 = \mathcal{L}\bar{\mathbf{U}} + \mathcal{N}(\bar{\mathbf{U}}, \bar{\mathbf{U}}) + \sum_{m \neq 0} \mathcal{N}(\mathbf{u}_m, \mathbf{u}_{-m})$$

Component 1:

$$i\omega \mathbf{u}_1 = \underbrace{\mathcal{L}\mathbf{u}_1 + \mathcal{N}(\bar{\mathbf{U}}, \mathbf{u}_1) + \mathcal{N}(\mathbf{u}_1, \bar{\mathbf{U}})}_{\mathcal{L}_{\bar{\mathbf{U}}}\mathbf{u}_1} + \underbrace{\mathcal{N}(\mathbf{u}_2, \mathbf{u}_{-1}) + \mathcal{N}(\mathbf{u}_{-1}, \mathbf{u}_2) + \dots}_{\text{small?}}$$

Evolution equation:

$$\partial_t \mathbf{U} = \mathcal{L}\mathbf{U} + \mathcal{N}(\mathbf{U}, \mathbf{U})$$

Temporal Fourier decomposition:

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$$\mathcal{N}_1$$

$\mathcal{N}(u_1, u_1)$ feeds u_2 $\mathcal{N}(u_1, u_{-1})$ feeds u_0

$\mathcal{N}_1 \equiv \mathcal{N}(u_2, u_{-1}) + \mathcal{N}(u_{-1}, u_2) + \dots$ feeds u_1

$$\|u_n\| \sim \epsilon^{|n|} \implies \mathcal{N}_1 \ll (i\omega - \mathcal{L}_{\bar{U}})u_1$$

Mean flow eigenvalue has **RZIF** property:

Real part is near **Zero**.

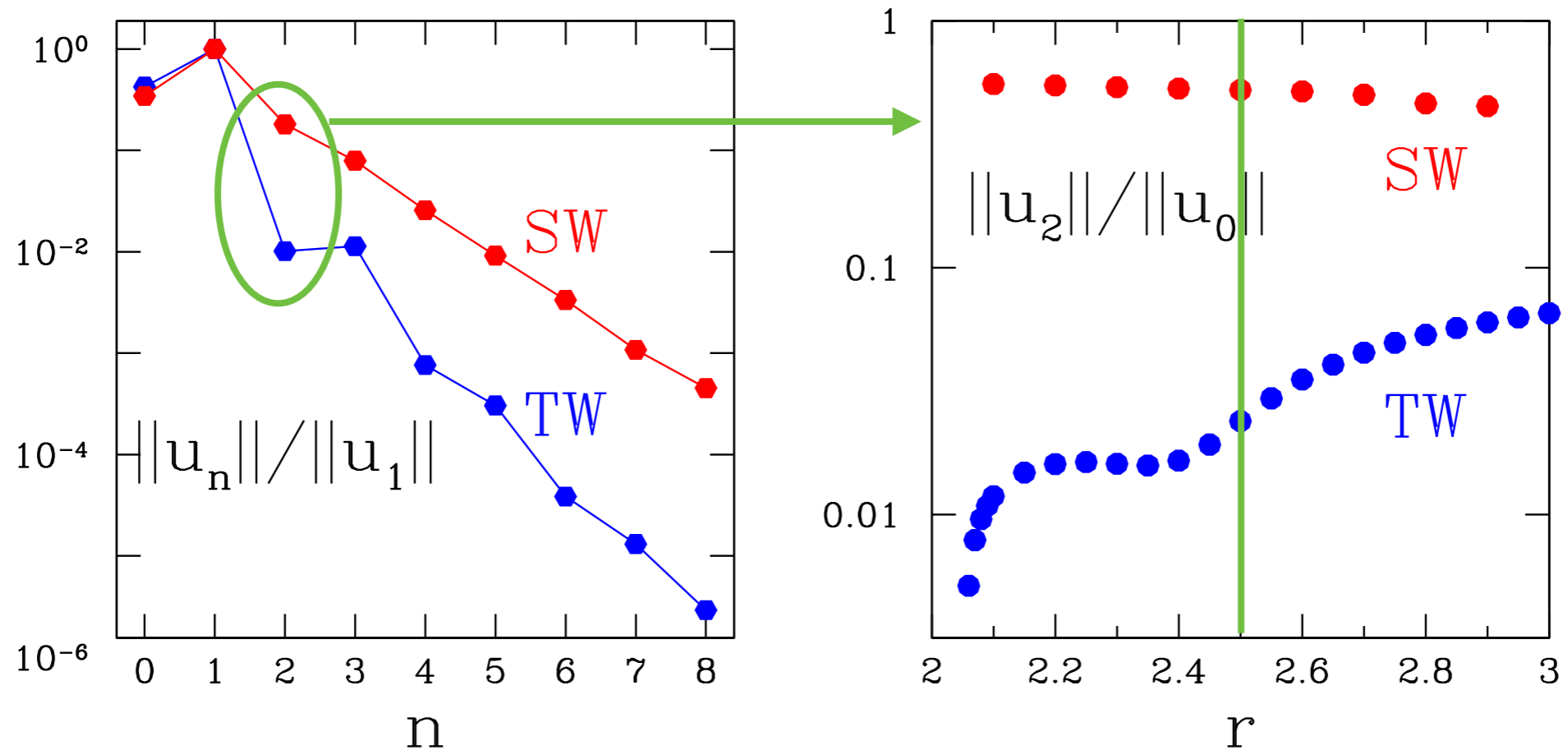
Imaginary part is near exact nonlinear **Frequency**.

Do **TW** generally have **highly peaked** temporal spectra?

Do **SW** generally have **broad** temporal spectra?

Yes!

temporal spectrum for $r=2.5$



And **WHY** do **TW** have **highly peaked** temporal spectra?

And **WHY** do **SW** have **broad** temporal spectra?

Traveling waves

(N. Périnet)

$$\psi = \psi_1 \sin(kx - \omega t) \sin \pi z$$

$$T = T_1 \sin(kx - \omega t + \Delta) \sin \pi z$$

$$\nabla \psi \times \nabla T = \frac{\pi k}{2} \psi_1 T_1 \boxed{\sin \Delta} \sin 2\pi z$$

mean flow generated by phase difference Δ between ψ and T

no generation of second temporal harmonic

Standing waves

$$\psi = \psi_1 \sin kx \sin \omega t \sin \pi z$$

$$T = T_1 \cos kx \cos(\omega t + \Delta) \sin \pi z$$

$$\nabla \psi \times \nabla T = \frac{\pi k}{4} \psi_1 T_1 \left[\boxed{\sin \Delta} + \boxed{\sin(2\omega t + \Delta)} \right] \sin 2\pi z$$

mean flow generated by phase difference Δ between ψ and T

generation of second temporal harmonic

Does this argument hold for other cases ?

\mathbf{u}_1 from temporal Fourier decomposition of DNS:

$$i\omega \mathbf{u}_1 = \mathcal{L}_{\bar{\mathbf{U}}} \mathbf{u}_1 + \mathcal{N}_1$$

\mathbf{u}_1 as eigenvector:

$$(\sigma + i\omega) \mathbf{u}_1 = \mathcal{L}_{\bar{\mathbf{U}}} \mathbf{u}_1$$

Back to purely hydrodynamic flow, e.g. cylinder wake

Traveling waves

$$\psi = |\psi_1| e^{i(kx - \omega t)} \sin \pi z + \text{c.c.}$$

$$\omega = -\nabla^2 \psi = (k^2 + \pi^2) \psi$$

$$\nabla \psi \times \nabla \omega = 0$$

no generation of mean flow

Standing waves

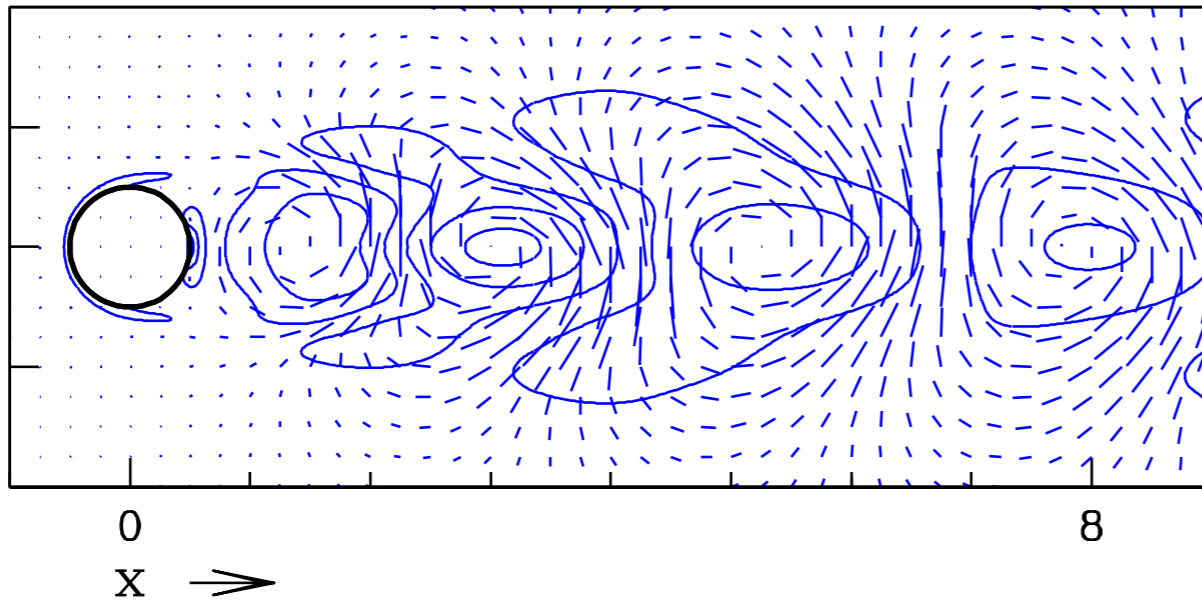
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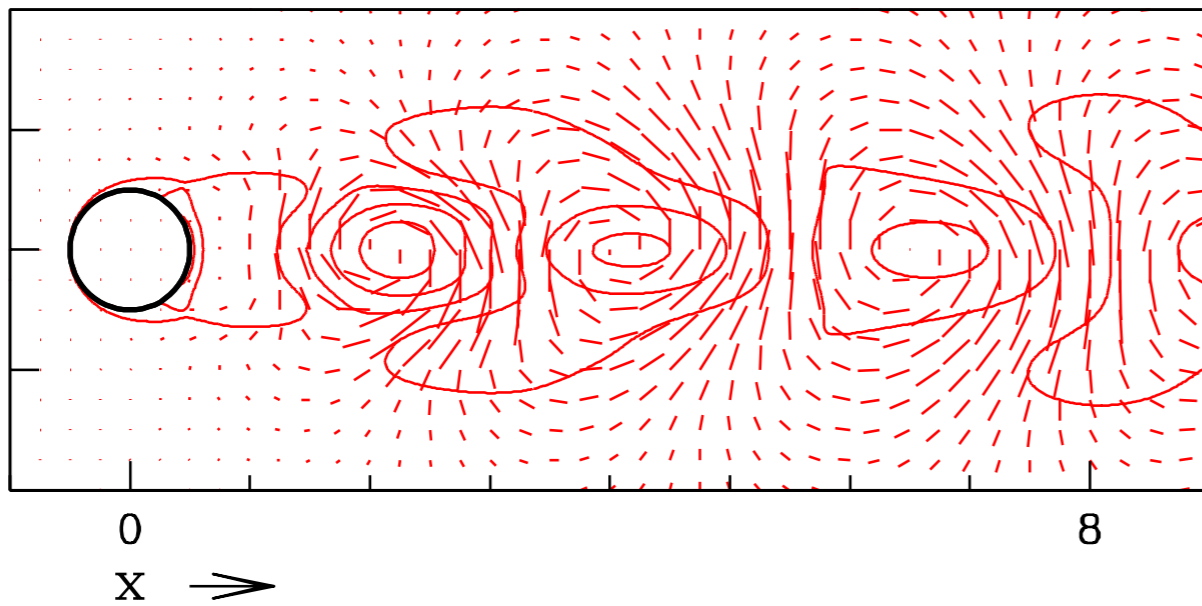
$$\nabla \psi \times \nabla \omega = 0$$

no generation of mean flow

Cylinder wake



$\nabla\psi_R \times \nabla\omega_R$ small



$\nabla\psi_I \times \nabla\omega_I$ small

Global stability of base and mean flows: a general approach and its applications to cylinder and open cavity flows

DENIS SIPP AND ANTON LEBEDEV

ONERA, 8 rue des Vertugadins, 92190 Meudon, France

Multiple scale expansion near Hopf threshold

$$Re^{-1} = Re_c^{-1} - \epsilon \quad U(t) = U_0 + \sqrt{\epsilon}U_1(t, t_1) + \epsilon U_2(t, t_1) + \epsilon\sqrt{\epsilon}U_3(t, t_1) + \dots$$

Asymptotic/numerical calculation of mean flow, limit cycle, eigenvectors, ...

Counter-example of open-cavity flow:
eigenvalues of mean flow do NOT predict the frequency.

Global stability of base and mean flows: a general approach and its applications to cylinder and open cavity flows

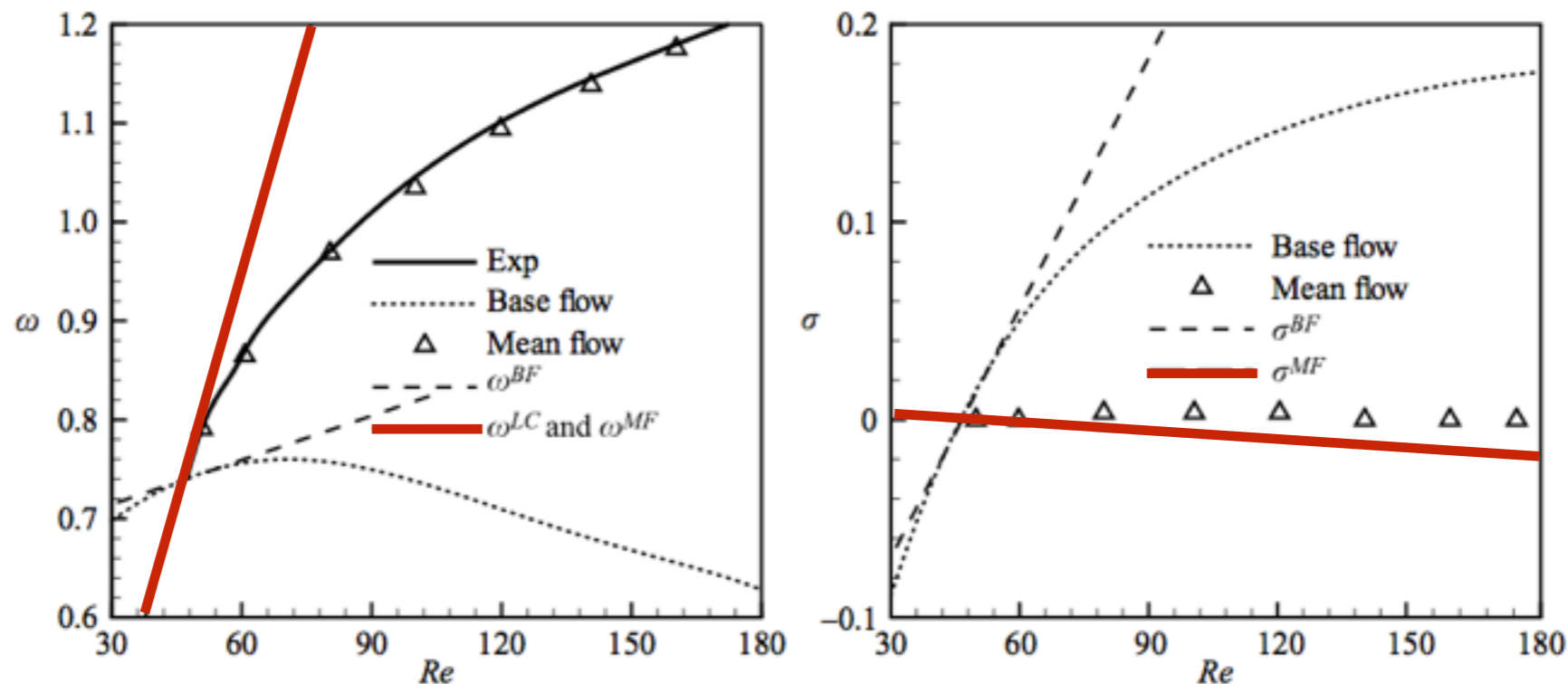
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Multiple scale expansion near Hopf threshold

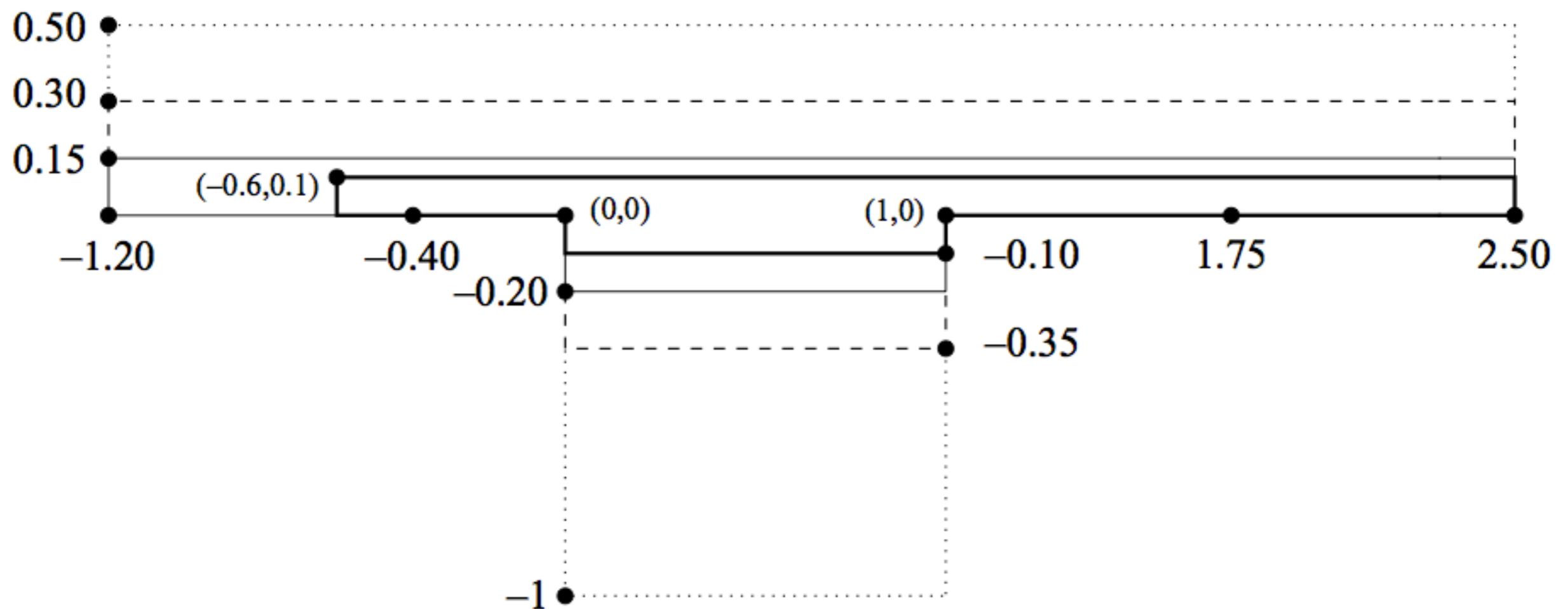
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Global stability of base and mean flows



**Global stability of base and mean flows:
a general approach and its applications to
cylinder and open cavity flows**

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Thermosolutal

Open flows

Traveling waves

OK

Cylinder wake

OK

Standing waves

NO

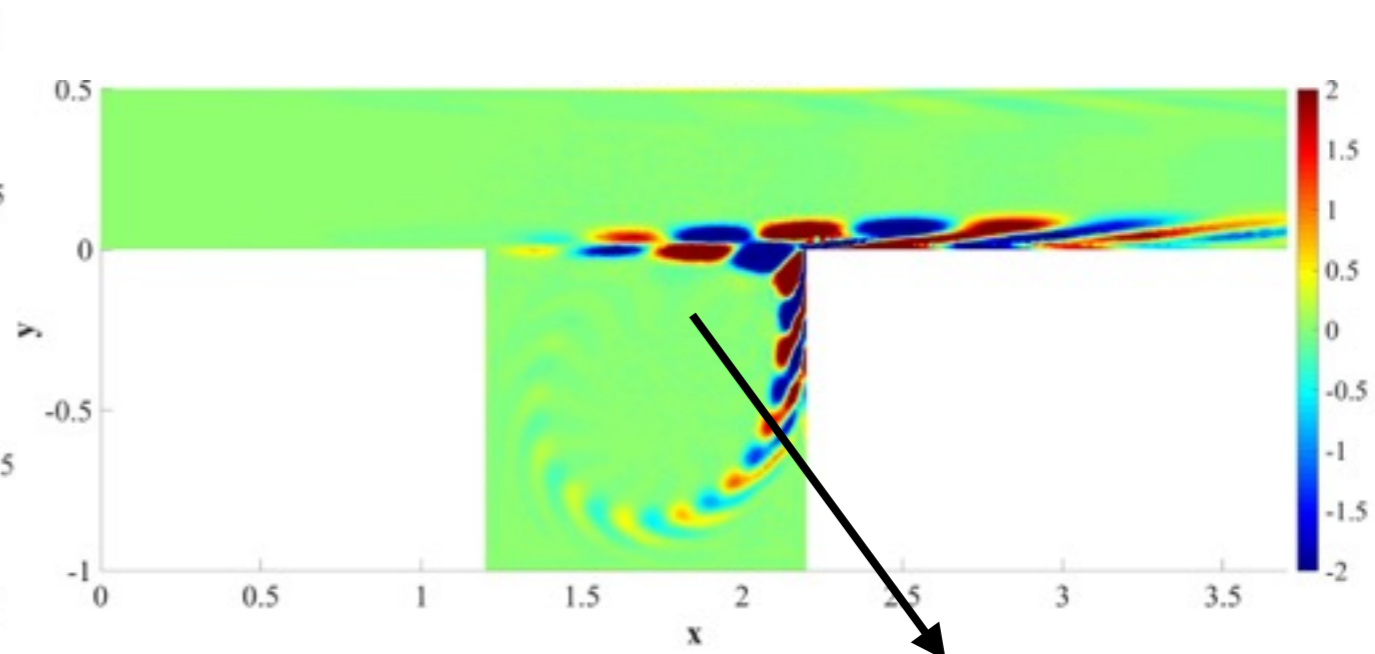
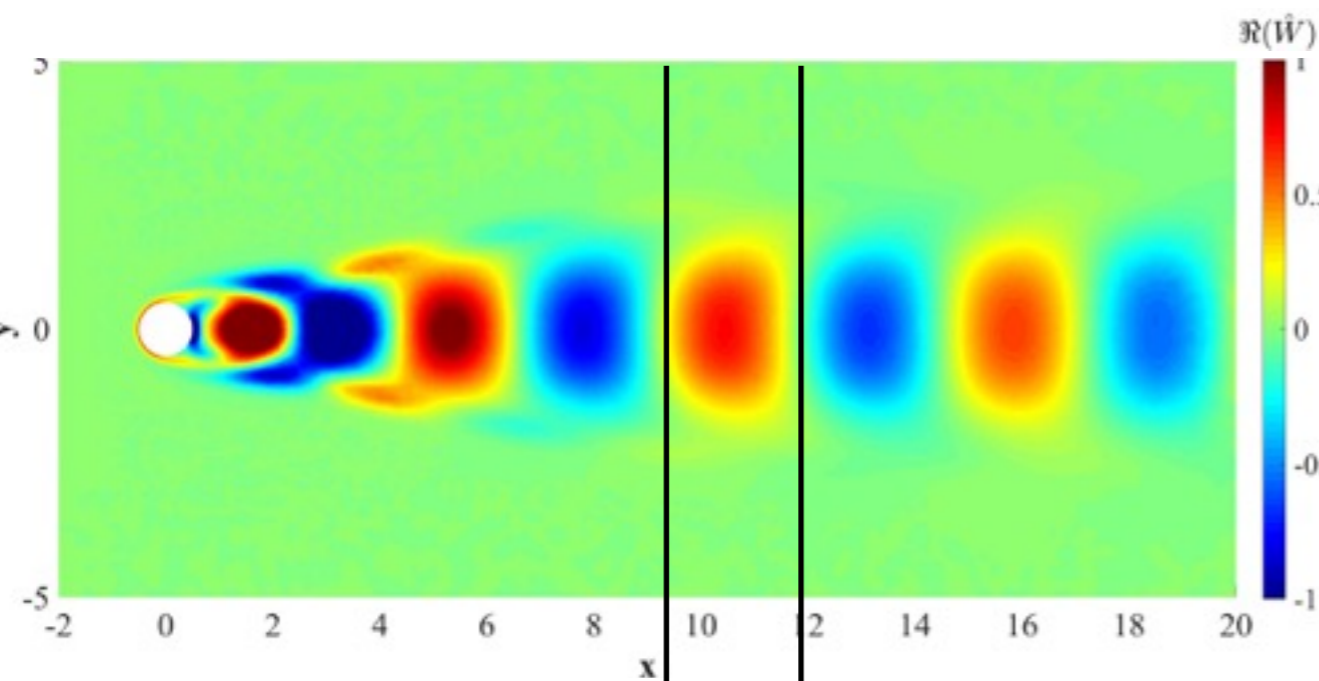
Open cavity

NO

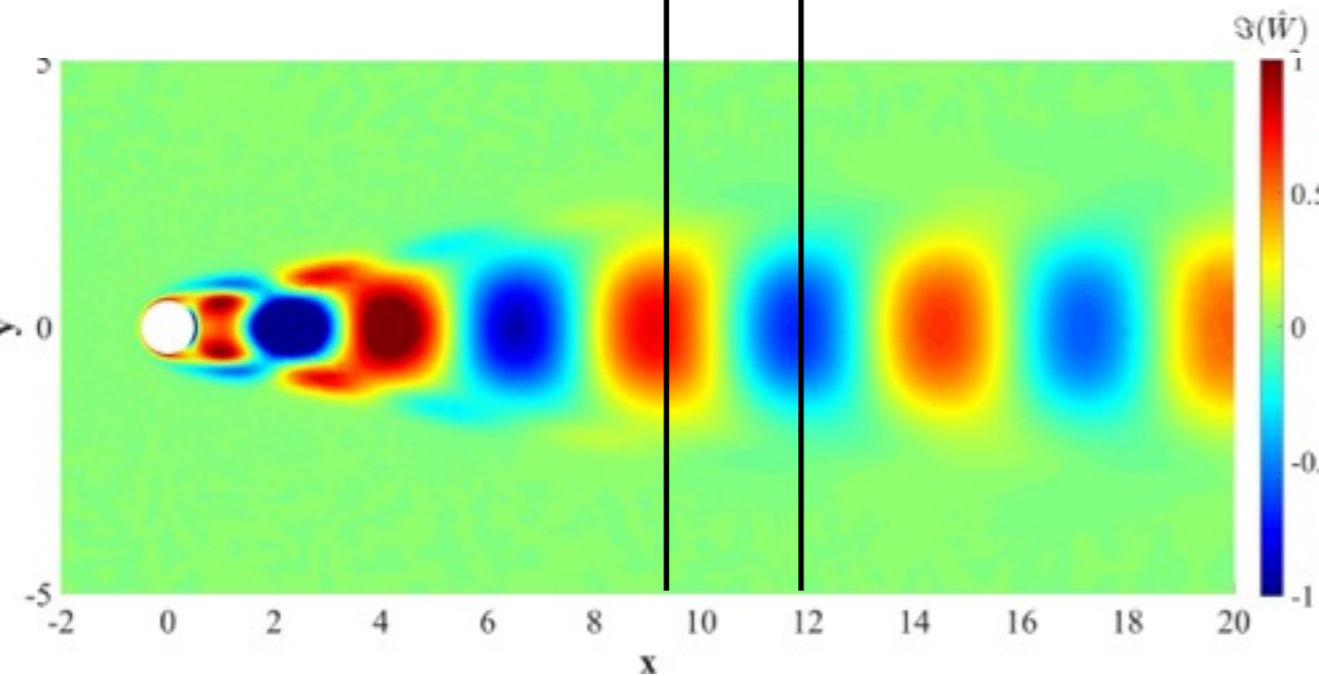
Is there an analogy between the

Cylinder wake with TW and open cavity with SW ????

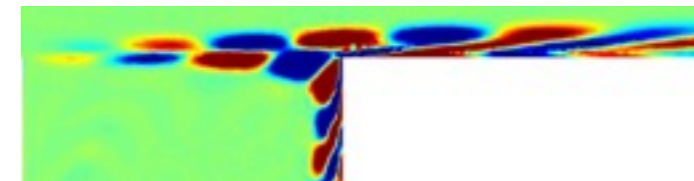
Real part of u_1



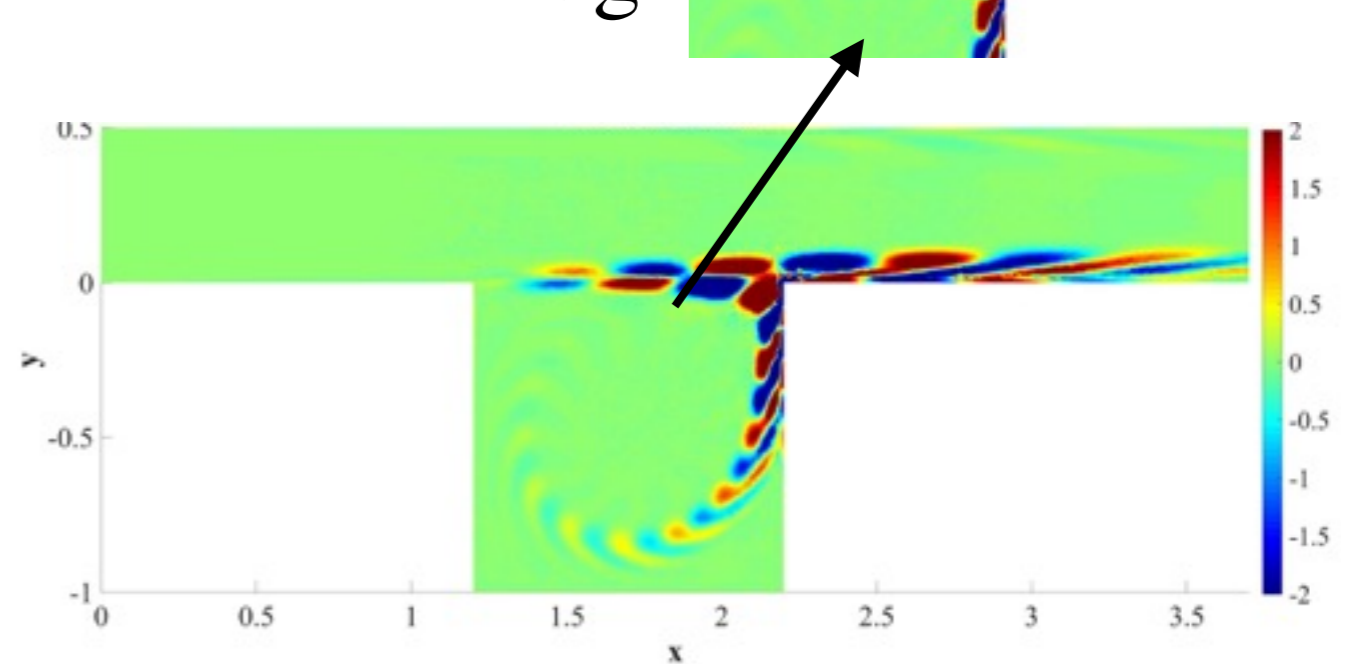
Imaginary part of u_1



Real



Imag

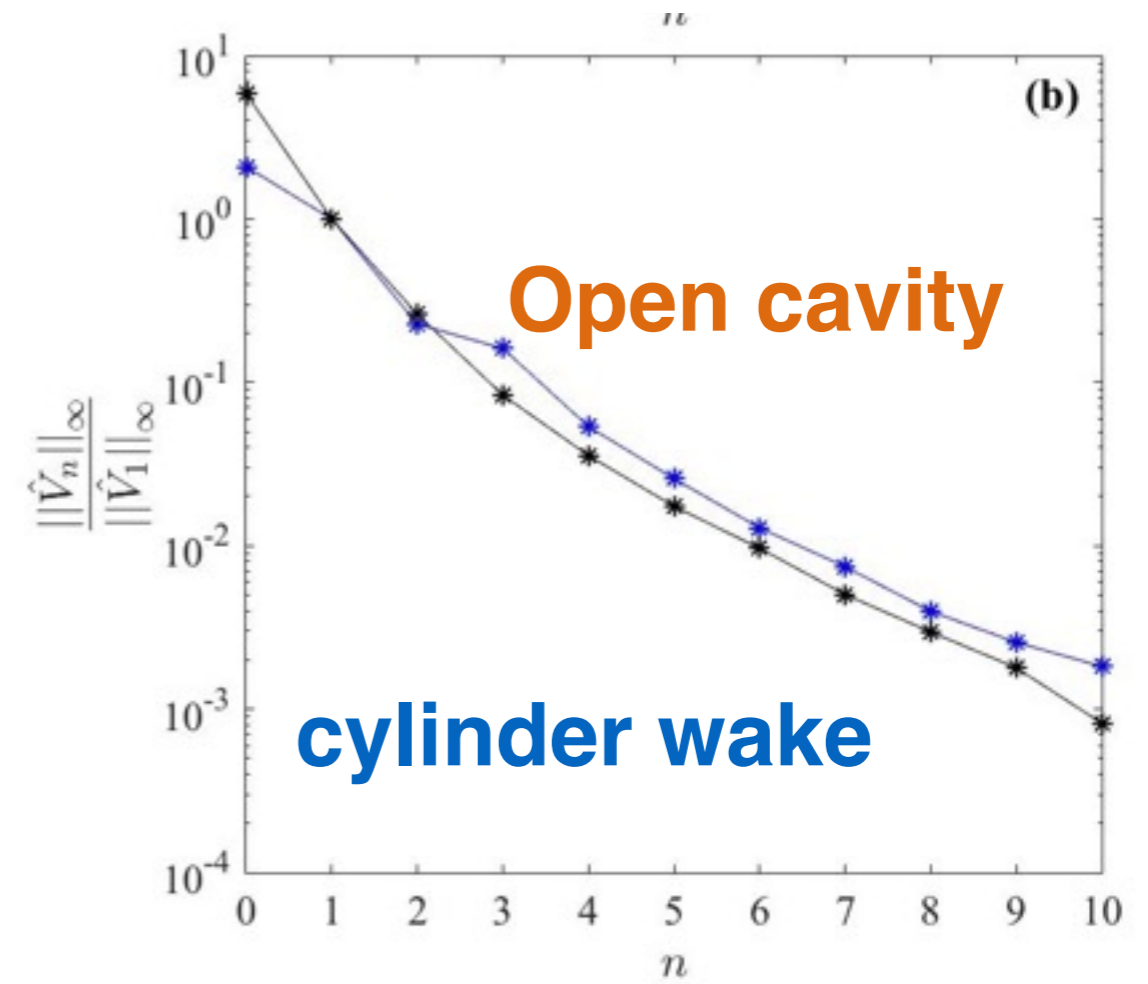
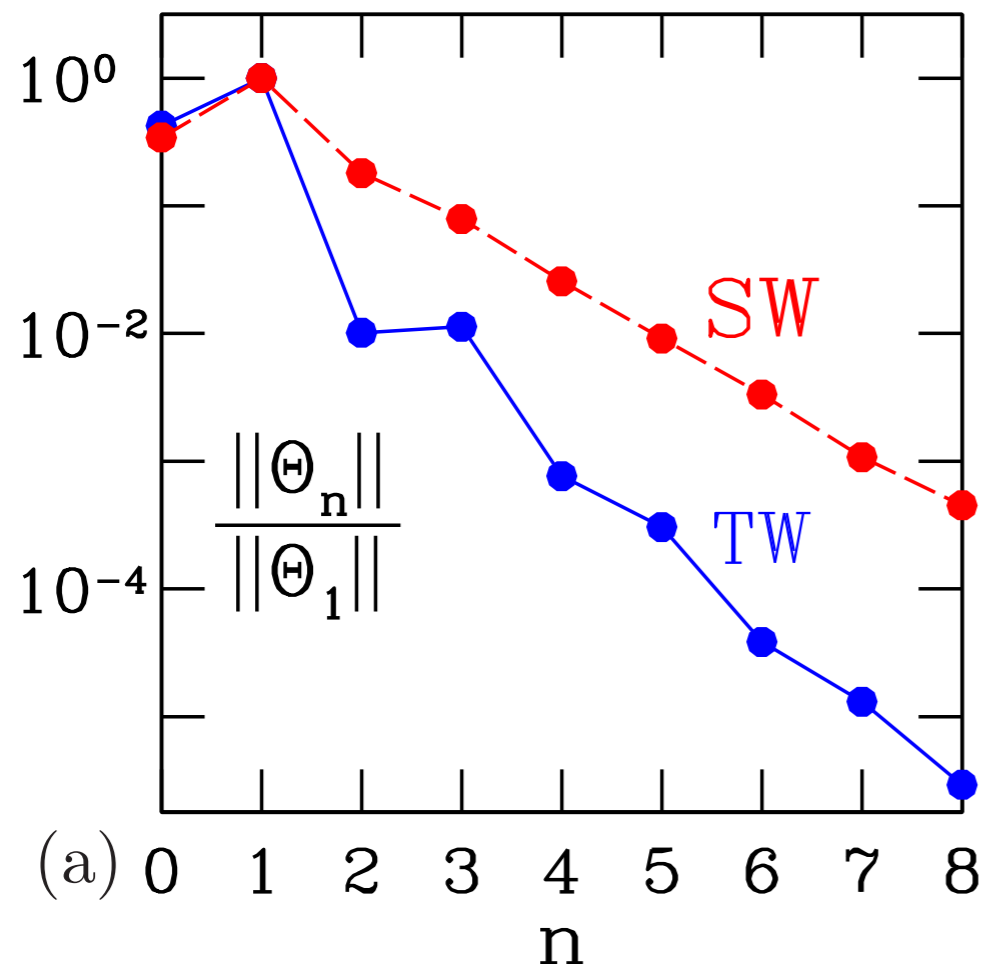


Traveling wave behavior :
real and imaginary parts are $L_x/4$ out of phase

Thermosolutal

Open flows

Spectrum normalized by the first harmonic



↑
Similar spectrum !!!

Self-Consistent Mean Flow Description of the Nonlinear Saturation of the Vortex Shedding in the Cylinder Wake

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(Received 19 December 2013; published 20 August 2014)

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doi:10.1017/jfm.2016.109

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Self-consistent model for the saturation mechanism of the response to harmonic forcing in the backward-facing step flow

V. Mantič-Lugo^{1,†} and F. Gallaire¹

J. Fluid Mech. (2016), vol. 800, pp. 327–357. © Cambridge University Press 2016
doi:10.1017/jfm.2016.390

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A self-consistent formulation for the sensitivity analysis of finite-amplitude vortex shedding in the cylinder wake

P. Meliga^{1,†}, E. Boujo^{2,‡} and F. Gallaire²

PHYSICS OF FLUIDS 27, 074103 (2015)

A self-consistent model for the saturation dynamics of the vortex shedding around the mean flow in the unstable cylinder wake

Vladislav Mantič-Lugo,^{1,a)} Cristóbal Arratia,^{1,2,b)} and François Gallaire^{1,c)}

Evolution equation:

$$\partial_t \mathbf{U} = \mathcal{L}\mathbf{U} + \mathcal{N}(\mathbf{U}, \mathbf{U})$$

Temporal Fourier decomposition:

$$\mathbf{U} = \bar{\mathbf{U}} + \sum_{n \neq 0} \mathbf{u}_n e^{in\omega t}$$

Substitute into evolution equation

Component 0:

$$0 = \mathcal{L}\bar{\mathbf{U}} + \mathcal{N}(\bar{\mathbf{U}}, \bar{\mathbf{U}}) + \sum_{m \neq 0} \mathcal{N}(\mathbf{u}_m, \mathbf{u}_{-m})$$

Component 1:

$$i\omega \mathbf{u}_1 = \underbrace{\mathcal{L}\mathbf{u}_1 + \mathcal{N}(\bar{\mathbf{U}}, \mathbf{u}_1) + \mathcal{N}(\mathbf{u}_1, \bar{\mathbf{U}})}_{\mathcal{L}_{\bar{\mathbf{U}}}\mathbf{u}_1} + \mathcal{N}_1$$

Self-Consistent Mean Flow Description of the Nonlinear Saturation of the Vortex Shedding in the Cylinder Wake

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Laboratory of Fluid Mechanics and Instabilities, École Polytechnique Fédérale de Lausanne, EPFL-STI-IGM-LFMI, Lausanne CH-1015, Switzerland

(Received 19 December 2013; published 20 August 2014)

Mean flows without time integration:

$$0 = \mathcal{L}\bar{\mathbf{U}} + \mathcal{N}(\bar{\mathbf{U}}, \bar{\mathbf{U}}) + \sum_{m \neq 0} \mathcal{N}(\mathbf{u}_m, \mathbf{u}_{-m}) \rightarrow \mathcal{N}(\mathbf{u}_1, \mathbf{u}_{-1})$$

Solve for $\bar{\mathbf{U}}$ with Newton's method

$$(\sigma + i\omega)\mathbf{u}_1 = \mathcal{L}_{\bar{\mathbf{U}}}\mathbf{u}_1 + \mathcal{N}_1 \quad \|\mathbf{u}_1\| = A$$

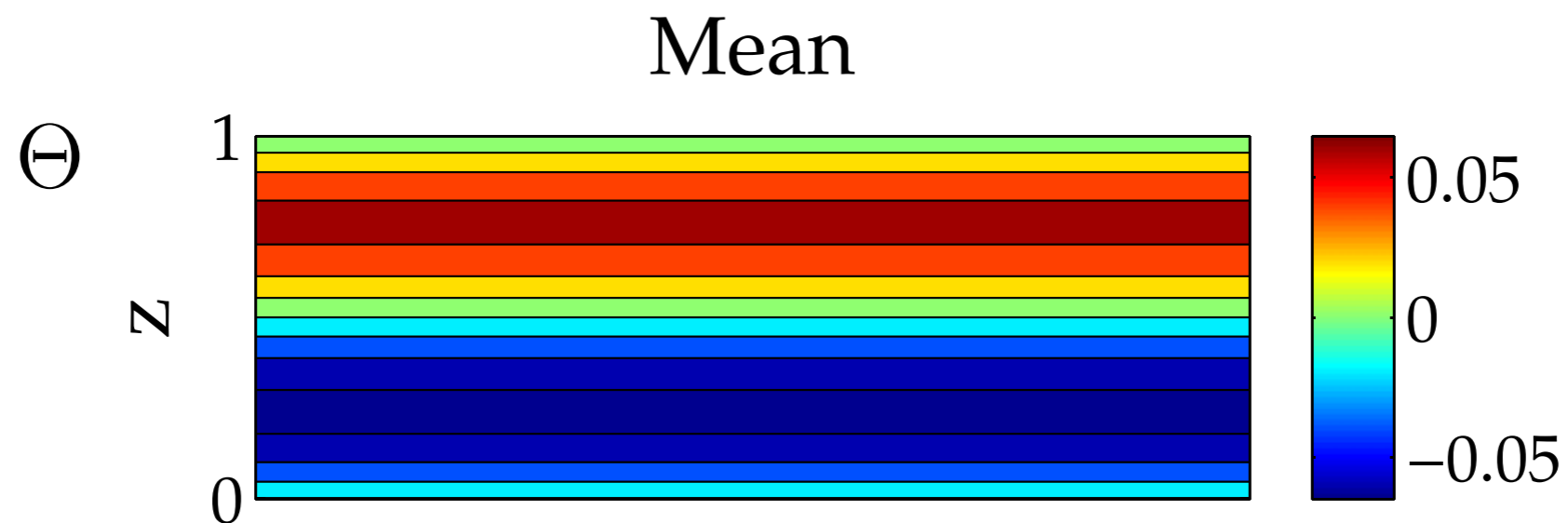
Solve for $(\mathbf{u}_1, \sigma, \omega)$ by diagonalisation

Find A such that $\sigma = 0$

Yields almost exact $\bar{\mathbf{U}}, \mathbf{u}_1, \omega$!

Thermosolutal in x-homogeneous domain :

Mean flow of TW is independent of x



$$0 = \mathcal{L}\bar{U} + \cancel{\mathcal{N}(\bar{U}, \bar{U})} + \mathcal{N}(u_1, u_{-1})$$

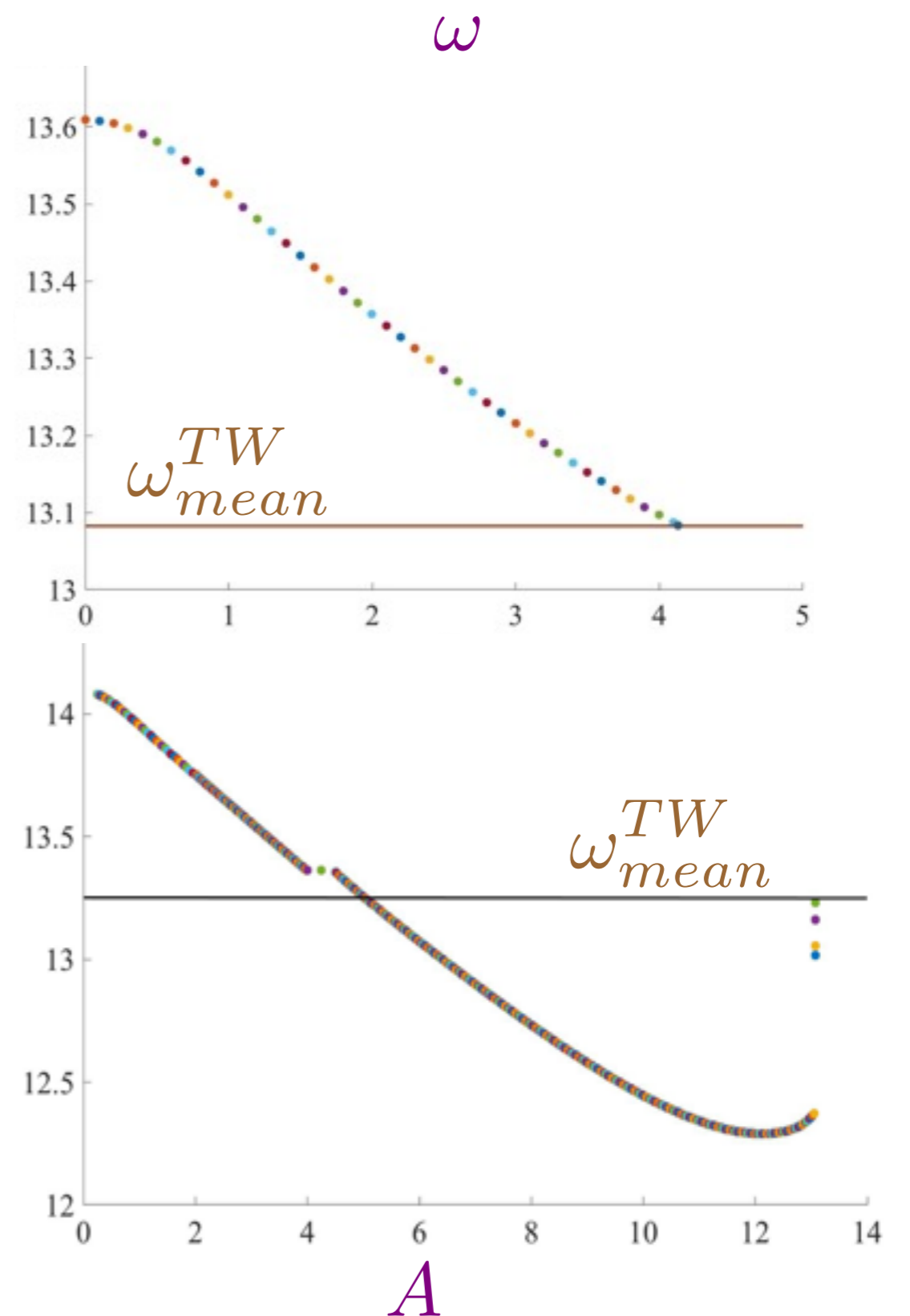
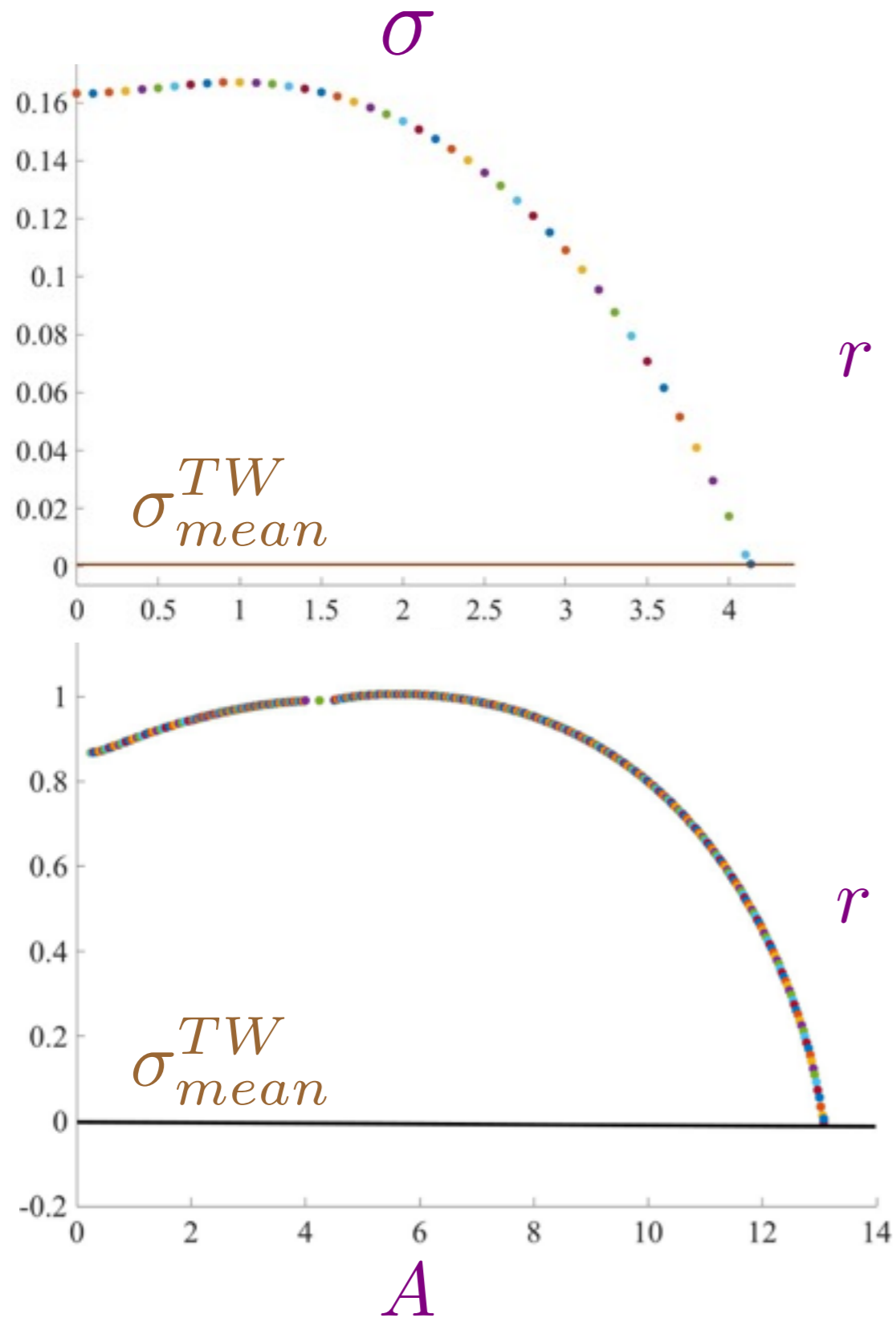
$$\bar{U}(z) = -\mathcal{L}^{-1}\mathcal{N}(u_1, u_{-1})$$

$$= -\partial_{zz}^{-1}\mathcal{N}(u_1, u_{-1})$$

~~Newton~~ \longrightarrow just invert Laplacian

\longrightarrow just invert ∂_{zz}

Convergence of SCM equations



Resolvent Analysis

McKeon & Sharma, JFM 2010

$$i\omega \mathbf{u}_1 = \mathcal{L}_{\bar{U}} \mathbf{u}_1 + \mathcal{N}_1$$

$$\mathbf{u}_1 = (i\omega - \mathcal{L}_{\bar{U}})^{-1} \mathcal{N}_1 \equiv \mathcal{R}(\omega) \mathcal{N}_1$$

More generally: $\mathbf{u}(\omega) = \mathcal{R}(\omega) \mathcal{N}(\omega)$

Singular value decomposition: $\mathcal{R}(\omega) \phi_j(\mathbf{x}, \omega) = \mu_j(\omega) \psi_j(\mathbf{x}, \omega)$

If resolvent has a highly dominant singular value μ_{dom} ,

then \mathcal{R} extracts and amplifies the component of mode ϕ_{dom} in \mathcal{N}

Independent of the details of \mathcal{N}

$$\mathbf{u} = \mathcal{R}(\omega) \sum_j \langle \mathcal{N}, \phi_j \rangle \phi_j = \sum_j \langle \mathcal{N}, \phi_j \rangle \mu_j \psi_j \approx \langle \mathcal{N}, \phi_{\text{dom}} \rangle \mu_{\text{dom}} \psi_{\text{dom}}$$

$$\mathbf{u}(\mathbf{x}, \omega) \approx \underbrace{\langle \mathcal{N}, \phi_{\text{dom}} \rangle(\omega) \mu_{\text{dom}}(\omega)}_{\text{scalar amplitude } \Lambda(\omega)} \underbrace{\psi_{\text{dom}}(\mathbf{x}, \omega)}_{\text{spatial dependence}}$$

Conditions for validity of mean flow stability analysis

Samir Beneddine^{1,†}, Denis Sipp¹, Anthony Arnault², Julien Dandois² and
Lutz Lesshafft³

Fully turbulent flow with broad spectrum,
rather than periodic flow with only $\omega, 2\omega, \dots$

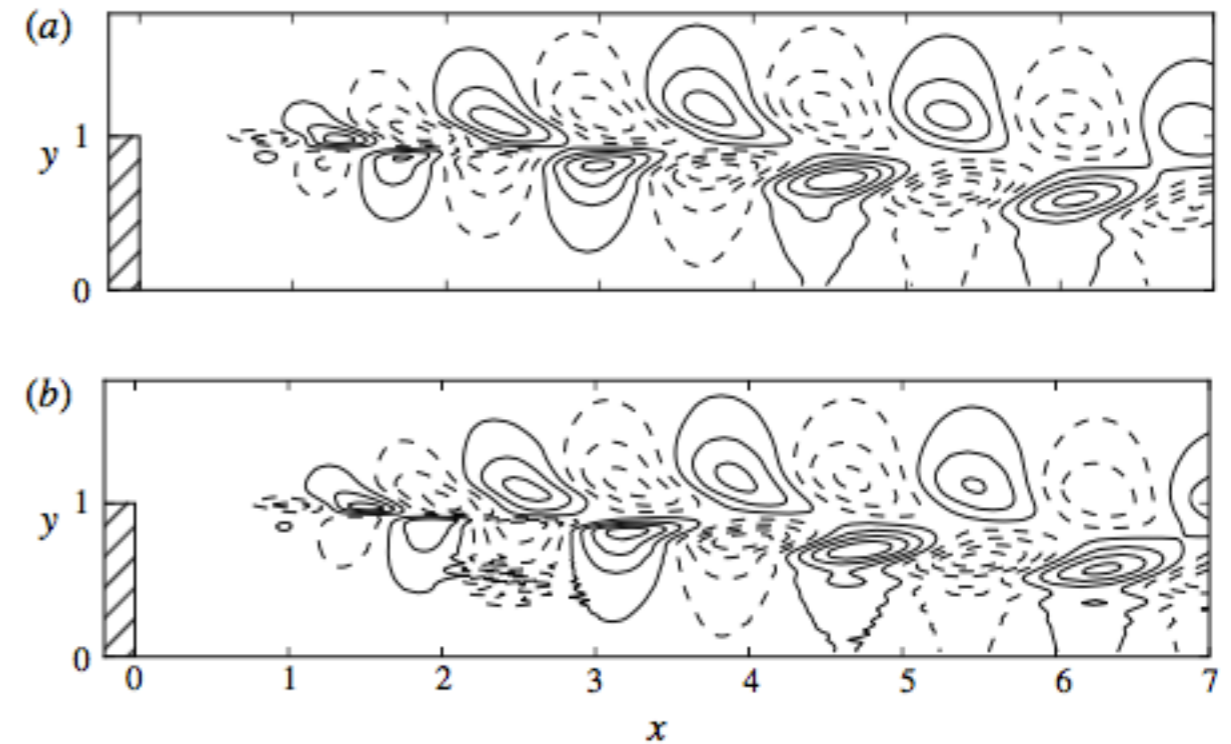
$$\mathcal{N}(\mathbf{x}, \omega) \equiv -(\tilde{\mathbf{u}} \cdot \nabla) \tilde{\mathbf{u}} + \langle (\tilde{\mathbf{u}} \cdot \nabla) \tilde{\mathbf{u}} \rangle$$

$$\mathbf{u}(\mathbf{x}, \omega) \approx \underbrace{\langle \mathcal{N}, \phi_{\text{dom}} \rangle(\omega) \mu_{\text{dom}}(\omega)}_{\text{scalar amplitude } \Lambda(\omega)} \underbrace{\psi_{\text{dom}}(\mathbf{x}, \omega)}_{\text{spatial dependence}}$$

Spatial dependence

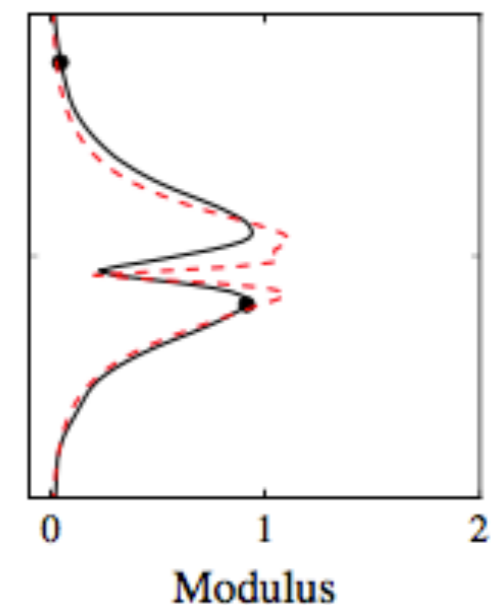
dominant optimal response
of resolvent $\psi_{\text{dom}}(\mathbf{x}, \omega)$

simulation $\mathbf{u}(\mathbf{x}, \omega)$

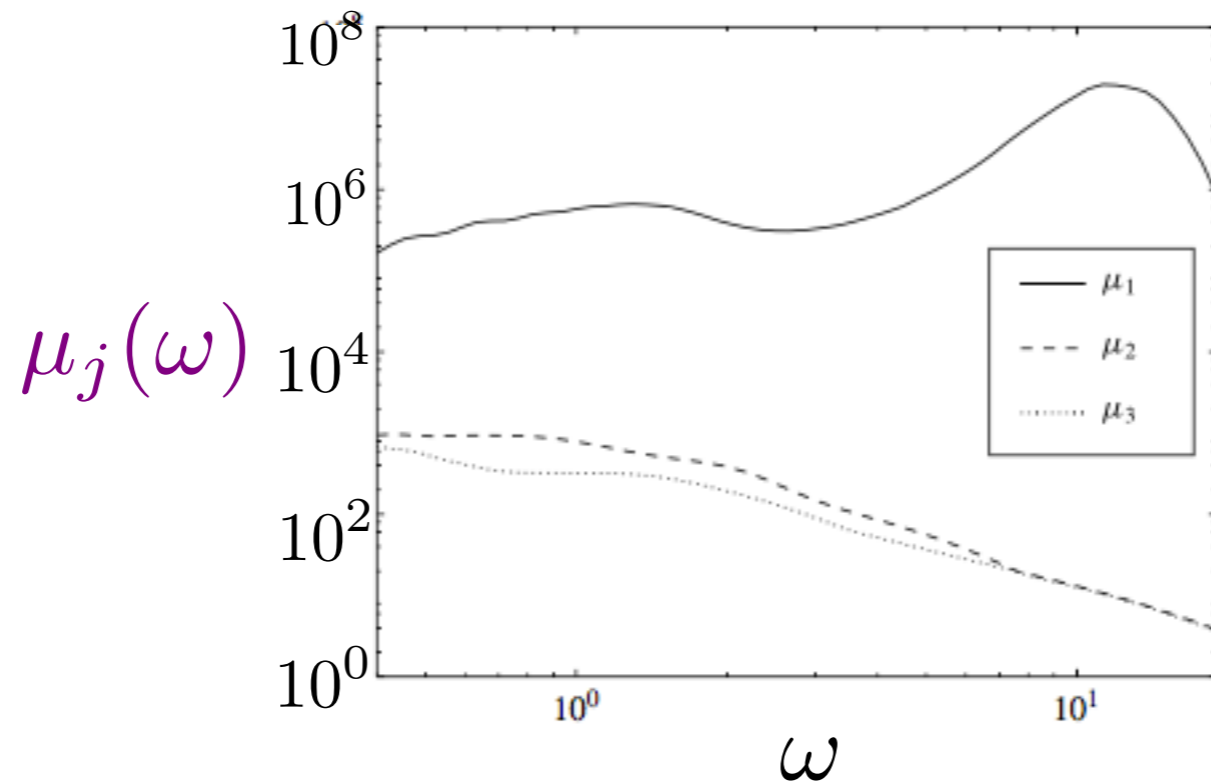


Scalar amplitude

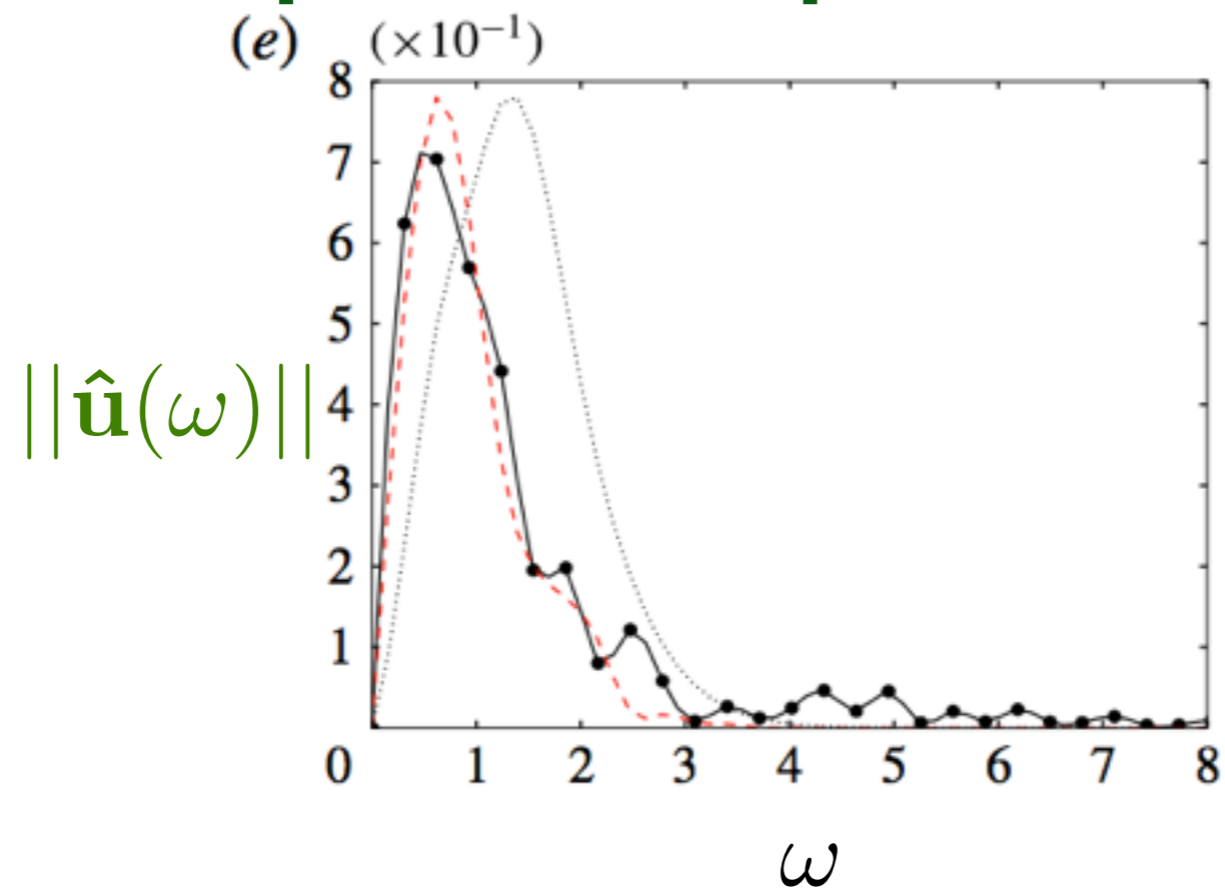
choose amplitude $\Lambda(\omega)$ so that dominant optimal
response and simulation agree at two points



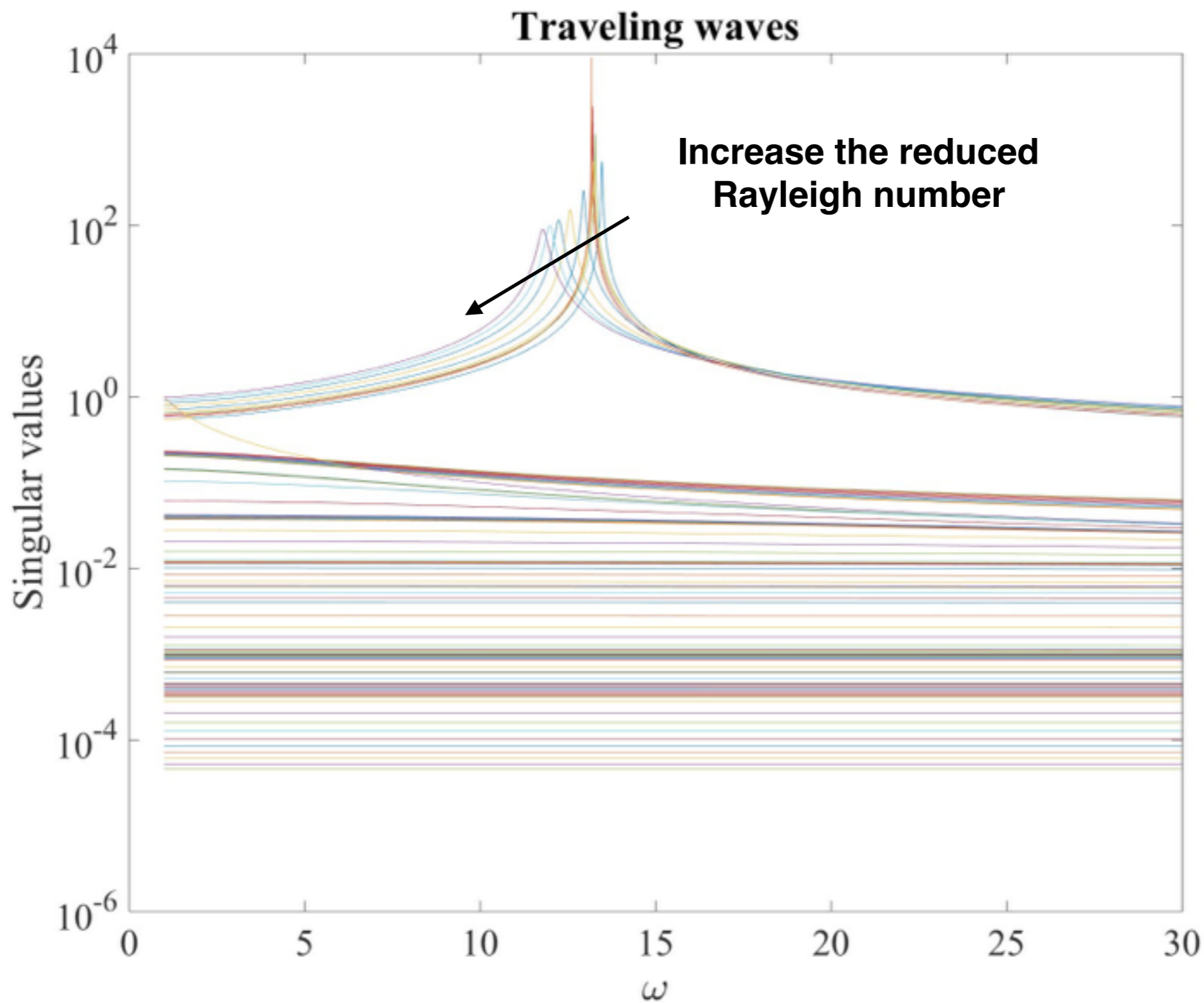
Dominant singular value



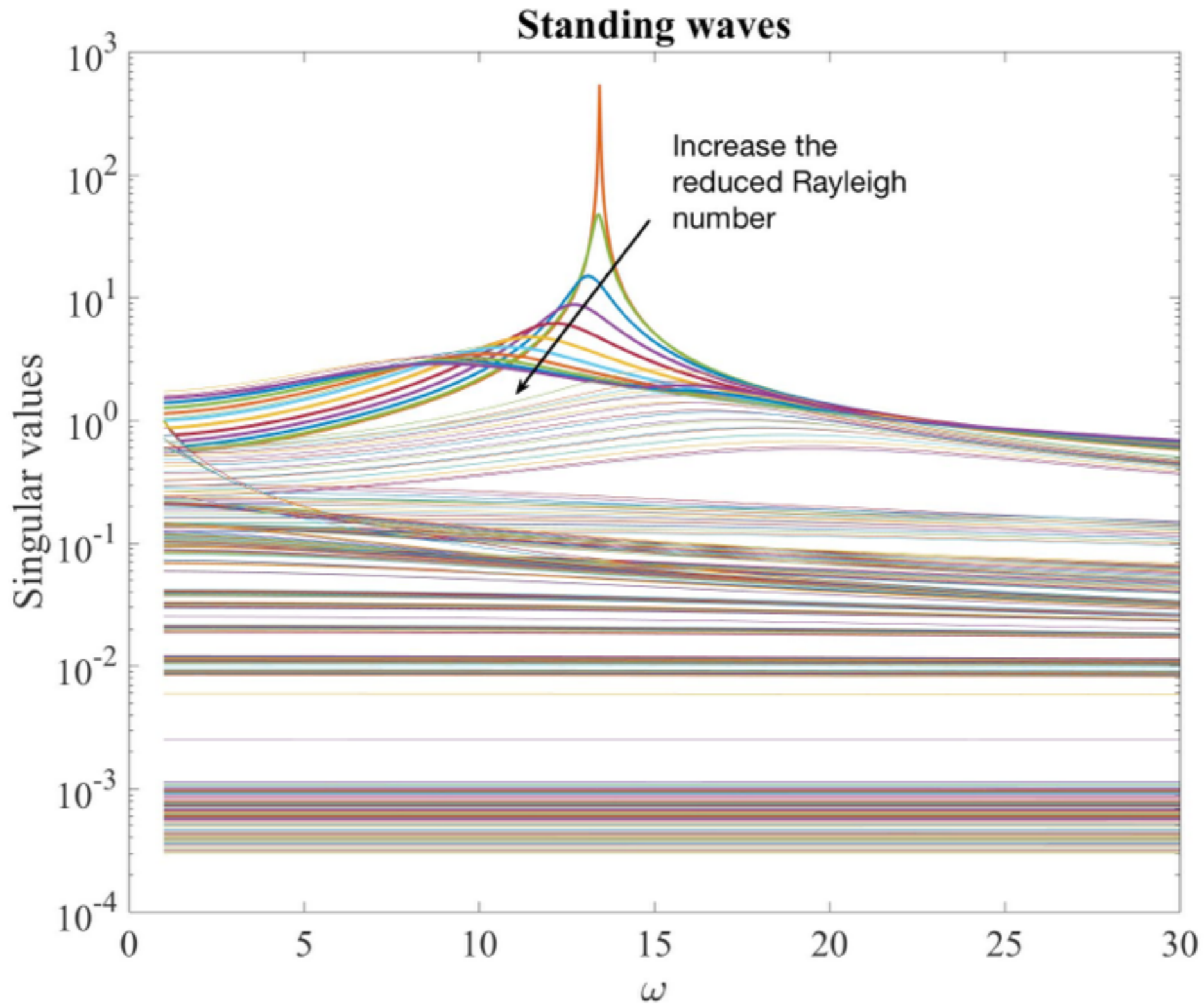
Spectrum reproduced!



Thermosolutal TW: SVD highly peaked



Thermosolutal SW: SVD not highly peaked



Stay tuned ...

Thank you!